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The Volumetrice properties of vapor-saturated aqueons potaesium hydroxide solutions from 0° to 400°C & vapor saturated aqueon solutions of Am 77-214 Sodium hydroxide from 0° to 350°C based on a requession of the 77-214 available literature data **UNIVERSITY OF UTAM** DL Brown + R. W. PoferII

RESEARCH INSTITUTE EARTH SCIENCE LAB.

Pressure-volume-temperature-composition (P-V-T-X) data for brines are required to establish optimum operating conditions for the production of geothermal brine fields; to minimize scaling and corrosion; and to intelligently design turbines for production of electricity. Precise thermodynamic data derived from the volumetric properties of the brines are prerequisite for chemical and reservoir modelling of geothermal brine systems. In view of the importance of P-V-T-X data to the utilization and understanding of geothermal brine systems, a compilation of the available literature data (Potter <u>et al.</u>, 1975) and evaluations of these data for NaCl, KCl, CaCl₂, Na₂SO₄, and K₂SO₄ have been completed (Potter and Brown, 1975, 1976a, 1976b, 1976c; Potter and Clynne, 1976).

Prior to this report, the only extensive tabulation of volumetric data for aqueous, vapor-saturated potassium and sodium hydroxide solutions was the International Critical Tables (National Research Council, 1928), in which a compilation of density values is presented for aqueous potassium hydroxide solutions for concentrations of 1 weight percent to 50 weight percent from 0°C to 100°C. There are no compilations available for potassium and sodium hydroxide solutions at pressures greater than the saturation vapor pressure (Potter, 1976). The purpose of this report is to provide an internally consistent set of density values for vapor-saturated, aqueous potassium hydroxide solutions from 0°C to 350°C based on the currently available experimental data summarized by Potter et al. (1975).

The density data presented in Tables 1, 2, 4, and 5 were obtained from regression analysis of the P-V-T-X data taken from the International Critical

Tables (National Research Council, 1928) and the 43 references cited by Potter <u>et al.</u> (1975). The data summarized in tables 1 and 2 are for vapor-saturated potassium hydroxide solutions from 0°C to 400°C and the data in tables 4 and 5 are for vapor-saturated sodium hydroxide solutions from 0°C to 350°C. The regression was accomplished by using a linear least-squares polynomial fit method in which each data point was weighted with respect to its relative uncertainty. The uncertainties used were for the most part those assigned by the experimentalist. However, in those cases where uncertainties were not stated, an estimate was supplied on the basis of the experimental method employed in the study.

The experimental densities were fit at constant temperature as a function of composition for each solute. In most cases a simple polynomial equation relating either the density, d, and the molality, m, of the solution,

$$d = \sum_{j=1}^{n} B_{j}(t)m^{j}, \qquad (1)$$

or the density and the square-root of the molality,

$$d = \sum_{j=1}^{n} C_{j}(t) m^{j/2}$$
, (2)

was used for regression purposes. However, it was found that converting the density data to apparent molal volume, ϕ_v , and then fitting this as a function of the square-root of molality resulted in a more accurate and economical (lower-order) representation of the data when very precise measurements were available. The equation used in this case is given by

The density can be calculated from the apparent molal volume by using the relation

$$I = \frac{1000d_{0} + M_{2}md_{0}}{1000 + \phi_{v}md_{0}}$$
(4)

where M_2 is the molecular weight of the solute and d_0 is the density of water. In general the order, n, of the fitting polynomial was chosen such that the standard deviation of the resulting regression would represent the internal consistency of the data used in the fit.

Tables 3 and 6 summarize the coefficients of the equations used to generate the density tabulations given here, and may be used for interpolation to determine densities of solutions with concentrations other than those given in tables 1, 2, 4, and 5.

Because of the inadequate data base, it was not possible to generate a set of density values at pressures greater than the saturation vapor pressure for either potassium hydroxide or sodium hydroxide which would accurately represent the behavior of each solution above its saturation surface.

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Table 1. Density of KOH Solutions (g/cm³).

			a					()	(HOFVEFIL	ROITARI	CONCERL		•			•		.:	. ((J [•]) a
	30.0	52.0	22.5	30.0	5.71	0.21	5.51	0.01	2.1	0.2	5.1	0.1	3.5	0.6	5.5	3.0	5'1	0.1	<u>ç.</u>	e
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\$,0002	695.1	812.1	687°T	\$\$7.1	LÍÝ'I	7/6-1	1.324	1.267	1.200	cz1•t	SOT-J	L90"T	690°T	050°t	0£0.1	600°1	896 .	L96°	976*	0
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\$000*7	164.1	876.1	99E*İ	016.1	1.269	1.222	L91'1	201-1	\$20.1	626.	106°	C88.	828.	168.	209.	111.	stl.	769 .	779.	. 0
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There as policity of Novi Cornetonic (K) cm)	Table 2.	Density	of KOH	Solutions	(g/cm^3)).
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5 1.0	0095	1.0281	1.0450	1.0596	1.0711	1.0788	1.0819	1.0794	1.1954	1.2463	1.2984	1.3520	1.4075	1.4653	1.5256					±.0002
s 1.0	0059	1.0238	1.0419	1.0602	1.0786	1.0973	1.1161	ļ.1352	1.1838	1.2338	1.2853	1.3386	1.3936	1.4505	1.5085					±.0002
) .9	9969	1.0144	1.0320	1.0498	1.0678	1.0860	1.1045	1.1233	1.1714	1.2211	1.2723	1.3250	1.3792	1.4353	1.4944			·		±.0004
i .9	983	1.000	1.017	1.034	1.052	1.070	1.088	1.107	1.155	1.205	1.256	1.310	1.364	1.420						±.0007
).	974	. 989	1.005	1.022	1.038	1.056	1.073	1.091	1.137	1.186	1.237	1.290	1.344	1.400	1.456	1.567				±.000 7
) .	935	. 948	.964	.981	. 999	1.018	1.036	1.055	1.104	1.153	1.204	1.257	1.311	1.366	1.422	1.537	1.653	1.76R		±.00 07
) .(873	.893	.914	.934	.954	.974	. 994	1.014	1.064	1.115	1.166	1.220	1.274	1.330	1.387	1.503	1.620	1.730	1.850	±.0005
)	797	.826	.851	.875	. 898	.920	.942	.964	1.018	1.071	1.125	1.180	1.235	1.292	1.350	1.467	1.583	1.692	1.800	±.0005
)	702	.742	.774	. 803	.830	.856	.880	. 905	.964	1.022	1.079	1.136	1.194	1.252	1.312	1.432	1.550	1.661	1.764	±.0005
) .(600	.650	. 689	.723	.754	.784	.812	.839	. 905	.968	1.030	1.091	1.152	1.213	1.275	1.398	1.517	1.626	1.722	±.0005
) .		***								_ _			1.108	1.174	1.237	1.360	1.480	1.594	1.685	±.0005

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Table 3. Interpolation Equation Coefficients for KOH Solutions.

The available density data for temperatures between 0° and 50° C were converted to apparent solal volumes and fit by the method of least squares to a polynomial equation of the form

 $\phi_v = \sum_{i=0}^{4} A_i m^{i/2}$, where m is the molality of the solution.

Density may be calculated by using the formula

$$d = (1000d_0 + M_2 m d_0) / (1000 + 4 m d_0),$$

where $M_2 = 56.109$ g/mole and d_0 is the density of water. The interpolation equations are valid for concentrations up to 17.8 molal (50 wt%).

Temp. (°C)	` A ₀	A ₁	A2	A ₃	А ₄	d _o (g/cm)
0	. 4093	2.7870	1.8974	5835	.04833	.999840
25	6.3465	-,46054	2.6470	07788	.05523	.997047
50	5.0719	3.47176	04192	.03755	011032	. 988038

For temperatures of 75° and 100°C, the available data were fit to a 3rd-order polynomial equation. The equation for 75°C solutions is valid for concentrations from 0 to 15.3 molai (0 to 46 wt%), while the equation for 100°C solutions is valid from 0 to 31 molal (0 to 64 wt%).

•	•	d = 1	3 ₀ + 81m +	Bym ² + B	300 ³ -
		B	IOxB1	-10 ² x8 ₂	10 ⁴ x83
75		.97508	. 4584	. 1321	. 1836
100		.96602	4296	.1073	. 1150

For temperatures from 150° to 400°C, the available data were fit to a 5th-order polynomial equation of the form

$$d = \sum_{j=0}^{5} C_{jm}^{j/2}$$

The range of concentrations for which these interpolation equations are valid vary, and are indicated in the table below with the coefficients:

Temp.	Range of va	lidity	1.12	•			_	
(°C)	(molality)	(wt\$)	Co	10xC ₁	10xC2	-10xC3	10 ³ xC ₄	-10 ⁴ xC5
150	0-108	0-86	.94076	4846	.9064	.1748	1.3858	. 40696
200	0-158	0 ∽90	.86476	09157	.7429	. 1407	1.048	.2822
250	0-158	0 90	.77552	. 2633	.6487	.1283	.9678	.2624
300	0-158	0-90	.660828	.76101	.51670	.11013	.8440	. 2299
350	0-158	0-90	.54334	1.1571	.45238	.10623	.8417	.2338
400	0-158	0-90	00875	5.1638	75017	066932	-, 3504	07993

Cor	contration (Molelity)		
Table 4. Dens	ity of NaOH Solutions (g/cm ³).		
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 $\mathbf{C} = \left\{ \begin{array}{c} \mathbf{C} \\ \mathbf{C} \end{array} \right\} = \left\{ \begin{array}{c} \mathbf{C} \\ \mathbf{O} \end{array} \right\} = \left\{ \begin{array}{c} \mathbf{O} \\ \mathbf{O} \end{array} \right\} = \left\{ \left\{ \begin{array}{c} \mathbf{O} \\ \mathbf{O} \end{array} \right\} = \left\{ \left\{ \begin{array}{c} \mathbf{O} \\ \mathbf{O} \end{array} \right\} = \left\{ \left\{ \begin{array}{c} \mathbf{O} \\ \mathbf{O} \end{array} \right\} = \left\{ \left\{ \left\{ \begin{array}{c} \mathbf{O} \\ \mathbf{O} \end{array} \right\} \right\} = \left\{ \left\{ \left\{ \left\{ \left\{ \mathbf{O} \right\} \right\} \right\} = \left\{ \left\{ \left\{ \left\{ \left\{ \mathbf{O} \right\} \right\} \right\} \right\} = \left\{ \left\{ \left\{ \left\{ \left\{ \mathbf{O} \right\} \right\} \right\} \right\} = \left\{ \left\{ \left\{ \left\{ \left\{ \mathbf{O} \right\} \right\} \right\} = \left\{ \left\{ \left\{ \left\{ \mathbf{O} \right\} \right\} \right\} = \left\{ \left\{ \left\{ \left\{ \mathbf{O} \right\} \right\} \right\} = \left\{ \left\{ \left\{ \left\{ \mathbf{O} \right\} \right\} \right\} = \left\{ \left\{ \left\{ \mathbf{O} \right\} \right\} = \left\{ \left\{ \left\{ \mathbf{O} \right\} \right\} \right\} = \left\{ \left\{ \left\{ \mathbf{O} \right\} \right\} = \left\{ \left\{ \left\{ \mathbf{O} \right\} \right\} = \left\{ \left\{ \left\{ \mathbf{O}$

								Concent	ration (Holality) .								
(0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0	7.5	10.0	12.5	15.0	17.5	20.0	22.5	25.0	
1.0	3240	1.0463	1.0674	1.0875	1.1067	1.1252	1.1430	1.1601	1.1766	1.1925	1.2641	1.3243	1.3750	1.4182	1.4551	1.4870	1.5150	1.5399	t.00 03
1.0	01867	1.03928	1.0591	1.0782	1.0966	1.1144	1.1316	1.1482	1.1642	1.1797	1.2499	1.3092	1.3595	1.4023	1.4389	1.4704	1.4976	1.5210	±.0003
1.0	1680(1.02873	1.0478	1.0663	1.0842	1.1015	1.1183	1.1346	1.1504	1.1656	1.2351	1.2939	1.3434	1.3850	1.4204	1.4511	1.4785	1.5039	±.0006
.9	984	1.0181	1.0371	1.0554	1.0731	1.0902	1.1068	1,1229	1,1384	1.1535	1.2220	1.2803	1.3297	1.3718	1.4076	1.4384	1.4644	1.4879	±.0006
. 9	0794	. 9992	1.0182	1.0366	1.0543	1.0715	1.0881	1.1042	1.1197	1.1348	1.2032	1.2609	1.3095	1.3504	1.3854	1.4161	1.4440	1.4706	±,0006
.9	937	.958	.978	. 997	1.016	1.034	1.051	1.067	1.083	1,099	1.167	1.224	1.272	1.313	1.349	1.380	1.408	1.432	±.002
. 8	486	. 908	.928	.949	.968	.986	ļ.004	1.021	1.038	1.054	1.125	1.183	1.233	1.274	1.311	1.342	1.370	1.395	±.002
. 8	126	. 849	.872	. 893	.914	.934	. 953	. 971	. 989	1.006	1.080	1.141	1.192	1.235	1.272	1.305	1.334	1.359	±.003
.7	/51	.776	. 800	.824	.846	. 867	.888	.908	, 927	.946	1.028	1.095	1.151	1.197	1.236	1.269	1.298	1.323	±.005
.6	539	,675	.709	.741	.771	.799	.825	.850	.873	. 895	. 986	1.054	1.108	1.153	1.193	1.229	1.261	1.285	±.005
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	Table	5.	Density	of	NaOH	Solutions	(g/¢	2m³])	•
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emp.			• .	-* •		CON	CENTRATI	on (Weig	HT PERCE	NT)							:	
-0)	1	3	5	7	9	11	13	15	20	25	30	35	40	45	\$0			
0	1.0124	1.0364	1.0597	1.0828	1.1057	1.1285	1.1512	1.1738	1.2299	1.2853	1.3397	1.3925	1.4434	1.4924	1.5399	±.0003		
-25	1.00813	1,03004	1.0519	1.0737	1.0956	1.1175	1,1395	1.1614	1.2163	1.2708	1.3244	1.3768	1.4274	1.4757	1.5210	±.0003		
50	.99876	1.01984	1,0409	1.0620	1.0832	1.1046	1.1260	1,1476	1.2018	1.2559	1.3089	1,3602	1.4092	1.4563	1,5039	±.0006		
70	.9884	1.0093	1.0302	1.0511	1.0721	1.0933	1.1145	1.1357	1.1892	1.2425	1.2952	1.3467	1.3963	1.4435	1.4879	1.0006		
100	. 9692	.9903	1.0113	1.0323	1.0534	1.0745	1.0957	1.1170	1.1/04	1.2236	1.2757	1.3261	1.3744	1.4214	1.4707	±.0006		
200 . 120	.940	. 946	. 9/1		1.015	1.037	1.039	1.051	1.134	1.147	1.238	1.285	1,337	1.350	1.432	1.002		
200 250	.9/3 R14	830	.921		.907	.990	1.012	1.022	1.045	1.102	1.120	1.249	1.299	1.348	1.393	1.002		
300	739	765	792		. #14 RAS	.930	ROR	. 200	080	1.052	1.112	1.209	1.200	1.310	1.328	+ 005		
350	. 623	659	697	784	769	804	.070	869	944	1.011	1.071	1.176	1 180	1 235	1 285	+ 005		
											1.071	1.120						
					,											•		
				•						÷				·				

Table 6. Interpolation equation coefficients for NaOH solutions.

The available density data for temperatures between 0° and 100° C were converted to apparent molal volume and fit by the method of least squares to a polynomial equation of the form

 $\phi_{v} = \sum_{j=0}^{n} A_{j} m^{j/2}$, where m is the molality of the solution.

Density may be calculated by using the formula

 $d = \frac{1000d_0 + M_2 m d_0}{1000 + \phi_v m d_0}, \text{ where } M_2 = 39.997 \text{ g/mole}$ and d_0 is the density of water

The interpolation equations are valid only for concentrations less than 26 molal (51 wt%).

Тетр.							
(°C)	n	AQ	A1	A ₂ .	A ₃	A _{te}	do
0	2	-13.313	7.667	5232			.999840
25	4	-5.2618	1.982	1,2730	28035	.017674	.997047
50	4	-4.8480	3,7608	14493	.08709	013618	.988038
70	4	-4.4239	2.5852	.71785	14439	.007130	.977766
100	'4	-7.5513	5.3277	-,60261	. 16848	020118	.958357

For temperatures between 150° and 350°C, the available data were fit by the method of least squares to a polynomial equation of the form

$$d = \sum_{j=0}^{4} B_{j} m^{j}.$$

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The interpolation equations are valid only for concentrations less than 26 molal (51 wt%).

Temp.	•	CC	DEFFICIENTS		
(°C)	B ₀	10xB1	$-10^2 \mathrm{xB}_2$	10 ⁴ xB ₃	-10 ⁶ xB ₄
150	.91499	.44439	.17615	.45910	.53917
200	.86315	.46138	.18182	. 45662	. 50933
250	.80098	.50260	. 21281	. 56943	.66109
300	.72533	. 52969	.19847	. 42286	.37630
350	.60082	.79142	. 48458	1.7063	2.38441