GLOIDDS

REPORT ON THE PASSIVE SEISMIC SURVEYS

ASSIVE SEISPIIC SURVEY.

CONDUCTED

TO ASSESS THE

GEOTHERMAL POTENTIAL

NEAR

BEOWAWE, NEVADA

FOR

STANDARD OIL OF CALIFORNIA

ΒY

SENTURION SCIENCES, INCORPORATED

TULSA, OKLAHOMA

June 2, 1975

Senturion Sciences has performed the field work and the resulting analysis and interpretation described in this report solely for Standard Oil of California. All data and information associated with and resulting from these surveys are the property of Standard Oil of California.

SEISMIC GROUNDNOISE SURVEY

LOCATION: Lander Co., Nevada, sec. 13, 24, T. 31 N.; R. 47 E., sec. 18, 19, T. 31 N.; R. 48 E.

DATES: October 29, 1974 through November 20, 1974.

CREW: Senturion Sciences RF #5, and GN #1.

NO. OF STATIONS: 139 Data Stations, 19 Base Stations.

STATION DENSITY: 500 ft. spacing.

AREA COVERED: Approximately 2 square miles.

GEOPHYSICISTS: Bob Graf, Keith Westhusing*

* Preliminary maps of the Beowawe survey that were previously submitted to Standard Oil of California (Dec., 1974) were analyzed by John Bailey and did not contain corrections for the reference station. This report contains those corrections and data have been interpreted by the designated geophysicists.



SENTURION SCIENCES, INC.

BEOWAWE, NEVADA GROUNDNOISE SURVEY

INTRODUCTION

Purpose

This survey was an experimental effort to determine the resolution capabilities of a high-density seismic groundnoise survey. In addition to the location of specific areas of geothermal interest as exhibited by anomalous noise characteristics; the delineation of structural features such as faults and other stratigraphic discontinuities have been investigated.

Geology

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The Beowawe geothermal prospect is located in the Shoshone Range of north central Nevada, approximately 25 miles southeast of the town of Battle Mountain. The area has typical Basin and Range topography with generally north-trending mountain ranges. The area surveyed is situated along the southeastern margin of the northeast trending Whirlwind Valley where it is in contact with Tertiary volcanic rocks broken by steeply dipping faults. The geysers of the Beowawe area are related to the active Malpais Fault (Oesterling, 1962), the prominent normal fault bordering the southeastern margin of the valley. Basalt and basaltic andesite make up the faulted mountains southeast of the survey area. Quaternary alluvium and alluvial fan material cover the valley floor and surround the prominent topographic high inlier of basaltic andesite situated along the southeastern margin of the area surveyed. Numerous northeast-southwest trending faults such as the Malpais are present and hydrothermal solution movement along these thermally-active normal faults has caused significant alteration of andesite with replacement by silica. A number of springs associated with valley floor marginal faults have shown surface temperatures to 205°F and have caused extensive deposition of siliceous sinter (Garside, et al., 1972). Eleven wells were drilled in the area from 1959 through 1965, the deepest of which was 2,052 feet. The Chevron-ATR GINN. 1-13 well drilled near station 1 to a depth of 7,900 feet showed apparent penetration of volcanic rocks in the 800 to 2,100 feet depths. Outcrops of Plio-Pleistocene basalt to the northwest of the area surveyed gives indication of a basaltic layer overlying the andesite under valley fill. Lower Paleozoic sediments underlie the volcanic rocks of the valley floor and are considered_potential reservoirs for geothermal fluids. These rocks, possibly the (upper plate of the Roberts Mountain Thrust, are inferred from geologic mapping in adjacent areas and are probably, in part, limestones, which may be a productive geothermal reservoir similar to that at Larderello, Italy.

Data Acquisition

In the course of the 23 day survey, approximately 160 stations were occupied including a daily base station monitor (Station 1). See Table 1, Data Acquisition Calendar. Some stations were not used due to reasons discussed in the Data Processing Section. Senturion utilized a Radio-Frequency Telemetered System as well as a Cable System to increase the daily production rate. On November 6, 1974, the two systems recorded at the same stations. This information was processed to show compatibility and the data is summarized in Table 2. Power Spectral Density curves reflect system similarities (see following PSD's for spectral comparisons). It is felt that these results provide sufficient evidence to support the validity of two-system acquisition. Computer listings in Appendix 4 show additional calculations concerning the systems separately and in combination.

RESULTS

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Data Analysis

In this survey three separate frequency bands were evaluated: 0.5 to 15.0 Hz.; 0.5 to 7.5 Hz.; and 0.5 to 3.5 Hz. The first two were derived from the same set of Power Spectral Density charts with a 0.5 frequency increment as shown in Appendix 2, while data on the 0.5 to 3.5 Hz. band was obtained from a PSD chart designed with a 0.25 Hz. frequency increment as indicated by Appendix 3.

It should be noted that varying numbers of data stations (and base stations) were useable on the three bands. This was due to the inconsistency of the high power levels on the 0.5 - 15.0 Hz. curves; and questionable data in the 0.75 - 1.50 Hz. range of the 0.5 - 7.5 Hz. curves used in the investigation of the 0.5 to 3.5 Hz. band. In the former case, the differential of the power values between 0.5 - 8.0 Hz. and the higher frequencies (10.5 - 15.0 Hz.) exceeded the scaling capability of the Signal Analyzer Integrator used in the 0.5 - 15.0 Hz. study proved to be acceptable for the 0.5 - 7.5 Hz. study. A similar situation occurred in the 0.75 - 1.50 Hz. range for the 0.5 - 3.5 Hz. analysis. PSD's not used are included for evaluation in the appendices. Comparative data and base station figures are shown below:

SPECTRUM	DATA STATIONS	BASE STATIONS
0.5 - 15.0	łz. 125	12
0.5 - 7.5	łz. 139	17
0.5 - 3.5	łz. 110	19

Table 1.	Data	Acquisition	Calendar	
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		STATIONS ALCOADED	·····
DATE	BASE	RF SYSTEM	CABLE SYSTEM
$10 - 29 \\ 10 - 30 \\ 10 - 31 \\ 11 - 1 \\ 11 - 2 \\ 11 - 3 \\ 11 - 4 \\ 11 - 5 \\ 11 - 6* \\ 11 - 7$	1 1 1 1 1 1 1 1	3 2, 5, 6, 8 9, 10, 11, 12 13, 14, 15, 16, 17 18, 19, 20, 21, 22 23, 24, 25, 26, 27 28, 29, 30, 32 31, 33, 34, 35, 36 37, 38, 39, 40, 41 42, 43, 44, 45, 46	37, 38, 39, 40, 41 155, 156, 157, 158, 159,
11 - 8 11 - 9	1 1	47, 48, 49, 50, 51 52, 53, 54, 55, 56	160 140, 150, 151, 152, 153, 154
$11 - 10 \\ 11 - 11$	1 1	57, 58, 59, 60, 61 62, 63, 64, 65, 66	144, 145, 146, 147, 148 138, 139, 140, 141, 142, 143
11 - 12	1		132, 133, 134, 135, 136, 137
11 - 13	1	67, 68, 69, 70, 71	126, 127, 128, 129, 130, 131
11 - 14 11 - 15	1 1	72, 73, 74, 75, 76 77, 78, 79, 80, 81	119, 120, 122, 123, 124, 125
11 - 16 11 - 17	1 1	84, 85 82, 83, 86, 87, 88,	114, 115, 116, 117, 118
11 - 18	1	90, 91, 92, 94	108, 109, 110, 111, 112,
11 - 19 11 - 20	1 · 1	95, 96, 97, 98, 99 100, 101, 102, 161	103, 104, 105, 106, 107

STATIONS RECORDED

* Compatibility Test

Table 2. Systems Comparison (Done for November 6, 1974)

A. Individual Stations

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SYSTEM/ STATION	INTEGRATED POWER	MEAN FREQUENCY
37 RF (RF Tele-	34.2	7.36
37 CA (Cable Sys- tem)	37.0	7.13
38 RF	30.1	7.15
38 CA	34.1	7.36
39 RF	30.4	6.98
39 CA	30.4	7.33
40 RF	31.2	7.09
40 CA	30.8	7.21
41 RF	28.6	7.05
41 CA	28.4	7.10

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B. Statistics of all Stations

	INTE	GRATED POL	IER	MEAN FREQUENCY					
	COMBINED	RADIO	CABLE	COMBINED	RADIO	CABLE			
AVERAGE	31.50	30.87	32.12	7.18	7.13	7.23			
SIGMA	2.74	2.08	3.41	.14	.14	.12			
PERCENT	8.70	6.72	10.61	1.89	2.02	1.64			
+ SIGMA	34.24	32.95	35.53	7.31	7.27	7.35			
- SIGMA	28.76	28.80	28.71	7.04	6.98	7.11			





















Data Processing

This portion of the report pertains to the three bands analyzed. In the following discussion the suffix A, B, or C will designate 0.5 - 15.0 Hz., 0.5 - 7.5 Hz., 0.5 - 3.5 Hz., respectively.

After the acceptable PSD functions were selected, the information was keypunched for subsequent input to the various data reduction applications. The processing sequence follows:

- 1. Calculation of integrated power, mean frequency, ratio, and statistics of the base stations.
- 2. Calculation of the above on uncorrected stations.
- 3. Evaluation and selection of the control base station. This was the base station exhibiting average power characteristics during the survey. See Tables 3A, 3B, and 3C.
- 4. Sort of the data stations to provide proper correction sequence and factors. In the instance where no base station was available, the particular data for that day was treated as an average day.
- 5. Recalculation of integrated power, mean frequency, ratio, and statistics on corrected data.
- 6. Computer derivation of surfaces for the above parameters.
- 7. Contouring of the surfaces.
- 8. Cross section development and plot.

Computer listings for procedures 1, 2, and 5 are included in Appendix 4. Table 4 contains a statistical summary from these listings.





TABLE 3B SENTURION SCIENCES, INC.



Table 4. Statistical Data

	Α		В		С			
	0.5 -	15 Hz.	0.5 - 7	.5 Hz.	0.5 - 3	.5 Hz.		
	INTEGRATED POWER	MEAN FREQUENCY	INTEGRATED POWER	MEAN FREQUENCY	INTEGRATED POWER	MEAN FREQUENCY		
AVERAGE	14.54	5.96	17.20	3.08	9.58	1.68		
STD. DEV.	4.23	.96	4.28	.39	.1.67	.14		
PER CENT	29.09	16.19	24.89	12.79	17.46	8.51		
+ SIGMA	18.77	6.92	21.48	3.47	11.25	1.83		
- SIGMA	10.31	4.99	12.92	2.69	7.91	1.54		
MIN. @ STA.	5.39 @ 109	3.26 @ 123	6.18 @ 125	1.12 @ 125	4.52 @ 100	1.14 @ 100		
MAX. @ STA.	24.16 @ 147	8.17 @ 147	25.29 @ 94	3.83 @ 50	14.31 @ 75	1.96 @ 76		
NO. OF STATIONS	1	25	13	9	110			

STRUCTURAL INTERPRETATION

Introduction

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An objective of the high-station density survey (station separations of approximately 500 feet) was to discern acoustical impedance mismatches caused by the juxtaposition of layered media of contrasting velocities and densities created by the extensive faulting known to exist in the area from surface exposures. Such acoustical impedance contrasts are indicated on cross sectional displays of Integrated Power and Mean Frequency by crossings of these computed values (Appendix 1). Crossover points can be caused by both faulting and flow fronts and are not readily distinguished from the computed data. Basalt underlying the valley floor outcrops approximately 1 1/3 mile northwest of the survey area indicating a southeastward dip to the volcanic basement surface. Individual flow units of basalt are not known nor are they distinguishable with groundnoise data. Accordingly, while flow front contacts are capable of causing acoustical impedance mismatches when in contact with less dense, lower velocity alluvial fill, they are not distinguishable from fault discontinuities and are not, therefore, mapped. All discontinuities reflected by crossovers of mean frequency and integrated power are indicated on plan maps as faults and joined in lineaments according to the general structural trends indicated by the topography and geology of the surveyed area.

Major lineaments occur in northeast-southwest trends such as the South and North Malpais Horst faults and in the northwest-southeast trending cross-faults that bound the topographic high located along the southeast corner of the surveyed area. These faults extend out into the Whirlwind Valley and apparently have possible bifurcations and numerous associated short-length segments of varying directions. Displacement direction or sense of faults is interpreted from the relation of mean frequency to integrated power. Where the mean frequency value is greater than integrated power an upthrown side is indicated; where the integrated power value exceeds mean frequency, a downthrown relationship is indicated. Measured fault displacements were not obtained from the interpreted data because accurate depth control was not established. Well log data from Chevron-ATR-GINN 1-13 well located near station #1 was examined as a depth control reference; however, the well velocity log showed considerable velocity variation for the large number of layers penetrated and the integrated power and mean frequency values computed from the power spectral density curves gave no indication of resolving the many layer parameter changes that occurred with depth. Senturion is currently in the process of combining telluric measurements with groundnoise measurements to provide more accurate determination of the depth function. Extreme northwest ends of cross sections G, M, F, and E for the 0.5 to 15 Hz and 0.5 to 7.5 Hz shown mean frequency values greater than integrated power values and with MF values having upward slopes which may be indicative of thinning of the alluvial layer toward the northwest where the known outcrops of basalt occurs. Alluvial thickness appears to be less than 1,000 feet within the valley and thinning of fill material is indicated toward the northwest.

Frequency Band Fault Mapping

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Fault maps were prepared from integrated power and mean frequency computations in the frequency band .5 to 15 Hz., .5 to 15 Hz., and .5 to 3.5 Hz. Fault locations are indicated on the fault maps as double lines implying the limits of resolution of the method. Since station separation is approximately 500 feet fault location accuracies can be no less than that value. Accordingly, actual fault locations may occur anywhere between the two stations whose measured values were used in computing the integrated power - mean frequency values.

0.5 to 15 Hz. Band Fault Delineations

Figure 3A shows faults mapped from IP/MF data in the frequency band .5 to 15 Hz. As previously mentioned major fault lineations were selected on the geologic-topographic reasonableness of structures and with consideration of the sense of fault displacement as indicated by the integrated power-mean frequency values measured on cross sections. The North and South Malpais Horst faults define the upthrown blocks along the southeast border of the area surveyed. The Southwest Cross Fault splits the horst block with the upthrown eastern portion forming the prominent topographic high of basaltic andesite. This cross fault extends out into Whirlwind Valley where it may have two or possibly three branches. The region of intersection of the North Malpais Horst Fault (NMHF) and the Southwest Cross Fault (SWCF) is not adequately resolved which may result from severe scattering and attenuation of seismic energy. The region along NMHF between stations 118 and 119 (Profile MM') has a reversal of fault displacement. This area is also an anomalous area, hence, power and frequency values may be affected to the extent that structural interpretation is obviated. The Northwest Cross Fault (NWCF) bounds the horst block on the northeast and extends northwestward into Whirlwind Valley.

Areas of geothermal interest are around stations 114, 116, and 117 where the major fault NMHF intersects the anomalous area shown in Figure 3A, and associated with the extension of the major fault, SMHF, at stations 74, 76, and 85 where an intersection of the fault occurs with the anomalies mapped for each of the three frequency bands.

0.5 to 7.5 Hz. Band Fault Delineations

The four major faults delineated by the 0.5 to 15 Hz. band are again delineated on the map shown in Figure 3B. The intersection of the Southwest_Cross Fault (SWCF) and the North Malpais Horst Fault (NMHF) remains unresolved and the possible branching of SWCF is more complicated with a graben structure indicated between the two branches north of NWHF. The Northeast Cross Fault is again defined as is the short fault to the northeast. The displacement sense change occurs again between stations 118 and 119 where a geothermal anomaly exists.

More numerous short-length faults occur over the surveyed area. If it can be considered that this lower frequency band samples deeper structure, the implication is that deeper layers of andesitic material may be more extensively fractured than the overlying basaltic material; however, the acoustical impedance differences between basalt and andesite are not considered to be substantially different and therefore differences in quantity and direction of faulting probably not discernible.

Geothermal areas of interest are near station 5 where the fault zone intersects an anomalous area (Figure 2) and stations 85, 75, 74, and 73 where the major South Malpais Horst Fault intersects the four station anomaly.

0.5 to 3.5 Hz. Band Fault Delineations

Three of the major faults are demarked from computations of data in the 0.5 to 3.5 Hz. band (Figure 3C). The Northeast Cross Fault is not defined owing to nonlinearities in narrowband data for stations in the northeast section of the area surveyed. Accordingly, these stations were deleted from the data base. Inversion of displacement sense along portions of the South Malpais Horst Fault is not easily explained. If the longer wavelength waves of this low-frequency band sample deeper layers, more complicated relative movements may occur along the fault zone. Variation in directions of short segment faults also occur compared to directions indicated for similar faults_shown on the two previous fault delineation maps. No ready explanation other than the previous statement can be made at this time. It is believed that this narrow, low frequency band is the one most likely to be composed of surface waves and, therefore, contain less contribution of energy from body waves. Accordingly, the band has the potential for sampling deeper structure, and, therefore, <u>capable of sensing</u> more accurately the direction of displacements of faults at greater depths. This hypothesis has not been adequately verified and is, at this time, only supposition.

Geothermal areas of interest in the extreme southwest corner of the area surveyed. Stations 65, 76, 75, and 99 are associated with the probable intersection of the South Malpais Horst Fault and warrant further study by other geophysical methods. The 0.5 to 3.5 Hz. anomaly around stations 83 and 89 may be related to extensions of the numerous faults detected in that area and also warrants further examination.

ANOMALOUS AREAS

The Anomalous Areas Composite, Figure 2, indicates three major areas of interest.

 Northern Anomaly - located in the center of sec. 18, T. 31 N., R. 48 E, (Stations 105, 106, 128, 114, 116, and 117), is situated due west of the hot spring and The Geysers and north of the topographic high in the southeastern quarter of sec. 18. Parameters of coincidence at mean +1 standard deviation include 0.5 - 15.0 Hz IP and MF, 0.5 - 7.5 Hz. IP. and 0.5 - 3.5 Hz IP. The proximity to the surface geothermal manifestations are favorable indications of a local heat/energy source at depth. The anomalous zone can also be related to the North Malpais Horst Fault and the Northeast Cross Fault that are delineated by groundnoise.

- 2. Western Anomaly on the western border of the survey, sec. 13, T. 31 N., R. 47 E. (stations 5 and 51). This anomaly has expression on the low-lying relatively flat expanse of alluvium in the center of Whirlwind Valley. Characteristics exceeding mean +1 standard deviation are 0.5 - 15.0 Hz IP, 0.5 - 7.5 Hz IP and MF. The lower frequency spectra possibly reflect a thicker alluvial accumulation in this area which filters the higher frequencies. The anomaly may be associated with an eastwest trending cross fault bounding the topographic high on the south.
- 3. The Southern Anomaly found in the southeast quarter of sec. 24, T. 31 N., R. 47 E., (stations 83, 88, and 89 and stations 74, 75, 76, 85, and 99). Anomalous groundnoise conditions encompass most of the southern tip of the survey. <u>All</u> parameters (0.5 -15.0 Hz IP and MF, 0.5 - 7.5 Hz IP and MF, and 0.5 - 3.5 Hz IP and MF) are indicated anomalous at Stations 76 and 89, with 74, 75, and 88 anomalous through five of the parameters. This high coincidence establishes the very interesting possibility of a separate geothermal reservoir untapped by prior drilling if the surface manifestations to the northeast are associated with the source underlying the Northern Anomaly. Again, association with the apparent northeast-southwest trending South Malpais Horst Fault is indicated adding credence to the possibility of a potential productive geothermal source.

COMMENTS - RECOMMENDATIONS

- The survey exhibits "edge anomalies"; however, examination of specific station values confirms the fact that anomalous conditions are indeed present. Furthermore, the validity of such anomalies is reinforced by the detected presence of fault systems with linear trend relations to surface geothermal manifestations and high temperature measurements resulting from drilling.
- The Southern Anomaly, with its high coincidence of anomalous parameters, is a primary area of interest. Additional work is recommended. Heat flow test holes and a resistivity survey would give further indications of the geothermal potential in this specific locale.

- 3. The GINN 1-13 well location and Station 1 are situated north of a 0.5 3.5 Hz integrated power high near the intersection of two fault systems (SWCF and NMHF) but not in an indicated anomalous area.
- 4. Isolated single-station anomalies are evident on the various anomaly maps some of which correlate with fault structures determined from acoustic impedance differences.

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5. All station data has been saved for additional processing if required.

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	INTEGRATED			PRE	DOMIN	ANT	
STA.	POWER PCDEV.	FREN. PCDE	<u>V.</u>	POWER P	COEV. FRE	Q. PCDEV.	POWER
0001	12 8 -11.9	5.42 -9.2		- 0.0	n n - n n	0 0 0	0.0.5
	14.52	5.02 -15.8	10-30	-0.0	0.0 -0.0	0 0.0	• 425
0005	19.1 31.5	6.37 6.8	10 20	-0.0	0.0 -0.0	0 0.0	.333
0006	15.4 6.1	5.65 -5.2		-0.0	0.0 -0.0	0 0.0	• 366
0008	12.4 -14.8	5.14 -13.7		-0.0	0.0 -0.0	0.0	.415
0003	12.9 -11.5	4.98 -16.5	<u></u>	-0.0	0.0 -0.0	0 0.0	.387
0009	10.5 -27.8	5.75 -3.5		-0.0	0.0 -0.9	0 0.0	•548
0013	11.0 -24.1	5.26 -11.8		-0.0	0.0 -0.0	0 0.0	.476
0014	9.5 - 34.8	4.44 -25.5		-0.0	0.0 - 0.0	0 0.0	•468
0015				-0.0	0.0 - 0.0		•483
0025	17.8 22.4	6.35 6.4		-0.0	$\frac{0.0 - 0.0}{0.0 - 0.0}$. 357
0024	12.4 -14.7	4.64 -22.2		-0.0	0.0 -0.0	0 0.0	.374
0027	12.0 -17.4	4.91 -17.7		-0.0	0.0 -0.0	0 0.0	•409
0031	15.9 9.0	6.21 4.1	•	0.0	0.0 0.0	0.0	•392
0033	13.2 -9.4	5.68 -4.8		0.0	0.0 0.0	0.0	.431
0034	17.4 19.9	6.22 4.2		0.0	0.0 0.0	0 0.0	•357
0035	9.3 -36.0	5.97 .2		0.0	0.0 0.0	0 0.0	•641
0036	16.9 16.5	6.55 9.8		0.0	0.0 0.0	0 0.0	•386
0047		5.85 -1.9		0.U			• 396
0048	11 9 -18 1	5-51 -7 6		0.0			• 384 1/2 R
0049	20.3 39.8	5.91 - 15.8		0.0			•483
	17.5 20.6	6.30 5.6		0.0	0.0 0.0	0 0.0	•359
0133	9.3 -35.4	6.87 15.2		-0.0	0.0 -0.0	0.0	•743
0134	12.4 -15.0	6.82 14.4		-0.0	0.0 -0.0	0 0.0	•552
9135	11.6 -20.0	7.23 21.3		-0.0	0.0 -0.0	0.0	.622
0135	13.7 -5.5	6.13 2.8		-0.0	0.0 -0.0	0.0	•446
0082	14.8 1.7	5.66 -5.1		-0.0	0.0 -0.0	0.0	•382
0083	15.4 6.0	5.57 -7.6		-0.0	0.0 -0.0	0 0.0	• 350
0087	10.0 14.4	- フ・ブロ ・	• • • • •	-0.0			• 307
0033	21.7 42.7	6.92 16.0		-0.0		0 0.0	• 310
00.90	13.3 -8.8	5.05 -15.3		-0.0	0.0 -0.0	0 0.0	• 381
0092	14.2 -2.6	5.25 -12.0		-0.0	0.0 -0.0	n 0.n	.370
0094	18.1 24.8	6.29 5.5		-0.0	0.0 -0.0	0.0	• 347
0108	11.7 -19.8	6.51 9.2		-0.0	0.0 -0.0	0.0	•558
0109	5.3 -63.5	3.85 -35.4		-0.0	0.0 -0.0	0.0	•726
0110	12.8 -11./	7.02 17.7	• • • • • • • • • • • • •	-0.0	0.0 - 0.0	0 0.0	•547
0111		- ち・ちフ ユビ・ビ - ム・Rワ 14 4		-0.0	$0 \cdot 0 - 0 \cdot 0$		●404 545
0112	18.3 25.8	6.50 8.9		-0.0			.355
0115	11.7 -19.3	5.45 -8.6		-0.0	0.0 -0.0	0 0.0	.454
0196	14.1 -3.1	6.49 8.9		-0.0	0.0 -0.0	0 0.0	.461
0097	11.5 -21.2	5.10 -14.5		-0.0	0.0 -0.0	0.0	.445
0099	18.1 24.7	6.73 12.9		-0.0	0.0 -0.0	0.0	.371
0103	13.9 -4.2	7.57 27.0		-0.0	0.0 -0.0	0.0	•543
0104	17.6 20.9	7.60 27.5		-0.0	0.0 -0.0	0 0.0	•432
0105	20.7 42.1	7.27 22.0		~0.0	0.0 -0.0		•352
0105	14 0 22 4	с. ис р. ис р.				0 U.U.	• 384 759
0107 	10.3 -29.2	5.56 -6.7		-0.0 	0.0 -0.0		• 507 540
0101	13.9 -4.7	5.14 -13.8		-0.0	0.0 -0.0	0.0	.371
0102	15.8 8.9	5.63 -5.5		-0.0	0.0 -0.0	n 0.0	•356

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	0107	10.0	23.9	6+40	0.4			0.0	-0.00	ULU	•359
	0100	10.3	-29.2	5.56	-6.7		-0.0	0.0	-0.00	0.0	.540
	0101	13.9	-4.7	5.14	-13.8		-0.0	0.0	-0.00	0.0	.371
	0102	15.8	8.9	5.63	-5.5		-0.0	0.0	-0.00	0.0	•356
•••	0161	20.3	39.7	6.57	10.2		-0.0	0.0	-0.00	0.9	.324
		15.8		5.64	-5.5		-0.0	0.0	-0.00	0.0	357
	0010	17 5	20 5	5 90	5	*	-0.0	0 0	-0.00	0 0	• J J I Z II O
<u> </u>	0019		20•J		ം പ	11-2		- 0 • 0	~_0.010	0_0	246.
	0020	14.6	• 5	5.38	-3.0		-0.0	0.0	-0.00	0.0	• 367
	0021	11.8	-19.0	4.55	-23.8		-0.0	U • 0	-0.00	U. U	• 386
	0055	13.0	-10.3	5.19	-13.0		-0.0	.0 • 0	-0.00	0.0	• 398
	0028	14.3	-1.6	5.21	-12.6	÷	0.0	0.0	0.00	0.0	•364
	0030	13.8	-5.1	4.76	-20.2	<u>n-4</u>	0.0	0.0	0,00	0.0	• 345
	0032	11.8	-18.8	4.87	-18.4		0.0	0.0	0.00	9.0	.412
	0037	19.1	31.4	7.05	18.2		0 - 0	0.0	0.00	0.0	. 369
	00007	18 4	26.4	7.05	18.2	11.7	0.0	n. n	0.00	0 0	- 307
	0030	15.4	7 6	7.03	<u> </u>	11-6	<u> </u>	0.0	0.00	0.0	• 385
	0039	11.0	1.0	6.30	7.0		0.0	0.0	0.00	0.0	• 4 0 2
	0()4()	14.5	6	6.37	1.2		U.U	0.11	0.10	U.U	•442
	0041	17.1	17./	6.88	15.5		0.0	0.0	0.00	0,0	•402
	0042	13.3	-8.4	5.77	-3.2	Y	0.0	0.0	0.00	0.0	•434
	0043	13.2	-9.5	5.56	-6.7	11-7	0.0	0.0	0.00	0.0	•423
	0044	14.2	-2.4	5.34	-10.4		0.0	0.0	0.00	0.0	•376
	0045	12.7	-12.5	5.05	-15.4		0.0	0.0	0.00	0.0	• • 397 ·
	0046	13.6	-6.5	5.25	-12.0		0_0	0.0	0.00	0.0	- 386
	0156	<u> </u>	-5× 6	- <u>6 88</u>	18.2		-0.0	0.0	-0.00	0.0	.723
	0150	10.0	- 0.0 1	F (1	-10.2		~0.0	0 0		0.0	•72J 527
	9128	10.4	-28.1	J •DT			-0.0	0.0	-0.00	0.0	• 337
	0160	6.1	-57.8	4.84	-18.9	— ``	-0.9	0.0	-0.00	0.0	• 788
	0053	15.5	6.3	5.49	-8.0	Ý .	0.0	0.0	0.00	0.0	•355
	0054	12.7	-12.8	5.14	-13.8	11-9	0.0	0.0	0.00	0.0	•405
	0154	13.2	-8.9	5.30	-11.1		-0.0	0.0	-0.00	0.0	.400
	0057	9.5	-34.9	5.45	-8.7	- ↓ .	0.0	0,0	0.00	0.0	•575
	0058	12.6	-13.2	5.31	-19.9	11-10	0.0	0.0	0.00	0.0	.421
	ີ້ທຸກລຸດ	10.6	-27.2	4.54	-23.9		0.0	0.0	0.00	0.0	.429
-	0060	13.6	-6.2	5.95	- 2		0.0	0.0	0.00	0.0	.437
	0001	10.0	-45 2	1 97	-19 7		-0.0	0 0	-0 00	<u> </u>	<u> </u>
	0144	0.0	-4.1.4	0 17	27 0		-0.0	0.0	-0.00	0.0	•011
	0147	24.2	65.2	8.1/	21.0		-0.0	U.U.	-0.00	0.0	• 3 3 0
	0148	7.0	-51.8	3.69	-38.2		-0.0	0.0	-0.00	0.0	• 526
	0065	15.0	3.2	6.27	5.1	Ý.	0.0	0.0	0.00	0.0	•417
	0086	12.7	-12.8	6.03	1.1	11-11	0.0	0.0	0.00	· 0 <u>.</u> 0	•476
_	0138	9.3	-36.1	4.35	-27.0		-0.0	0.0	-0.00	0.0	.468
	0139	12.0	-17.2	6.36	6.6		-0.0	0.0	-0.00	0.0	•528
	0140	14.9	2.5	6.61	10.8		-0.0	0.0	-0.00	0.0	•443
·	0141	10.8	-25.9	5.73	-3.9		-0.0	0,0	-0.00	0.0	•532
	0142	12.5	-13.9	5.98	.3		-0.0	0.0	-0.00	0.0	.478
	0067	13.9	-4.3	5.77	-3.2		-0.0	0.0	-0.00	0.0	.415
	0059	11 5	-20 7	5 48	-4 A	11 12	-0.0	0.0	-0.00	0 0	. 492
·	0020	17 0	20.1	2 05	15	11-13	-0.0	0 0	-0 00	- 0 0	340
	0037	1/.0	22.J	6+0J	7.0		-0.0	0.0			- 279
	0071	10.2	11.2	5.93	∠•* స‴≘ •		<u> </u>	0.0	-0.00	0.0	• 360
	0125	11.6	-20.5	6.90	12.8		-0.0	0.0	-0.00	0.0	• 390
	0127	15,5	-3,8	7.32	22.8		-0.0	0.0	-0.00	0.0	•552
	0128	19.3	32.5	7.69	29.0		-0.0	0.0	-0.00	0.0	• 399
·	0129	17.8	22.5	7.07	18.6		-0.0	0.0	-0.00	0.0	• 397
	0130	12.9	-11.0	7.01	17.5		-0.0	0.0	-0.00	0.0	•541
	0131	7.5	-48.1	4.01	-32.7	·	-0.0	0.0	-0.00	0.0	.532
•====	0072	15.4	5.7	5.23	-12.3		-0.0	0.0	-0.00	0.0	.340
	0073	15.6	7.2	5.36	-10.1	11-14	-0-0	0.0	-0.00	0.0	344
	0074	23 3	60.5	7.11	14 2		_n _n	<u> </u>	<u>_n na</u>	<u> </u>	205
	0075	20.0	<u>и</u> я 5	6.55			_ <u>n</u> _n	0 0	-0.00	0.0	202
	0070	27.0	 		10 0	· · · · · · · · · · · · · · · · · · ·			-0.00		• 303
	00/5	20.7	04•1	1.03	<u> </u>	- -	~U.U		-0.00	U.U	•532
		14.U	-0.7	2.89	-1.2	·	-0.0	U.0	-0.00	U.U.	.422
	5673	12.9	-11-S	6.03	1.2	11-12	-0.0	U • 0	-0.00	0.0	•467
·	0079	13.5	-7.1	5.38	-9.7		-0.0	0.0	-0.00	0.0	.399
	0080	14.6	•7	5.93	~.5		-0.0	0.0	-0.00	0.0	.405
	0091	14.5	0	5.49	-7.9		-0.0	0.0	-0.00	0.0	.377
	0119	15.0	3.2	7.81	31.0	· · · · · · · · · · · · · · · · · · ·	-0.0	0.0	-0.00	0.0	.521

0072	15.4 5.7				
0073		5. 25 -12.5 V	-0.0 0.0 -	0.00 0.0	• 34
	15.6 7.2	5.36 -10.1 11-14	-0.0 0.0 -	0.00 0.0	• 34
0074	23.3 60.5	7.11 19.2	-0.0 0.0 -	0.00 0.0	• 30
0075	21.6 48.5	6.55 7.7	-0.0 0.0 -		•36
0076	23.7 64.1	<u>7.05 10.0</u>			•29
0078	$17 \cdot 0 = 2 \cdot 2$	<u> </u>		0.00 0.0	
0070	$12 \cdot 7 = 11 \cdot 2$ 13 5 = 7.1	5.38 -9.7		0.00 0.0	•46 zg
0077	14.6 .7	5.93 -5	-0.0 0.0 -		<u>•37</u>
0081	14.50	5.49 -7.9	-0.0 0.0 -	0.00 0.0	. 37
0119	15.0 3.2	7.81 31.0	-0.0 0.0 -	0.00 0.0	-52
0120	7.5 -48.4	6.37 6.9	-0.0 0.0 -	0.00 0.0	.84
0122	7.4 -49.0	4.79 -19.7	-0.0 0.0 -	0.00 0.0	•64
0123	5.3 -63.3	3.26 -45.4	-0.0 0.0-	0.00 0.0	.60'
0124	7.3 -49.6	4.85 -18.5	-0.0 0.0 -	0.00 0.0	•66.
0084	20.2 38.8	6.30 5.7 😽	-0.0 0.0 -	0.00 0.0	•31
0085	20.6 41.8	6.22 4.3 11-16	-0.0 0.0 -	0.00 0.0	•302
0114	23.1 58.7	8.11 36.0	-0.0 0.0 -	0.00. 0.0	•352
0115	18.2 25.0	7.52 26.2	-0.0 0.0 -	0.00 0.0	•41'
0116	22.9 57.5	7.81 31.0	-0.0 0.0 -	0.00 0.0	•343
U117	23.9 64.5	7.29 22.3	-0.0 0.0 -	0.00 0.0	•305
0118	22.3 53.5	6.92 16.0	-0.0 0.0 -	0.00 0.0	.31(
N0. OF	STATIONS 1	25	0		
	INTEGRATED POWER	MEAN FREQUENCY	PREDOM POWER F	I N A N T REQUENCY	Powe
	E 14.54	5.96	0 000	0.000	
AVERAG			0.000		•
SIGMA	4.23	•96	0.000	0.000	•
AVERAG SIGMA PER CEN	4.23 T 29.08	•96 16•13	0.000	0.000	24.'
SIGMA PER CEN + SIGM	4.23 T 29.08 A 18.77	•96 16•13 6•92	0.000	0.000 0.000 0.000	• •
AVERAG SIGMA PER CEN + SIGM - SIGM	4.23 T 29.08 A 18.77 A 10.31	•96 16•13 6•92 5•00	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	. 24.
AVERAG SIGMA PER CEN + SIGM - SIGM MIN/ST	4.23 T 29.08 A 18.77 A 10.31 A 5.31/01	•96 16•13 6•92 5•00 3•26/0123	0.000 0.000 0.000 0.000 0.000 *0.00/0001 *0	0.000 0.000 0.000 0.000	24. 29/

BEOWAWE THE FOLLOWING ARE PERCENTAGE DEV STATISTICS AND DEVIATIONS 0.5 - 7.5 Hz.

5		ም እነ ም ሮ* ···		u.a /~	A 61				Thin	NI	
1	STA.	POWER	PCDEV -	FRED.	PCOEV	•	POWER P		FRED.	PCDEV	
년 3년 8월 <u></u>			· • • • • •	• • • • • • • • •		-			j t t (N) ●		PU
(0001	17.4	1.0	3.17	2.8	₹	-0.0	0.0	-0.00	0.0	•
c (1084	23.4	35.4	3,39	10.1	11-16	-0.0	0.0	-0.09	0.0	•.
. (0085	24.6	43.2	3.47	12.8		-0.0	0.0	-0.00	0.0	•
<u> </u>	<u>)114</u>	17,4	1.3	3.34	. 8,4		-0.0	0.1	-0,00	0.0	
4 (0115	15.5	-10.1	3.16	2.6		-0.0	0.0	-0.00	0.0	•
(0116	19.2	11.9	3.46	12.4	· · · ·	-0.0	0.0	-0.00	0.0	an an an 🖕
[]	<u>)117</u>	22.7	32.2	3.40	10.4		-0,0	<u> </u>	-0.00	0	•
	J118	22.7	31.8	3.28	6.6		-0.0	U ()	-0.00	0.0	•
	10.51	17.1	11.5	3.UJ 7.0%	-,9		U_U	0.0	0.00	0.0	•
	1033	L/ + 4	$\frac{1.4}{22}$	2 10	<u>-1.0</u>		0.0	0.0	0.00		•••••••••••••••••••••••••••••••••••••••
	1034	21.2	R.	5 97	-3.5	· · · · ·	- U.U.	n b	0.00	0.0	e grat 📍
	1035	· 19 6	1 4 8	3.26	5.8		0.0	0.0			•
·	1047	19 5	17.6	3.47	12 8		<u> </u>	0 0	0.00	<u> </u>	••-
	1047 1043	20.1	16.6	3.53	14.6		0.0	0.0	0.00	0.0	. •
	1049	15.7	-8.4	2,90	-5.7		0.0	0.0	0.00	0.0	. •
	0050	21.0	22.3	3.83	24.3		0.0	0.0	0.00	0.0	······································
1 (0051	21.9	27.5	3.60	17.0	• •	0.0	0.0	0.00	0.0	
	0133	9.0	-47.4	2.60	-15.6	· . · ·	-0.0	.0.0	-0.00	0.0	
(0134	12.7	-26.3	2.79	-9.3		-0.0	0.0	-0.00	0.0	•
:)135	11.1	-35.6	2.89	-6.0		-0.0	0.0	-0.00	0.0	
(1136	16.3	-5.4	2.96	-3.9		-0.0	0.0	-0.00	0,0	<u> </u>
. (2600	19.3	12.4	3.17	3.0	••	-0.0	0.0	-0.00	0.0	•
	0083	21.4	24.7	3.36	9.0		-n.0	0.0	-0.00	0.0	•
(086_	13.6	3.1	2,98	-3.4		-0.0	0.0	-0.00	0.0	•
(0087	21.1	22.5	3.31	7.4	•	-0.0	0.0	-0.00	0.0	•
(8800	22,6	31.5	3.54	14.9		-0.0	0. 0	-0.00	0.0	•
(01189	22.5	30,9	3.48	12.9		-0.0	0.0	-0.00	0.0	•
· · · · (0095	15.7	-8.5	3.12	1.2		-0.0	0.0	-0.00	0.0	•
l l	096	16.0	-7.0	-3.21	6.2		-0.0	0.0	-0.00	0.0	•
i	1097_	15.1	-6.3	2.94	<u></u>		-0.0	0.0	±9•.0 <u>0</u>		•
l	1098	13.4	-22.1	2.14	-10.9		· ~0.0	0.0	-9.00	0.0	•
	JU99	20.5	19.0	3,43	11.2	•	-0.0	0,0		0.0	•
	1100	<u>13.6</u>	15 3	3 17	ـــــــــــــــــــــــــــــــــــــ		0_0			0.0	•
	J 4 1) 3 A T A T	20 A	21 2	3 18	· ∠.,) スス		-0 <u>0</u> 0	0,0 10 0	-0.00	0.0	•
	1161	20.0	34.3	3.45	12.1		-0.0	0.0 ·	-0.00		•
	0103	12.5	-27.4	3.10	. 6		-0.0	0.0	-0.00	0.0	
(0104	15.9	-7.5	3.05	- 8		-0,0	0.0	-0.00	0.0	
<u>í</u>	0105	20.0	16.3	3.14_	1.9		-0.0	0.0	-0.00	0.0	
(0106	24.3	41.4	3.28	5.6	•	-0,0	0.0	-0.00	0.0	
	0107	20.8	20.9	3.08	1	instantina (h. 1947). 1	-0.0	0.0	-0.00	0.0	•
	0003		29.3	3.44	11.7		-0.0	0_0	-0.00_	00	
	2000	20.2	17.6	3.38	9.8	♥	-0.0	0.0	-0.00	0.0	•
l l	0005	21.6	25.6	3.53	14.6	10-30	-0.0	0.0	-0.00	0.0	•
1	0006_	18.7_	8.9				-0.0	_ 0., 0:	-0.00_	0	
	0009	16.2	-5.6	3.29	5.8		-0.0	0.0	-0.00	0.0	•
· •	0009	19.3	12.4	3.23	5.0	*	-0.0	0.0	-0.00	0.0	•
(010		204	_3.28_	<u> </u>	10-31			-0.00_	0	
	0011	19.6	14.0	3.16	2.5	ı.	-0.0	0,0	-0.00	0.0	٠
i	0013	19.9	12.1	5.10	2.5	▼ 111	-0.0	U.0 ·	-0.00	0.0	•
.	0014		11.5	<u>_3.12</u>	1.5	• • •	-0.0	U.0	-0.00	0.0	
		19.9	10.0	<u>3.15</u>	2.6		-0.0	<u> </u>	-0.00	<u> </u>	
	0010	10.7	12.0	2.17	<u>-1.6</u>		• U • U	U.U ·	-U.UU	U.U	•
,	0010	17.3	16.6	0+1/ 2 0≝	5 •0	, 11_7	∽U,U	U . 9	→U.UU	U . U	•

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		0105	20,0	16.3	<u>3 • 14</u>	<u> </u>		-0.0	<u> </u>	-0.00	0.0	- 14
1	1.y.	0105	24.3	41.4	3.28	6.6		-0.0	0.0	-0.00	0.0	
	4	0:07	20.8	20.9	3.08	- 1		-0.0	0.0	-0.00	0.0	• 1
	-	0003	22.2	24 3	3 44	11 7		-0.0	0.0 0 0	-0.00	0.0	· • 14
		0005	<u> </u>		2 20	. 11.07		·····			0.0	•1!
	-	0012	20.2	11.0	3.33	9.8	•	~U_U	0.0	-0.00	0.0	•1f
,	× ±	0005	21.6	25.6	3.53	14.6	10-30	-0.0	υ.Ο	-0.00	⁻ 0₊0	. 14
I		0005	18.7	8.9	3.34			-0.U	0.0	-0.00	0.0	1.
•	a set	0003	16.2	-5.6	3.29	6.8	·	-0.0	0.0	-0.00	0.0	
~	1	0009	14 3	12 4	3 23	5 6	-1	-0.0	0 0	-0 00	ຄົດ	• 21
1		0007	12.3	22.	7 20		¥ (5-3)	-3.0	0,0		0.0	∑∙Lt
						<u> </u>	10-51	<u> </u>		-1.00	U	
		0011	19.6	14.0	5.16	2.5		-0.0	0,0	-0.00	0.0	•1f
2		0013	19.9	15.7	3.16	2.6	4	-0.0	0.0	-0.00	0.0	.15
1		0014	19.2	11.5	3.12	1.5	11-1	-0.0	0.0	-0.00	· 0.0	16
Ę	÷	0015	19 9	15 6	3.16	2 6	• •	-0 0	0 0	-0 00	0 0	• • • • • • • • • • • • • • • • • • •
~ .		0015	100		0 95	7 /		0.0	0 0	0 00	0.0	• 1:
9		0016	10.0		2.00	-1.5		-0.0	0.0	-0.00	0.0	•1/
ŧ,		0019	19.3	15.5	3.17	3.0	Y	-0.0	U . 0	-0.00	0.0	•16
		0019	20.3	18.3	3.25	្ភ ្5	11-X	-0.0	0.0	-0.00	0,0	•1ć
2		0020	18.3	6.5	2.95	-4.1		-0.0	0.0	-0.00	N . 0	•1f
9 9 7		0021	16.5	-4.0	2.73	-11.4		-0.0	0.0	-0.00	0.0	.16
100		6022	16 9	9	2 97	-3 (1		-0 0	0 0	-0 00		• • •
_	· .	2200	10.7	77.0	7.00	10 /		0.0	0.0	-0.00	0.0	• 1 /
ð (1	0023	23.6	J/.U	5.45	12.4	- T	-0.0	U . U	-0.00	U _U	•14
<u>ا</u> د	2 ·	0024	22.3	29.7	3.41	10.8	<u>د -اا ا</u>	-0.0	0.0	-0.00	0.0	.15
1	1	0025	20.0	16.3	3.06	6	• .	-0.0	0.0	-0.00	0.0	.15
5	-	0026	18.1	5.3	2.89	-6.1		-0.0	0.0	-0.00	0.0	.16
.		0020	18 9	9.2	3 19	37		-0.0	0 0	-0 00	0 0	17
1	•	0021	10.0	7 0	2 00			0 0	0.0	0.00	0.0	
1	7	0028	- 10-0	1.0	2.07	~6.1	Tara di si	0.0	.0.0	0.00	0.0	.1:
-	5	0030	18.6	8.0	2.77	-9.9	11-4	΄ υ ,υ	0.0	0.00	0.0	•14
	· · ·	0032	15.7	-3.9	2.70	-12.2		0.0	0_0	0.00	0.0	.17
1		0037	18.2	6.0	3.08	1	1	0.0	0.0	0.00	0.0	.16
۰ ۲	-	0039	17.6	2.6	3.15	2.3		ດ. ແ	0.0	0.00	0.0	.17
¥ :	•	0000	17.0	2.0U	2 42		11-6	0 0	0.0	0.00	0.0	• 1 1
1	: م الم الم الم الم الم الم الم الم الم الم	0034	17.2	~ • <u>८</u>	2.03	-0.1		0.0	0.0	0.00	0.0	•15
	1	0040	15.2	-11.8	2.14	-10.9		U . U	0.0	0.00	0.0	•18
9.3		0041	16.8	-2.5	3.08	1		0.0	0.0	0.00	0,0	•18
- ,		0156	8.2	-52,1	2.30	-25.2	¥	-0.9	0.0	-0.00	0.0	.27
		0158	12.5	-27.2	2.75	-10.8	11-7	-0.0	0.0	-0.00	0.0	.22
		0160	. 7 1	-59.9	2.18	-29 1		-0.0	0 0	-0 00	0.0	30
<u>.</u>		0100	16 0	- 50+2	2 0 2			-0.0	0.0	-0.00	0.0	• 30
	•	0042	13.9	- / • 0	3.03	<u>-1-5</u>		0.0	0.0	0.00	<u> </u>	• 17
		0043	16.6	-3.2	3.10	• 8		0.0	0.0	0.00	0.0	18
* - :		0044	18.6	8.3	3.19	3.5		0.0	0.0	0.00	0.0	•17
:		0045	17.4	1.4	3.14	1.9		0.0	0.0	0.00	0.0	.18
• •		0046	18.3	6.7	3.18	3.3	· · · · · · · · · · · · · · · · · · ·	0.0	0_0	0.00	0.0	.17
<u>م</u>		0052	20.2	175	2 47	4 6	<u> </u>	0 0	0 0	0 00	ີກິດ	16
6	÷ ;	0000	40.2		0 + 0 fr - 0 - 0 - 0		¥ 11-0		0.U n n			• 10
•		0054	16.3	-5.4	2.99	-2.9	11-7	0.0	0.0	0.00	<u> </u>	•18
_ !	22	0055	14.9	-13.6	3.07	5		. 0 . 0	υ.Ο	U.00	0.0	20
3		0154	16.8	-2.4	3.42	- 1 Ŭ •9		-0.0	0.0	-0.00	0.0	•20
,		0144	10.4	-39.6	2.62	-14.8		-0.0	0.0	-0.00	0.0	.25
÷.		0147	18.9	10.2	3.59	15.6	11-10	-0.0	0_0	-0.00	0.0	.19
3		<u>П</u> 1ЦЯ	9.9	-42.3	1.85	-40.0		-0_0	0.0	-0.00	0_0	_ 1 R
7		0170	11 1	_75 5	2 57	_1_ F		0 0	n n	0.00		
1		0057	11.1	-55.5	2.17	-10.5		0.0		0.00	0.0	•23
1.1		0058	12.8	-8.3	3.13	1.6		0.0	0.0	0.00	0.0	•19
3	2	0059	12.3	-28.7	2.28	-26.1		0.0	0.0	0.00	0.0	.18
• 1	1	0060	14.7	-14.6	2.63	-14.7		0.0	0.0	0.00	0,0	.17
	J	0061	15.6	-9.0	2.86	-7.0		0.0	0.0	0.00	0.0	.18
۵.	•	0138	127	-26 11	2.60	-15 7		-0 ŭ	0 0	-0 00	0 0	20
2		0100		2040	2 10	7 9	v		0 0		0.0	
	;	0139	12.7	-24.7	3.17	3.1		-0.0	U . U	-1.00	······································	•24
_	1	0140	15.1	-11.9	3.06	-,6		-0,0	U.O	-0.00	U.U	.20
€:	-	0,1.41	12.0	-30.1	2.78	-9.7		-0,0	0.0	-0.00	0.0	.23
•		0142	13.6	-20.8	2.97	-3.6		-0.0	0.0	-0.00	0.0	.21
· ·		0042	144	-16 5	2.95	-4 2		<u>n n</u>	<u>n</u> n	0 00	<u> </u>	nc
3		0092	1 <u>_</u>	_11 7		2 0			0.0	0.00	0.0	• ~ 0
1			10.1	~~ (J+1/	U.U.			0.0	0.00	0.0	•17
-		0064	11.6	2.0	3.20	4.0		<u> </u>	0.0	U.UU	<u>U.U</u>	.18
	1	0065	16.3	-5.0	3.40	10.4		0 . Ŭ	0.0	0.00	0.0	•20
)	: · _	0066	13.6	-20.7	2.99	-2.9		0.0	0.0	0.00	0.0	21
	.)	0125	10.9	-35.6	2.96	-3.9		-0.0	0.0	-0.00	0.0	.27
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		• 7 7 1	7 1111 11 11						
- 	012/ 1	1.3 -34.4	3.04 -1.1		-0.0	0.0 -0.00	0.0		• ?
•	0128 1	6.1 -6.5	3.22 4.4		-0.0	0.0 -0.00	0.0		• 7
	0129 1	6.8 -2.5	3.19 3.7		-0.0	0.0 -0.00	0_0		3
	0130 1	1 6 -32 7	2,911 -5 9		-0 0	n - n - n			• • •
	0100 1				0.0	0.0.0.00	0.0		• 6
) _ +	0121 1		2.21 -20.2		-0.0	0.0 -0.00	0.0		• 7
	0067 1	6.7 -2.8	3.49 13.3		-0.0	0.0 -0.00	0.0		• 2
;	0068 1	3.5 -21.7	3.04 -1.3		-0.0	0.0 -0.00	0.0		
ing.	0.069 2	0.9 21.7	3.51 14.1		-0.0	0 0 -0 00	0 0		•
	0000 2	× 0 . 24 2	0 68 . 10 8		. 0 . 0		0.0		• 1
<u></u>	0070 1	5.0 -24.2	2.00 -12.0	· · · · · · · · · · · · · · · · · · ·	-0.0	0.0 -0.00	<u>u</u> .u		• 2
-	0071 1	9.4 13.1	5.28 6.4		-0.0	0.0 -0.00	0.0		• 1
)	0972 2	0,3 18.1	3.23 4.9	4	-0.0	0.0 -0.00	0.0		.1
- (0073 2	1.0 21.9	3.44 11.6	11-14	-0.0	0.0 -0.00	0.0		1
<u> </u>	0074 2	2 9 24 8	3 58 16 3		-0.0		0 0		•
•	0077 2		7 E0 17 E		-0.0		0.0		• 1
•	0075 2	4.2 49.6	2.20 13.2		-0.0	0.0 -0.00	0.0		•1
	0076 2	4.7 43.4	3.67 19.1		~0.0	0.0 -0.00	0.0		.1
	0119 1	1.5 -32.9	3.29 7.0	-1	-0.0	0.0 -0.00	0.0		2
1	0120	7.0 -59.1	2.51 -18.5	11-1-1-	<u></u>	0 0 -0.00	0 0		•
2	0120	$\mathbf{r} = 0 - 0 \mathbf{r} = 0$		11-12	-0.0		0.0		• 3
-	0122	9.6 -44.0	2.47 -17.0		-0.0	0.0 -0.00	0.0		•5
_, !	0123	7.1 -58.5	1.21 -60.8		-0.0 ·	U.0 -0.00	0.0		.1
	0124	9.4 -45.0	2.66 -13.7		-0.0	0.0 -0.00	0.0		2
	0125	6 2 -64 1	1.12 -63 5		-0 0		ດັດ		•
		50.75	7 07 -1 7		-0.0	0.0 0.00			• L
	0077 1	5.7 -1.5	5.05 -1./		#U_U		ប្រូប		•1
) =	0078.1	4.0 -18.7	3.08 .1		-0.0	0.0 -0.00	0.0	•	•2
	0079 1	6.8 -2.4	3.26 5.7		-0.0	0.0 -0.00	0.0	•.	•1
	0080 1	6.3 -5.4	3.06 -5.5		-0.0	0.0 - 0.00	0.0		1
	0081 1	8 2 5 9	X 11 9		-0.0	0 0 - 0 00	0.0		• 1
7		0.2 3.7			-0.0	0.0 -0.00	0.0		• 1
s	<u> </u>	1.18	3.14 2.0	\$	-11.0	<u>u.n -0.00</u>	0.0		. 1
	0109 1	2.6 -26.4	2.85 -7.4	11-18	-0.0	0,0 -0,00	0.0		.2
) [a]	0110 1	7.3 .8	3.33 8.1		-0.0	0.0 -0.00	0.0		. 1
	0111 2	n u 21 7	ζ ζη 7 μ		-0.0	$\partial \rho = \rho \rho \rho$	0 0		• -
ľ <u> </u>					0.0	0.0.00			0 .
	0112 1	1.2 .2	3,28 6,4		-0.0 -	0,0 -0,00	0.0		•1
	0113 2	5.0 45.4	3.27 6.1		-0.0	0.0 -0.00	0.0		.1
2.138 2.138	0090 2	3.3 35.6	3.36 9.1		-0.0	0.0 -0.00	0.0		. 1
1	0091 2	1 4 24 3	3.28 6.4		- 0 0	0 0 -0 00	0.0		1
	0002 2				0 0		0.0		• 1
	0092 2	4.2 40.0	3.49 13.2		-0.0	0.0 -0.00	0.0	• .	•1
<u>.</u>	0094 2	5.3 47.1	3.42 10.9		-0.0	0.0 -0,00	0_9		1
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4	STATION	POW. FRQ.	POW. FRQ.	POW. FRQ.	POW. FRQ.	POW. FRO. PO
	• 0023	11.91 1.73	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.
	11-030024	11.56 1.77	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.
T.	<u> 1025</u>	11.60 1.76	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.
	0026	11.18 1.68	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.
	0027	10.37 1.75	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.
h	0031	10.73 1.68	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.
	0033	8,98 1,72	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.
H	0034	11.14 1.69	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 n.
Ē	0035	6.64 1.49	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.
577	0036	9.41 1.74	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.
μų	0047	7.90 1.61	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.
1.7	0048	8.44 1.62	0.00 0.00		0.00 0.00	0.00.0.00 0.
	0049	7.98 1.46	9.00 0.00	0.00 0.00		0.00 0.00 0.
	0050	8.27 1.42	0.00 0.00	0.00 0.00		0.00 0.00 n.
	11051	0.34 1.07	0.00 0.00			
	0052				0.00 0.00	
	0.055	2,90 1,40 2,84 1,34	0.00 0.00			
1	0055	10.03 1.74				
	7 0001	9 34 1 74				
	(0-30 0002	9 56 1 74	0.00 0.00			
	0.005	9 92 1 74	0.00 0.00	0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.
-	0000	9.20 1 74	0.00 0.00			
19-11 19-21	0008	7 81 1 68	0.00 0.00			
	9000	9.91 1.76		0 00 0 00	0.00 0.00	
	⁶⁻³¹ 0010	10.75 1.83	0.00 0.00	0 00 0 00		
-	0011	10.24 1.73	0.00 0.00			0.00 0.00 0.0
	0012	9.11 1.71	0.00 0.00	0.00 0.00	0.08 0.00	0.00 0.00 0.0
	÷ 0013	11.79 1.77	0.00 0.00	0.00 0.00	N.00 0.00	0.00 0.00 0.0
	11-1 0014	11.09 1.69	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.0
-	0015	10.25 1.71	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.0
	0016	9.46 1.59	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.0
1	0017	10.62 1.65	0.00 0.00	0.00 0.00	0.00 0.00	0.00 9.00 0.0
z -	0018	10.27 1.74	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.0
14	0019	11.02 1.74	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.0
	0020	11.15 1.72	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.0
	0021	10.24 1.71	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.0
	0022	9.94 1.77	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.0
<u> </u> -	0028	10.65 1.75	0.00 0.00	0.00 0.00	0.00 0.00	<u>0.00</u> 0.00 0.00
•••	0030	11.21 1.75	0.00 0.00	0,00 0,90	0.00 0.00 =	
·		9.14 1.81	0.00 0.00	0.00 0.00	0.00 0.00	
	• 0.03.7	9.41 1.77	_0.00_0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.00
	0038	9.16 1.75	0.00 0.00	0.00 0.00	0.00 0.00	0.00 2.00 0.00
ł	0039	9.75 1.71	n.0n 0.00	0.00 0.00	0.00 0.00	
	0040	8.63 1.60	0.00 0.00	0.00 0.00	0.00 0.00	0.00 1 00 0.0(
	0041	3.81 1.67	0.00 0.00	0.00 0.00	0.00 0.00	
	<u>+ 0042</u>	9.63 1.69	0.00 0.00	0.00 0.00	0.00 0.00	0.00 5.00 0.0(
	11-7 0043	10.17 1.76	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.00
	0044	10.82 1.76	9.00 0.00	0.00 0.00	0.00 0.00	0 00 0.00 0.00
	0045	10.10 1.67	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00 0.00
\subseteq	0164	<u>10.12 1.10</u> 5 50 1 H1		U.UO 0.00	0.00 0.00	0.00 0.00 0.00
L_{i}	0120	J.J7 1.441	0.00 0.00	U_8A 0_00		1967 - J. S. M. N.

		6000	7,410	1. I J	$\mathbf{U} \bullet \mathbf{U} \mathbf{U}$	0.00	0.00	0.00	0.96	0.00	0.07	ע עיי	11
		0039	9.75	1.71	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0,00	£
	• •	0040	8.63	1.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
	:	0041	8.61	1.67	0.00	0.00	n.ao	ກີ່ຄຸ	0.00	0.00	0.00	0 00	r l
~ ·	*	0041	9.63	7 29	0 00	0 00	n un	0 00	0 00		0 00	0.00	
		11.7 0042	10.17	1 7/	0.00	0.00	0,00	0.00	0.00	0.00		0.00	2
		0043	10.17	1.70	0.00	0.00	0,00	0.00	0.00	0.00	0.00	0.00	
		0044	10.82	1.76	0.00	0.00	0.09	0.00	0.00	0.00	0.00	0.00	0
0		0045	10.08	1.69	0.00	0.00	0.00	0.00	0,00	0.00	0.00	0,00	Ũ
		0046	10.12	1.78	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0
	í l	0156	5,59	1.41	0.00	0,00	0.00	0.00	0.00	0.00	0.00	0.00	0
-	14	0158	6.16	1.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	Û
·		10057	7.34	1.62	0.00	0.00	0.00	0,00	0.00	0.00	0.00	0,00	0
I	F	11-10 0054	<u>, , , , , , , , , , , , , , , , , </u>	1 72	0 00	0 00	0.00	<u> </u>	0 00	0 00	0 0 0	0.00	ň
		0000	7.e≤1 007	1 / 2	0.00	0.00	0,00	3 00	0.00	0.00	0.00	0.00	
$\mathbf{\mathbf{U}}$	17	0059	8.57	1.00	0.00	0.00	0.00	0.00	0,00	0.00		0,00	
	<u> </u>	0060	10,05	1.6/	0.00	<u> </u>	<u> </u>		<u> </u>	<u> </u>	<u>.0</u> •00 -		U
	Č.	0061	9.11	1.75	0.00	0.00	0,00	0.00	0.00	0.00	0.00	0.00	0
11	[ŋ145	6,71	1.45	0.00	0.00	0.00	0,00	0.00	0.00	0.00	0.00	6 '
		0147	8.16	1.78	0.00_	0.00	0.00	_0.00 _	0.00	_0.00_	0.00	0.00	.0
	7.	0148	7.42	1.36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0
	- 1	1 0.042	9.22	1.74	0.00	0.00	0,00	0.00	0.00	.0.00	0.00	0.00	0
i T	7.1 20	11-11 000%	0 73	1 49	0 00	. n nn	0 00	0 00	0 00	0 00	0 0 0	0 00	õ
	ļ. :	0055	7•12_		0.00	<u> </u>	0.00	0 00	0 00	0 00	_0,00. 	0.00	U
1	1	0064	10.07		0.00	0.00			0.00	0.00	0.00	0.00	0
3 1	e -	0065	8,66	1.78	0.00	0.00	0.00	0,00	0.00	U,UU	0.00	0.00	U
1	· · · · · · · · ·	0.0.66	8.56_	1.77	0.0.0	0_00_	0.00		0.0.	0,00	_0.00	00	. 0
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ξı.	24	11-13 0068	7.46	1.63	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0
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BEOWAWE CROSS SECTIONS

for

CHEVRON OIL COMPANY

SENTURION SCIENCES, INC. TULSA, U.S.A.





BEOWAWE AREA GROUNDNOISE CROSS SECTION B-B'

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FIGURE 18 Senturion Sciences, INC.





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FIGURE 20 SENTURION SCIENCES, INC.



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APPENDIX 1a BEOWAWE, NEVADA INTEGRATED POWER/MEAN FREQUENCY CROSS SECTIONS

> SENTURION SCIENCES, INC. TULSA, U.S.A.



SENTURION SCIENCES, INC.

1539 NORTH 105TH EAST AVENUE, TULSA, OKLAHOMA P.O. BOX 15447, TULSA, OKLAHOMA 74115 PHONE (918) 838-6746

IMAGINEERING for EXPLORATION, ENGINEERING and ENVIRONMENT



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BEOWAWE AREA GROUNDNOISE CROSS SECTION M-M' .5 - 15.0 Hz T 31 N SSE NNW R 48 E M м SEC. 18 UNITS 10.77 + 1 DE H DECIBEL z FREQUENCY 14 54 AVG. POWER IN 10.51 - 1 DEV. 134 450'SW 1 NMHF INTEGRATED POWER FIGURE IBA SENTURION SCIEN MEAN FREQUENCY OF THE INTEGRATED POWER -----, INC .







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----- INTEGRATED POWER ----- MEAN PREQUENCY OF THE INTEGRATED POWER FIGURE IBC SENTURIC SCIENCES, INC.

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BEOWAWE AREA SHALLOW SEISMIC REFLECTION SURVEY

File copy

Chevron Recourses

LANDER COUNTY, NEVADA

I. Introduction

During the period from May 13 through September 1, 1975, a shallow seismic reflection survey was carried out in the southwest part of the Whirlwind Valley, Lander County, Nevada, near the small town of Beowawe (see Figure No. 1, Location Map).Approximately 17.5 miles of data were recorded, consisting of four northeast-southwest lines (Lines BW-1 through BW-4) and four northwest-southeast lines (Lines BW-1 through BW-4) The purpose of the survey was to investigate the geologic structure, especially faulting, as an aid to continued exploration for geothermal steam in the area.

II. <u>Technique</u>

Line positions in the field were established by reference to topographic features, as the magnetic compass tended to be sometimes erratic in the presence of so much magnetite-bearing lava. After the position of a given line was established, stations were located along it at intervals of 165 ft. (50M) by chaining with a measured drag rope 165 feet long. Difficult terrain made it necessary for parts of lines BW-3, BW-6 and BW-7 to depart from the program positions.

The seismic source used for the first two lines recorded (Line BW-1 and Line BW-6) was a 300 lb. steel weight dropped free-fall a distance of $3\frac{1}{2}$ feet for approximately 1000 ft. lbs. of energy per drop. Three drops per station on the average were made and summed in the field. Detection was by means of a receiver array of 12 digital grade 10 Hz geophones inline spaced 12 feet apart. Where possible, the source weight was dropped one or two times at each of two locations beside the one-third positions of the receiver array and offset about 8 feet laterally (see sketch below).





Recording was done by a Seaman Nuclear Corporation engineering type single-channel seismograph (with summing digital memory) modified to include frequency filters, programmed gain expansion, a paper strip chart recorder, and a magnetic cassette digital recorder. A recording length of 0.5 second after weight impact was used. As successive drops were recorded at each station, the summed results were viewed by the operator on a cathode ray tube. When the operator judged that enough thumps had been recorded (the number varied from one to six) the summed data were recorded on paper and magnetic tape and the crew moved on to the next station. During the recording of BW-1 and BW-6 it became evident that though the data in the top 1,000 feet were good, the rate of energy decay with depth was unusually great. As a result, the operation was suspended in late May and the equipment returned to Albuquerque for modifications. A new and larger weight drop system using a 700 pound steel weight which could

returned to Albuquerque for modifications. A new and larger weight drop system using a 700 pound steel weight which could be dropped as much as $6\frac{1}{2}$ feet was built, and the type of programmed gain expansion was changed to allow far greater range in rate of gain increase with time. When the modifications were complete and field-tested, the crew returned to the Beowawe area, renewing work July 21, 1975. The remaining lines of the project (BW-2 through BW-5 and BW-7 through BW-8) were recorded dropping the 700 lb. weight about 5 3/4 feet free-fall for about 4000 ft. lbs. of energy per drop. This increased source energy plus the improved available gain increase allowed the recording of 1.0 second as opposed to the previous 0.5 second. Practical depth of penetration was increased from about 1,000 feet to about 2,500-3,000 feet, which considerably improved ability to detect faults. The change, however, was not all favourable; the quality of data in the top 1,000 feet was noticeable reduced, as shown by a comparison recorded on Line BW-1. Consequently, after completion of the Beowawe survey and before initiation of the next (Hot Springs Point) survey, experimental work was done in an attempt to find an energy input level which would provide penetration deeper than 1,000 feet but without sacrificing detail or quality in the top 1,000 feet. In this expeimentation it was found that dropping the 700 lb. weight 3壹 feet (for about 2,500 ft. lbs. of energy) greatly improved the data in the top 1,000 feet while sacrificing little in the way of depth penetration. It is therefore recommended that in any future shallow reflection work in the Beowawe area this level of energy input be used.

After each day's field work, the records made during the day were corrected to a reference plane of +5000 feet using a correction velocity of 3,000 feet per second (determined at the start of the survey by refraction probes recorded on Line BW-1 near the Chevron Ginn No. 1-13 well). The paper records were then colored, trimmed and combined to form corrected variable area/wiggle trace record sections (see Enclosures Nos. 1 through 8). These record sections were then studied and picked, with an attempt being made to recognize both reflections and diffractions, the latter for their value in fault detection (see Enclosures Nos. 9 through 16). The timed events were then converted to depth using a velocity function fitted to the pseudo-sonic log data from the Chevron Ginn No. 1-13 well, located within the prospect (see Table No. 1). Migrated depth sections were next made using the point-arc method (see Enclosures Nos. 17 through 24). In this method, which is well suited to shallow single-channel recording, for each event picked on the record section a circular arc is swung from each station at which the event is picked. This arc has its center at the station position (at reference plane elevation) and its radius equal to the depth calculated

for the event at that station. A curve is then drawn tangent to each of the arcs representing a given event at successive stations. If the velocity function is accurate such curves are a good representation of the corresponding reflectors. In cases where three or more arcs from a single event intersect at a single point, the event is probably a diffraction. Such apparent diffraction centers are indicated on the migrated sections and are often helpful in fault interpretation.

After completion of field recording in the Beowawe area, the locations of 12 of the 16 line intersections were determined by plane-table triangulation from three known positions (see map, Enclosure No. 25). In cases where a given point could be shot from all three triangulation stations, the apparent error indicated was less than 30 feet, so that these intersections can be regarded as very accurately located. The four intersections involving Line BW-4, unfortunately, could not be shot in from the triangulation stations, and are consequently less certain in location. However, even these are probably actually located within 100-200 feet of their mapped positions.

III. <u>Results</u>

The seismic results obtained in the Beowawe area are generally of poor quality. Experience elsewhere, however, suggests that in this complexly-faulted area the data are almost certainly superior to data which might be obtained by more conventional seismic techniques. In hindsight, it appears that the improvement gained by using 50 meter (165 feet) spacing rather than 100 meter (330 feet) spacing as in other prospects was probably not worth the additional cost (almost twice as much per mile). However, the Beowawe area, because of its complexity, was a particularly good test example to determine if the closer spacing is worth the additional cost in exploration of this type.

The writer's interpretation of the structure of the project area is shown by the Structure Contour Map, Enclosure No. 25. This map is drawn on a seismic phantom which it is hoped may be at approximately the same stratigraphic position throughout the area. Because of the difficulty of correlating from one fault block to another, however, the likelihood of its being the same horizon everywhere is not good. The general structural form shown, however, is probably reasonably accurate.

Folding in general appears to be of much less importance than faulting. Only one fold, the east-plunging anticlinal nose in Section 14, seems to suggest that it may have formed independently of and prior to the present fault system.

Only faults judged to be of importance are shown. Many lesser faults are indicated by the seismic data. The faults considered

to be of greatest significance are those shown on the map by heavier green lines. Two faults in particular are believed worthy of notice. These are (1) the arcuate fault at the foot of the Malpais Range (extreme southeast margin of the survey area) and (2) the opposing subparallel fault near the northwest edge of the survey area (and cutting Line BW-1 at Stations 55-56). Between these two major faults there appears to be a significant graben trending northeast-southwest and creating the smaller southwest extension of Whirlwind Valley which is the survey area. About 2/3 of a mile northwest of the main Malpais Range frontal fault is another fault set, also down to the northwest. Between these step faults and the main Malpais Range frontal fault is a fault block intermediate in depth between the valley graben and the Malpais Range. Its most obvious manifestation is the large hill in the south half of Section 18. The remaining fault considered of major importance crosses the valley graben north-northwesterly in the east half of section 13. This fault may not be of great throw, but it does appear to mark a major dip reversal in the graben and cause the northwest quarter of Section 13 to be the lowest point in the graben. It (the fault) was probably penetrated at shallow depth in the Chevron Ginn 1-13 well (SE/SE Sec. 13).

A few faults are shown which are not believed to be of great importance, at least in the survey area proper. Of particular interest is a set of faults encountered along the northeast side of the survey. These faults appear to strike a few degrees north of east and evidently die out westward near the position of Line BW-2. Those faults of this set which lie southeast of the center of the southeast quarter of Section 12 are apparently downthrown to the north; those farther northwest are apparently downthrown to the south. It seems likely that these faults are the west ends of a step fault system forming the main Whirlwind Valley graben to the east. If this is true, it would appear that the deepest downthrown part of the main Whirlwind Valley graben to the east lies about 3/4 of a mile north of the Malpais Range front, making the Whirlwind Valley graben highly assymetric.

Seismic evidence regarding the attitudes of the major faults in the survey area can be seen in several places. On Lines BW-1 and BW-4, the main Malpais Range frontal fault appears to dip about 70 degrees northwest (corrected for line angle on BW-4). The large step fault system about 2/3 mile northwest of the main Malpais Range frontal fault evidently dips about 60 degrees northwest on Line BW-2, and about 75 degrees on Lines BW-1, BW-3, and BW-4. The large cross-graben fault in the east half of Section 13 is apparently nearly vertical, but does dip southeast, as seen on Lines BW-1, BW-6, and BW-7. The large fault on the northwest side of the survey area graben also appears to be nearly vertical but does evidently dip southeast (see Line BW-2 especially). In summary, all the major faults appear to be normal faults, with dips ranging from about 60 degrees to nearly vertical. Only one or two doubtful cases of possible minor high-angle reverse faults were observed.

On some of the seismic lines the nearest reflector to the mapped phantom shows a large number of diffraction points (see especially Lines BW-2 and BW-8). This may indicate that the horizon is an unconformity with a great deal of irregularity (not strange in a volcanic sequence) or is perhaps a thick, competent unit subject to a great deal of small faulting and fracturing.

IV. Conclusions

A. The survey area appears to be basically a smaller graben extending southwestward from the main Whirlwind Valley graben. B. Folding in the area seems to be very minor compared to faulting.

C. All the major faults as interpreted are evidently normal faults, with dips in the range from 60 degrees to nearly vertical.

D. The seismic reflection method seems to be clearly applicable to exploration of this type, despite the complex faulting present.

V. <u>Recommendations</u>

A. To penetrate the main Malpais Range frontal fault at about 4000 ft. depth, wells should be located on the downthrown side about 1200 feet from the fault as mapped.

B. In future investigations of this type, close station spacing (165 feet or 50M) should be reserved for cases where increased detail is needed, and normal station spacing (330 feet or 100M) should be the standard, for reasons of economy.

Respectfully submitted,

charles & Reynolds

l Figure l Table 25 Enclosures Charles B. Reynolds Registered Geophysicist (Calif.) Certified Professional Geologist

Page 5

RAND MONALLY STATE COUNTY-CITY MAP

NEVADA SIZE 8½ x 11



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This Map is also available with County Outlines only. 4725

LANDER COUNTY, NEVADA

٧i	=	2000 +	10.02	2 <750'	Breakover	time	0.312
Vi	=	8000 =	2.02	2 ≥7.50 ·	Br eakover	time	0.172

(Accurate only to 4200' depth) Datum +5000'

(T=one-way time)

(two-w Time	ay)	(feet) Depth	(two-wa Time	ay)	(feet) Depth	(two-way) Time	(feet) Depth
	ft/ms	- -		ft/m	s p	ft/	ms
0.005		5	0.200		344	0.385	1110
0.010		Ĩ0	0.205		357	0.390	1135
0.015		16	0.210		371	0.395	1161
0.020		21	0.215		386	0.400	1187
0.025		27	0.220	3	401	0.405	1213
0.030		32	0.225		416	0.410	1239
0.035	1	38	0.230		432	0.415	1264
0.040		4 4	0.235		448	0.420 5	1292
0.045		50	0.240		464	0.425	1318
0.050		57	0.245		481	0.430	1345
0.055		63	0.200		-493	0.435	1372
0.060		70	0.255		516	0.440	1399
0.065		77	0.260		534	0.445	1426
0.070		84	0.265		552	0.450	1453
0.075		91	0.270		571	0.455	1480
0.080		98	0.275	4	591	0.460	1508
0.085		106	0.280	-	611	0.465	1535
0.090		114	0.285		631	0.470	1563
0.095		122	0.290		653	0.475	1591
0.100		130	0.295		674	0.480	1619
0.105		138	0.300		696	0.485	1647
0.110		147	0.305	F	719	0.490	1675
0.115		155	0.310	2	742	0.495	1704
0.120		164	breakov	rer		0.500	1732
0.125	2	174	0.312		7 50	0.505	1761
0.130	2	183	0.315		764	0.510	1790
0.135		193	0.320		788	0.515	1819
0.140		203	0.325		812	0.520	1848
0.145		212	C.330		836	0.525	1877
0.150		223	0.335		861	0.530	1907
0.155		234	0.340		885	0.535	1937
0.160		245	0.345		909	0.540	1966
0.165		256	0.350	5	934	0.545	1996
0.170		268	0.355		959	0.550	2026
0.175		280	0.360		984	0.555	2057
0.180		292	0.365		1009	0.560	2087
0.185		304	0.370		1034	0.565	2117
0.190		317	0.375		1059	0.570	2148
0.195		330	0.380		1084	0 . 575	2179

 (two-w	av)	(feet)	(two-wav))	(feet)	Pa
Time	tt/ms	Depth	Time	(+ 1 m c	Depth	L
0.580 0.585 0.590 0.595 0.600 0.605 0.610	6	2210 2241 2272 2304 2335 2367 2399	0.840 0.845 0.850 0.855 0.860 0.865 0.870	8	4054 4094 4135 4175 4216 4258 4299	
0.615 0.620 0.625 0.630 0.635 0.640		2432 2463 2496 2528 2561 2594	0.875 0.880 0.885 0.890 0.895 0.900		4 341 4 382 4425 4467 4 509 4 552	
0.650 0.655 0.660 0.665 0.667 0.675 0.680 0.685	7	2660 2693 2727 2761 2795 2829 2863 2897	0.903 0.910 0.915 0.920 0.925 0.930 0.935 0.940 0.945	9	4638 4681 4725 4768 4812 4856 4901 4945	
0.690 0.695 0.700 0.705 0.715 0.720 0.725 0.725 0.730 0.735 0.740 0.745		2932 2967 3002 3037 3107 3143 3170 3215 3287 3287 3324	0.950 0.955 0.960 0.965 0.970 0.975 0.980 0.985 0.985 0.990 0.995 1.000		4990 5035 5081 5126 5172 5218 5264 5310 5357 5404 5451	
0.750 0.755 0.760 0.765 0.770 0.775 0.780 0.785 0.780 0.795 0.790 0.795 0.800 0.805 0.810	8	3361 3397 3435 3472 3509 3547 3585 3623 3661 3699 3738 3777 3816				
0.815 0.820 0.825 0.830 0.835		3855 3894 3934 3974 4014	CHEVRON	GINM	1 1-13	VELOCITY

- August 18, 1975

FUNCTION



SENTURION SCIENCES, INC.

1539 NORTH 105TH EAST AVENUE, TULSA, OKLAHOMA P.O. BOX 15447, TULSA, OKLAHOMA 74115 PHONE (918) 836-6746

June 2, 1975

Mr. Bill Mero Chevron Oil Company Post Office Box 3495 San Francisco, California 94119 JUN 0 4 1975

JEM?

Dear Mr. Mero:

At long last we are transmitting, under separate cover, the report on the detailed groundnoise survey done for Chevron near Beowawe, Nevada. We apologize for the long delay in completing this task, but we believe you are aware of the difficulties that were encountered. Senturion feels that the area exhibits excellent potential for geothermal resources, and recommendations appropriate to that conclusion are included in the report.

After your evaluation and at your convenience, we will be glad to personally discuss with you our analysis, interpretation, and thoughts on Beowawe.

Again, we are sincerely sorry for the delay which became much too protracted because of our reliance on the principal analyst who had committed to the study effort. Please feel free to contact us should you have any questions.

> Sincerely, SENTURION SCIENCES, INC.

Bob G

R. G. Graf

Keith Westhusing

RGG:KW/rf



BEOWAWE PSD'S (.5 to 15 Hz) As Of December 4, 1974

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SENTURION SCIENCES, INC. _ TULSA, U.S.A.







































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