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GEOHERMAL GRADIENTS AND HEAT FLOW IN THE SALT VALLEY ANTICLINE, UTAH

RIASSUNTO

Le temperature sono state misurate in 5 pozzi dislocati sull'anticlinale di Salt Valley, Utah o nei pressi. I gradienti geotermici nella sezione dal Cretaceo al Giurassico variano da 37.4° C/km a 39.4° C/km. Invece nel sale esso varia da 15.7° C/km a 12.3° C/km. In un pozzo ad Est e fuori della struttura il gradiente geotermico è 19.4° C/km.

Il flusso di calore alla superficie è sull'anticlinale 1.32 $\mu\text{cal/cm}^2$ sec; nell'area a Sud 1.11; nell'area ad Est 1.01. Viene proposto un metodo per valutare le curve temperatura-profondità.

SUMMARY

Temperatures were measured 5 wells located on or near the Salt Valley anticline, Utah. Geothermal gradients in the section of Mancos Shale (Cretaceous) to Morrison Formation (Jurassic) in the graben area of the anticline ranged from 0.02053°F to 0.02160°F per foot, or 37.4°C to 39.4°C per km. In the Hermosa Formation (Pennsylvanian) in the southern area of the anticline, the geothermal gradient is 0.01621°F per foot, or 31.4°C per km. In the Paradox salt of the graben area, the geothermal gradient is 0.00861°F per ft, or 15.7°C per km. In the southern anticlinal area, the geothermal gradient in the Paradox salt is 0.00676°F per ft, or 12.3°C per km. In a well east of and off the structure, the geothermal gradient is 0.01064°F per ft, or 19.4°C per km.

Heat flow to the surface in the graben area of the anticline is 1.32 $\mu\text{ cal/cm}^2$ sec; in the southern area of the anticline it is 1.11 $\mu\text{ cal/cm}^2$ sec. To the east and off the anticlinal structure, heat flow to the surface is 1.01 $\mu\text{ cal/cm}^2$ sec. A method for evaluating temperature-depth curves is introduced.

INTRODUCTION

Drilling records exist for 110 wells in Grand County, Utah (Hansen and Scoville, 1955) but temperatures have been measured in only a few of them. Those measured are: Reeder No. 1 (10-61) (1), Crescent Eagle No. 1 (10-62), Brendell No. 1 (10-65), Balsley No. 1-C (10-90), and Hyde No. 1 (10-80). The first four wells listed are located on the Salt Valley anticline (Figure 1). The fifth well is between the South Cisco anticline and the Salt Valley anticline, about 11 miles southwest of the former structure and about 7 miles northeast of the latter. The Yellow Cat dome is approximately 3 miles southeast of Hyde No. 1 well (Dane, 1935, pl. II), Figure 1.

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The effect of anticlinal structure on geothermal gradients and heat flow can be determined from the temperatures measured in the wells. Drilling records and geophysical studies (Joesting and Case, 1960) have shown that a thick deposit of salt underlies the anticline. Salt is a good conductor of heat in comparison with many other rocks, and the effect of this material on the geothermal gradients and heat flow can be determined.

The wells had been idle for varying periods of time. Temperatures were measured in one well soon after drilling stopped and were again measured after several years. In another well, temperatures were measured at three different times. It was thus possible to determine the effects of idle time on the geothermal constants.

ACKNOWLEDGMENTS

Core samples from the salt section of the Reeder No. 1 well were obtained from the U. S. Bureau of Mines through the cooperation of Paul T. Allsman, J. H. East, Jr., and W. E. Rice. Outcrop samples of formations in the area were collected by J. E. Case and Robert Hite of the U. S. Geological Survey. Cores from drill holes in the area were provided by D. P. Elston of the U. S. Geological Survey and R. R. Norman of the Delhi-Taylor Company, Moab, Utah. Thermal conductivity determinations on the above specimens were made by S. A. H. Goldstein, J. S. Karp, and W. E. Huff, U. S. Geological Survey, under the direction of E. C. Robertson. The writer wishes to express his appreciation for this assistance.

GEOLOGY

The geology of the Salt Valley anticline and adjacent area is described by Dane (1935), and this brief summary is extracted therefrom. A recent stratigraphic and structural interpretation of Salt Valley and nearby structures is given by Shoemaker et al (1958).

In the vicinity of the Salt Valley anticline, the general structure, though simple, is complicated by several folds with steeply dipping flanks. The rocks are in general inclined northward, away from the Uncompahgre Plateau and the laccolithic uplift of the La Sal Mountains. The most prominent fold is the northwest-trending Salt Valley anticline. The crest of this fold has been dropped into a trough or graben by a rather complex system of normal faults which have displacements ranging from a few to more than a thousand feet. The resistant sandstone flanks of the anticline stand as ridges. Within the trough, the softer Mancos Shale is more deeply eroded and is widely covered with alluvium and valley fill.

At the northwest end of the anticline, the Mancos Shale is dropped against successively older formations and is covered with a thin layer of alluvium. The main graben of Mancos Shale to the north is separated from the intrusive salt body of the Paradox Member of the Hermosa Formation to the south by a group of cross faults and a narrow tapering wedge consisting of Morrison, Mancos, and Dakota (?) Formations. The Paradox is intruded into the graben in the Crescent area; there, below the Dakota (?) Sandstone (Cretaceous), only about 140 ft of the shales and sandstones of the Morrison were

encountered above the Paradox in the ...
mal to the geologic section between them are missing.

The intrusion of Paradox salt beneath the Crescent Junction area seems to be wholly within the graben block. The minor complex faulting in Salt Valley probably was in part subsequent to the intrusion of the Paradox salt and was a result of withdrawal or redistribution underground of the plastic and soluble material, as a consequence of which overlying beds collapsed. The structure now visible is the result of deformation which took place at the end of Cretaceous time. (See Shoemaker et al, 1958, for another interpretation).

Crystalline rocks are estimated to be at a depth of approximately 16,000 ft at the Thompson No. 1 well located in Sec 33, T 21 S, R 21 E, approximately 12 mi ENE of the Reeder No. 1 well (Joesting and Case, 1960, Figure 114.2). Granite was encountered at a depth of 2,431 ft in the State No. 1 well, Utah Southern Oil Company (Dane, 1935, p. 166), about 11 mi NE of the Hyde No. 1 well, but was not reported in the log of the Hyde well.

DESCRIPTION AND HISTORY OF DRILL HOLES AND MEASUREMENTS

Well locations are shown on *Fig. 1*, a reproduction of part of Plate II from Dane (1935). Drilling was started on the Crescent Eagle No. 1 well, located in Sec 4, T 22 S, R 19 E, in 1920 and was continued intermittently by cable tools until September 1941, when drilling stopped at 4,006 ft. A log of the well is given by Dane (1935, p. 162-164). The hole was dry to 497 ft when the temperatures were measured by the writer on August 10, 1942. The hole was bridged or plugged below 1,950 ft, and deeper measurements could not be made.

The Brendell No. 1 well, located 400 ft S 10° E of Crescent Eagle No. 1, Sec 9, T 22 S, R 19 E, was started in September 1928. Drilling continued intermittently until late in 1932 with cable tools and was discontinued at 4,125 ft. This well was drilled as an exploratory test for oil and was producing a very small amount of gas and fluid when the writer measured the temperatures.

Formations penetrated in drilling are like those of the Crescent Eagle, but the top of the salt is a few feet deeper. The hole was plugged, and observations below 1,500 ft could not be obtained. Temperatures were also measured in this well by E. W. Henderson (unpublished data), U. S. Geological Survey, in December 1933.

Reeder No. 1 well, located 218 ft N 40° W of Crescent Eagle No. 1 and in the same section, was spudded in May 5, 1942. Drilling was suspended August 3, 1942, at 4,207 ft. Drilling was resumed in 1948, and the well was completed September 26, 1949, at 10,350 ft, still in salt of the Paradox Member of the Hermosa Formation. This rotary well was drilled by the Bureau of Mines and the Geological Survey for the Defense Plant Corporation to evaluate the deposits for magnesium. It was reentered and deepened later as an exploratory tests for oil, but there was no production. A complete log and other drilling information to 4,207 ft is given by Severy et al (1949). A bottom-hole temperature was obtained August 4, 1942, and a complete set of temperatures October 4 to 6, 1942, by the writer.

Balsley No. 1-C well, located in Sec 32, T 23 S, R 21 E, nearly 15 miles southeast of the Reeder No. 1 well, was started December 18, 1930. Drilling

ceased October 27, 1932, at 6,120 ft, still in salt of the Paradox Member. This well was drilled by cable tools as an exploratory test for by the Utah Southern Oil Company. The only oil and gas found was a showing at 3,410 and 3,436 ft. Temperatures were first measured in this well by W. B. Lang (unpublished data) of the Geological Survey on September 18, 1931. Next measu-

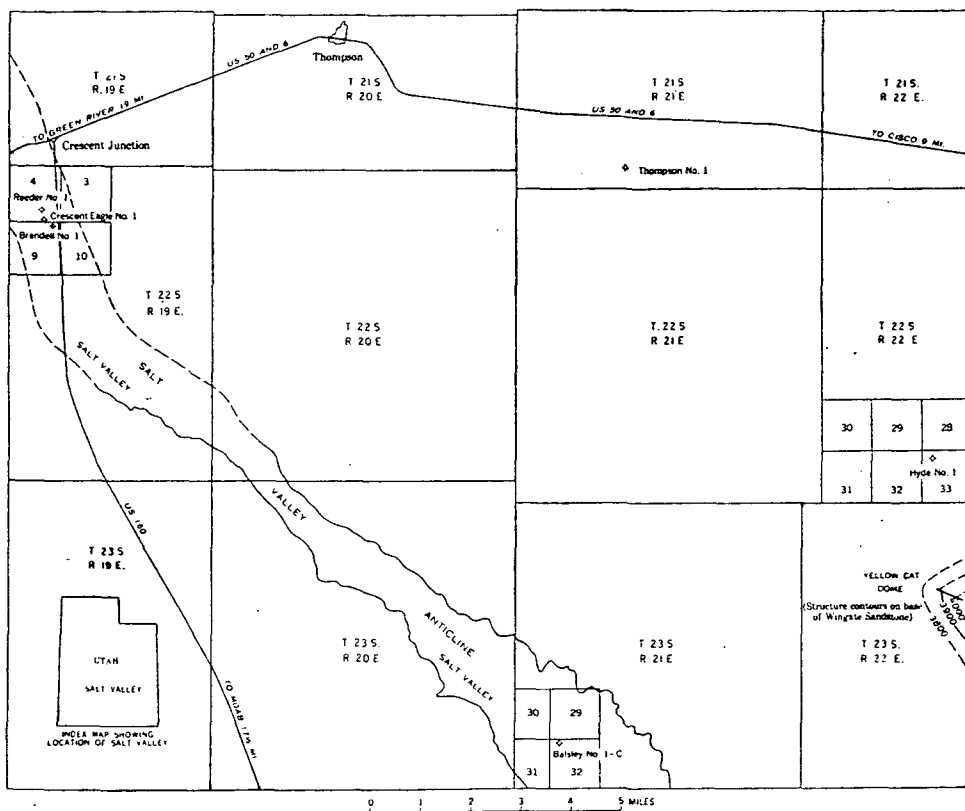


Fig. 1 - Map showing the general location of the area, the structure, and the locations of wells on the structure and in the adjacent area. After Dane (1935).

rements were by E. W. Henderson (Unpublished data) on December 7 and 8, 1933. In July 1936, a third attempt was made by Henderson and C. E. Van Orstrand (unpublished data), but the well was plugged below 3,000 ft, having been abandoned in August 1935.

The Hyde No. 1 well, located in Sec 33, T 22 S, R 22 E, about 18 mi ESE of the Reeder No. 1 well, was started October 1, 1935. Drilling ended March 31, 1937, at 6,715 ft. This well was drilled with cable tools by the Utah Southern Oil Company as an exploratory test for oil. It was a dry hole. According to the interpretation of the drilling log by E. W. Henderson (unpublished data), the well begins in shale of the Summerville Formation (Jurassic) and bottoms in the Cutler Formation (Permian). A revised interpretation of this log is shown on Fig. 6. Temperatures were first measured in this well by Hen-

was idle. In July 1936, Henderson and Van Orstrand (unpublished data) attempted another measurement of the well, but the hole was bridged or plugged below 1,000 ft and no deeper measurements were possible.

MEASURING EQUIPMENT

A steel tape with a container for holding three thermometers and an attached weight was used by Lang and Henderson for some of their temperature measurements in the deep wells. The thermometers in their container were also attached to the sand line for deeper observations.

Wire-line equipment designed and built in the equipment shops of the Geological Survey was used for the other temperature measurements. A description of the equipment, with modifications and applications, is given by Van Orstrand (1930). It is possible with this equipment to lower three maximum thermometers to more than 9,000 ft in an open hole without undue difficulty.

TEMPERATURE-DEPTH PROFILES AND INTERPRETATIONS

Temperature-depth profiles, hereafter termed T-D profiles, for the five wells under discussion are shown as *Figures 2 to 6*. Mean annual air temperature (M.A.T.) is taken from U. S. Weather Bureau (1960). Gradient lines having one depth zero were determined by the two-point method. A summary log is given on each figure.

The observations were adjusted by two methods to obtain the geothermal constants, by the methods of least squares and by using the temperature and depth at two selected points. The latter method may be expressed as

$$b = (T_b - T_a) / (d_b - d_a). \quad (1)$$

Each solution gives the constants for a straight line whose equations is

$$T = a + b d \quad (2)$$

where T is temperature at depth d ; a is intercept on the temperature axis and is therefore the computed temperature at zero depth in the earth; b is the slope of the line, which is the geothermal gradient.

Another constant, which has been termed e , is obtained from the difference between mean annual temperature of the air and constant a ,

$$e = (\text{M.A.T.} - a). \quad (3)$$

It may be regarded as the temperature difference required to maintain heat flow from the earth across the surface-air contact. Constant e has long been recognized and applied. Everett (1862, 1904) noted that the difference between the temperature of the ground and of the air at sea level in the humid climate of England was about -1.5°F . Benfield (1939) found e to be about -2.2°F at Holford bore near Liverpool, England. He considered this to be « ...additional evidence corroborating the systematic difference found by others ». Bullard (1939) applied a difference of -1.8°F for geothermal gradient determinations from South African temperature measurements. Krige (1939) reported observations of temperature in a South African well with an e value of -2.2°F .

Spicer (1941) reported an e value of -0.7°F obtained from temperatures measured in mines at Grass Valley, California. Van Orstrand (1951) reported an average value of -1.54°F for e that was obtained from more than 500 determinations in oil field areas. The computations by Spicer for Lang (1937) showed the value of e to be about -1.8°F in a New Mexico well. Recent measurements by Penrod et al (1960) reported e to be -1.2°F at Lexington, Kentucky. Cook (1961) reported e to be -1.2°F at Resolute, Northwest Ter-

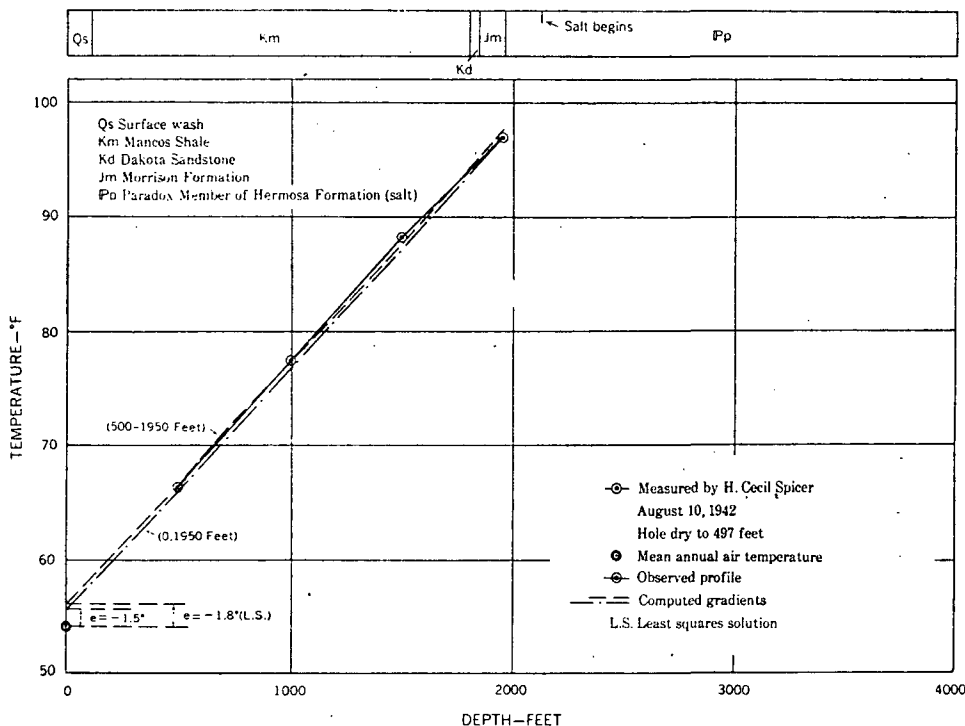


Fig. 2 - Temperature-depth profile of Crescent Eagle No. 1 well, located on anticlinal structure.

ritories, Canada. Bullard and Niblett (1951) stated that « ... the extrapolated surface temperature should agree with the observed temperature near the surface ». The observed surface temperatures they gave were derived from observations of air temperature at meteorological stations nearby. The theory for the calculation of soil temperatures at various depths from ordinary synoptic air temperatures is given by Gutman (1960), Penrod et al (1960), Lettau and Haugen (1960), Carslaw and Jaeger (1959), Ingersoll et al (1954), and others.

In the two-point solution, temperature at zero depth in the ground is assumed to be $(\text{M.A.T.} + e)^{\circ}\text{F}$. Intervals and points used for the computation of the geothermal constants for the T-D profiles are given in Table 1. Values of e , obtained from the least squares solution, are indicated by « L.S. » on the figures. Values of the geothermal gradients in the formations of the area, computed by both methods, are given in Table 1. The probable er-

ror r_b of the gradient, from the least squares solution, is also given in Table 1.

Table 1 - Computed geothermal gradients in formations of the area.

| By least squares | | | | By $(T_b - T_a)/(d_b - d_a)$ (Equation (1) p. 9) | |
|---|---------------|---------------------------------|-------------------------------------|---|---------------------------------|
| Well | Interval feet | Geothermal gradient b F/ft | Probable error $r_b \times 10^5$ | Depths feet | Geothermal gradient b F/ft |
| <i>Mancos Shale, Dakota Sandstone, Morrison Formation</i> | | | | | |
| Reeder No. 1 | 100 - 2,000 | 0.01743 | ± 38 | 0, 2,100 | 0.02053 |
| Crescent Eagle No. 1 | 500 - 1,950 | 0.02117 | ± 36 | 0, 1,950 | 0.02119 |
| Brendell No. 1 | 500 - 1,500 | 0.02160 | ± 33 | 0, 1,500 | 0.02200 |
| <i>Paradox Member of Hermosa Formation above salt</i> | | | | | |
| Balsley No. 1-C | 100 - 900 | 0.01621 | ± 11 | 0, 900 | 0.01723 |
| <i>Paradox salt</i> | | | | | |
| Balsley No. 1-C | 900 - 3,000 | 0.00675 | ± 7 | 900, 3,000 | 0.00676 |
| Reeder No. 1 | 2,100 - 3,095 | 0.00882 | ± 17 | 2,100, 3,095 | 0.0861 |
| <i>Section off anticline</i> | | | | | |
| Hyde No. 1 | 100 - 5,750 | 0.01037 | ± 25 | 0, 5,500 | .01064 |

An inspection of Figures 2 to 6 and Table 1 shows the following:

1) Observed temperatures in the Crescent Eagle well differ by very small amounts from the gradient line obtained by least squares. The gradient line obtained for the points (0, 1,950 ft) is closely adjacent to the least squares gradient, and the gradients are nearly identical in numerical value. The value of e is -1.8°F and only -0.3°F above the mean value, -1.5°F (Van Orstrand, 1951).

2) Geothermal gradients in the Crescent Eagle, Brendell (later measurements), and Hyde wells are essentially linear and without a pronounced change in slope.

3) Geothermal gradients in the Reeder and Balsley wells show a pronounced change in slope at the Paradox salt boundary. Such a change in slope would be expected also in the Crescent Eagle and Brendell wells had it been possible to obtain temperatures in the deeper salt section.

4) Geothermal gradients in the Paradox salt sections of the Reeder and Balsley wells are less steep than those in the two sections above. In the Reeder well the section consists of the Mancos, Dakota, and Morrison Formations, and in the Balsley it consists of the Paradox Member of the Hermosa Formation. The ratio of gradients is approximately 1 : 2.5.

5) The geothermal gradient in the Paradox Member of the Hermosa Formation of the Balsley well is less steep than those in the section of Mancos, Dakota, and Reeder wells.

6) The geothermal gradient in the Paradox salt is steeper in the Reeder than in the Balsley well.

7) If the gradients in the Reeder and Balsley wells may be considered representative of geothermal conditions in the anticlinal area, it appears that the geothermal gradient varies with location on the anticline. The cause of this variations is not apparent.

8) Geothermal gradients in the two well sections above the salt are steeper than the gradient in the section off the anticline in the Hyde well. The ratio is approximately 2 : 1.

9) The geothermal gradient obtained by least squares in the Mancos, Dakota, and Morrison section of the Reeder well $0.01743^{\circ}\text{F}/\text{ft}$, differs greatly in value from those obtained in this same section of the Crescent Eagle and Brendell wells, 0.02117 and $0.02160^{\circ}\text{F}/\text{ft}$, respectively. Also note that the value of e is -7.9°F , and that the separation of the above gradient from the one computed for points (0, 2, 100 ft) is large.

10) Temperatures in the Brendell well, as measured by Henderson (unpublished data) in 1933, depart widely and erratically from the geothermal gradient computed by least squares for this T-D profile. After the well stood idle for about 9 years, temperatures were remeasured in this well by the writer. These temperatures depart but little from the geothermal gradient computed by least squares. The gradient has steepened over the idle period, increasing from 0.01937 to $0.02160^{\circ}\text{F}/\text{ft}$. Note also that the value of e followed this change and has been reduced from -6.1°F to -1.8°F . A gradient line for points (0, 1,500 ft) is not shown, as it coincides with the one for (500-1,500 ft) except near the temperature axis.

(11) In the Balsley well the geothermal gradient by least squares in the Paradox Member of the Hermosa Formation became steeper with increasing idle time. It was $0.01437^{\circ}\text{F}/\text{ft}$ when measured about 14 months after the well was completed, and $0.01621^{\circ}\text{F}/\text{ft}$ when measured about 2-1/2 years later. Note that, accompanying this steepening of the gradient, the value of e decreased from -3.7°F to -2.2°F . Also note that as the idle time increased, the gradients by least squares approached coincidence with the gradient for points (0, 900 ft).

12) Observed temperatures in the Hyde well depart rather erratically, and frequently somewhat widely, from the geothermal gradient determined by least squares. Such departures in the geothermal values are to be expected from the history of this well. Nevertheless, this gradient of $0.01037^{\circ}\text{F}/\text{ft}$ is considered representative as the gradient computed for the points (0, 5,500 ft) is only a little steeper, $0.01064^{\circ}\text{F}/\text{ft}$. The value of e is -2.6°F .

These comparisons, statements, and conclusions are derived from the above observations:

The history of the Crescent Eagle well indicated it had a T-D profile which closely represented predrilling undisturbed temperature conditions in the earth. The observed temperatures differed only slightly from the gradient computed by least squares. Table 1 shows that the geothermal gradients, computed by both methods, are numerically almost identical. Furthermore, they are nearly in coincidence as seen on Figure 2. Computed and mean values of e differ by only 0.3°F on this T-D profile. As this is essentially the same as the values of e for the other wells, these are basic principles

The Brendell well had been idle about a year when first tested in 1933 by Henderson. These temperature values are widely dispersed about the gradient computed by least squares. The gradient for points (0, 1,800 ft) is not included on Figure 3, if it as it would depart markedly from the gradient by least squares. The computed value of e is -6.1°F , which is -4.6°F higher than the mean value. The well had been idle almost 10 years when the writer remeasured the temperatures. The later measurements differ by only small amounts from the gradient computed by least squares. The gradient computed for points (0, 1,500 ft) is nearly in complete coincidence with the gradient by least squares and is therefore omitted from Figure 3. The value of e , as mentioned earlier, is -1.8°F , the same as that of the Crescent Eagle well.

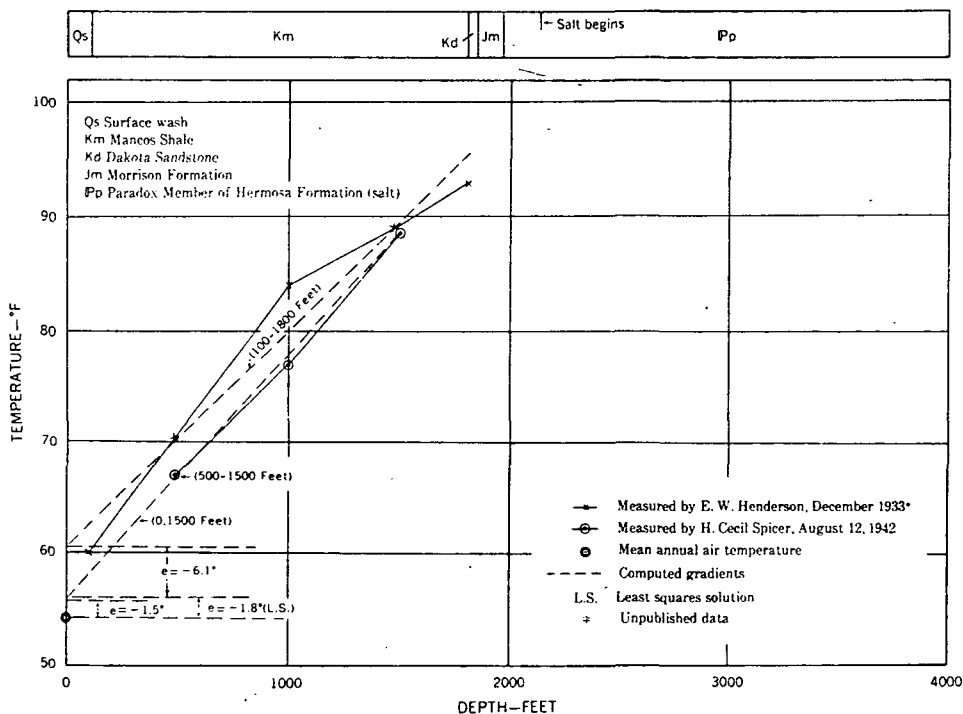


Fig. 3 - Temperature-depth profile of Brendell No. 1 well, located on anticlinal structure.

Application of these principles is next made in the Balsley well (fig. 5). Temperatures were measured in the section above the Paradox salt at two different times. Measurements by Lang (unpublished data) were only in the Paradox salt. Because the gradient lines computed by least squares nearly coincide with the observed temperatures, they are omitted from Fig. 5, but their application will be evident. The observed values depart but little from the gradient obtained by least squares in the measurements both of Henderson and of Henderson and Van Orstrand (unpublished data). Both gradients by least squares diverge somewhat from the gradient line obtained from the points (0, 900 ft). The value of e (observation 11 above) has redu-

longer interval perhaps 5 to 10 years, in the Hermosa Formation would probably coincide with the gradient for points (0,900 ft). Another principle may now be added to those given above: As the idle time for a drilled well increases, the geothermal gradient steepens and approaches the gradient for points (0 and deepest measurement). « Deepest measurement » is restricted and does not include abrupt changes in slope of the gradient, such as were found in the Balsley and Reeder wells.

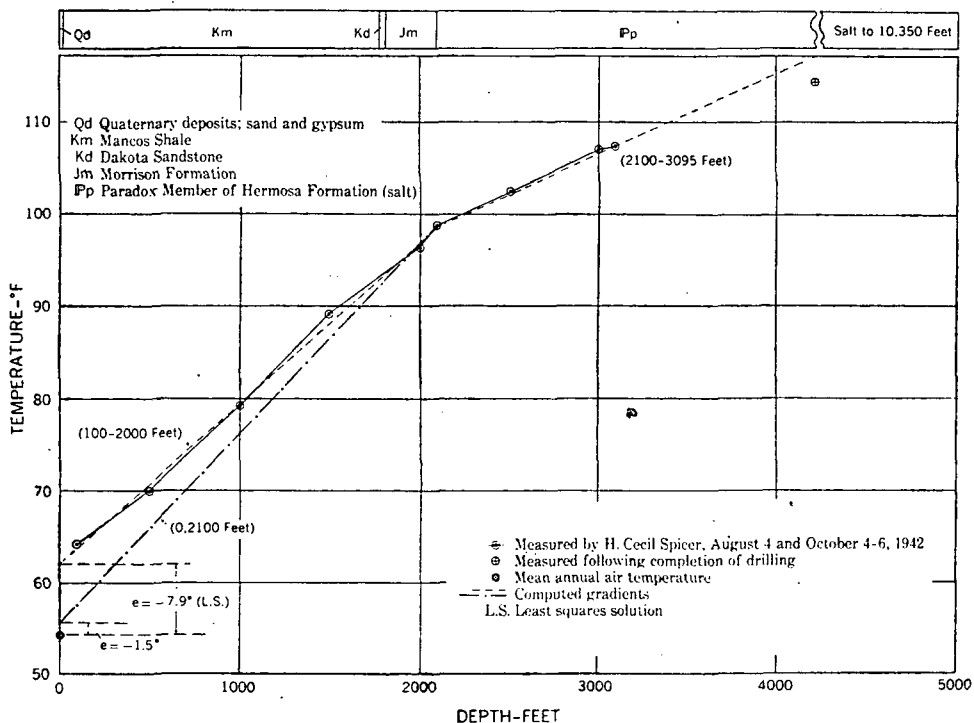


Fig. 4 - Temperature-depth profile of Reeder No. 1 well, located on anticlinal structure.

The principles given above are applied next to the Reeder well (*Fig. 4*), in the section of Mancos, Dakota, and Morrison, above the Paradox salt. Temperatures in this well were disturbed primarily by the drilling fluid used in the rotary method. The fluid had a temperature near 90°F during the entire drilling period. Circulation of this fluid in the hole caused temperatures to rise in its upper part and to fall in the lower part. Consequently, more heating than cooling took place. The zone of this change in temperatures is plainly visible on the T-D profile between 1,500 and 2,100 ft. That cooling took place in the salt is indicated by the difference of approximately 3.0°F between the bottom-hole temperature obtained when drilling stopped and the computed temperature for that depth. The idle period prior to temperature measurements was only 2 months. Such a short time is inadequate for the entire well to return to predrilling undisturbed values, as has been shown in previous examples.

The observed temperatures are dispersed relatively close to the gradient obtained by least squares, but the value of e , -7.9° , is large; it is

—6.4°F above the mean value. A large divergence exists between the gradient by least squares and the one for points (0, 2,100 ft). However, the gradient for the points (0, 2,100 ft) is closely representative of what the undisturbed gradient should be in the Reeder well. A comparison with the gradients in the Crescent Eagle and Brendell Wells in *Table 1* verifies this. As these wells are close together and are nearly identical in geology and location on the structure, they would be expected to have identical gradients. The large departure of the value of e from the mean and the large divergence between the gradients indicates that this well has disturbed temperatures in the section above the salt. This corresponds with known conditions in the well.

In the application of these criteria to the Hyde well (*Fig. 6*), the following conditions are noted: The observed temperatures depart from the geothermal gradient obtained by least squares in a manner indicating that heating has taken place in the upper and lower sections and cooling has occurred in the middle section of the well. The gradient obtained from points (0, 5,500 ft) is located close to the gradient by least squares. The value of e is —2.6°F, —1.1°F above the mean. In the 2 months intervening between measurements, the temperature at 100 ft dropped 0.7°F. Temperatures were somewhat di-

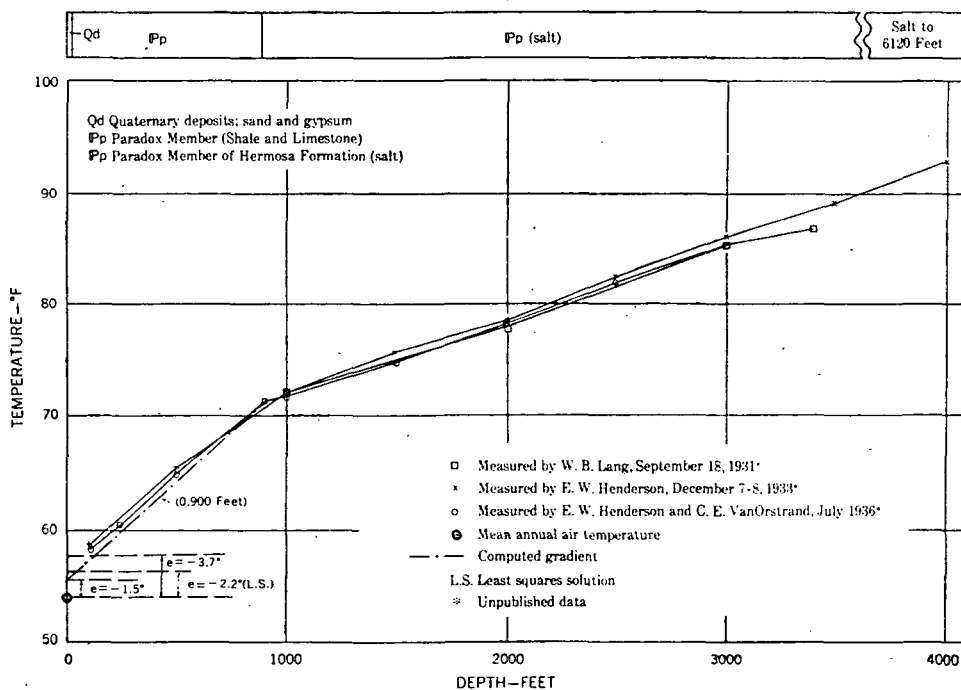


Fig. 5 - Temperature-depth profile of Balsley No. 1-C well, located on anticlinal structure.

sturbed in this well, but not to the extent found in the Reeder well. The difference is largely due to the drilling methods employed. The geothermal gradient is considered to be closely representative of geothermal conditions here. No abrupt change, such as those found in the Reeder and Balsley wells at the boundary between salt and overlying formation, occurs in the

slope of the geothermal gradient at any of the formation boundaries in the Hyde well.

A comparison of all the geothermal gradients shows that the gradient for the Hyde well, off the anticline, is lower than those in the other four wells on the anticline, which are in the formations above the Paradox salt.

Temperatures in the Paradox salt section of the Balsley well (*Fig. 5*) seem to have been undisturbed by drilling. Temperatures measured by Henderson and Van Orstrand in 1936 (unpublished data) are almost the same as Lang obtained in 1931 (unpublished data), but the slightly higher temperatures obtained by Henderson in 1933 (unpublished data) cannot be explained from the available information. Gradients computed by both methods given in *Table 1* are nearly the same. Temperatures in the Paradox salt section of the Reeder well were also very close to predrilling values when measured. If the temperature measurement at 3,095 ft had not been about 0.5°F low, thus departing from the linearity held by the three other temperatures measured in the salt, both computed gradients would have been identical. As it is, the gradient computed for two points is slightly low. Therefore, the gradient computed by least squares is believed to represent thermal conditions better in the Paradox salt.

HEAT FLOW.

The methods used by Bullard (1939), Benfield (1939), Spicer (1941), Birch (1945), and others in computing heat flow to the surface are all based on heat-conduction theory (Carslaw and Jaeger, 1959). When the uncertainties in the measured values are negligible, the method used by Bullard and Benfield gives somewhat better results, but with uncertainties in the measurements of temperatures in the wells and in the thermal conductivities of the rocks, the method used by the other authors gives a satisfactory estimate.

Heat flow is determined by the product of geothermal gradient and thermal conductivity. Thermal conductivity of the formations in the Salt Valley area was determined from measurements made on a large number of drill cores and on outcrop samples. It was measured on equipment similar to that described by Clark (1941) and Birch (1950). Mean thermal conductivity of a series of rocks is determined with the formula given by Carslaw and Jaeger (1959).

$$1/K = \sum_i w_i/K_i \quad (4)$$

where

K = mean conductivity over the entire interval,

K_i = conductivity of unit homogeneous bed,

w_i = (bed unit thickness) (entire interval thickness).

THERMAL CONDUCTIVITY.

Cores and outcrop samples may not be completely representative of actual thermal conductivities in a drill hole, but neither method nor equipment had been developed for *in situ* measurements of thermal conductivity in drill holes when these studies were begun. Furthermore, as most oil

wells and deep drill holes are cased throughout, and casing is cemented and mudded in place, *in situ* measurements are not feasible.

Thermal conductivities determined in the laboratory for a series of cores and samples from the Utah-Colorado area adjacent to that being studied are given in Appendix I. All values of thermal conductivity are tabulated in hundredths of a unit of K (cal/cm sec°C) as reported to the writer. However, it should not be implied that the values are considered this precise. Some repeat measurements of thermal conductivity on selected samples indicated a variable accuracy which depended on the operator and condition of the equipment. Perhaps ± 5 per cent is a fair estimate of the overall accuracy of the conductivity measurements.

Thermal conductivities K used in computing the mean thermal conductivity \bar{K} for the various sections are given in Appendix II. In the Reeder well the lithology and thicknesses of the formations encountered in drilling were taken from the log by Ralph H. King (Severy et al., 1949). A detailed log was not available for the Crescent Eagle and Brendell wells. But the upper section above the salt is similar to and slightly thicker than in the Reeder well. A thin bed of the Paradox Member of the Hermosa Formation was reported above the Paradox salt. A log of the Balsley well provided by D. F. Russell (personal communication, 1959), showed the salt section to be slightly different in composition from that in the Reeder well. An interpretation of the drilling log for the Hyde well is shown on *Figure 6*. The deepest formation reached in the Hyde well, indicated on the log as (X?), may be granitic rock or wash, but it was not reported as such by the driller.

Heat flow values for all the wells, and terms used in their determinations, are summarized in *Table 2*.

Table 2 - Summary of values for mean thermal conductivity \bar{K} , geothermal gradient b , and heat flow.

| Geological material | $\bar{K} \times 10^3$ cal/cm sec °C | b °C/km | Heat flow μ cal/cm ² sec |
|-------------------------------|--|--------------|--|
| <i>Reeder No 1</i> | | | |
| Formations overlying salt | 3.54 | 37.4 | 1.32 |
| Paradox salt | 8.44 | 15.7 | 1.32 |
| <i>Crescent Eagle No 1</i> | | | |
| Formations overlying salt | 3.38 | 38.6 | 1.30 |
| <i>Brendell No 1</i> | | | |
| Formations overlying salt | 3.38 | 39.4 | 1.33 |
| <i>Balsley No 1-C</i> | | | |
| Formations Mbr. Hermosa Fm. | 3.51 | 31.4 | 1.10 |
| Paradox salt | 9.00 | 12.3 | 1.11 |
| <i>Hyde No 1</i> | | | |
| Morrison through Hermosa Fms. | 5.23 | 19.4 | 1.01 |

SUMMARY AND CONCLUSIONS.

Some interesting information and important conclusions have developed from the findings of this study of earth temperatures in drill holes of Grand County, Utah. It was fortunate that such a location was chosen for drilling a new well, for the following reasons: The location was on a previously drilled anticlinal structure. The moderately thick sediments are underlain by salt, a very good conductor of heat. A rather varied group of geological formations occur here. Two wells were present within a few hundred feet of the new well. In one of these wells temperatures had been measured previously; the other well had been idle for a long time. A well in which temperatures had been measured several times was located in a different part of the structure and another well was located a short distance from the new well and off the structure. Also, tests of thermal conductivity on the core and outcrop samples made it possible to evaluate the much earlier observations and to determine the heat flow.

Geothermal measurements in drill holes are of very questionable value, unless temperatures have returned to their predrilling state throughout the hole. This very fundamental point has been overlooked or neglected in most published reports on geothermal measurements in wells.

It has been assumed previously that drilling with cabletools produces only a small disturbance to temperatures in a well. That this may be a very misleading, or even erroneous assumption will be seen by reference to the measurements by Henderson (unpublished data) in the Brendell well, *Figure 3*, and by Henderson and others in the Hyde well, *Figure 6*.

Observations in the wells tested are inadequate to prove that definite changes occur in slope of the geothermal gradient at all boundaries between formations having different K values. When the formations are thick and

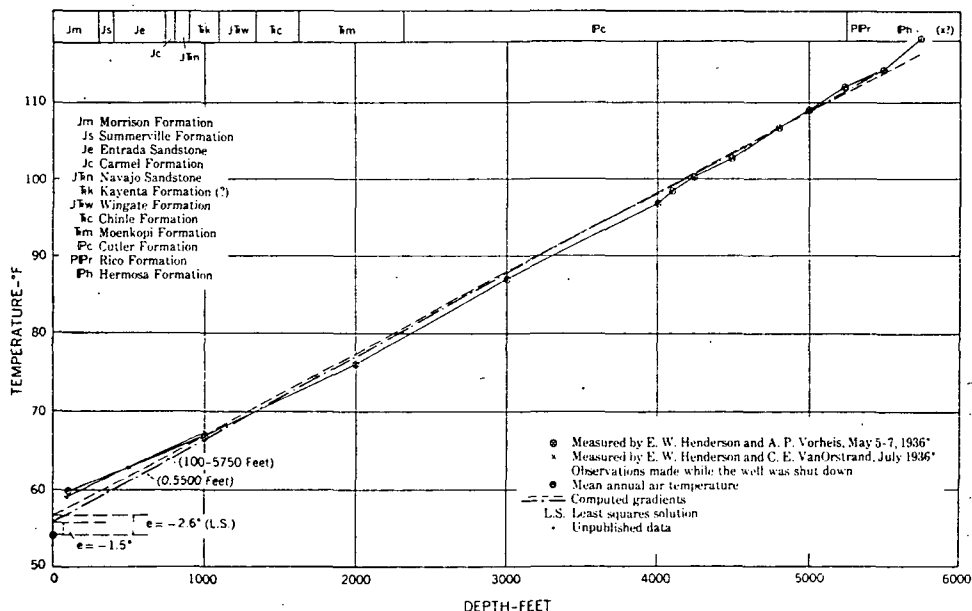


Fig. 6 - Temperature-depth profile of Hyde No. 1 well, located east of the Salt Valley anticline and off the structure.

the difference between their K values is large, as in the Reeder and Balsley wells (Fig. 4 and 5), there is a pronounced change in the slope of the geothermal gradient. When the differences between K values of adjacent formations is small, however, no changes in slope of the geothermal gradients is indicated. If the formations are thin and the difference between K values is large, no change in slope of the geothermal gradient is indicated. Such arrangements of the formations are found in the Hyde well (Fig. 6). The Paradox Member contains beds of shale, anhydrite, etc., but the geothermal gradients in it, as shown by the Reeder and Balsley wells, show no change in slope, thus indicating no apparent change in thermal conductivity within the section measured.

Thermal conductivities of the natural salt cores from the Reeder well (Table 2) are lower than values given elsewhere (Birch et al, 1942; Herrin and Clark, 1956; and others). The variations in these measured conductivities of salt seem to depend more on crystal arrangement and size in the samples tested than on composition when the individual measurements are compared. For example, the conductivity of sylvite in one core is 9.33×10^{-3} cal/cm sec °C, but in another it is 11.03×10^{-3} . Crystals of halite that are 7 inches in diameter (Hite and Gere, 1958, p. 223) have been measured from this area.

Moisture has an appreciable effect on the K values of certain rock samples. This is evident (Appendix II) for the Salt Wash Sandstone Member of the Morrison Formation; limestone of the Summerville Formation; Brushy Basin Shale Member of the Morrison Formation; and Mancos Shale. The area from which these rocks and cores were collected is semidesert. Natural water content of rocks from such an area is low. K values measured on dry samples that are more nearly in the natural state were used in most instances for the heat-flow calculations.

Sandstones of the area have the greatest range of K values, varying from 2.04×10^{-3} for the Burro Canyon Formation (Cretaceous) to 11.97×10^{-3} for the Dakota with values for various sandstones intervening. A comparison can be made between the K values of outcrop sample and core for two sandstones. For the Entrada Sandstone (Jurassic) mean values are 2.95×10^{-3} and 6.05×10^{-3} and for sand of the Moenkopi Formation (Triassic and Triassic (?)) 5.04×10^{-3} and 6.34×10^{-3} respectively. A larger group of samples from each would give a much better comparison.

The geothermal gradient and heat flow are highest in the graben area and somewhat lower in the area of the exposed Hermosa Formation of the anticline. Lowest geothermal conductivity and disposition, apparently exerts a definite and pronounced effect on the heat flow in the anticlinal area. Heat-flow values similar to those in the Paradox salt were reported by Herrin and Clark (1956) in the Salado salt of the New Mexico-Texas area: 1.0 to 1.3 μ cal/cm² sec.

A temperature-depth profile may be examined for undisturbed temperature conditions, using the following as criteria: (1) the observed temperature differ only by small amounts from those computed by least squares; (2) the geothermal gradient computed by using temperatures and depths at two selected points is nearly in coincidence with the gradient computed by least squares; (3) the values of e is very close to the mean value of -1.5°F ; (4) the geothermal gradient in a drilled well becomes steeper with increased idle time as temperatures approach the undisturbed pre-drilling values.

Appendix I - Thermal conductivity of rocks of Utah and Colorado

| Speciment | | | | Conductivity K x 10 ³ (cal/cm sec °C) | | |
|--|-----------------------|--------|--------------------|---|-------|---------------------|
| Material and geologic unit | Place a/ Collected | Number | Kind ^{b/} | Range | | Mean |
| Chert, Summerville Fm. | ANM | 2 | S | 10.10; | 10.47 | 10.28 |
| Conglomerate, Shinarump Mbr. of Chinle Fm. | ANM | 2 | S | 4.11; | 5.13 | 4.62 |
| Limestone, Summerville Fm. | ANM | 1 | S | — | | 6.75 ^{c/} |
| Limestone, Summerville Fm. | ANM | 2 | S | 5.42; | 6.47 | 5.94 |
| Sandstone, Salt Wash Mbr. of Morrison Fm. | ANM | 4 | S | 8.95 | 9.37 | 9.15 ^{d/} |
| Sandstone, Salt Wash Mbr. of Morrison Fm. | ANM | 2 | S | 3.12; | 3.36 | 3.24 |
| Sandstone, Dakota Ss. | ANM | 5 | S | 9.20 | 11.97 | 10.52 ^{d/} |
| Sandstone, Entrada Ss. | ANM | 3 | S | 2.36 | 3.99 | 2.95 |
| Sandstone, Burro Canyon Fm. | ANM | 1 | S | — | | 2.04 |
| Sandstone, Chinle Fm. | CR | 7 | S | 3.92 | 5.76 | 4.75 |
| Sandstone, Wingate Ss. | CR | 2 | S | 3.27; | 3.30 | 3.28 |
| Sandstone, Kayenta Fm. | CR | 8 | S | 2.48 | 5.09 | 3.86 |
| Sandstone, Moenkopi Fm. | CR | 2 | S | 4.96; | 5.12 | 5.04 |
| Sandstone, Navajo Ss. | CR | 2 | S | 3.19; | 3.30 | 3.24 |
| Shale, Brushy Basin Mbr. of Morrison Fm. | ANM | 2 | S | 6.03; | 6.62 | 6.32 ^{c/} |
| Shale, Brushy Basin Mbr. of Morrison Fm. | ANM | 1 | S | — | | 4.59 |
| Shale, Mancos Sh. | ANM | 2 | S | 2.96 ^{c/} ; | 3.23 | 3.23 ^{c/} |
| Shale, Mancos Sh. | ANM | 1 | S | — | | 2.70 ^{d/} |
| Shale, Carmel Fm. | ANM | 4 | S | 2.69 | 6.18 | 4.11 |
| Sandy shale, Summerville Fm. | ANM | 1 | | — | | 3.70 |
| Limestone, shaly, Cutler Fm. | CP | 1 | C | — | | 5.73 |
| Sandstone, silty, Cutler Fm. | CP | 9 | C | 4.68 | 5.96 | 5.19 |
| Sandstone, Cutler Fm. | CP | 1 | C | — | | 6.28 |
| Sandstone, shaly, Cutler Fm. | CP | 2 | C | 5.48; | 5.72 | 5.60 |
| Sandstone, Rico Fm. | CP | 2 | C | 4.82; | 4.85 | 4.84 |
| Sandstone, Entrada Ss. | CP | 9 | C | 3.31 | 7.90 | 5.21 |
| Sandstone, Moenkopi Fm. | CP | 2 | C | 6.45; | 7.10 | 6.78 |
| Sandstone, Summerville Fm. | CP | 3 | C | 3.69 | 4.03 | 3.92 |
| Sandstone, Salt Wash Mbr. | CP | 29 | C | 3.24 | 7.18 | 4.88 |
| Shale, Cutler Fm. | CR | 1 | C | — | | 2.14 |
| Shale, silty, Cutler Fm. | CR | 3 | C | 2.88 | 3.78 | 3.43 |
| Siltstone, Cutler Fm. | CR | 3 | C | 3.66 | 4.54 | 4.05 |
| Siltstone, Cutler Fm. | CP | 2 | C | 6.05; | 7.21 | 6.63 |
| Siltstone, Chinle Fm. | CP | 2 | C | 4.64; | 5.77 | 5.21 |

| Speciment | | | | Conductivity K x 10 ³ (cal/cm sec °C) | |
|---|-----------------------|--------|--------------------|---|-------|
| Material and geologic unit | Place a/ Collected | Number | Kind ^{b/} | Range | Mean |
| Siltstone, Moenkopi Fm. | CP | 1 | C | — | 8.32 |
| Siltstone, Salt Wash Mbr. | CP | 3 | C | 1.97 - 4.41 | 3.38 |
| Siltstone, Summerville Fm. | CP | 6 | C | 2.89 - 6.52 | 4.28 |
| Sandstone Salt Wash Mbr. | CP | 21 | C | 2.24 - 8.32 | 5.30 |
| Sandstone, Summerville Fm. | CP | 1 | C | — | 2.81 |
| Salt, Paradox (containing halite, sylvite, carnallite, and anhydrite) | TU | 14 | C | 9.33 - 12.39 | 10.81 |

a/ ANM - Arches National Monument, near Moab, Utah; CR - Colorado River, near Moab, Utah; CP - Colorado Plateau, near Montrose, Colorado; TU - near Thompsons, Ut.

b/ S - Hand sample; C - Core.

c/ Wet.

d/ Partly saturated.

e/ Thin disc; chipped edge.

Appendix II - Source of K values^{a/}

[For rock types not collected or tested, values of thermal conductivity for similar rocks were taken from published tables (Birch et al., 1942).]

| | K x 10 ³ cal/cm sec °C |
|--|---|
| <i>Reeder No. 1</i> | |
| Mancos Shale - best value | 3.23 |
| Dakota Sandstone - average value | 10.52 |
| Salt Wash sandstone - average value of partly saturated | 9.15 |
| Shale - median value of Brushy Basin shale and of Salt Wash siltstone and mudstone | 5.75 |
| Limestone - from Birch et al. (1942) | 4.00 |
| <i>Paradox salt</i> | |
| Shale - mean value of Cutler Formation silty shale | 3.26 |
| Sandstone - mean value of Morrison Formation | 9.15 |
| Salt - mean value | 10.61 |
| Anhydrite - only a few streaks included with salt. | |
| Dolomite - only a few streaks included with sandstone | |
| <i>Crescent Eagle No. 1 and Brendell No. 1</i> | |
| Same as in Reeder No. 1 except Hermosa Formation - mean value determined from sandy limestone, K = 5.94, and shale, K = 2.72 | 3.14 |
| <i>Balsley No 1-C</i> | |
| Sandstone - same as in Reeder No. 1 (only 4 ft in well, so value used is unimportant.) | |
| Gypsum - from Birch et al. (1942) | 2.98 |
| Anhydrite - from Birch et al. (1942) | 10.80 |
| Limestone - from Birch et al. (1942) | 4.00 |
| (only 2 ft in well, so value used is unimportant.) | |
| Paradox salt - same as for Reeder well. | |

Hyde No. 1

| | |
|---|------|
| Shale - median value of Brushy Basin, Mancos, Carmel, Summerville shales, Summerville silstones and mudstones, and Salt Wash silstones used in upper section to 1,348 ft. | 3.23 |
| Shale - mean value of Cutler, Chindle, Moenkopi siltstones used in lower section | 4.96 |
| Limestone - mean value of Summerville Formation high values | 6.61 |
| Sandy shale - mean value of Carmel, Summerville, Cutler Formations | 3.70 |
| Sandstone - average value of Morrison, Summerville, Entrada Formations used in upper section to 1,348 ft | 6.05 |
| Sandstone - average value of Navajo, Kayenta, Wingate, Chinle, Moenkopi, Cutler, Rico Formations used in lower section | 6.34 |
| Talc - from Birch et al. (1942) | 2.20 |
| Sandy limestone - average of Summerville Formation values and values from Birch et al. (1942) used in the upper section to 1,348 ft | 5.45 |
| Sandy limestone - mean value of Summerville Formation used for middle section to 2,300 ft | 6.61 |
| Sandy limestone - Summerville Formation high value used in deep section | 6.75 |

a/ From Appendix I unless source is given.

Appendix III - *Temperature observations in wells.*

| Well | Depth-feet | Temperature °F | Location |
|----------------------|------------|--------------------|---|
| Crescent Eagle No. 1 | 100 | 60.1 | Sec. 4, T 22 |
| | 500 | 66.5 | S, R 19 E |
| | 1,100 | 77.2 | measured by |
| | 1,500 | 88.3 | H. Cecil Spicer |
| | 1,950 | 97.0 | 8-10-42 |
| Brendell No. 1 | 100 | 62.7 ^{a/} | Sec. 9, T 22 |
| | 500 | 67.1 | S, R 19 E |
| | 1,000 | 77.0 | measured by |
| | 1,500 | 88.7 | H. Cecil Spicer 1942 |
| Reeder No. 1 | 4,209 | 114.3 | Sec. 4, T 22 S, R 19 E measured by H. Cecil Spicer 8-4-42 |
| Reeder No. 1 | 100 | 64.1 | As above; |
| | 500 | 70.0 | measured by |
| | 1,000 | 79.2 | H. Cecil Spicer |
| | 1,500 | 89.2 | 10-4-6-42. |
| | 2,000 | 96.3 | |
| | 2,100 | 98.8 | |
| | 2,500 | 102.4 | |
| | 3,000 | 107.0 | |
| | 3,095 | 107.4 | |

a/ In error; no ice for thermometers.

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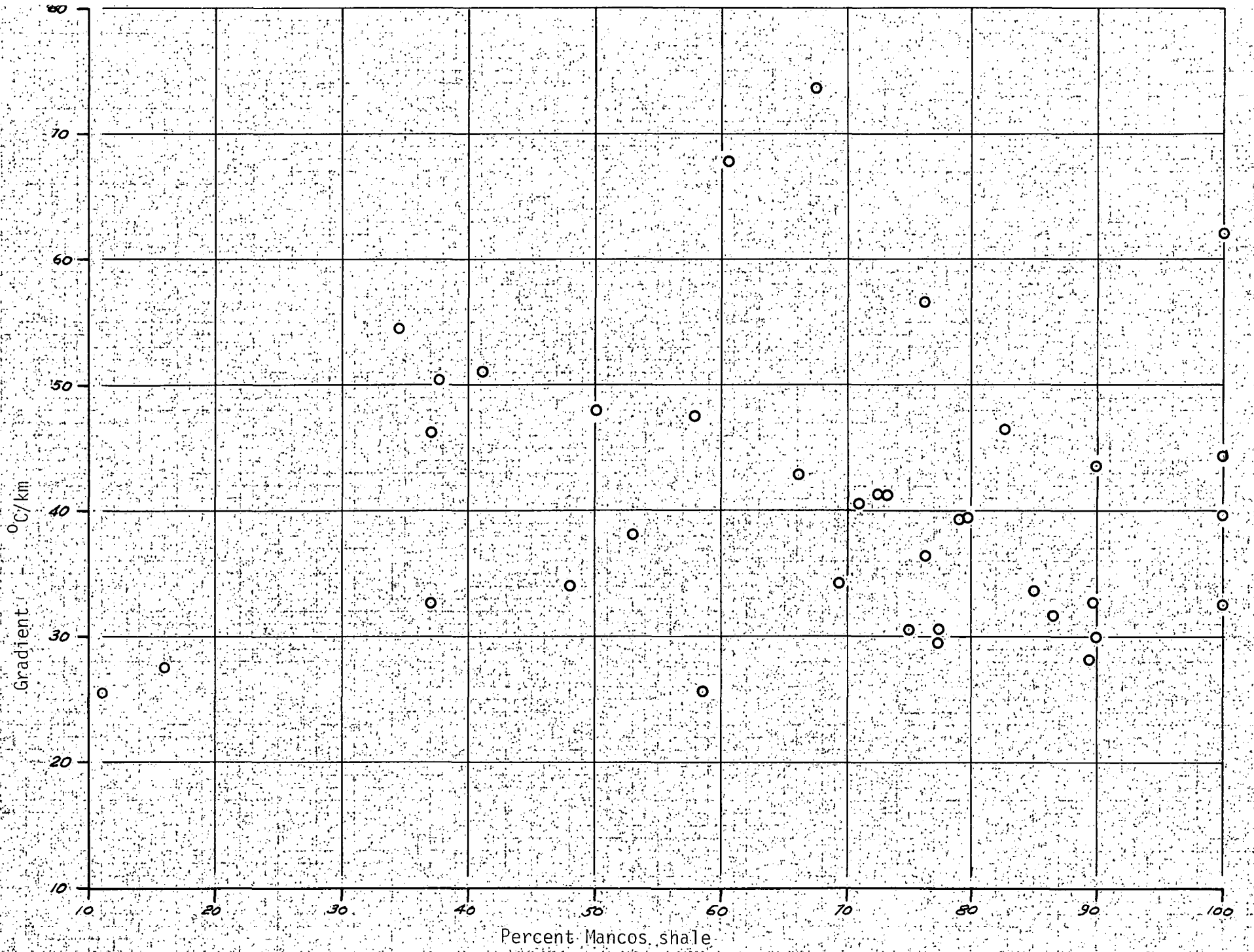
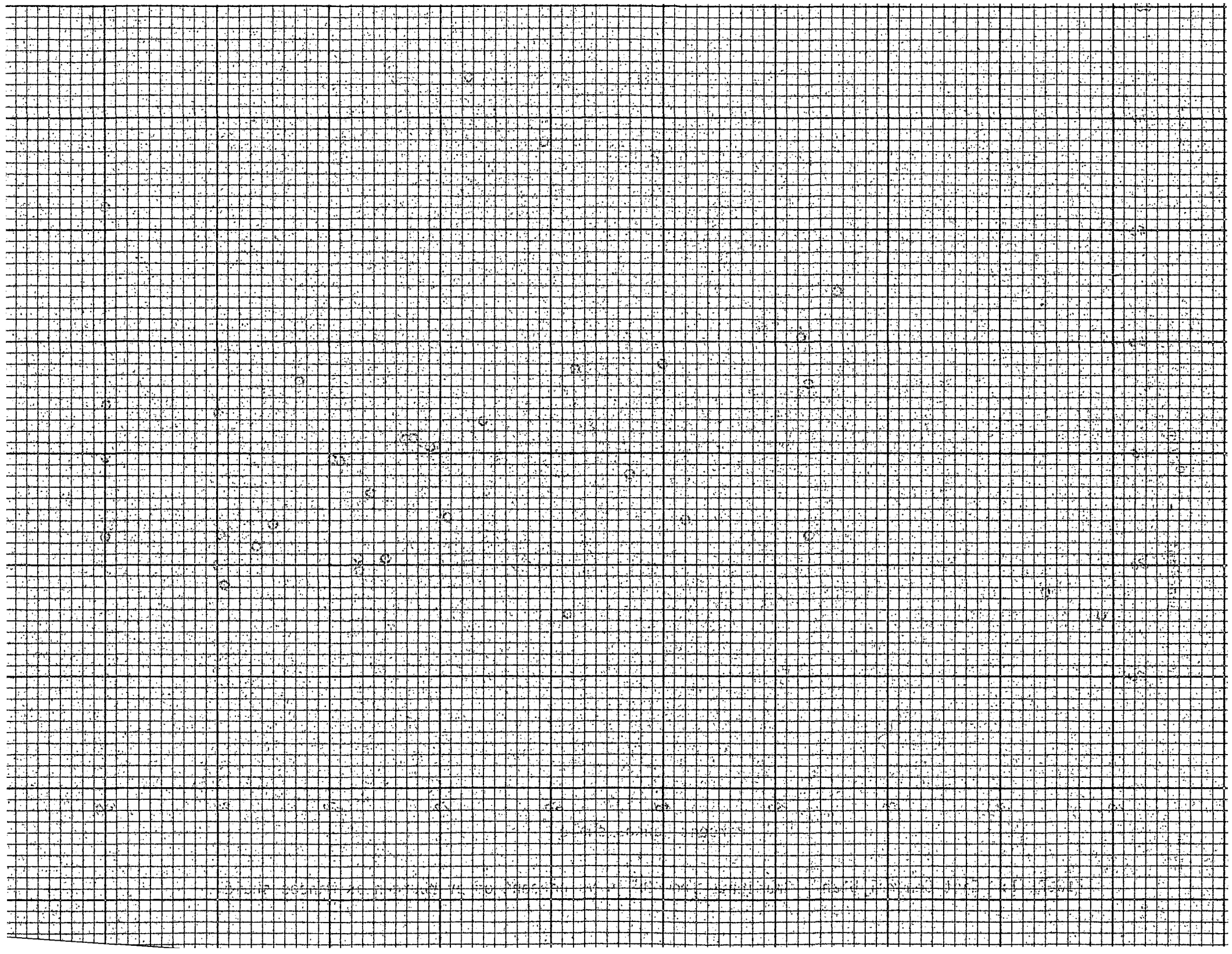
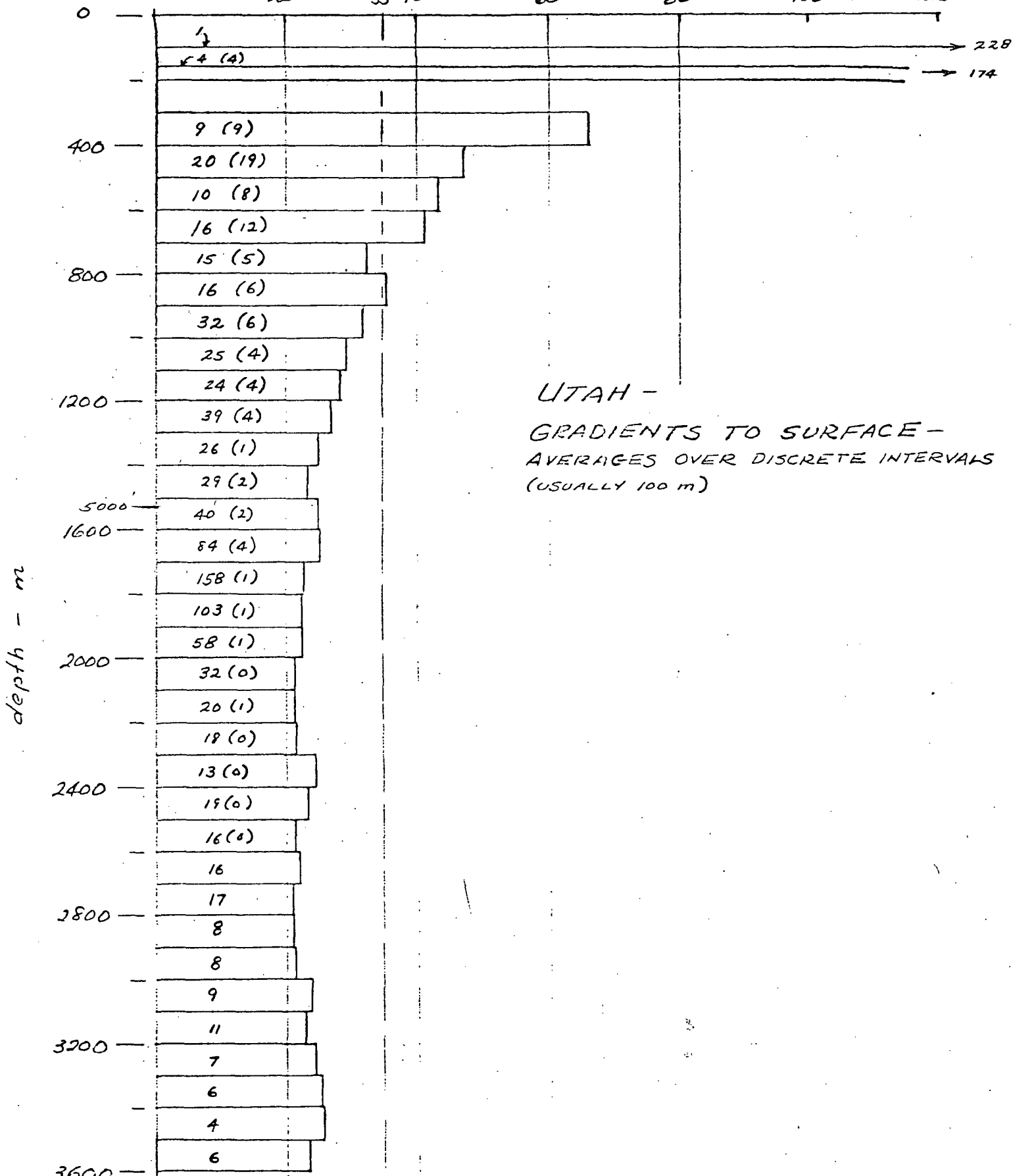


FIGURE 1: East Central Utah - Gradients from BHT's vs percent of overburden as Mancos shale.



GRADIENT $^{\circ}\text{C}/\text{km}$

20 35 40 60 80 100 120



UTAH -
GRADIENTS TO SURFACE -
AVERAGES OVER DISCRETE INTERVALS
(USUALLY 100 m)

↑ No. of GRADIENTS $\geq 35^{\circ}\text{C}/\text{km}$
↑ No. OF SAMPLES

**UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY**

SUBMIT IN DUPLICATE

(See other instructions on reverse side)

Form approved
Budget Bureau No. 42-R355.5

71

WELL COMPLETION OR RECOMPLETION REPORT AND LOG *

1a. TYPE OF WELL: OIL WELL GAS WELL DRY Other

b. TYPE OF COMPLETION:
NEW WELL WORK OVER DEEP-EN PLUG BACK DIFF. RESVR. Other

2. NAME OF OPERATOR
ALPINE OIL COMPANY, INC.

3. ADDRESS OF OPERATOR
722 Patterson Building, Denver, Colorado

4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements)*
At surface
At top prod. interval reported below
At total depth

14. PERMIT NO. _____ DATE ISSUED _____

15. DATE SPUNDED **1/30/64** 16. DATE T.D. REACHED **2/3/64** 17. DATE COMPL. (Ready to prod.) _____

18. ELEVATIONS (DF, REB, RT, GE, ETC.)* _____ 19. ELEV. CASINGHEAD _____

20. TOTAL DEPTH, MD & TVD _____ 21. PLUG, BACK T.D., MD & TVD _____ 22. IF MULTIPLE COMPL. HOW MANY* _____ 23. INTERVALS DRILLED BY _____ ROTARY TOOLS **04608** CABLE TOOLS _____

24. PRODUCING INTERVAL(S), OF THIS COMPLETION—TOP, BOTTOM, NAME (MD AND TVD)* _____ 25. WAS DIRECTIONAL SURVEY MADE _____

26. TYPE ELECTRIC AND OTHER LOGS RUN
Gamma Ray & Temperature

28. CASING RECORD (Report all strings set in well)

| CASING SIZE | WEIGHT, LB./FT. | DEPTH SET (MD) | HOLE SIZE | CEMENTING RECORD | AMOUNT PULLED |
|-------------|-----------------|-------------------|-----------|------------------|---------------|
| 7" | | 375'-surf. | | 70 sacs | |
| | | | | | |
| | | | | | |

29. LINER RECORD

| SIZE | TOP (MD) | BOTTOM (MD) | SACKS CEMENT* | SCREEN (MD) |
|------|----------|-------------|---------------|-------------|
| | | | | |
| | | | | |

30. TUBING RECORD

| SIZE | DEPTH SET (MD) | PACKER SET (MD) |
|------|----------------|-----------------|
| | | |
| | | |

31. PERFORATION RECORD (Interval, size and number)

| DEPTH INTERVAL (MD) | AMOUNT AND KIND OF MATERIAL USED |
|---------------------|----------------------------------|
| | |
| | |
| | |

33.* PRODUCTION

| DATE FIRST PRODUCTION | PRODUCTION METHOD (Flowing, gas lift, pumping—size and type of pump) | WELL STATUS (Producing or shut-in) |
|-----------------------|--|------------------------------------|
| | | |

| DATE OF TEST | HOURS TESTED | CHOKE SIZE | PROD'N. FOR TEST PERIOD | OIL—BBL. | GAS—MCF. | WATER—BBL. | GAS-OIL RATIO |
|--------------|--------------|------------|-------------------------|----------|----------|------------|---------------|
| | | | | | | | |

| FLOW. TUBING PRESS. | CASING PRESSURE | CALCULATED 24-HOUR RATE | OIL—BBL. | GAS—MCF. | WATER—BBL. | OIL GRAVITY-API (CORR.) |
|---------------------|-----------------|-------------------------|----------|----------|------------|-------------------------|
| | | | | | | |

34. DISPOSITION OF GAS (Sold, used for fuel, vented, etc.) _____ TEST WITNESSED BY _____

35. LIST OF ATTACHMENTS _____

36. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records.

SIGNED [Signature] TITLE _____ DATE _____

5. LEASE DESIGNATION AND SERIAL NO.
Utah 0122460

6. IF INDIAN, ALLOTTEE OR TRIBE NAME _____

7. UNIT AGREEMENT NAME
Wild Cow

8. FARM OR LEASE NAME _____

9. WELL NO.
#1 Government

10. FIELD AND POOL, OR WILDCAT
Wildcat

11. SEC., T., R., M. OR BLOCK AND SURVEY OR AREA
Sec 4-T17S - R 25E

12. COUNTY OR PARISH
Grand

13. STATE
Utah

*(See Instructions and Spaces for Additional Data on Reverse Side)

Salt Lake City U. S. LAND OFFICE SERIAL NUMBER SLC 067164 LEASE OR PERMIT TO PROSPECT

Grid for well location with '19' in the center and '0' in the top right corner.

UNITED STATES DEPARTMENT OF THE INTERIOR GEOLOGICAL SURVEY

LOG OF OIL OR GAS WELL

LOCATE WELL CORRECTLY

Company American Climax Petroleum Corp. Address 1845 Sherman St., Denver 3 Lessor on Tract Government Field So. Bar-X State Utah Well No. 3 Sec. 19 T. 17S R. 26E Meridian SL County Grand Location 660 ft. S. of N Line and 660 ft. W. of E Line of Section 19 Elevation 5101' (Derrick floor relative to sea level)

The information given herewith is a complete and correct record of the well and all work done thereon so far as can be determined from all available records. Signed W. C. Johnson Date December 12, 1958 Title Field Engineer

The summary on this page is for the condition of the well at above date. Commenced drilling October 21, 1958 Finished drilling October 26, 1958

OIL OR GAS SANDS OR ZONES

(Denote gas by G)

No. 1, from None to No. 4, from to No. 2, from to No. 5, from to No. 3, from to No. 6, from to

IMPORTANT WATER SANDS

No. 1, from to No. 3, from to No. 2, from to No. 4, from to

CASING RECORD

Table with columns: Size casing, Weight per foot, Threads per inch, Make, Amount, Kind of shoe, Cut and pulled from, Perforated (From-To), Purpose. Row 1: 10-3/4", 32.75#, 8, 152.92', Hal., -

MUDDING AND CEMENTING RECORD

Table with columns: Size casing, Where set, Number sacks of cement, Method used, Mud gravity, Amount of mud used. Row 1: 10-3/4", 149', 110, Disp., Air, None

PLUGS AND ADAPTERS

Heaving plug—Material Cement Length 78' Depth set 3200-3278'

FOLD MARK

FOLD MAY

87

LIU Disp. Air None

PLUGS AND ADAPTERS

Heaving plug—Material **Cement** Length **78'** Depth set **3200-3278'**
 Adapters—Material _____ Size **25'** **150-175'**

SHOOTING RECORD

| Size | Shell used | Explosive used | Quantity | Date | Depth shot | Depth cleaned out |
|------|------------|----------------|----------|------|------------|-------------------|
| | | | | | | |
| | | | | | | |
| | | | | | | |

TOOLS USED

Rotary tools were used from **Surface** feet to **3278'** feet, and from _____ feet to _____ feet
 Cable tools were used from _____ feet to _____ feet, and from _____ feet to _____ feet

DATES

_____, 19____ Put to producing **Oct 10-28-58** _____, 19____
Dry Hole

The production for the first 24 hours was _____ barrels of fluid of which _____% was oil; _____% emulsion; _____% water; and _____% sediment. Gravity, °Bé. _____

If gas well, cu. ft. per 24 hours _____ Gallons gasoline per 1,000 cu. ft. of gas _____
 Rock pressure, lbs. per sq. in. _____

EMPLOYEES

George Ginder, Driller **C. H. Baker**, Driller
W. L. Dougless, Driller

FORMATION RECORD

| FROM— | TO— | TOTAL FEET | FORMATION |
|-------|------|------------|----------------------|
| 0 | 2468 | 2468 | Mancos |
| 2468 | 2618 | 150 | Dakota |
| 2618 | 2940 | 322 | Morrison |
| 2940 | 3149 | 209 | Morrison - Salt Wash |
| 3149 | 3264 | 115 | Summerville |
| 3264 | 3278 | 14 | Entrada |

OCT 17 1958

EXAMPLE - WELL 68

① $116^{\circ}\text{F} = 46.7^{\circ}\text{C}$

$2900' = .884 \text{ km}$

$22.4^{\circ}\text{F}/1000 = 40.8^{\circ}\text{C}/\text{km}$

$\Delta z = \frac{50 - 46.7}{40.8} = .081, \underline{Z_T = .965 \text{ km (actual .960)}}$

② $133^{\circ}\text{F} = 56.1^{\circ}\text{C}$

$3700' = 1.128 \text{ km}$

$22.2^{\circ}\text{F}/1000 = 40.4^{\circ}\text{C}/\text{km}$

$\Delta z = \frac{50 - 56.1}{40.4} = .151, \underline{Z_T = .977 \text{ (actual .960)}}$

③ From case ① above - use as $U_T \text{ grad} = 33^{\circ}\text{C}/\text{km}$

$\Delta z = \frac{50 - 46.7}{33} = .1, \underline{Z_T = .984 \text{ (actual .960)}}$

④ From case 2 above as $U_T \text{ grad} = 28^{\circ}\text{C}/\text{km}$

$\Delta z = \frac{50 - 56.1}{28} = .218, \underline{Z_T = .910 \text{ (actual .960)}}$

EXAMPLE - WELL 16

① $116^{\circ}\text{F} = 46.7^{\circ}\text{C}$ depth to 50°C isotherm

$$3100' = .945 \text{ km}$$

$$20.97^{\circ}\text{F}/1000 = 38.2^{\circ}\text{C}/\text{km}$$

$$\Delta z = \frac{50 - 46.7}{38.2} = .086$$

$$Z_T = .945 + .086 = \underline{1.031 \text{ m}} \text{ (actual = } \underline{1.068})$$

② $143^{\circ}\text{F} = 61.7$

$$4650' = 1.417$$

$$19.78^{\circ}\text{F}/1000 = 36.1^{\circ}\text{C}/\text{km}$$

$$\Delta z = \frac{50 - 61.7}{36.1} = -.324$$

$$Z_T = 1.417 - .324 = \underline{1.093} \text{ (actual } \underline{1.068})$$

③ From case ① above use av grad. (Utah)

$$\text{at } .945 \text{ km} = 31^{\circ}\text{C}/\text{km} \text{ (UTAH GRAPH)}$$

$$\Delta z = \frac{50 - 46.7}{31} = .106, Z_T = \underline{1.051} \text{ (actual } \underline{1.068})$$

④ from case ① above use av grad at $1.051 \text{ m} = 29$ (UTAH GRAPH)

$$\Delta z = \frac{50 - 46.7}{29} = .114, Z_T = \underline{1.059} \text{ (actual } \underline{1.068})$$

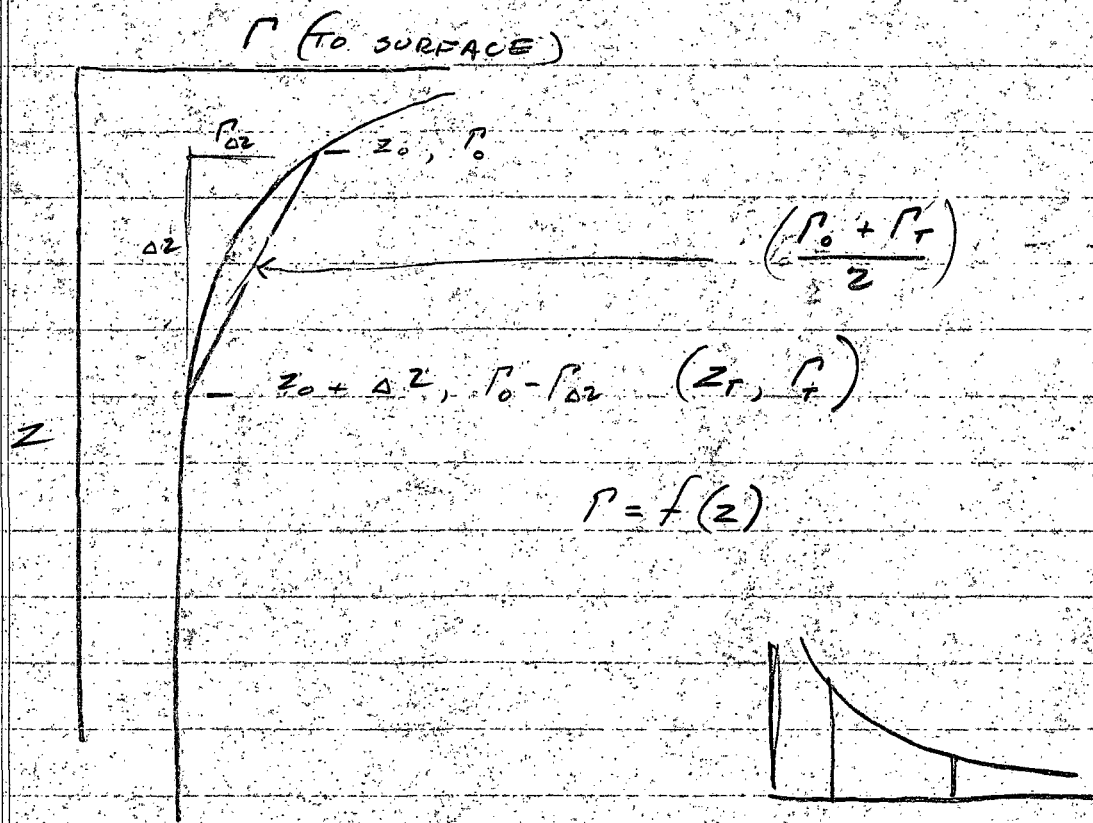
$$\text{av Chart grad at } 1.068 = 29^{\circ}\text{C}/\text{km}$$

$$\text{" " " " " } .945 = 31^{\circ}\text{C}/\text{km}$$

$$\text{av} = 30^{\circ}\text{C}/\text{km}$$

$$\frac{50 - 46.7}{30} = .11$$

$$Z_T = .945 + .11 = \underline{1.055 \text{ km}} \text{ actual } \underline{1.068}$$



$$\left(\frac{\rho_0 + \rho_T}{2}\right) \Delta z + T_0 = T_T = 50^\circ\text{C}$$

$$\text{TRY } \rho_0 \Delta z + T_0 = 50$$

$$\Delta z = \frac{50 - T_0}{\rho_0}$$

FROM GRAPH ρ between 200m - 3600m

| | | |
|-------------|-----------|---------|
| d | T | = 17.35 |
| 200 | 28 | |
| <u>3600</u> | <u>87</u> | |
| 3400 | 59 | |

(Log) T_d at depth d

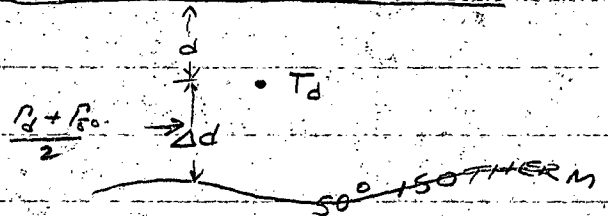
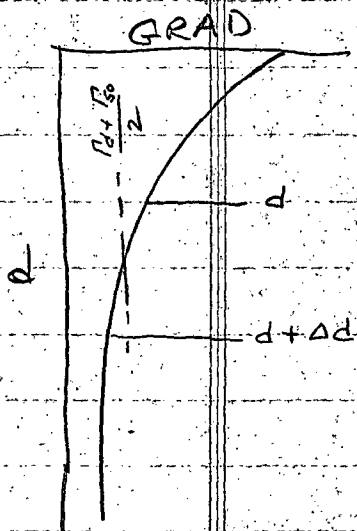
Mean grad at depth $d = \bar{\Gamma}$

50°C ISOTHERM

$$T_d < 50^\circ\text{C}$$

depth to isotherm

$$(50^\circ\text{C} - T_d) = \Delta T$$



$\Gamma_{50} = \Gamma$ at 50° isotherm (variable)

$$\left(\frac{\Gamma_d + \Gamma_{50}}{2}\right) \Delta d + T_d = 50^\circ$$

uniform Γ
in critical
region

$$\Gamma \Delta d + T_d = 50^\circ$$

$$\Delta d = \frac{50^\circ - T_d}{\Gamma}$$

$$\Gamma_{d+\Delta d} = \Gamma_{50} = \Gamma_d = \Gamma$$

GRAND CO

WELL No. 68

P from surface to 3700' 40.4°C/ft
P between 2900' - 3700' 38.7°C/ft

WELL No. 61

P from surface to 3250' 35.9°C/ft
P between 2000' - 3250' 30.6°C/ft

WELL No. 16

P from surface to 4650' 36.1°C/ft
P do 3100' 38.2
between 3100' - 4650' 31.8°C/ft

WELL No. 120

P from surface to 3600' 51.1°C/ft
do 3000' 56.5°C/ft
do 2000' 65.6°C/ft
do 1300' 56.1°C/ft
do 1000' 65.6°C/ft
P between 3000' - 3600' 24°C/ft
do 2000' - 3000' 38.3°C/ft
do 1300' - 2000' 83.3°C/ft
do 1000' - 2000' 65.6°C/ft
do 1000' - 3600' 45.6°C/ft

WELL No.

over

GRAND CO. cont.

WELL No 71

| | | |
|-------------------|-------------|----------|
| P from surface to | 4607' | 46.7°/hr |
| do | 3800' | 49.4 |
| do | 3500' | 49.5 |
| P between | 3800 - 4607 | 33.9 |
| do | 3500 - 4607 | 37.9 |

EXAMPLE - WELL 120 (wild prod. near 50°C)

①

$$87^{\circ}\text{F} = 30.56$$

$$1000' = .3048$$

$$36^{\circ}\text{F}/1000 = 65.6^{\circ}\text{C}/\text{km}$$

$$\Delta z = \frac{50 - 30.56}{65.6} = .296, Z_T = .601 \text{ (actual .597 km)}$$

②

$$152^{\circ}\text{F} = 66.67$$

$$3600' = 1.097$$

$$28.0^{\circ}\text{F}/1000 = 51.1$$

$$\Delta z = \frac{50 - 66.67}{51.1} = -.326, Z_T = .771 \text{ (actual .597)}$$

③

$$91^{\circ}\text{F} = 32.78^{\circ}\text{C}$$

$$1300' = .396 \text{ km}$$

$$30.8^{\circ}\text{C}/1000 = 56.1^{\circ}\text{C}/\text{km}$$

$$\Delta z = \frac{50 - 32.78}{56.1} = .307, Z_T = .703 \text{ km (actual .597)}$$

④

$$94.5^{\circ}\text{F} = 34.7$$

$$1500' = .457$$

$$29.0^{\circ}\text{F}/1000 = 52.8^{\circ}\text{C}/\text{km}$$

$$\Delta z = \frac{50 - 34.7}{52.8} = .290 \text{ km}, Z_T = .747 \text{ (actual .597)}$$

⑤

$$135^{\circ}\text{F} = 57.2^{\circ}\text{C}$$

$$2500' = .762 \text{ km}$$

$$33.6^{\circ}\text{F}/1000 = 61.2^{\circ}\text{C}/\text{km}$$

$$\Delta z = \frac{50 - 57.2}{61.2} = -.118, Z_T = .644 \text{ km (actual .597)}$$

⑥

$$144^{\circ}\text{F} = 62.2^{\circ}\text{C}$$

$$3000' = .914 \text{ km}$$

$$31^{\circ}\text{F}/\text{km} = 56.5^{\circ}\text{C}/\text{km}$$

$$\Delta z = \frac{50 - 62.2}{56.5} = -.216 \text{ km}$$

$$Z_T = .914 - .216 = .698 \text{ km (actual .597)}$$

OVER

⑦

123°F = 50.56°C

2000' = .610 km

36°F/1000 = 65.6°C/km

ΔZ_T = (50 - 50.56) / 65.6 = .008, Z_T = .610 - .008 = .602 km
actual 597

⑧ Use ex ② and P from chart for 1100m
P = 28

ΔZ = (50 - 66.67) / 28 = .595

Z_T = 1.097 - .595 = .502 km

FROM CHART P at 597 = 40°C/km

ΔZ = (50 - 66.67) / 40 = .417

Z_T = .680 km

av of (28 + 40) / 2 = 34

ΔZ = (50 - 66.67) / 34 = .490

Z_T = 607
597

⑩ Use ex ① and P from chart for 305m
P = 64

Chart P at 597°C = 40

av of (64 + 40) / 2 = 52

ΔZ = (50 - 30.56) / 52 = .374

Z_T = .374 + .305 = 679
597

GRAND CO.
CALC. DEATHS
TO 50°C ISOTHERM

No EVENTS

5

1

-50%

30 20 10 10 20 30

+50%

% ERROR

27 EVENTS

5

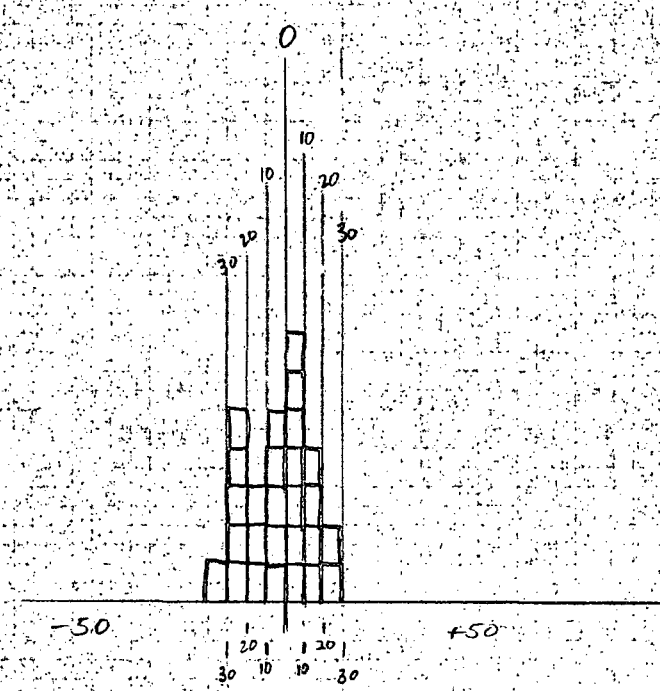
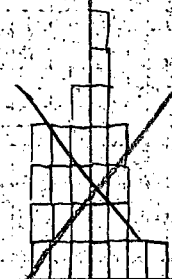
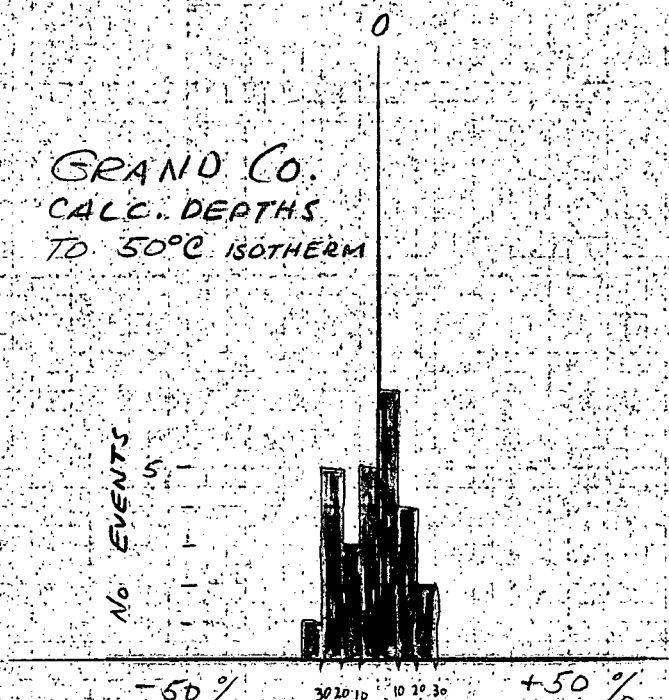
-50

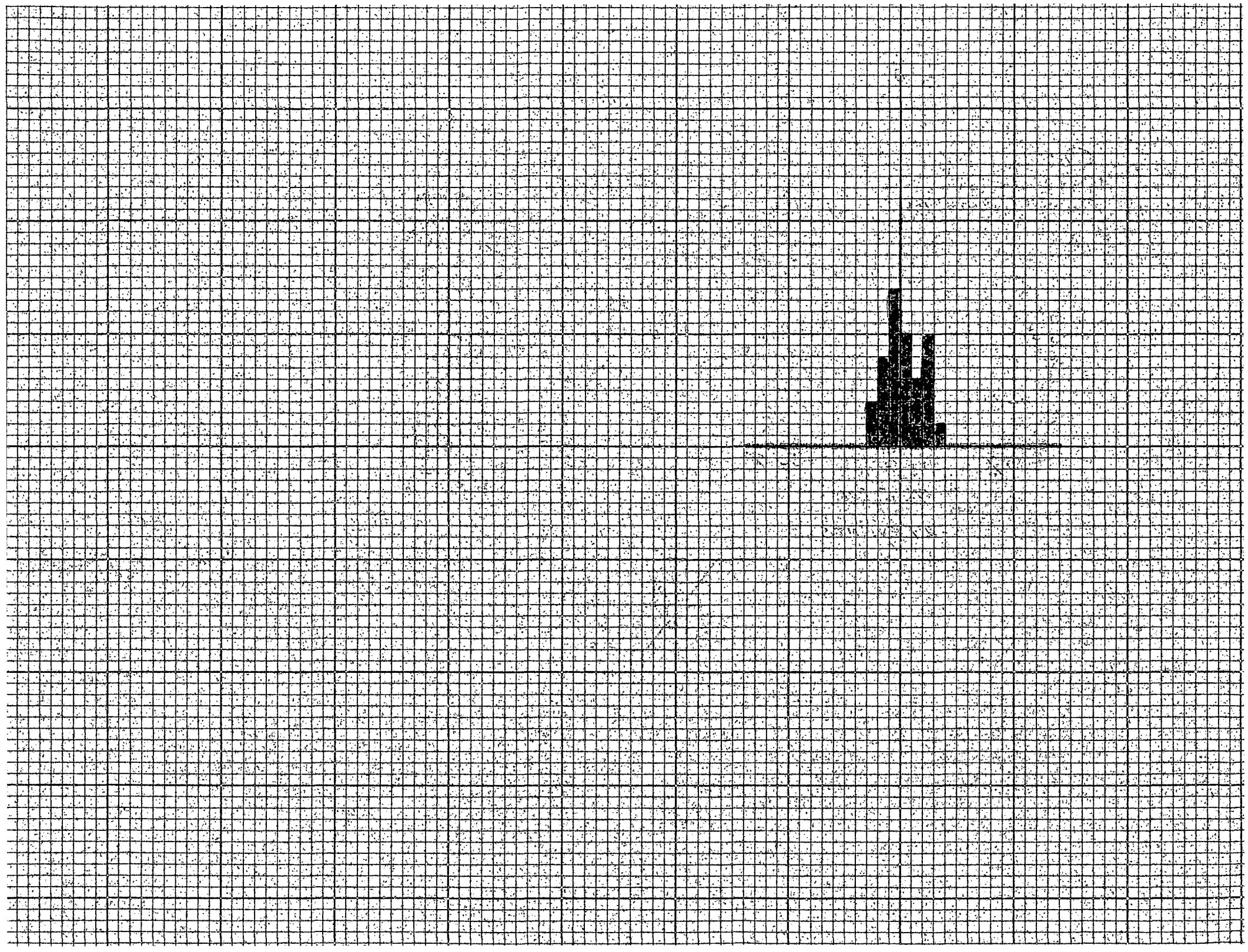
30 20 10 10 20 30

+50

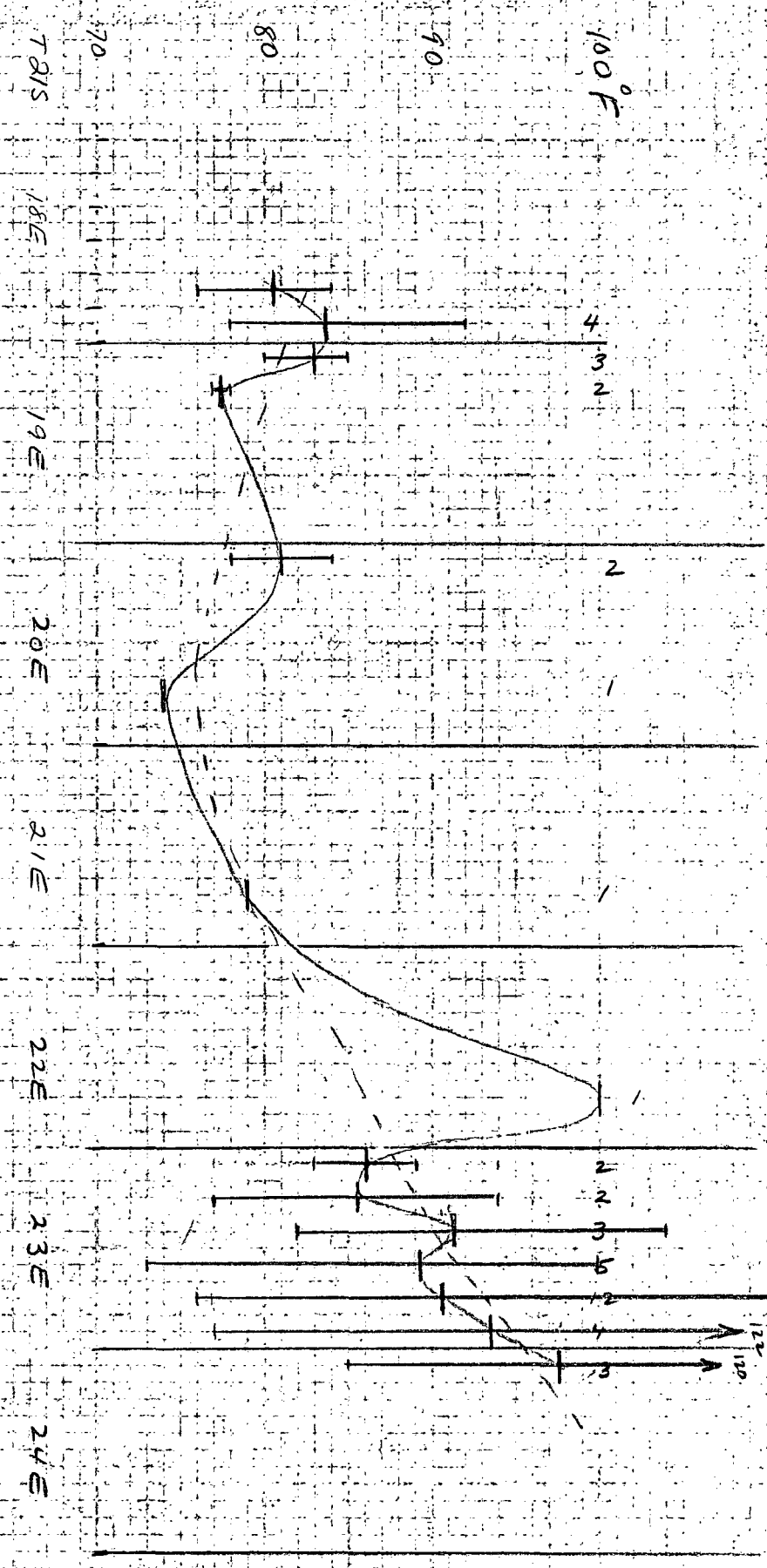
-50

+50





T215 - GRAND Co
TEMPERATURES AT 3000' ASL



| | | | | | | | | | | |
|---|-----|-----|------|-----|--|--|--|--|--|--|
| 5 | 256 | 106 | 1081 | 291 | | | | | | |
|---|-----|-----|------|-----|--|--|--|--|--|--|

* From E-Logs

GRAND CO - T-LOGS

Calculating d to 50°C isotherm

| | CALC. | | | | | | | 8 | 9 |
|----|-------------|--------------|--------------|---------------|------------------------|--------------|--------------|---------|---|
| | 1 WELL | 2 °C | 3 depth m | 4 °C/m | 5 Depth 50°C meters | 6 ERROR m | 7 % ERROR | | |
| 1 | 16 | 46.7 | 945 | 38.2 | 1031 | 0 | 0 | my plot | |
| 2 | 1031 To 50° | 61.7 83.9 | 1417 1769 | 36.1 41.4* | 1091 952 | +60 -79 | +5.8 +7.7 | | |
| 3 | 28 | 41.7 | 1250 | 24.9 | 1582 | +82 | +5.4 | | |
| 4 | | 50 | 1500 | 26.26 | 1500 | - | - | | |
| 5 | | 51.1 | 1524 | 26.6 | 1368 | -132 | -8.8 | | |
| 6 | | 65 | 1829 | 29.8 | 1322 | -178 | -11.9 | | |
| 7 | | 44.2 | 979 | 34.3* | 1149 | -351 | -23.4 | | |
| 8 | | 73.9 | 2068 | 30.6* | 1288 | -212 | -14.1 | | |
| 9 | | 60 | 2099 | 23.6* | 1669 | +169 | +11.3 | | |
| 10 | 43 | 40.6 | 1859 | 16.1 | 2447 | +362 | +17.4 | | |
| 11 | | 50 | 2085 | 18.9 | 2085 | - | - | | |
| 12 | | 51.7 | 2134 | 19.3 | 2041 | -44 | -2.1 | | |
| 13 | | 65.6 | 2438 | 22.6 | 1743 | -342 | -16.4 | | |
| 14 | | 77.8 | 2743 | 24.5 | 1608 | -477 | -22.9 | | |
| 15 | | 85 | 2896 | 25.7 | 1533 | -552 | -26.5 | | |
| 16 | | 88.9 | 3002 | 26.1* | 1510 | -575 | -27.6 | | |
| 17 | | 47.2 | 1840 | 19.9* | 1980 | -105 | -5.0 | | |
| 18 | 68 | 46.7 | 884 | 40.8 | 966 | +6 | +0.6 | | |
| 19 | | 50 | 960 | 41.0 | 960 | - | - | | |
| 20 | | 56.1 | 1128 | 40.4 | 975 | +15 | +1.6 | | |
| 21 | | 79.4 | 1340 | 51.4* | 766 | -194 | -20.2 | | |
| 22 | | 64.4 | 1342 | 40.2* | 980 | +20 | +2.1 | | |
| 23 | 120 | 30.56 | 305 | 65.6 | 601 | +4 | +0.7 | | |
| 24 | | 32.78 | 396 | 56.7 | 702 | +105 | +17.6 | | |
| 25 | | 34.7 | 457 | 52.8 | 746 | +149 | +25.0 | | |
| 26 | | 50 | 597 | 66.0 | 597 | - | - | | |
| 27 | | 57.2 | 762 | 61.2 | 643 | +46 | +7.7 | | |
| 28 | | 62.2 | 914 | 56.5 | 697 | +100 | +16.8 | | |
| 29 | | 66.67 | 1,097 | 51.1 | 771 | +174 | +29.1 | | |
| 30 | | 64.4 | 1099 | 49.0* | 804 | +207 | -34.7 | | |
| 31 | | 66.67 | 1097 | 51.1* | 771 | DUPLICATE | | | |

EFFICIENCY® LINE No. 2636



P. E. LOG

FROM T LOGS - GRAND CO.

| WELL # | ° F | DEPTH FT | To SURFACE °C/km | | | | | |
|-------------------------|--------------------------|----------|------------------|-----------------|---------|-------|---------------------------------------|------|
| 41 5805 101 | 16 actual | 116 | 3100 | 38.2 | | 29.6 | 0.68 96' 107 | |
| | 50°C at 1068m (3505') | 129 | 3900 | 36.4 | | | | 31.8 |
| | | 143 | 4650 | 36.1 | | | | 34.0 |
| 40 5253 | 61 | 94 | 2000 | 39.2 | | 30.6 | | |
| | | 115 | 3250 | 35.9 | | | | |
| 51 4395 19 (3150) | 68 | 116 | 2900 | 40.8 | | 38.7 | 960 772 180 | |
| | 50°C 960m actual | 133 | 3700 | 40.4 | | | | |
| 47 4607 | 71 | 146 | 3500 | 49.5 | | 48.6 | | |
| | | 154 | 3800 | 49.4 | | | 37.9 | |
| | | 169 | 4607 | 46.7 | | | 33.9 | |
| 51 3600 | 120 ✓ | 87 | 1000 | 65.6 | ✓ | | | |
| | ✓ | 91 | 1300 | 56.1 | ✓ | | | |
| | → | ✓ | 94.5 | 1500 | 52.8 | ✓ | BETWEEN 1650-1750 <u>BIG ANOMALY?</u> | |
| | actual | ✓ | 123 | 2000 | 65.6 | | | |
| | 50°C @ 597m (1960') | ✓ | 135 | 2500 | 61.2 | ✓ | | |
| | ✓ | 144 | 3000 | 56.5 | ✓ | | | |
| | 152 | 3600 | 51.1 | Depth to 50°C m | | | | |
| 28 | 107 | 4100 | 24.9 | 1.582 | 111.5 F | 3213' | 34.3 | 1149 |
| | 122 | 4920 | 26.3 | 1.498 | 165 | 6785 | 30.6 | 1288 |
| | 124 | 5000 | 26.6 | 1368 | 140 | 6886 | 23.6 | 1669 |
| | 149 | 6000 | 29.8 | 1322 | | | | |
| 43 | 105 | 6100 | 16.1 | 2447 | 192 | 9851 | 26.1 | 1510 |
| | 122 | 6840 | 18.9 | 2085 | 117 | 6036 | 19.9 | 1980 |
| | 125 | 7000 | 19.3 | 2041 | | | | |
| | 150 | 8000 | 22.6 | 1743 | | | | |
| | 172 | 9000 | 24.5 | 1608 | | | | |
| | 185 | 9500 | 25.7 | 1533 | | | | |

41.3 ✓ 2000 - 2199

1200 ✓ 1399

47.4 ✓ 1400 - 1599

35.6 ✓ 2200 - 2500

1000 ✓ 1199

44.4 ✓ 1600 - 1799

43.0 ✓ 1800 - 1999

Between 0 and

VARIANCE FROM MEAN Γ

WELL

No BHT Depth Collar

$\mu^{\circ}C/m$

σ

| | | | | | | |
|-----|-----|--------|------|-------|------|---------|
| 362 | 94 | 2311 ✓ | 7211 | | 38.6 | 125-15E |
| 367 | 115 | 2294 ✓ | 6150 | | 55.6 | 12-16 |
| 367 | 115 | 2419 ✓ | 6150 | | " | " |
| 370 | 76 | 2452 ✓ | 6855 | | 23.0 | 12-16 |
| 379 | 100 | 2128 | 6715 | +11.5 | 47.1 | 13-17 |
| 390 | 97 | 1545 | 4820 | +6.6 | 54.3 | 17-16 |
| 418 | 85 | 1393 | 5128 | | 44.8 | 25-15 |
| 502 | 85 | 2163 | 6235 | -1.9 | 33.7 | 14-22 |
| 503 | 117 | 1848 | 7022 | +49.6 | 97.3 | 14-23 |
| 19 | 92 | 2259 ✓ | 6520 | | 33.1 | 16-24 |
| 27 | 112 | 1540 | 6481 | +24.5 | 72.2 | 16-25 |
| 56 | 90 | 1135 | 6043 | | 67.6 | 17-24 |
| 59 | 90 | 11343 | 6136 | | 52.9 | 17-24 |
| 65 | 90 | 1451 | 6789 | +1.3 | 49.0 | 17-24 |
| 65 | 90 | 1770 | 6789 | | 40.2 | " |
| 66 | 80 | 815 | 5618 | | 64.9 | 17-24 |
| 67 | 80 | 1146 | 5613 | | 46.1 | 17-24 |
| 88 | 82 | 2222 ✓ | 5070 | | 25.4 | 17-26 |
| 90 | 121 | 2347 ✓ | 5013 | | 54.4 | 17-26 |
| 91 | 102 | 2100 | 5010 | +11.7 | 44.3 | 17-26 |
| 98 | 80 | 1797 | 5825 | | 29.4 | 18-22 |
| 99 | 92 | 1802 | 5872 | | 41.5 | 18-22 |
| 109 | 120 | 2350 ✓ | 4933 | | 53.5 | 18-24 |
| 112 | 89 | 1880 | 4786 | | 36.7 | 18-25 |
| 113 | 92 | 1973 | 4900 | | 37.9 | 18-25 |
| 114 | 95 | 2799 | 4713 | | 28.7 | 18-25 |
| 115 | 80 | 1790 | 4806 | -12.2 | 35.5 | 18-25 |
| 104 | 85 | 1198 | 4813 | | 51.7 | 18-25 |
| 117 | 106 | 2200 ✓ | 5975 | | 45.6 | 19-18 |
| 125 | 92 | 2155 | 7473 | -0.9 | 34.7 | 19-21 |
| 126 | 88 | 2100 | 5706 | | 39.9 | 19-22 |
| 136 | 104 | 2436 ✓ | 7892 | | 39.6 | 19-23 |
| 139 | 81 | 1598 | 4576 | -13.5 | 34.2 | 19-24 |
| 140 | 80 | 1575 | 4575 | -14.1 | 33.6 | 19-24 |
| 141 | 107 | 1475 | 4647 | +15.3 | 63.0 | 19-24 |
| 143 | 100 | 1954 | 4598 | | 45.7 | 19-25 |
| | | | 2450 | | | |

6.94-99.9

| | BHT | Depth | Collar | VARIENCE | °C/ft | Loc |
|-------|-----|-----------------|--------|----------|-------|----------|
| (161) | 91 | 2238✓ | 5185 | | 32.6 | 20-21 |
| (163) | 112 | 1800 | 5072 | | 61.8 | 20-21 |
| (169) | 94 | 2455✓ | 5085 | | 31.9 | 20-22 |
| (173) | 92 | 2334✓ | 4986 | | 32.0 | 20-22 |
| (177) | 92 | 2257✓ | ? | | 33.1 | 20-23 |
| (178) | 80 | 1420 | 4584 | | 31.3 | 20-27 OK |
| (179) | 80 | 1610 | 4592 | | 31.5 | 20-24 |
| (182) | 90 | 2049 | 4826 | -0.9 | 34.7 | 20-23 |
| (183) | 96 | 2498✓ | 4828 | | 32.8 | 20-23 |
| (184) | 100 | 1999 | 4849 | | 44.7 | 20-23 |
| (185) | 100 | 2119 | ? | +6.5 | 42.1 | 20-23 |
| (186) | 98 | 2057 | 4812 | +6.0 | 41.6 | 20-23 |
| (187) | 92 | 2233✓ | ? | | 33.5 | 20-23 |
| (188) | 106 | 2449✓ | 4828 | | 40.9 | 20-23 |
| (189) | 115 | 1998 | 4764 | | 58.4 | " |
| (190) | 98 | 2105 | ? | +5.1 | 40.7 | " |
| (394) | 90 | 1630 | 4671 | | 43.6 | " |
| (191) | 96 | 1766 | 4672 | | 46.4 | " |
| (192) | 90 | 2283✓ | 4715 | | 31.1 | " |
| (193) | 88 | 186.2 | 4718 | | 36.2 | " |
| (194) | 70 | 2004 | ? | -18.3 | 17.3 | " |
| (195) | 125 | 1840 | ? | | 73.3 | " |
| (196) | 97 | 2369✓ | ? | | 35.4 | " |
| (197) | 90 | 2143 | ? | -2.4 | 33.2 | " |
| (198) | 100 | 155.2 | 4756 | | 57.5 | " |
| (199) | 88 | 2278✓ | 4848 | | 29.6 | " |
| (201) | 95 | 2345✓ | 4855 | | 34.2 | " |
| (202) | 77 | 1841 | 4511 | | 25.7 | " |
| (203) | 87 | 1663 | 4604 | | 39.5 | 20-24 |
| (204) | 86 | 1663 | 4573 | | 39.8 | " |
| (350) | 95 | 1583 | 4566 | | 50.7 | " |
| (205) | 90 | 1330 | 4595 | | 53.4 | " |
| (206) | 82 | 1496 | 4600 | | 37.8 | " |
| (207) | 90 | 1663 | 4589 | | 42.8 | " |
| (208) | 82 | 1663 | 4593 | | 34.3 | " |
| (209) | 86 | 1663 | ? | | 39.2 | " |
| (210) | 88 | 2116 | 4703 | -3.7 | 31.9 | " |
| (211) | 87 | 2078 | 4653 | -4.0 | 31.6 | " |
| | | | 2455 | | | |

| well # | BHT | d | collar | oc/hr | Loc. |
|--------|-----|------|--------|-------|-------------|
| 212 | 85 | 1848 | 4642 | 33.5 | 20-24 |
| 213 | 84 | 1586 | 4583 | 39.9 | " |
| 214 | 88 | 1563 | 4583 | 43.2 | " |
| 215 | 87 | 1610 | 4586 | 40.8 | " |
| 216 | 82 | 1611 | 4587 | 35.1 | " |
| 217 | 85 | 1558 | 4596 | 39.8 | " |
| 218 | 87 | 1670 | 4610 | 39.3 | " |
| 219 | 86 | 1607 | ? | 39.8 | " |
| 220 | 85 | 1504 | 4572 | 41.2 | " |
| 221 | 80 | 1537 | 4592 | 34.4 | " |
| 222 | 85 | 1624 | 4583 | 38.2 | " |
| 223 | 84 | 1344 | 4601 | 44.8 | " |
| 224 | 73 | 1363 | 4605 | 29.4 | " |
| 225 | 94 | 1650 | 4616 | 47.5 | " |
| 226 | 85 | 1075 | 4518 | 57.6 | " |
| 227 | 78 | 1057 | 4517 | 46.6 | " |
| 228 | 84 | 1507 | 4570 | 39.9 | " |
| 229 | 75 | 1200 | 4523 | 36.5 | " |
| 230 | 80 | 1024 | 4519 | 51.6 | " |
| 231 | 73 | 733 | 4521 | 54.7 | " |
| 232 | 75 | 802 | 4480 | 54.5 | " |
| 234 | 105 | 1777 | 4452 | 55.4 | 21-17 |
| 245 | 104 | 1807 | 4681 | 53.5 | 21-22 |
| 246 | 78 | 1411 | 4906 | 34.9 | 21-23 |
| 248 | 82 | 1685 | 4575 | 33.5 | 21-23 |
| 249 | 82 | 1425 | ? | 39.7 | 21-23 |
| 250 | 85 | 1500 | 4650 | 41.3 | " |
| 251 | 95 | 1414 | 4577 | 56.7 | " |
| 252 | 68 | 1128 | 4487 | 27.5 | " |
| 253 | 100 | 1302 | 4206 | 68.6 | " |
| 254 | 80 | 1176 | 4484 | 44.9 | 21-23 sec 4 |
| 255 | 96 | 1828 | 4577 | 44.9 | 21-23 sec 5 |
| 256 | 106 | 1889 | 4490 | 53.1 | " sec 5 |
| 257 | 85 | 1332 | 4502 | 46.5 | " sec 7 |
| 258 | 82 | 1482 | 4485 | 38.1 | " sec 9 |
| 259 | 85 | 1136 | ? | 54.6 | 21-23 |
| 260 | 93 | 1244 | ? | 43.9 | 21-23 |
| 261 | 86 | 1186 | 4444 | 53.8 | " |

4

| well# | BHT | d | Collor | °C/hm | Loc. |
|-------|-----|-----------------|--------|-------|-------|
| 262 | 85 | 1306 | 4454 | 47.5 | 21-23 |
| 263 | 80 | 1117 | 4458 | 48.0 | " |
| 264 | 87 | 1288 | 4419 | 50.9 | " |
| 265 | 102 | 1234 | 4515 | 56.9 | " |
| 266 | 98 | 1164 | 4482 | 73.6 | " |
| " | 99 | 1290 | " | 67.8 | " |
| 267 | 76 | 1391 | 4235 | 32.8 | " |
| 268 | 74 | 1230 | 4412 | 34.1 | " |
| 269 | 75 | 1320 | 4363 | 33.1 | " |
| 351 | 92 | 1994 | 4577 | 37.5 | " |
| 271 | 90 | 1391 | 4411 | 51.1 | " |
| 272 | 73 | 925 | 4347 | 43.4 | " |
| 273 | 82 | 992 | 4666 | 57.0 | " |
| 274 | 75 | 704 | 4611 | 62.1 | " |
| 275 | 78 | 504 | 4332 | 97.6 | " |
| 276 | 78 | 710 | 4338 | 69.3 | " |
| 352 | 80 | 1016 | 4372 | 52.0 | " |
| 277 | 81 | 1128 | 4362 | 48.5 | " |
| 270 | 92 | 970 | 4467 | 77.0 | 21-24 |
| 279 | 80 | 1141 | 4323 | 46.3 | " |
| 280 | 82 | 1122 | 4323 | 50.4 | " |
| 287 | 94 | 1439 | 4697 | 54.5 | 22-21 |
| 288 | 94 | 1492 | ? | 52.5 | 22-23 |
| 353 | 79 | 2402 | 4362 | 21.2 | 23-17 |
| 307 | 95 | 1474 | 4479 | 54.4 | 24-17 |
| 316 | 86 | 2081 | 5142 | 30.7 | 25-18 |
| 319 | 85 | 2375 | 5487 | -9.5 | 25-18 |

~~2402~~

Calc
Tot
2350
= 716 m
(°C)

21 values

Depths 2200-2500

| | Well No | BAT | DEPTH | ELEV COLLAR | °/km | Loc |
|--------|---------|-----|-------|----------------|------|-------|
| ✓ 34.8 | 362 | 94 | 2311 | 7211 | 38.6 | 12-15 |
| ✓ 47.0 | 367 | 115 | 2294 | 6150 | 55.6 | 12-16 |
| ✓ 44.9 | 367 | 115 | 2419 | 6150 | 52.7 | " |
| ✓ 23.7 | 370 | 76 | 2452 | 6855 | 23.0 | 12-16 |
| ✓ 34.3 | 19 | 92 | 2259 | 6520 | 33.1 | 16-24 |
| ✓ 28.8 | 88 | 82 | 2222 | 5070 | 25.4 | 17-26 |
| ✓ 49.6 | 90 | 121 | 2347 | 5013 | 54.4 | 17-26 |
| ✓ 48.9 | 109 | 120 | 2350 | 4933 | 53.5 | 18-24 |
| ✓ 43.2 | 117 | 106 | 2200 | 5975 | 45.6 | 19-18 |
| ✓ 39.0 | 136 | 104 | 2436 | 4892 | 39.6 | 19-23 |
| ✓ 33.9 | 161 | 91 | 2238 | 5185 | 32.6 | 20-21 |
| ✓ 33.4 | 169 | 94 | 2455 | 5085 | 31.7 | 20-22 |
| ✓ 33.5 | 173 | 92 | 2334 | 4986 | 32.0 | 20-22 |
| ✓ 34.3 | 177 | 92 | 2257 | — | 33.1 | 20-23 |
| ✓ 34.1 | 183 | 96 | 2498 | 4828 | 32.8 | 20-23 |
| ✓ 34.6 | 187 | 92 | 2233 | — | 33.5 | 20-23 |
| ✓ 39.9 | 188 | 106 | 2449 | 4828 | 40.9 | 20-23 |
| ✓ 32.9 | 192 | 90 | 2283 | 4715 | 31.1 | " |
| ✓ 35.9 | 196 | 92 | 2369 | — | 35.4 | " |
| ✓ 31.8 | 199 | 88 | 2278 | 4848 | 29.6 | " |
| ✓ 35.1 | 201 | 95 | 2345 | 4855 | 34.2 | " |

Ambient
Change
between
145 + 155

from
45 to
7.2°C

51
10.6°C

> 6000 (1)

| WELL | BHT | DEPTH | LOCATION |
|------|-----|-------|----------|
| 356 | 132 | 6020 | 12-14 |
| 359 | 190 | 8460 | 12-15 |
| 361 | 130 | 7194 | 12-15 |
| 362 | 134 | 7005 | 12-15 |
| 363 | 150 | 6395 | 12-15 |
| 364 | 207 | 12980 | 12-15 |
| " | 304 | 17259 | " |
| 371 | 155 | 9089 | 12-16 |
| 374 | 117 | 6371 | 13-14 |
| " | 131 | 8016 | " |
| " | 148 | 9644 | " |
| 377 | 162 | 9114 | 13-16 |
| 379 | 144 | 8308 | 13-17 |
| 382 | 146 | 7764 | 11-14 |
| 383 | 125 | 6374 | 11-14 |
| 386 | 133 | 7955 | 11-16 |
| 388 | 162 | 8747 | 16-15 |
| 389 | 151 | 8510 | 17-14 |
| 390 | 146 | 8479 | 17-16 |
| 391 | 122 | 7082 | 18-14 |
| 392 | 175 | 9884 | 18-15 |
| 393 | 185 | 11450 | 18-16 |
| " | 212 | 12854 | " |
| 394 | 130 | 6522 | 19-14 |
| 395 | 160 | 8018 | 19-14 |
| " | 168 | 8781 | " |
| 396 | 141 | 8736 | 19-14 |
| " | 137 | 6902 | " |
| 397 | 159 | 10812 | 19-15 |
| 398 | 130 | 6992 | 20-14 |
| " | 125 | 7446 | " |
| 401 | 125 | 6578 | 21-15 |
| " | 150 | 9594 | " |
| " | 154 | 10605 | " |
| 402 | 141 | 9434 | 21-16 |
| 404 | 140 | 8900 | 22-15 |
| 405 | 140 | 8485 | 22-15 |

6000-6999

7000-7999

8000-8999

9000-9999

~~17259~~

>6000 (2)

| WELL | OF | FT | T | R |
|------|-----|-------|----|----|
| 406 | 120 | 6196 | 22 | 15 |
| 408 | 118 | 6061 | 23 | 14 |
| 410 | 145 | 9449 | 23 | 16 |
| 411 | 138 | 8440 | 23 | 16 |
| 412 | 150 | 7282 | 24 | 14 |
| 413 | 162 | 7645 | 24 | 14 |
| 416 | 122 | 6991 | 25 | 14 |
| 417 | 108 | 6469 | 25 | 15 |
| 419 | 134 | 7382 | 25 | 16 |
| 420 | 132 | 6698 | 25 | 16 |
| 422 | 127 | 6699 | 26 | 14 |
| 425 | 109 | 6461 | 26 | 17 |
| 427 | 158 | 8638 | 11 | 19 |
| 428 | 139 | 6559 | 11 | 21 |
| " | 172 | 9812 | " | " |
| 429 | 173 | 7601 | 11 | 21 |
| 430 | 157 | 8402 | 11 | 21 |
| 441 | 138 | 6179 | 11 | 23 |
| 433 | 146 | 6508 | 11 | 23 |
| 442 | 135 | 6510 | 11 | 23 |
| " | 139 | 7368 | " | " |
| 436 | 134 | 6648 | 11 | 23 |
| 437 | 126 | 6461 | 11 | 23 |
| 435 | 124 | 6238 | 11 | 23 |
| 440 | 131 | 6588 | 11 | 23 |
| " | 140 | 7382 | " | " |
| 449 | 130 | 6568 | 11 | 24 |
| 452 | 145 | 7720 | 12 | 20 |
| 456 | 142 | 6524 | 12 | 21 |
| 457 | 125 | 6908 | 12 | 21 |
| 458 | 138 | 6521 | 12 | 21 |
| " | 159 | 8294 | " | " |
| 459 | 135 | 7594 | 12 | 22 |
| 462 | 148 | 7780 | 12 | 22 |
| " | 275 | 15078 | " | " |
| 463 | 142 | 7400 | 12 | 22 |
| 469 | 157 | 8297 | 12 | 25 |

yellow

~~15078~~

>6000 (3)

| WELL | °F | FT | T | R |
|------|-----|--------|----|----|
| 453 | 140 | 7792 | 13 | 20 |
| " | 148 | 8516 | " | |
| 471 | 120 | 6901 | 13 | 20 |
| " | 155 | 7314 | " | |
| 472 | 138 | 6913 | 13 | 20 |
| 473 | 142 | 7439 | 13 | 21 |
| 475 | 230 | 12236 | 13 | 21 |
| 476 | 228 | 12072 | 13 | 22 |
| 477 | 177 | 10358 | 13 | 22 |
| " | 218 | 10783 | " | |
| 478 | 129 | 6601 | 13 | 22 |
| 479 | 139 | | 13 | 22 |
| 480 | 194 | 10534 | 13 | 22 |
| 481 | 126 | 8545 | 13 | 22 |
| " | 238 | 113122 | " | |
| 482 | 224 | 10746 | 13 | 22 |
| 483 | 209 | 8260 | 13 | 22 |
| " | 205 | 10220 | " | |
| 486 | 168 | 8839 | 13 | 25 |
| 488 | 132 | 6137 | 13 | 25 |
| 489 | 146 | 8996 | 14 | 17 |
| 490 | 134 | 7364 | 14 | 19 |
| 492 | 169 | 7900 | 14 | 20 |
| 493 | 134 | 7298 | 14 | 20 |
| 494 | 120 | 6794 | 14 | 20 |
| 497 | 128 | 7331 | 14 | 20 |
| " | 224 | 12431 | " | |
| " | 230 | 12884 | " | |
| 499 | 205 | 11942 | 14 | 22 |
| " | 200 | 12154 | " | |
| 500 | 120 | 6015 | 14 | 22 |
| " | 165 | 9322 | " | |
| 501 | 175 | 9694 | 14 | 22 |
| 503 | 192 | 9728 | 14 | 23 |
| 506 | 164 | 7901 | 14 | 25 |
| 509 | 215 | 10302 | 15 | 21 |
| 511 | 128 | 6231 | 15 | 21 |

13122
11942
12154

>6000 (4)

| WELL | °F | FT | T. R |
|------|-----|-------|-------|
| 512 | 163 | 8584 | 15-22 |
| 513 | 168 | 9601 | 15-22 |
| " | 180 | 10019 | 15-22 |
| 515 | 208 | 9609 | 15-23 |
| 516 | 153 | 8485 | 15-23 |
| 517 | 186 | 8988 | 15-23 |
| 518 | 118 | 6052 | 15-24 |
| " | 190 | 8588 | " |
| 519 | 170 | 8414 | 15-24 |
| 2 | 218 | 10300 | 16-21 |
| " | 182 | 6279 | " |
| 3 | 224 | 9899 | 16-21 |
| 4 | 118 | 6150 | 16-21 |
| " | 207 | 9913 | " |
| 6 | 208 | 10345 | 16-21 |
| 7 | 190 | 9574 | 16-22 |
| 8 | 152 | 7666 | 16-22 |
| " | 176 | 9752 | " |
| " | 190 | 9861 | " |
| 9 | 196 | 10040 | 16-22 |
| 10 | 176 | 8364 | 16-22 |
| 11 | 174 | 8765 | 16-23 |
| 12 | 160 | 8801 | 16-23 |
| 13 | 185 | 7580 | 16-24 |
| 15 | 144 | 6242 | 16-24 |
| 18 | 170 | 6270 | 16-24 |
| 19 | 145 | 6602 | 16-24 |
| 20 | 150 | 6261 | 16-24 |
| 21 | 184 | 6032 | 16-24 |
| 22 | 171 | 8290 | 16-25 |
| 23 | 162 | 6643 | 16-25 |
| 25 | 160 | 6156 | 16-25 |
| 26 | 153 | 6198 | 16-25 |
| 28 | 165 | 6785 | 16-25 |
| 339 | 160 | 6456 | 16-25 |
| 29 | 145 | 6530 | 16-25 |
| 30 | 146 | 6497 | 16-25 |

End of small book

10345

>6000

(5)

| Well | °F | Fr. | T | R |
|------|-----|-------|----|----|
| 42 | 118 | 6094 | 17 | 21 |
| " | 181 | 9803 | " | " |
| 43 | 192 | 9851 | 17 | 21 |
| " | 117 | 6036 | " | " |
| 44 | 135 | 7700 | 17 | 21 |
| 45 | 179 | 7643 | 17 | 22 |
| 47 | 183 | 6910 | 17 | 23 |
| 48 | 146 | 6411 | 17 | 23 |
| 49 | 190 | 7024 | 17 | 23 |
| 50 | 160 | 6439 | 17 | 23 |
| 52 | 159 | 470 | 17 | 23 |
| 55 | 114 | 6271 | 17 | 24 |
| 58 | 151 | 6543 | 17 | 24 |
| 60 | 140 | 6323 | 17 | 24 |
| 62 | 148 | 6224 | 17 | 24 |
| 65 | 150 | 6006 | 17 | 24 |
| " | 170 | 6251 | " | " |
| 93 | 173 | 9869 | 18 | 20 |
| " | 176 | 10787 | " | " |
| 96 | 183 | 7023 | 18 | 22 |
| 100 | 147 | 6010 | 18 | 23 |
| 101 | 167 | 7056 | 18 | 23 |
| 118 | 152 | 6711 | 19 | 21 |
| 125 | 142 | 6800 | 19 | 21 |
| 127 | 165 | 6247 | 19 | 22 |
| 234 | 190 | 11885 | 21 | 17 |
| " | 161 | 8468 | " | " |
| " | 146 | 7559 | " | " |
| 235 | 149 | 7515 | 21 | 18 |
| 238 | 151 | 7788 | 21 | 18 |
| 241 | 157 | 8496 | 21 | 19 |
| " | 159 | 8928 | " | " |
| 242 | 144 | 6114 | 21 | 20 |
| 244 | 158 | 7416 | 21 | 21 |
| 282 | 122 | 6754 | 22 | 16 |
| 283 | 152 | 9512 | 22 | 16 |
| 284 | 170 | 10172 | 22 | 17 |
| " | 175 | 10291 | " | " |

~~11885~~

>6000 (6)

| WELL | °F | FT. | T | R |
|------|-----|-------|----|-----|
| 286 | 236 | 12123 | 22 | -20 |
| " | 245 | 14992 | " | |
| 289 | 138 | 9056 | 23 | -17 |
| 290 | 156 | 9653 | 23 | -17 |
| 291 | 146 | 9080 | 23 | -17 |
| 292 | 142 | 8902 | 23 | -17 |
| 293 | 138 | 8908 | 23 | -17 |
| 354 | 142 | 8924 | 23 | -17 |
| 294 | 141 | 8828 | 23 | -17 |
| 295 | 130 | 8679 | 23 | -17 |
| 296 | 148 | 8842 | 23 | -17 |
| 297 | 164 | 10330 | 23 | -18 |
| 299 | 186 | 12074 | 23 | -19 |
| 301 | 135 | 6138 | 23 | -19 |
| 304 | 138 | 9262 | 23 | -21 |
| 305 | 130 | 8829 | 23 | -22 |
| " | 179 | 11735 | " | |
| 306 | 154 | 8647 | 23 | -24 |
| " | 226 | 13580 | " | |
| 307 | 143 | 9125 | 24 | -17 |
| 308 | 106 | 646 | 24 | -19 |
| " | 119 | 7808 | " | |
| 310 | 112 | 7197 | 24 | -20 |
| " | 119 | 7532 | " | |
| 313 | 200 | 13257 | 24 | -23 |
| " | 288 | 14281 | " | |
| 316 | 116 | 6561 | 25 | -18 |
| " | 120 | 7850 | " | |
| 317 | 148 | 6912 | 25 | -18 |
| 318 | 122 | 6775 | 25 | -18 |
| 319 | 125 | 8126 | 25 | -18 |
| 320 | 145 | 8867 | 25 | -19 |
| 321 | 115 | 7724 | 25 | -19 |
| 322 | 131 | 6654 | 25 | -19 |
| " | 140 | 7238 | " | |
| " | 121 | 7629 | " | |
| 323 | 118 | 6493 | 25 | -23 |

14992

>6000 (7)

| Well | °F | Ft | T R |
|------|-----|-------|-------|
| 324 | 114 | 7691 | 26-18 |
| 325 | 149 | 7282 | 26-18 |
| 326 | 124 | 8105 | 26-19 |
| " | 130 | 8242 | " |
| 327 | 100 | 7777 | 26-19 |
| " | 112 | 6370 | " |
| 328 | 121 | 6713 | 26-19 |
| 329 | 131 | 7792 | 26-20 |
| 330 | 112 | 8070 | 26-20 |
| 331 | 118 | 7888 | 26-20 |
| " | 120 | 8134 | " |
| " | 113 | 7498 | " |
| 332 | 121 | 7444 | 26-20 |
| " | 126 | 8043 | " |
| 333 | 136 | 8592 | 26-20 |
| 334 | 115 | 6047 | 26-20 |
| 335 | 113 | 7289 | 26-20 |
| " | 140 | 7348 | " |
| " | 148 | 8004 | " |
| 336 | 170 | 11204 | 26-22 |
| 337 | 140 | 10289 | 26-22 |
| " | 160 | 10703 | " |
| " | 146 | 10303 | " |
| " | 125 | 8105 | " |
| 338 | 115 | 7015 | 26-25 |
| " | 168 | 12719 | " |
| " | 180 | 14558 | " |
| " | 205 | 15876 | " |

~~15876~~

2500-5000

SMALL BOOK

①

T. R

| WELL | °F | DEPTH | °C/m | LOC | |
|--------|-----|-------|------|-------|-------|
| 355 | 126 | 4494 | 32.9 | 12-14 | |
| 359 | 117 | 4503 | 29.1 | 12-15 | |
| 366 | 87 | 3040 | 25.2 | 12-16 | |
| 368 | 110 | 3275 | 36.2 | 12-16 | |
| 369 | 92 | 3535 | 24.2 | 12-16 | |
| 370 | 86 | 2950 | 25.3 | 12-16 | |
| " | 112 | 3052 | 40.0 | " | |
| 371 | 112 | 2986 | 40.9 | 12-16 | |
| " | 116 | 3097 | 41.8 | " | |
| " | 118 | 3258 | 40.8 | " | |
| 373 | 102 | 4530 | 22.9 | 12-16 | |
| " | 110 | 4984 | 23.8 | 12-16 | |
| 375 | 92 | 2683 | 31.9 | 13-14 | |
| 376 | 102 | 4753 | 21.9 | 13-16 | |
| 377 | 132 | 4982 | 31.8 | 13-16 | |
| 378 | 125 | 3155 | 46.2 | 13-16 | |
| " | 130 | 4685 | 33.1 | " | |
| 380 | 105 | 4840 | 22.6 | 13-17 | |
| 381 | 119 | 4504 | 29.9 | 11-14 | |
| 384 | 116 | 4859 | 26.6 | 11-15 | |
| 388 | 100 | 3777 | 23.6 | 16-15 | |
| " | 106 | 4334 | 23.1 | " | |
| 396 | 110 | 3740 | 28.8 | 19-14 | |
| 397 | 112 | 4600 | 24.2 | 19-15 | |
| 407 | 86 | 3151 | 20.2 | 23-14 | |
| 414 | 95 | 4616 | 17.4 | 24-16 | |
| 418 | 101 | 4880 | 18.7 | 25-15 | |
| 419 | 114 | 4538 | 25.3 | 25-16 | |
| 422 | 117 | 3000 | 40.1 | 26-14 | |
| Carbon | 424 | 102 | 4990 | 18.6 | 26-16 |
| Umtah | 442 | 104 | 4175 | 25.8 | 11-23 |
| 445 | 97 | 2619 | 36.2 | 11-23 | |
| 440 | 112 | 4813 | 25.4 | 11-23 | |
| 447 | 116 | 4732 | 27.3 | 11-24 | |
| 449 | 100 | 2520 | 39.8 | 11-24 | |
| 450 | 110 | 4494 | 26.4 | 11-24 | |
| 451 | 95 | 3358 | 27.1 | 11-24 | |
| 452 | 148 | 4570 | 41.1 | 12-20 | |

2501-2999

3000-3499

3500-3999

4000-4499

4990

| | WELL | °F | FT | °C/km | Loc | |
|-----|------|-----|------|-------|-------|-------------------------------|
| DUP | 152 | 145 | 4406 | 41.4 | 12-20 | |
| | 464 | 110 | 3329 | 35.6 | 12-24 | |
| | 466 | 90 | 2830 | 29.0 | 12-24 | |
| | " | 107 | 3828 | 29.5 | " | |
| | 468 | 112 | 3302 | 37.0 | 12-24 | |
| | 469 | 108 | 4317 | 26.6 | 12-25 | |
| | 470 | 105 | 4708 | 23.2 | 12-25 | |
| | 473 | 98 | 3927 | 24.6 | 13-21 | |
| | 474 | 112 | 3945 | 31.0 | 13-21 | |
| | 485 | 115 | 4414 | 28.9 | 13-23 | |
| | 491 | 100 | 4997 | 20.1 | 14-19 | |
| | 495 | 111 | 4652 | 25.9 | 14-20 | |
| | 496 | 114 | 4597 | 27.4 | 14-20 | |
| | 498 | 100 | 4747 | 21.1 | 14-20 | |
| | 500 | 105 | 3931 | 27.8 | 14-22 | |
| | " | 120 | 4372 | 31.3 | " | |
| | 505 | 108 | 4517 | 25.4 | 14-24 | |
| | 507 | 103 | 3497 | 30.2 | 14-25 | |
| | " | 115 | 4945 | 25.8 | " | |
| | 508 | 119 | 4605 | 29.3 | 14-25 | |
| | 512 | 123 | 4829 | 27.2 | 15-22 | |
| | 516 | 104 | 4640 | 20.8 | 15-23 | |
| | 518 | 103 | 4802 | 19.7 | 15-24 | |
| | 1 | 100 | 4102 | 21.8 | 15-25 | end well book miss located |
| | 7 | 120 | 4899 | 25.7 | 16-22 | |
| | 10 | 118 | 3867 | 31.6 | 16-22 | |
| | 11 | 116 | 4693 | 25.2 | 16-23 | |
| | 14 | 106 | 3486 | 28.8 | 16-24 | |
| | 28 | 112 | 3213 | 34.3 | 16-25 | |
| | 34 | 153 | 4953 | 37.5 | 16-25 | |
| | 35 | 158 | 4937 | 39.5 | 16-25 | |
| | 36 | 122 | 4048 | 32.0 | 16-25 | |
| | 37 | 126 | 4692 | 29.1 | 16-25 | |
| | 39 | 133 | 4760 | 31.4 | 16-26 | |
| | 40 | 142 | 4347 | 38.2 | 16-26 | |
| | 41 | 145 | 4178 | 41.0 | 16-26 | |
| | 45 | 95 | 3435 | 23.3 | 17-22 | |
| | 46 | 110 | 3368 | 31.9 | 17-22 | |

4943
4997

ECU
2500-5000

| WELL | °F | FT | °/hr | LOC |
|------|-----|-----------------|------|-------|
| 49 | 105 | 3607 | 37.5 | 17-23 |
| 68 | 175 | 4395 | 51.4 | 17-24 |
| 11 | 148 | 4402 | 40.2 | " |
| 70 | 125 | 4117 | 32.8 | " |
| 71 | 169 | 4607 | 46.7 | 17-25 |
| 72 | 128 | 3804 | 36.9 | 17-25 |
| 73 | 121 | 3896 | 32.7 | 17-25 |
| 74 | 117 | 3997 | 40.1 | 17-25 |
| 11 | 118 | 3735 | 32.7 | " |
| 75 | 120 | 3956 | 31.8 | 17-25 |
| 76 | 125 | 3811 | 35.4 | 17-25 |
| 77 | 121 | 3682 | 34.7 | 17-25 |
| 78 | 122 | 4694 | 31.6 | 17-25 |
| 79 | 95 | 3282 | 24.4 | 17-25 |
| 81 | 118 | 2818 | 43.3 | 17-25 |
| 82 | 109 | 2960 | 35.7 | 17-25 |
| 83 | 152 | 4275 | 43.1 | 17-25 |
| 84 | 116 | 3890 | 30.5 | 17-26 |
| 85 | 105 | 3633 | 27.1 | 17-26 |
| 86 | 116 | 3600 | 32.9 | 17-26 |
| 87 | 100 | 3281 | 27.2 | 17-26 |
| 88 | 86 | 2736 | 23.3 | 17-26 |
| 89 | 101 | 2528 | 36.0 | 17-26 |
| 92 | 105 | 3137 | 31.4 | 17-26 |
| 93 | 110 | 4713 | 22.8 | 18-20 |
| 105 | 108 | 2767 | 37.5 | 18-24 |
| 106 | 135 | 4604 | 33.3 | 18-24 |
| 107 | 129 | 4773 | 29.8 | 18-24 |
| 108 | 128 | 4409 | 31.8 | 18-24 |
| 110 | 108 | 3282 | 31.7 | 18-24 |
| 111 | 106 | 2884 | 34.8 | 18-24 |
| 114 | 95 | 2799 | 28.7 | 18-25 |
| 116 | 98 | 2620 | 32.7 | 18-26 |
| 119 | 117 | 4745 | 25.4 | 19-21 |
| 120 | 148 | 3606 | 49.0 | 19-21 |
| 11 | 152 | 3600 | 51.1 | " |
| 123 | 135 | 4768 | 32.1 | 19-21 |
| 124 | 140 | 3944 | 41.1 | 19-21 |

} av 150°F 3603 50.1 19-21
4773

ECU

④

2500 - 5000

| WELL | °F | FT | °C/km | LOC |
|------|-----|-----------------|-------|-------|
| 125 | 89 | 2754 | 25.1 | 19-21 |
| 128 | 120 | 4392 | 28.6 | 19-22 |
| 130 | 138 | 4679 | 33.9 | 19-23 |
| 131 | 125 | 4417 | 30.5 | 19-23 |
| 132 | 117 | 3793 | 31.7 | 19-23 |
| 133 | 110 | 3550 | 30.3 | 19-23 |
| 144 | 116 | 3318 | 35.7 | 19-23 |
| 134 | 107 | 3442 | 29.6 | 19-23 |
| 135 | 115 | 3203 | 36.4 | 19-23 |
| 137 | 122 | 3363 | 38.5 | 19-23 |
| 342 | 98 | 2797 | 30.6 | 19-23 |
| 138 | 96 | 2604 | 31.5 | 19-24 |
| 142 | 147 | 4084 | 42.8 | 19-25 |
| 343 | 127 | 3501 | 39.6 | 20-21 |
| 145 | 118 | 3670 | 33.3 | 20-21 |
| 146 | 128 | 3208 | 43.7 | 20-21 |
| 147 | 133 | 3800 | 39.3 | 20-21 |
| 148 | 125 | 3937 | 34.3 | 20-21 |
| 149 | 124 | 4191 | 31.7 | 20-21 |
| 150 | 120 | 4323 | 29.1 | 20-21 |
| 151 | 124 | 3592 | 37.0 | 20-21 |
| 152 | 145 | 4062 | 42.2 | 20-21 |
| 344 | 110 | 3290 | 32.7 | 20-21 |
| 153 | 118 | 3834 | 31.4 | 20-21 |
| 154 | 110 | 3506 | 30.7 | 20-21 |
| 155 | 117 | 3319 | 36.2 | 20-21 |
| 156 | 96 | 2988 | 27.4 | 20-21 |
| 157 | 105 | 2540 | 38.7 | 20-21 |
| 345 | 124 | 3230 | 41.2 | 20-21 |
| 158 | 121 | 3230 | 39.5 | 20-21 |
| 159 | 108 | 2922 | 35.6 | 20-21 |
| 160 | 130 | 2549 | 56.5 | 20-21 |
| 346 | 100 | 2781 | 32.1 | 20-21 |
| 162 | 113 | 2782 | 40.6 | 20-21 |
| 163 | 109 | 2761 | 38.3 | 20-21 |
| 164 | 124 | 3006 | 44.3 | 20-22 |
| 165 | 105 | 3231 | 30.5 | 20-22 |
| 166 | 108 | 3432 | 30.3 | 20-22 |

~~4679~~

ECU
2500 - 5000

5

| Well | °F | FT | %m | Loc |
|------|-----|------|------|-------------|
| 167 | 99 | 2896 | 30.2 | 20 - 22 |
| 168 | 90 | 2528 | 28.1 | 20 - 22 |
| 170 | 98 | 2504 | 34.2 | 20 - 22 |
| 171 | 163 | 2844 | 71.8 | 20 - 22 |
| 172 | 108 | 2522 | 41.2 | 20 - 22 |
| 347 | 119 | 2883 | 43.0 | 20 - 22 |
| 174 | 116 | 2747 | 43.1 | 20 - 22 |
| 175 | 93 | 2602 | 29.4 | 20 - 22 |
| 348 | 110 | 2736 | 39.3 | 20 - 22 |
| 176 | 112 | 2694 | 41.3 | 20 - 23 |
| 180 | 100 | 2805 | 31.8 | 20 - 23 |
| 181 | 120 | 2530 | 49.7 | 20 - 23 |
| " | 128 | 3342 | 42.0 | " |
| 198 | 112 | 2599 | 42.9 | 20 - 23 |
| 200 | 92 | 2509 | 29.8 | 20 - 23 |
| 233 | 121 | 4983 | 25.6 | 21 - 16 |
| 237 | 105 | 3028 | 32.5 | 21 - 18 |
| " | 110 | 3587 | 30.0 | " |
| 239 | 112 | 4519 | 24.6 | 21 - 19 |
| 240 | 106 | 3490 | 28.7 | 21 - 19 |
| " | 108 | 3690 | 28.2 | " |
| 242 | 108 | 4626 | 22.5 | 21 - 20 |
| 285 | 114 | 2921 | 39.3 | 22 - 19 |
| 299 | 117 | 4378 | 27.5 | 23 - 19 |
| 300 | 76 | 2653 | 17.2 | 23 - 19 |
| 302 | 100 | 2779 | 32.1 | 23 - 20 |
| 303 | 97 | 3972 | 21.1 | 23 - 21 |
| 310 | 96 | 2938 | 27.9 | 24 - 20 |
| 311 | 90 | 4785 | 14.9 | 24 - 21 |
| " | 94 | 4965 | 15.8 | " |
| 314 | 86 | 3830 | 16.7 | 25 - 17 1/2 |
| 315 | 137 | 4191 | 37.4 | 25 - 18 |
| 316 | 102 | 4059 | 22.9 | 25 - 18 |
| 318 | 102 | 4078 | 22.8 | 25 - 18 |
| " | 130 | 4916 | 29.3 | " |
| 319 | 103 | 4209 | 22.5 | 25 - 18 |
| 326 | 104 | 4436 | 21.8 | 26 - 19 |

~~4983~~
4963

ECU
2500 - 5000.

6

| WELL | OF | FT. | °/km | LOC |
|------|-----|-----------------|------|-------|
| 330 | 80 | 3811 | 13.9 | 26-20 |
| 332 | 95 | 2716 | 29.5 | 26-20 |
| " | 115 | 3375 | 34.6 | " |
| 335 | 113 | 3700 | 30.5 | 26-20 |

3811

using Max depth on DST's

all perf in WSTC & DRCK

SWPI well 54 some question on position

Use 5480' 200°F (?) 49.6°C/lm
in Desert Creek fm (Pennsylvanian)

ambient 51°F.

← can't be
is younger than
WSTC
& GRV

NE NE SW sec 17 T15S-R19E

PI-145

21S-18E

SW NE SW sec 12 T21S-R18E

Producing Navajo
bottom Paradox at 7615

DST 551 NVJO 5140-5203 142°F 31.8°C/lm
water in NVJO

DST 563 WNGT 5934-5989 140°F 27.0

perf NVJO 5140-5203
WNGT 5934-5989
TOP KROT GUESS
P.

PI-104 ✓ X

SE NWNW sec 2 T16S-R24E

producing DKOT
bottom MRSN 7250

DST 3220-3250 Castlegate 180°F 72.3°C/lm
(Cretaceous)

perf DKOT 7015-7034
COMN 7016-7062
TOP DKOT
GUESS: 6940 depth

PI-97 ✓ X

NE SE SW sec 27, T13S-R21E

producing DKOT
bottom 553 ENRD at 10605

DST 2465-2550 in watch 103°F 41.4°C/lm

DST 9613-9710 in Mancos 223°C 33.4

overlap DKOT note: P higher above Mancos
than below.

No perf
TOP DKOT
GUESS: 9700'

GRAND CO. DEEPEST BHTs / TSHP

3

| | LOCATION | | | BHT | DEPTH | ELEVATIONS | | GRAD | No. WELLS TSHP | | | |
|--|----------|-----|--------------|-----|-------|------------|-----|------|-------------------|-----|------|---|
| | S | T | R | °F | FT | SURFACE | BHT | °/km | | | | |
| | 23 | 18S | 20E | 176 | 10787 | 8952 | | 21.1 | 2 | | 19.8 | 4 |
| | | 18 | 21 | | | | | | 0 | | - | |
| | 15 | 18 | 22 | 183 | 7023 | 6065 | | 34.3 | 5 | ✓ | 31.1 | 5 |
| | 4 | 18 | 23 | 167 | 7056 | 6507 | | 30.6 | 4 | ✓ | 26.7 | 5 |
| | 5 | 18 | 24 | 129 | 4773 | 5058 | | 29.8 | 8 | ⊙ | - | |
| | 23 | 18 | 25 | 95 | 2799 | 4713 | | 28.7 | 5 | ⊗ ✓ | - | |
| | 18 | 18 | 26 | 98 | 2620 | 4873 | | 32.7 | 1 | ⊗ ✓ | - | |
| | 11 | 19 | 14 | 168 | 8781 | 5015 | | 24.3 | 3 | ✓ | 22.5 | 5 |
| | 14 | 19 | 15 | 159 | 10814 | 6075 | | 18.2 | 1 | ✓ | 18.2 | 1 |
| | | 19 | 16 | | | | | | 0 | | - | |
| | | 19 | 17 | | | | | | 0 | | - | |
| | 36 | 19 | 18 | 106 | 6427 | 5975 | | 15.6 | 1 | ✓ | 15.6 | 1 |
| | | 19 | 19 | | | | | | 0 | | - | |
| | | 19 | 20 | | | | | | 0 | | - | |
| | 9 | 19 | 21 | 142 | 6800 | 7473 | | 24.4 | 8 | ✓ | 30.0 | 4 |
| | 6 | 19 | 22 | 165 | 6247 | 6125 | | 33.3 | 4 | ✓ | 31.7 | 3 |
| | 7 | 19 | 23 | 138 | 4679 | 5275 | | 33.9 | 10 | ⊙ ✓ | - | |
| | 14 | 19 | 24 | 96 | 2604 | 4674 | | 31.5 | 4 | ⊗ | - | |
| | 4 | 19 | 25 | 147 | 4084 | 5603 | | 42.8 | 2 | ⊙ ✓ | - | |
| | | 19 | 26 | | | | | | 0 | | - | |
| | 33 | 20 | 14 | 125 | 7446 | ? | | 18.1 | 1 | ✓ | 19.4 | 2 |
| | | 20 | 15 | | | | | | 0 | | - | |
| | 17 | 20 | 16 | 118 | 2640 | 4197 | | 46.3 | 1 | ⊗ ✓ | ? | 0 |
| | | 20 | 17 TO 20E | | | | | | 0 | | - | |
| | 4 | 20 | 21 | 120 | 4323 | | | 29.1 | 23 | ⊙ ✓ | - | |
| | 14 | 20 | 22 | 108 | 3432 | 4863 | | 30.3 | 14 | ⊙ ✓ | - | |
| | 5 | 20 | 23 | 100 | 2805 | 4851 | | 31.8 | 27 | ⊗ ✓ | - | |
| | 6 | 20 | 24 | 88 | 2116 | 4703 | | 31.9 | 31 | ⊗ ✓ | - | |
| | 5 | 21 | 14 | 120 | 5992 | 4577 | | 21.0 | 1 | ✓ | 21.0 | 1 |
| | 24 | 21 | 15 | 154 | 10605 | 4224 | | 17.7 | 1 | ✓ | 19.0 | 3 |
| | 33 | 21 | 16 | 141 | 9434 | 4282 | | 17.4 | 2 | ✓ | 18.6 | 2 |
| | 26 | 21 | 17 | 190 | 11885 | 4452 | | 21.3 | 1 | ✓ | 21.3 | 1 |
| | 23 | 21 | 18 | 151 | 7788 | 4924 | | 23.4 | 4 | ✓ | 26.0 | 6 |
| | 17 | 21 | 19 | 159 | 8928 | 5169 | | 22.0 | 3 | ✓ | 22.4 | 2 |
| | 18 | 21 | 20 | 144 | 6114 | 5187 | | 27.7 | 2 | ✓ | 23.9 | 2 |
| | 11 | 21 | 21 | 158 | 7416 | 4963 | | 26.3 | 1 | ✓ | 26.3 | 1 |

E. CENT. U. - DEEPEST WELL / TSHP

(4)

| LOCATION | | | BHT | DEPTH | ELEVATION | | GRAD | No. WELLS / TSHP | | | | |
|----------|-----|-----------|-----|-------|-----------|-----|------|------------------|---|---|------|----|
| S | T | R | °F | FT. | SURFACE | BHT | °/Km | | | | | |
| 2 | 21S | 22E | 104 | 1807 | 4681 | | 53.5 | 1 | ⊗ | ✓ | - | |
| 19 | 21 | 23 | 92 | 1994 | 4577 | | 37.5 | 32 | ⊗ | ✓ | - | |
| 30 | 21 | 24 | 80 | 1141 | 4323 | | 46.3 | 4 | ⊗ | ✓ | - | |
| 9 | 22 | 15 | 140 | 8900 | 4441 | | 18.2 | 3 | | ✓ | 19.2 | 4 |
| 25 | 22 | 16 | 152 | 9512 | 4132 | | 19.4 | 2 | | | 19.3 | 2 |
| 34 | 22 | 17 | 175 | 10291 | 4220 | | 22.0 | 1 | | | 21.2 | 4 |
| | 22 | 18 | | | | | | 0 | | | - | |
| 22 | 22 | 19 | 114 | 2921 | 4685 | | 39.3 | 1 | ⊗ | ✓ | - | |
| 17 | 22 | 20 | 245 | 14992 | 4780 | | 23.6 | 1 | | ✓ | 25.7 | 2 |
| 10 | 22 | 21 | 94 | 1439 | 4697 | | 54.5 | 1 | ⊗ | ✓ | - | |
| | 22 | 22 TO 26E | | | | | | 0 | | | - | |
| 19 | 23 | 14 | 118 | 6061 | 4378 | | 20.1 | 2 | | | 21.9 | 2 |
| 21 | 23 | 15 | 116 | 5636 | 4687 | | 21.0 | 1 | | ✓ | 21.8 | 1 |
| 3 | 23 | 16 | 145 | 9449 | 4038 | | 18.1 | 2 | | | 19.5 | 3 |
| 11 | 23 | 17 | 156 | 9653 | 4298 | | 19.8 | 9 | | | 19.1 | 12 |
| 21 | 23 | 18 | 164 | 10330 | 4525 | | 19.9 | 2 | | ✓ | 22.4 | 3 |
| 15 | 23 | 19 | 186 | 12074 | 4589 | | 20.4 | 3 | | ✓ | 22.6 | 2 |
| 6 | 23 | 20 | 100 | 2779 | 4834 | | 32.1 | 1 | ⊗ | | - | |
| 5 | 23 | 21 | 138 | 9262 | 4707 | | 17.1 | 2 | | ✓ | 17.1 | 1 |
| 9 | 23 | 22 | 179 | 11735 | 4886 | | 19.9 | 1 | | ✓ | 18.9 | 2 |
| | 23 | 23 | | | | | | 0 | | | - | |
| 31 | 23 | 24 | 226 | 13580 | 4307 | | 23.5 | 1 | | ✓ | 22.6 | 2 |
| 21 | 24 | 14 | 162 | 7645 | 4320 | | 26.5 | 2 | | | 25.9 | 3 |
| | 24 | 15 | | | | | | 0 | | | - | |
| 19 | 24 | 16 | 130 | 8648 | 4774 | | 16.7 | 2 | | | 17.6 | 2 |
| 1 | 24 | 17 | 143 | 9125 | 4479 | | 18.4 | 3 | | ✓ | 29.1 | 2 |
| | 24 | 18 | | | | | | 0 | | | - | |
| 22 | 24 | 19 | 119 | 7808 | 4777 | | 15.9 | 1 | | ✓ | 15.7 | 2 |
| 36 | 24 | 20 | 119 | 7532 | 4448 | | 16.5 | 2 | | ✓ | 15.5 | 3 |
| 7 | 24 | 21 | 94 | 4965 | 4855 | | 15.8 | 1 | ⊙ | ✓ | - | |
| | 24 | 22 | | | | | | 0 | | | - | |
| 13 | 24 | 23 | 288 | 14281 | 4569 | | 30.2 | 1 | | ✓ | 25.4 | 2 |
| 22 | 25 | 14 | 122 | 6991 | 4775 | | 18.5 | 1 | | ✓ | 18.5 | 1 |
| 15 | 25 | 15 | 108 | 6469 | ? | | 16.1 | 2 | | ✓ | 18.9 | 2 |
| 10 | 25 | 16 | 134 | 7382 | 4751 | | 20.5 | 2 | | ✓ | 20.4 | 3 |
| | 25 | 17 | | | | | | 0 | | | - | |

E. CENT. UTAH - DEEPEST BHT/TSHP (5)

| LOCATION | | | BHT | DEPTH | ELEVATION | | GRAD. | No WELLS | | | |
|----------|-----|------------|-----|-------|-----------|-----|-------|----------|-----|------|----|
| S | T | R | °F | FT. | SURFACE | BHT | °C/km | TSHP | | | |
| 35 | 25S | 18E | 125 | 8126 | 5488 | | 16.6 | 5 | ✓ | 18.7 | 6 |
| 26 | 25 | 19 | 145 | 8867 | 5454 | | 19.3 | 3 | ✓ | 19.1 | 5 |
| | 25 | 20 TO 22E | | | | | | 0 | ✓ | — | |
| 16 | 25 | 23 | 118 | 6493 | 5122 | | 18.8 | 1 | ✓ | 18.8 | 1 |
| 26 | 26 | 14 | 127 | 6699 | 5645 | | 20.7 | 3 | | 23.4 | 3 |
| | 26 | 15 | | | | | | 0 | | — | |
| 31 | 26 | 16 | 102 | 4990 | 5157 | | 18.6 | 1 | ✓ ⊙ | 1— | |
| 5 | 26 | 17 | 109 | 6461 | ? | | 16.4 | 1 | ✓ | 16.4 | 1 |
| 4 | 26 | 18 | 114 | 7691 | 5302 | | 14.9 | 2 | ✓ | 19.7 | 2 |
| 14 | 26 | 19 | 130 | 8242 | ? | | 17.5 | 3 | ✓ | 17.7 | 5 |
| 29 | 26 | 20 | 136 | 8592 | 5934 | | 18.0 | 7 | ✓ | 17.9 | 13 |
| | 26 | 21 | | | | | | 0 | ✓ | — | |
| 1 | 26 | 22 | 170 | 11204 | 5300 | | 19.4 | 2 | ✓ | 17.4 | 5 |
| | 26 | 23 AND 24E | | | | | | 0 | | — | |
| 12 | 26 | 25 | 205 | 15876 | 8594 | | 17.7 | 1 | | 17.1 | 4 |

5000-5250
 5250-5500
 5500-5750
 5750-6000

VARIANCE FROM MEAN
 OF 23.8°C/ftm

PROJ BHT column 8
 ON 24.0°C/ftm +9, +10

Ambient
 this page
 7.2

E. CENT. LIT. - 5000-6000
 (YELLOW OUTLINE)

T- PROJ. BY GRAD.
 TO 5500' (1676 m)

EFFICIENCY LINE No. 2636



| | 1 LOC | 2 WELL NO. | 3 BHT | 4 DEPTH | 5 ELEV. COLLAR | 6 °/ftm | 7 °C | 8 Proj. meters UP-DOWN | 9 ΔT | 10 °C |
|------|------------------|----------------|----------------|-----------------|-----------------|-----------------|-----------------|------------------------|-------|-------|
| 1 | 11-19 | 426 | 123 | 5363 | 5795 +2 | 26.5 | 51.6 | 41.8+ | 1.00+ | 51.6 |
| 2 | 11-21 | 430 | 125 | 5898 | 5726 +9 | 24.7 | 48.4 | 121.3- | 2.9- | 48.8 |
| 3 | " | 431 | 107 | 5016 | 5766 -3 | 22.5 | 44.9 | 147.5+ | 3.5+ | 45.2 |
| 4 | 11-22 | 432 | 125 | 5348 | 5358 +3 | 27.3 | 53.0 | 46.3+ | 1.1+ | 52.8 |
| 5 | 11-23 | 434 | 137 | 5670 | 5992 +5 | 29.6 | 56.8 | ✓ | | |
| 6 | " | 443 | 128 | 5895 | 6000 +1 | 25.7 | 50.3 | ✓ | | |
| 7 | " | 444 | 130 | 5856 | 5617 +2 | 26.5 | 51.6 | ✓ | | |
| 8 | " | 438 | 126 | 5263 | 5964 +1 | 28.1 | 54.3 | ✓ | | |
| 9 | " | " | 143 | 5950 | 5964 +6 | 30.0 | 57.5 | ✓ | | |
| 10 | " | 439 | 123 | 5275 | 6094 +3 | 27.0 | 52.4 | ✓ | | |
| 11 | " | 445 | 127 | 5851 | 5861 +1 | 25.5 | 49.9 | ✓ | | |
| 12 | 11-24 | 446 | 128 | 5943 | 5208 +1 | 25.5 | 49.9 | ✓ | | |
| 13 | " | 447 | 130 | 5839 | 5400 +1 | 26.5 | 51.6 | ✓ | | |
| 14 | " | 450 | 122 | 5580 | 5579 +1 | 25.2 | 49.4 | ✓ | | |
| 15 | " | 448 | 128 | 5598 | 5620 +3 | 27.0 | 52.4 | ✓ | | |
| 16 | 12-20 | 452 | 120 | 5596 | 5648 +6 | 24.4 | 48.1 | ✓ | | |
| 17 | 12-21 | 454 | 134 | 5831 | 5945 +1 | 27.8 | 53.8 | ✓ | | |
| 18 | " | 455 | 126 | 5306 | 6027 +1 | 27.8 | 53.8 | ✓ | | |
| 19 | " | " | 130 | 5547 | 6027 +1 | 27.9 | 54.0 | ✓ | | |
| 20 | " | 457 | 123 | 5324 | 6185 +2 | 26.7 | 51.9 | ✓ | | |
| 21 | 12-22 | 460 | 130 | 5781 | - | 26.8 | 52.1 | ✓ | | |
| 22 | " | 461 | 140 | 5820 | 6036 +6 | 29.8 | 57.1 | ✓ | | |
| 23 | 12-24 | 465 | 122 | 5199 | 5900 +3 | 27.0 | 52.4 | ✓ | | |
| 24 | " | " | 126 | 5692 | " | 25.9 | 50.6 | ✓ | | |
| 25 | " | 467 | 140 | 5270 | 6208 +1 | 32.9 | 62.3 | ✓ | | |
| ? 26 | 13-20 | 453 | 110 | 5196 | 6163 | 33.3 | 63.0 | | | |
| ? 27 | " | " | 123 | 5984 | 6163 | 23.8 | 47.1 | ✓ | | |
| 28 | 13-23 | 484 | 115 | 5835 | - | 21.9 | 43.9 | ✓ | | |
| 29 | 13-25 | 486 | 111 | 5005 | 7290 +2 | 24.0 | 47.4 | 150.9+ | 3.6+ | 47.5 |
| 30 | " | 487 | 124 | 5797 | 7523 +1 | 24.8 | 48.8 | ✓ | | |
| 31 | 14-24 | 504 | 128 | 5149 | 6374 +5 | 29.4 | 56.5 | ✓ | | |

~~57.84~~

ECU
5000' - 6000'

(2)

PROJ. BY GRAD.
TO 5500'

EFFICIENCY LINE No. 2636



| | 1 LOC | 2 WELL | 3 BHT | 4 DEPTH | 5 COLLAR ELEV. | 6 °C/m | 7 °C | 8 | 9 | °C |
|------|------------------|--------|---------------|-----------------|-----------------|-----------------|----------------------------------|----------|------|-----------------|
| 1 | 14-24 | 505 | 132 | 5899 | 7306 | 26.9 | 52.3 | ✓ 121.6- | 2.9- | 52.6 |
| 2 | 15-21 | 510 | 116 | 5694 | 7414 | 20.8 | 45.5 | ✓ 59.1- | 1.4- | 45.3 |
| 3 | 16-21 | 3 | 118 | 5792 | 8129 | 21.1 | 46.0 | ✓ | | |
| 4 | " | 6 | 124 | 5778 | 7786 | 23.0 | 49.1 | ✓ | | |
| 5 | 16-22 | 7 | 106 | 5335 | 7509 | 18.8 | 42.1 | ✓ | | |
| 6 | " | 8 | 120 | 5930 | 7325 | 21.2 | 46.1 | ✓ | | |
| 7 | " | 9 | 147 | 5918 | 7436 | 29.6 | 60.2 | ✓ | | |
| 8 | 16-24 | 16 | 183 | 5805 | 6973 | 41.4 ✓ | 80.0 | ✓ 93.0- | 2.2- | 81.7 |
| 9 | 16-25 | 24 | 127 | 5940 | 8357 | 23.3 | 49.6 | ✓ | | |
| 10 | " | 26 | 148 | 5803 | 7001 | 30.5 | 61.7 | ✓ | | |
| 11 | " | 31 | 130 | 5199 | 6844 | 27.7 | 57.0 | ✓ | | |
| 12 | " | 32 | 158 | 5544 | 6470 | 35.2 | 69.6 | ✓ | | |
| 13 | " | 33 | 137 | 5132 | - | 30.5 | 61.7 | ✓ | | |
| 14 | " | 36 | 140 | 5106 | 6001 | 31.8 | 63.9 | ✓ | | |
| 15 | " | 37 | 139 | 5892 | 7326 | 27.2 | 56.2 | ✓ | | |
| 16 | 17-23 | 53 | 140 | 5526 | 5426 | 29.4 | 59.9 | ✓ | | |
| 17 | 17-24 | 340 | 166 | 5249 | 5935 | 40.1 | 77.8 | ✓ | | |
| 18 | " | 54 | 142 | 5596 | 6093 | 29.6 | 60.2 | ✓ | | |
| 19 | " | 59 | 156 | 5680 | 6136 | 33.7 | 67.1 | ✓ | | |
| 20 | " | " | 162 | 5851 | " | 34.6 | 68.6 | ✓ | | |
| 21 | " | 61 | 167 | 5253 | 5917 | 40.2 | 78.0 | ✓ | | |
| 22 | " | 63 | 168 | 5249 | 5838 | 40.7 | 78.8 | ✓ | | |
| 23 | " | 64 | 133 | 5162 | 5804 | 29.0 | 59.2 | ✓ | | |
| 24 | " | 69 | 154 | 5956 | 5759 | 31.5 | 63.4 | ✓ 139.0- | 3.3- | 64.5 |
| P 25 | 18-20 | 93 | 98 | 5407 | 8952 | 15.8 | T-LOG ON HAND ISOTHERMAL FROM | | | 4000' |
| 26 | " | " | 110 | 5447 | " | 19.7 | 43.1 | ✓ | | |
| 27 | 18-22 | 95 | 144 | 5433 | 5655 | 31.2 | 62.9 | ✓ | | |
| 28 | " | 97 | 145 | 5597 | 6007 | 30.6 | 61.9 | ✓ | | |
| 29 | " | 98 | 158 | 5703 | 5825 | 34.2 | 67.9 | ✓ | | |
| 30 | " | 99 | 126 | 5386 | 5872 | 25.4 | 53.2 | ✓ | | |
| 31 | 18-23 | 102 | 134 | 5947 | 6164 | 25.4 | 53.2 | ✓ | | 5956 |

ECU
5000' - 6000'

3

EFFICIENCY LINE No. 2636
AVGRAD

| | 1 LOC | 2 WELL | 3 BHT | 4 DEPTH | 5 COLLAR ELEV | 6 °C/ft | 7 | 8 | 9 | |
|----|---|----------------|----------------|-----------------|-----------------|-----------------|------|-----------------|--------|------|
| 1 | 18-23 | 103 | 114 | 5461 | 5647 | 21.0 | | OMIT | | |
| 2 | " | (103) | 138 | 5410 | " | 27.6 | 56.8 | ✓ | | |
| 3 | 19-21 | (122) | 165 | 5209 | 6767 | 39.9 | 77.5 | ✓ | | |
| 4 | 19-22 | (126) | 147 | 5213 | 5706 | 33.6 | 66.9 | ✓ | | |
| 5 | " | (129) | 140 | 5772 | 5570 | 28.1 | 57.7 | ✓ | | |
| 6 | 21-18 | (235) | 141 | 5792 | 5155 | 28.3 | 58.0 | ✓ | | |
| 7 | " | (236) | 145 | 5114 | 5217 | 33.5 | 66.7 | ✓ | | |
| 8 | 21-20 | (243) | 108 | 5172 | 5068 | 20.1 | 44.3 | ✓ | | |
| 9 | 22-16 | (282) | 108 | 5351 | 4419 | 19.4 | 43.1 | ✓ | | |
| 10 | 22-17 | (284) | 109 | 5185 | 4220 | 20.4 | 44.8 | ✓ | | |
| 11 | " | () | 115 | 5582 | " | 20.9 | 45.6 | ✓ | | |
| 12 | 23-17 | (289) | 110 | 5320 | 4463 | 20.2 | 44.4 | ✓ | | |
| 13 | " | (291) | 118 | 5222 | 4291 | 23.8 | 50.5 | ✓ | | |
| 14 | 23-18 | (297) | 130 | 5734 | 4525 | 25.1 | 52.7 | ✓ | | |
| 15 | " | (298) | 115 | 5282 | 4474 | 22.1 | 47.6 | ✓ | | |
| 16 | 24-17 | (307) | 119 | 5211 | 4465 | 23.8 | 50.5 | ✓ | | |
| 17 | 24-20 | (309) | 96 | 5606 | 4648 | 14.6 | 35.1 | ✓ | | |
| 18 | 26-19 | (328) | 110 | 5895 | 6017 | 18.2 | 41.1 | ✓ | 120.4- | 2.9- |
| 19 | 26-20 | (332) | 120 | 5636 | 4349 | 22.3 | 47.9 | ✓ | | 40.4 |
| 20 | | | | | | | | | | |
| 21 | | | | | | | | | | |
| 22 | NOTE: | | | | | | | | | |
| 23 | THE ASSUMED AMBIENT T WILL INTRODUCE LESS | | | | | | | | | |
| 24 | ERROR IF AV GRAD FOR ENTIRE STATE FOR THIS INTERVAL (5000'-6000') | | | | | | | | | |
| 25 | IS USED TO PROJ MEASURED BHT FROM ITS LOCATION TO 5500' | | | | | | | | | |
| 26 | (SEE LAST COLUMN) | | | | | | | | | |
| 27 | | | | | | | | | | |
| 28 | | | | | | | | | | |
| 29 | | | | | | | | | | |
| 30 | | | | | | | | | | |
| 31 | | | | | | | | | | |

137

~~5895~~

24.0 °C/ft

5000-6000

ECU
ADDITIONAL EMERY CO

(4)

EFFICIENCY LINE No. 2636



| | 1 LOC | 2 WELL | 3 BHT | 4 DEPTH | 5 COLLAR ELEV | 6 °/100' | 7 °C | 8 | 9 |
|----|-------|--------|--------|---------|---------------|----------|------|---|---|
| 1 | 17-16 | 390 | 118 °F | 5485 | 4820 | 22.3 | 48.0 | ✓ | |
| 2 | 21-14 | 400 | 120 | 5992 | 4577 | 21.0 | 45.8 | ✓ | |
| 3 | 21-16 | 402 | 112 | 5600 | 4282 | 19.9 | 44.0 | ✓ | |
| 4 | 22-15 | 405 | 114 | 5911 | 4356 | 19.4 | 43.6 | ✓ | |
| 5 | 23-14 | 407 | 122 | 5456 | 4234 | 23.7 | 50.3 | ✓ | |
| 6 | 23-15 | 409 | 116 | 5636 | 4687 | 21.0 | 45.8 | ✓ | |
| 7 | 23-16 | 410 | 116 | 5504 | 4038 | 21.5 | 46.6 | ✓ | |
| 8 | 24-14 | 412 | 134 | 5730 | 4320 | 26.4 | 54.8 | ✓ | |
| 9 | 24-16 | 415 | 105 | 5320 | 4773 | 18.5 | 41.6 | ✓ | |
| 10 | 25-15 | 418 | 120 | 5787 | 5128 | 21.7 | 47.0 | ✓ | |
| 11 | 25-16 | 420 | 103 | 5030 | 4866 | 18.8 | 42.1 | ✓ | |
| 12 | 26-14 | 421 | 138 | 5736 | 5122 | 27.6 | 56.8 | ✓ | |
| 13 | 26-14 | 423 | 123 | 5998 | 5374 | 21.9 | 47.3 | ✓ | |
| 14 | | | | | | | | | |
| 15 | | | | | | | | | |
| 16 | | | | | | | | | |
| 17 | | | | | | | | | |
| 18 | | | | | | | | | |
| 19 | | | | | | | | | |
| 20 | | | | | | | | | |
| 21 | | | | | | | | | |
| 22 | | | | | | | | | |
| 23 | | | | | | | | | |
| 24 | | | | | | | | | |
| 25 | | | | | | | | | |
| 26 | | | | | | | | | |
| 27 | | | | | | | | | |
| 28 | | | | | | | | | |
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T PROJ. BY GRAD.
TO 5500' (1676m)

5992
5700







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



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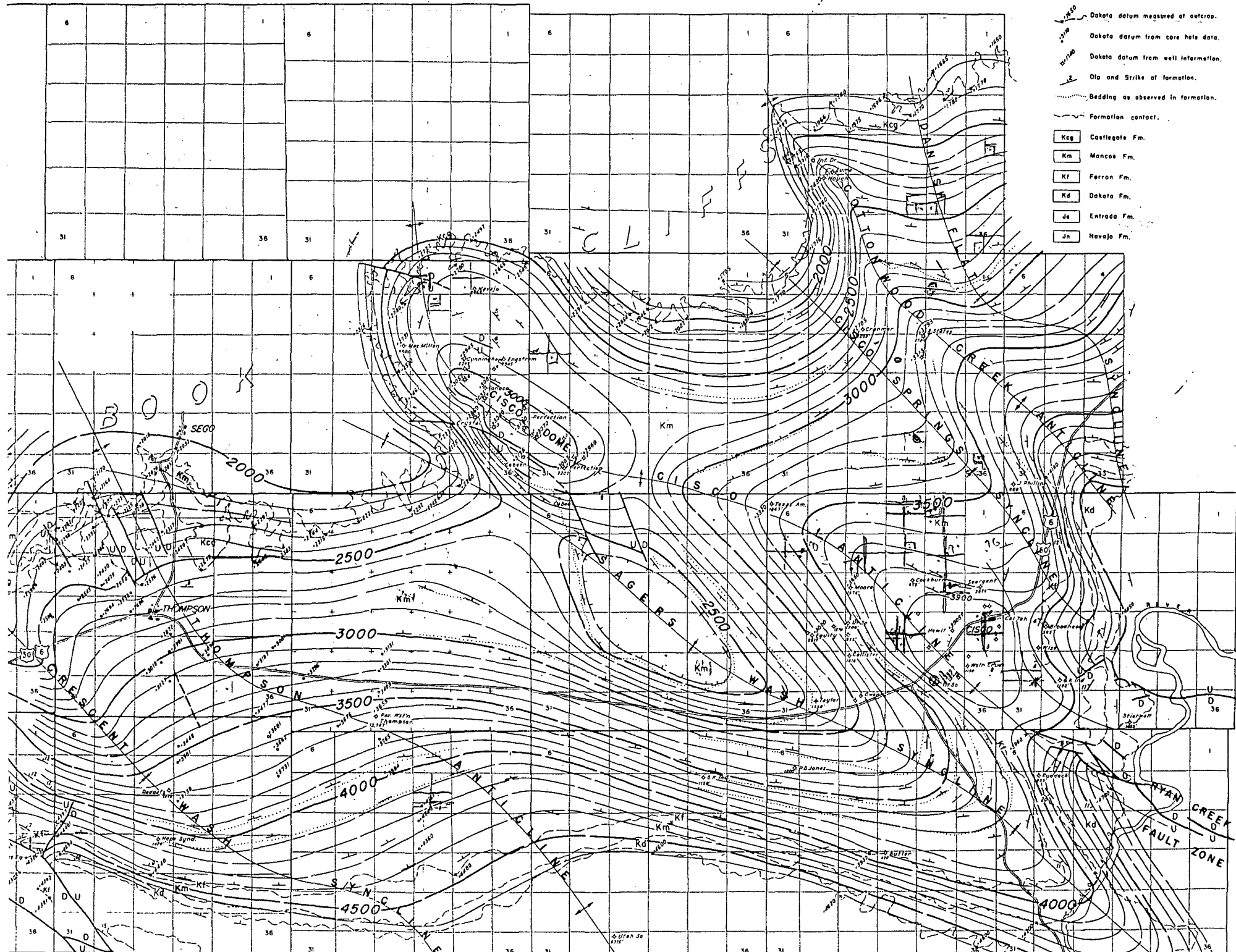
R 22 E

R 23 E

LEGEND

-  Dakota datum measured at outcrop.
-  Dakota datum from core hole data.
-  Dakota datum from well information.
-  Dip and Strike of formation.
-  Bedding as observed in formation.
-  Formation contact.

-  Kcg Castlegate Fm.
-  Km Mancoes Fm.
-  Kf Ferron Fm.
-  Kd Dakota Fm.
-  Ja Entrada Fm.
-  Jn Navajo Fm.



T 20 S

T 21 S

T 22 S

R 18 E

R 19 E

R 20 E

R 21 E

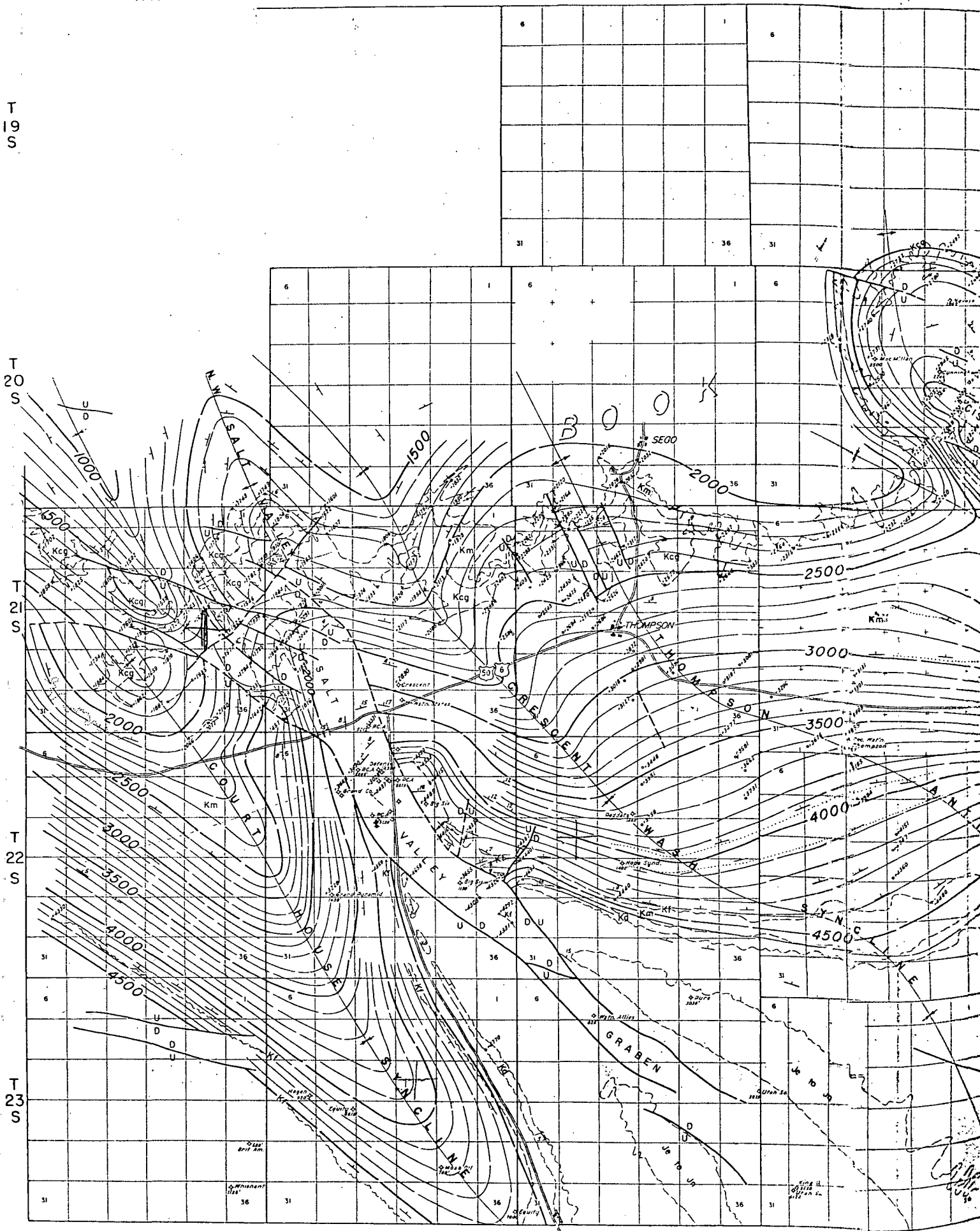
T 19 S

T 20 S

T 21 S

T 22 S

T 23 S



R 18 E

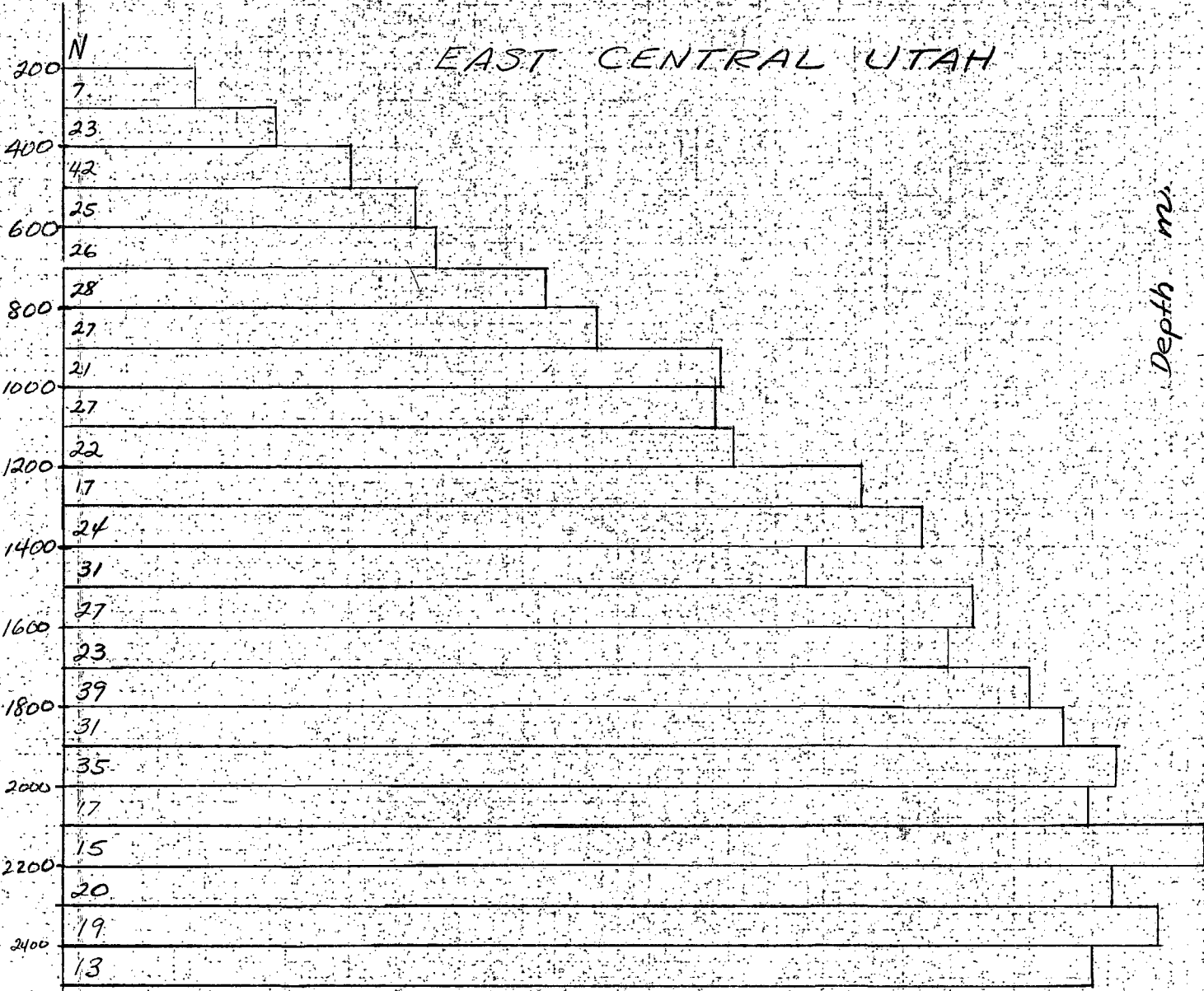
R 19 E

R 20 E

R 21 E

70 80 90 100 110 120 130 140
°F

EAST CENTRAL UTAH



Depth m.

ELEVS

| WELL # | COLLAR | 3 TOP KD | DEPTH | 5 FOOTAGE km | 6 % km | 9 F. °C | 8 % km | 9 |
|----------|-----------|----------|-------|-----------------|--------|---------|--------|---|
| 25-20-21 | 5030 | 3050 | 2982 | 1980 | 71.1 | 113 | 40.6 | |
| 31-20-22 | 4986 | 3000 | 2334 | | 85.0 | 94* | 33.6 | |
| 10-20-21 | 5656 | 2950 | 3566 | | 77.2 | 110 | 30.7 | |
| 3-20-21 | 5706 | 2820 | 3208 | 2886 | 90.0 | 128* | 43.7 | |
| 2-20-21 | 5805 | 2800 | 3800 | 3005 | 79.1 | 133 | 39.3 | |
| 2-20-21 | 5704 | 2750 | 3290 | 2954 | 89.8 | 110 | 32.7 | |
| 2-20-21 | 344 | 5648 | 3501 | 2788 | 79.6 | 127 | 39.6 | |
| 6-20-22 | 5565 | 1880 | 3006 | 3685 | 100.0 | 124 | 44.3 | |
| 8 | 5091 | 2830 | 2528 | 2261 | 89.4 | 90 | 28.1 | |
| 19-20-22 | 4863 | 3432 | | | 108 | | 30.3 | |
| 14-20-22 | 4840 | 2896 | | | 99 | | 30.2 | |
| 5-20-21 | 4584 | 1690 | | | 80 | | 31.3 | |
| 5-20-21 | 4592 | 1678 | | | 80 | | 31.5 | |
| 5-20-23 | 4851 | 2805 | | | 60 | | 31.8 | |
| 5-20-23 | 4972 | 2530 | 3342 | | 120 | | 49.7 | |
| 27-20-23 | 4855 | 2345 | | | 95 | | 34.2 | |
| 36-20-23 | 4511 | 1841 | | | 77 | | 25.7 | |
| 3-20-24 | 4583 | 1586 | | | 84 | | 37.9 | |
| 8-20-24 | 4583 | 1562 | | | 100 | | 43.2 | |
| 8-20-24 | 4586 | 1610 | | | 87 | | 40.8 | |
| 8-20-24 | 4587 | 1611 | 1655 | | 82 | | 34.1 | |
| 8-20-24 | 4596 | 1558 | | | 85 | | 39.8 | |
| 9-20-24 | 4610.5 | 1670 | | | 87 | | 39.3 | |
| 9-20-24 | NOT GIVEN | 1602 | | | 86 | | 39.8 | |
| 9-20-24 | 4572 | 1504 | | | 85 | | 41.2 | |
| 9-20-24 | 4592 | 1537 | | | 80 | | 34.4 | |
| 9-20-24 | 4583 | 1624 | | | 85 | | 38.2 | |
| 5-20-24 | 4601 | 1344 | | | 84 | | 49.8 | |
| 16-20-24 | 4605 | 1363 | | | 73 | | 29.4 | |
| 26-21-19 | 4452 | 8468 | 1777 | | 161 | | 23.7 | |
| 26-21-19 | 234 | 105 | 105 | | 105 | | 55.4 | |
| 23-21-18 | 4867 | 3028 | 3587 | | 165 | | 32.5 | |
| 23-21-18 | 1630 | 328 | 3587 | | 110 | | 30.0 | |
| 7-21-19 | 5150 | 3490 | 3690 | | 108 | | 28.7 | |

(*MART) BHT

EFFICIENCY RAME No. 2636

Dec: June Mar. Mar. N N

ELEVS

BHT

| S-T-R | 1 WELL # | 2 COLLAR | 3 TOP KD | 4 DEPTH | 5 FOOTAGE Km | 6 % Km | 7 F C | 8 C/Km | 9 | Month |
|-------------|-----------------|-----------------|----------|-----------------|-----------------|--------------|---------------|-----------------|---|--------------|
| 17-21-19 1 | 241 | 5169 | | 8996 8928 | | | 157 159 | 22.7 22.0 | | Jan. Jan. |
| 11-21-21 2 | 244 | 4963 | | 7416 | | | 158 | 26.3 | | N |
| 1-21-23 3 | 246 | 4906 | | 1411 | | | 78 | 34.9 | | S |
| 2-21-23 4 | 247? | 4558 | | 1510 | | | | | | |
| 2-21-23 5 | 248 | 4575 | | 1685 | | | 92 | 33.5 | | D |
| 3-21-23 6 | 249 | Not given | - | 1425 | | | 82 | 39.7 | | N |
| 2-21-23 7 | 250 | 4650 | 3550 | 1500 | 1100 | 73.3 | 85 | 41.3 | | Ap. |
| 3-21-23 8 | 251 | 4577 | 3500 | 1414 | 1077 | 76.2 | 95 | 56.7 | | N. |
| 3-21-23 9 | 252 | 4487 | - | 1126 | | | 68 | 27.5 | | My. |
| 4-21-23 10 | 253 | 4207 | - | 1302 | | | 100 or 108 | 60.6 or 79.8 | | Ap. |
| 7-21-23 11 | 257 | 4502 | 3400 | 1332 | 1102 | 82.7 | 85 | 46.5 | | Ja. |
| 9-21-23 12 | 258 | 4485 | 3700 | 1482 | 785 | 53.0 | 82 | 38.1 | | D. |
| 10-21-23 13 | 259 | Not given | - | 1136 | | | 85 | 54.6 | | O. |
| 10-21-23 14 | 260 | " | - | 1744 | | | 73 | 43.9 | | S. |
| 10-21-23 15 | 261 | 4444 | - | 1186 | | | 86 | 53.8 | | N. |
| 10-21-23 16 | 262 | 4454 | 3700 | 1306 | 754 | 57.7 | 85 | 47.5 | | F. |
| 11-21-23 17 | 263 | 4458 | - | 1117 | | | 80.9 | 48.0 | | O. |
| 11-21-23 18 | 264 | 4419 | - | 1288 | | | 50.9 | 50.9 | | Au. |
| 11-21-23 19 | 265 | 4507 | - | 1634 | | | 162 | 56.9 | | Jy |
| 11-21-23 20 | 266 | 4482 | 3700 | 1164 1290 | 782 | 67.2 60.6 | 98 79 | 73.6 87.8 | | Au. |
| 12-21-23 21 | 267 | 4235 | 3700 | 1391 | 515 | 37.0 | 76 | 32.8 | | Oc. |
| 14-21-23 22 | 268 | 4412 | 3820 | 1230 | 592 | 48.1 | 74 | 34.1 | | D |
| 9-21-24 23 | 270 | 4467 | ? | 870 | | | 92 | 77.0 | | Au. |
| 22-21-23 24 | 271 | 4411 | 3840 | 1391 | 571 | 41.0 | 90 | 51.1 | | Ja. |
| 24-21-23 25 | 274 | 4611 | 3905 | 704 | 706 | 100.0 | 75 | 62.1 | | Au. |
| 26-21-23 26 | 277 | 4362 | 3800 | 1128 | 562 | 49.8 | 81 | 48.5 | | O. |
| -27 | 278? | | | | | | | | | |
| 30-21-24 28 | 279 | 4323 | 3900 | 1141 | 423 | 37.1 | 80 | 46.3 | | Ap. |
| 30-21-24 29 | 280 | 4323 | 3900 | 1122 | 423 | 37.7 | 82 | 50.4 | | S. |
| 17-22-20 30 | 286 | 4780 | 4100 | 12123 14992 | 680 | 5.6 4.5 | 236 245 | 27.8 23.6 | | D. Ja. |
| 31 | | | | | | | | | | |

EFFICIENCY @ LINE No. 2636

ANIPAC

ELEVS

| S-T-R | 1 WELL # | 2 COLLAR | 3 TOP KL | 4 DEPTH | 5 FOOTAGE KM | 6 % KM | 7 PF | 8 °C | 9 °C/KM | Month |
|------------|----------|----------|----------|---------------|-----------------|-------------|------------|------|--------------|-------------|
| 16-22-21 1 | 287 | 4697 | 4200 | 1439 | 497 | 34.5 | 94 | | 54.5 | Je. |
| 2-22-23 2 | 288 | negative | 3700 | 1992 | | | 94 | | 52.5 | Aug. |
| 15-23-19 3 | 299 | 4589 | 3890 | 4378 12074 | 699 | 16.0 5.8 | 117 186 | | 27.5 20.4 | Apr. Jy. |
| | 4 | 395 | | | | | | | | |
| | 5 | 396 | | | | | | | | |
| | 6 | 397 | | | | | | | | |
| | 7 | 401 | | | | | | | | |
| | 8 | 404 | | | | | | | | |
| | 9 | | | | | | | | | |
| | 10 | | | | | | | | | |
| | 11 | | | | | | | | | |
| | 12 | | | | | | | | | |
| | 13 | | | | | | | | | |
| | 14 | | | | | | | | | |
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| | 30 | | | | | | | | | |
| | 31 | | | | | | | | | |

EFFICIENCY LINE No. 2636



WELLS COLLARED IN MANCOS

| S-T-R | 1 Well # | Elevs | | | 5 Depth | 6 Footage Km | 7 FIT OUT 400 | 8 % Km | SAT | |
|---------------------------------|----------------|-----------------|-----------------|-----------------|-----------------|----------------|------------------|-----------------|---------------|-----------------|
| | | 2 COLLAR | 3 TOP Kd | 4 BOT TOM | | | | | 9 F °C | 10 °C/km |
| 19-19-23 ¹ | 70 | 5178 | 1900 | 1385 | 3793 | 3278 | 5/5 | 86.4 | 125 | 31.7 |
| 26-21-23² | 277 | 4362 | 3800 | 3072 | 1128 | 562 | 1/28 | 45.8 | 81 | 48.5 |
| 2-20-23 ³ | 176 | 4854 | 2900 | 2160 | 2694 | 1954 | | 72.5 | 112 | 41.3 |
| 36-20-23 | 202 | 4511 | 3470 | | 1814 | 1041 | | 57.4 | 77 | 25.7 |
| 27-20-23 | 201 | 4855 | 3230 | | 2345 | 1625 | | 69.3 | 95 | 34.2 |
| 15-20-28 | 198 | 4756 | 3050 | | 2590 | 1706 | | 65.9 | 112 | 42.9 |
| 2-22-16 | 233 | 4067 | 3520 | | 4983 | 547 | | 11.0 | 121 | 25.6 |
| 3-17-26 ⁸ | 84 | 5278 | ✓ | | 3890 | | | | 116 | 30.5 |
| 8-17-26 ⁹ | 86 | 5158 | ✓ | | 3600 | | | | 116 | 32.9 |
| 17-17-25 ¹⁰ | 77 | 5521 | - | | 3682 | | | | 121 | 34.7 |
| 15-18-25 ¹¹ | 112 | 4786 | ✓ | | 1888 | | | | 89 | 36.7 |
| 19-18-25 ¹² | 113 | 4900 | ✓ | | 1973 | | | | 92 | 37.9 |
| 5-18-24 ¹³ | 107 | 5058 | ✓ | | 4773 | | | | 129 | 29.8 |
| 6-18-24 ¹⁴ | 108 | 5159 | ✓ | | 4409 | | | | 128 | 31.8 |
| 5-18-24 ¹⁵ | 105 | 5168 | ✓ | | 2767 | | | | 108 | 37.5 |
| 5-18-24 ¹⁶ | 106 | 5254 | ✓ | | 4604 | | | | 135 | 33.3 |
| 5-18-24 ¹⁷ | 341 | 5147 | ✓ | | 4470 | | | | 126 | 30.6 |
| 4-19-25 ¹⁸ | 142 | 5603 | ✓ | | 4084 | | | | 147 | 42.8 |
| 16-18-24 ¹⁹ | 110 | 5019 | ✓ | | 3282 | | | | 108 | 31.7 |
| 21-18-24 ²⁰ | 111 | 5004 | ✓ | | 2884 | | | | 106 | 34.8 |
| 30-19-25 ²¹ | 143 | 4598 | ✓ | | 1954 | | | | 100 | 45.7 |
| 14-19-24 ²² | 138 | 4674 | ✓ | | 2604 | | | | 96 | 31.5 |
| 35-19-24 ²³ | 139 | 4576 | ✓ | | 1598 | | | | 81 | 34.2 |
| 35-19-24 ²⁴ | 140 | 4575 | ✓ | | 1575 | | | | 80 | 33.6 |
| 36-19-24 ²⁵ | 141 | 4647 | ✓ | | 1475 | | | | 102 | 63.0 |
| 20-19-24 ²⁶ | 133 | 5050 | ✓ | | 3550 | | | | 110 | 30.3 |
| 24-19-23 ²⁷ | 134 | 4833 | 2170 | | 3442 | 2663 | | 77.4 | 107 | 29.6 |
| 6-19-23 ²⁸ | 135 | 4872 | 2430 | | 3203 | 2442 | | 76.2 | 115 | 36.4 |
| 7-19-23 ²⁹ | 136 | 4892 | 2420 | | 2436 | 2472 | | 100.0 | 104 | 39.6 |
| 16-19-23 ³⁰ | 342 | 4813 | 2720 | | 2797 | 2093 | | 74.8 | 98 | 30.6 |
| 26-20-21 ³¹ | 163 | 5081 | ? | | 2761 | | | | 109 | 38.3 |
| " | " | " | " | | 1800 | | | | 112 | 61.8 |

PERCENTAGE OF HOLE IN MANCOS SHALE VS. GRADIENT TO BOTTOM

EAST CENTRAL UTAH

HOLES ON MANCOS ETC.

Wells Collared in Mancos

37

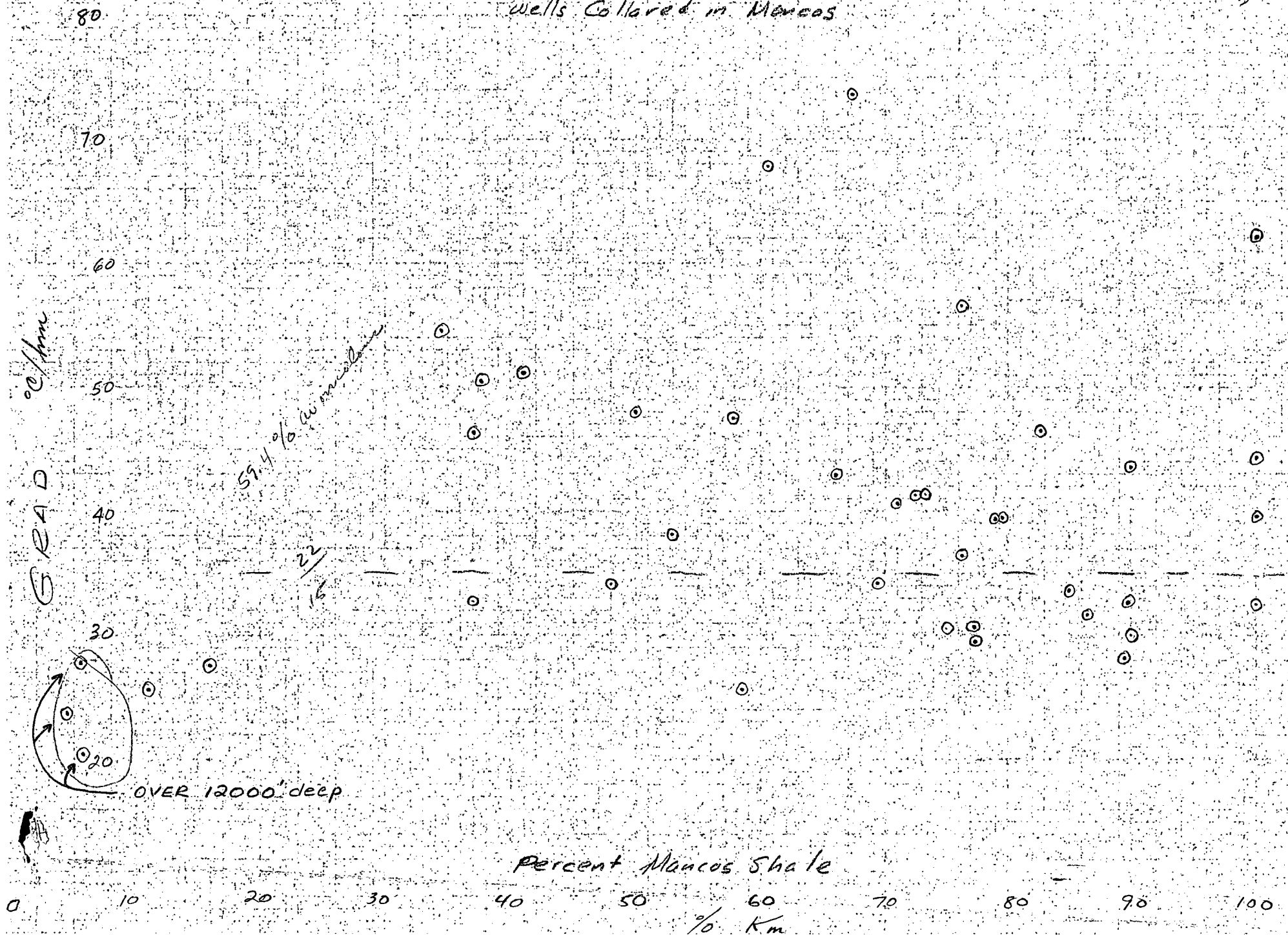


Table 1 — Generalized description and water-bearing properties of rocks in central and eastern parts of Uinta Basin, Utah

Sources: Abbott, Ward, 1957; Kay, J. L., 1934; Kinney, D. N., 1949 and 1955; MacLachlan, M. E., 1957; Sanborn, A. F., Darrow, D. L., and Liscomb, R. L., 1957; Stokes, W. L., 1952 and 1957; and Walton, P. T., 1957.

| System | Series | Formation | Map symbol | Thickness (feet) | Description | Distribution and structure | Water-bearing properties |
|---------------------------------|--------------------------------|---|------------------|---|--|--|--|
| Quaternary | Recent and Pleistocene | Alluvium and outwash gravel | Qao | 1 - 200 | Gravel, sand, and silt; generally unconsolidated | Outwash gravel prominent along Uinta River drainage. Recent alluvium occurs in most stream valleys | Probably will supply water to shallow wells wherever it is more than 20 feet thick |
| Tertiary | Miocene(?) | Bishop conglomerate | Tb | 1 - 800 | Conglomerate of rounded to subangular boulders in sandstone matrix | South slope of Uinta Mountains dipping gently away from mountains | Unknown |
| | Oligocene or Eocene | Duchesne River formation | Tdr | 50 - 300 | Mudstone, siltstone, sandstone in beds 2 to 6 ft thick, commonly separated by unconsolidated beds of shaly material | Underlies surface over northern and eastern parts of basin. Normally flat lying; maximum dips 2° - 4° | Probably poor |
| | Upper Eocene | Uinta formation | Tu | 1,500± | Green to reddish shale capped in places by 30 to 50 ft of sandstone in beds a few inches to a few feet thick | Underlies surface over southern half of basin; underlies Duchesne River formation elsewhere. Normally flat lying; maximum dips 2° - 4° | Probably poor, except that sandstone cap may supply small quantities of water to wells |
| | Eocene | Green River formation (divided into Evacuation Creek, Parachute Creek, Garden Gulch, and Douglas Creek members) | Tgr | About 1,500 ft where exposed; as much as 4,000 ft in subsurface (5,600 ft recorded in one well) | Black shale, sandstone, and oolitic limestone. Oil- and gas-producing sandstone and shale | Underlies entire basin but is several thousand feet below surface along axis of basin | Water occurs with oil in sandstone lenses, but it is generally too highly mineralized for use |
| | Lower Eocene | Wasatch formation | Tw | 1,500 - 5,000 | Mudstone, sandstone, conglomerate, and minor amounts of limestone; predominantly fluviatile red beds | Underlies entire basin - is more than 10,000 ft below surface at deepest part. See figure 3 for structure. May include older rocks | Unknown |
| Tertiary and Cretaceous | Paleocene and Upper Cretaceous | North Horn formation | Not shown on map | 500 - 1,600 | Interbedded sandstone conglomerate, shale, and limestone | Probably does not crop out within area of this report. May occur in the subsurface | Unknown |
| Cretaceous | Upper Cretaceous | Mesaverde formation | Kmv | 400 - 1,200 | Fine- to medium-grained sandstone, dark-gray shale, lignitic shale and lignite. Sandstone predominates in lower half of formation, and lignitic shale and lignite are present only in upper part | Crops out at eastern end of basin. Probably underlies entire basin | Probably can supply small quantities of water to wells from sandstone |
| | | Mancos shale (includes rocks equivalent to Emery and Ferron sandstone members and Frontier sandstone member, and intertonguing sandstone lenses of the Mesaverde formation) | Knd | 3,500 - 5,000 | Gray marine mudstone with eastward-thinning sandstone lenses | Crops out northeast of basin. Probably underlies entire basin | Sandstone lenses may supply water, which is likely of poor quality because enclosing shale contains gypsum, to wells |
| | | Dakota sandstone (included with Mancos shale on generalized map) | Knd | 50 - 90 | Conglomeratic sandstone that represents advance of Cretaceous sea; transects time lines | Crops out north and northeast of basin. Probably underlies entire basin | Rock is probably too dense to supply water to wells in quantity |
| | Lower Cretaceous | Cedar Mountain formation (includes Buckhorn conglomerate member; Stokes 1952) | Not shown on map | | Green, purple, and maroon mudstone with discontinuous conglomerate and conglomeratic sandstone at base | Probably underlies entire basin; thickens to southwest | Unknown |
| Jurassic | Upper Jurassic | Morrison formation (probably mostly equivalent to the Brushy Basin shale member of southeastern Utah) | Ja | 800 - 1,000 | Varicolored mudstone and claystone | Crops out north and northeast of basin. Probably underlies entire basin | Probably poor |
| | | Curtis formation | Jcu | 250 - 300 | Fossiliferous, glauconitic sandstone, shale, and sandy limestone | do. | Do. |
| | | Entrada sandstone | Jcu | 100 - 175 | Principally crossbedded eolian sandstone | do. | Can supply small quantities of good water to wells |
| | Upper and Middle Jurassic | Carmel formation | Jcu | 125 - 170 | Red sandstone, shale, and siltstone | do. | Probably poor |
| Jurassic and Triassic(?) | | Navajo sandstone | | 700 - 900 | Crossbedded calcareous sandstone | do. See figure 3 for structure | Can supply moderate quantities of good water to wells near outcrop area on south slope of Uinta Mts. Quality of water may be poor where Navajo is 2,000 - 3,000 feet or more below surface |
| Triassic | Upper Triassic | Chinle formation (includes Shinarump member) | Tcm | 250 | Basal sandstone or conglomerate overlain by red-orange, purple, or green claystone to conglomerate. Conglomerate of Shinarump member fills channels in Moenkopi formation | Crops out north and northeast of basin. Probably underlies entire basin | Probably poor except in Shinarump |
| | Middle(?) and Lower Triassic | Moenkopi formation (included with Chinle formation on map) | Tcm | 700 - 800 | Red beds of unfossiliferous sandstone, siltstone, and claystone both above and below a middle fossiliferous limestone member | do. | Probably poor |
| Permian | | Park City formation | Ppc | 200± | Thick limestone with intercalated quartzite and sandstone | do. | Supplies water from springs in Ashley Creek valley north of Vernal and in Whiterocks River valley |
| | | Phosphoria formation (included with Park City formation on map) | Ppp | 40 - 60 | Phosphatic shale with thin limestone beds | Reported as a separate unit only in well logs | Water reported from Phosphoria may come from underlying Weber sandstone or deeper limestone |
| Pennsylvanian | | Weber sandstone | Pwm | 1,000 - 1,200 | Massive, crossbedded, fine- to coarse-grained sandstone | Crops out north and northeast of basin. Probably underlies entire basin | In Ashley Valley field water produced from 4,000 ft below surface is usable for irrigation |
| | | Morgan formation (included with Weber sandstone on map) | Pwm | 1,100 - 1,300 | Thick-bedded, cherty, fossiliferous limestone in lower member and red sandy shale, buff and red crossbedded sandstone, and thin beds of gray to pink cherty limestone in upper member | do. | Probably poor |
| Pennsylvanian and Mississippian | | Pennsylvanian and Mississippian rocks undivided. Probably includes rocks equivalent to Manning Canyon shale, Humbug formation, Deeret and Madison limestone | Pwu | 1,000± | Principally massive limestone with a black fissile shale unit at top | do. | May supply water from caverns or solution channels |
| Cambrian | Upper Cambrian | Lodore formation | Cl | 100 - 1,200 | Thick-bedded, coarse-grained, arkosic sandstone and arenaceous shale | do. | Unknown |
| Precambrian | | Uinta Mountain group | pCu | 12,000 - 15,000 | Red, pink, or white quartzitic sandstone, with thin shale partings, and thin-bedded sericitic and sandy shale interbedded with slabby sandstone | Forms core of Uinta Arch in eastern part of Uinta Mountains | Do. |

May 8, 1979

MEMORANDUM

TO: Ross Whipple
FROM: Lorie Cahn
SUBJECT: Conversation with Jim Hood, USGS Water Resources Division, SLC,
regarding ground water in Grand Co., Utah.

SUMMARY

The Water Resources division of the USGS has not conducted any field investigation in the Cisco Dome area of Grand County, Utah. Both the Mancos Shale and the Dakota Sandstone are extremely poor aquifers in this area. The water bearing members of the Mancos Shale (the Ferron and Emery Sandstones) thin to the east. The Emery member is nonexistent and the Ferron member is extremely thin near Cisco. Hood suggested that shale hydration (anhydrite hydrating to gypsum) might be a source of heat.

NOTES

Conversation with Jim Hood, Water Resources, USGS, 5-3-79.

Lithology and relation to aquifers in East Central Utah

Km - Mancos sh

Ferron and Emery ss members are best aquifers but pinch out and disappear to east.

Kd - Dakota ss

Discount as reliable aquifer.

K - Cedar Mtn. Fm

Bottom of fm - not reliable as aquifer but could carry water.

J - Morrison Fm

Has bentonite but Salt Wash ss memb. yields small quantities of water under artesian pressure. Some water due to poor sorting.

J - Summerville Fm

Minutely interbedded ss, slts. Fractures filled with gypsum. Yields little water.

J - Curtis Fm

Not good aquifer.

J - Entrada ss

Varies in thickness. Potential aquifer of low permeability.

J - Carmel ss

Thins eastward, <100' in Cisco area. Not very permeable, okay for stock well.

J - Navajo ss

Best aquifer but not too good. Thins to east, thin in Cisco area. Very jointed and fractured. Extremely uniform grn size and is more permeable than poorly sorted material of same grain size.

T - Kayenta Fm

Zone of lower permeability between Navajo and Wingate.

T - Wingate ss

Not as good aquifer as Navajo but permeability enhanced by fracturing and jnting.

T - Chinle

Tight ss layer, nothing much for ground water.

P - Kaibab Ls

Not in Cisco area.

P - Cutler Fm

Upper ss memb. middle sh, slst memb. Thickens to S. As good as Navajo for water. Poor sorting, reduces permeability. Potential for flow of water upward thru column.

P - Hermosa Fm

Paradox Salt mem. is ~2000' thick out of Cisco. Flows plastically, low permeability. Well in Green River got good flow of brine in Paradox. Mostly tight.

P - Molas Fm

Dolomite ls, sh, ~200' thick, Karst topog.

Mississippian - A lot of permeability, but water moves slowly. Is major aquifer in NW Colorado.

HYDRAULIC CONDUCTIVITIES

(figures are off the top of his head)

Navajo - 0.2 to 2.0 ft/day; highest hydr. K due to fracture permeability.

Mancos - 10^{-10} to 0.01 ft/day

Norm. - 1 ft/day

Fracturing as a local anomaly can triple hydral. K.

OTHER FACTORS WHICH MAY CONTROL THERMAL ANOMALIES

Faulting - Many compression and tension faults west of Cisco and Crescent Junction and probably in Cisco. In Green River find deep fluids leaking to surface along faults (tar seeps, brine seeps). Thrusting to west.

- young igneous activity in subsurface??
- + interformational transfer of water at depth.
- shale hydration-- Anhydrite hydrating to gypsum is exothermic under certain conditions. Find old fractures filled w/ gypsum, selenite.
- radioactive heat generation from plutons.

Lorie Cahn

Lorie Cahn
Geologist

LC/kg

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GEOLOGIC MAP OF EAST CENTRAL UTAH

Compiled by: Lorie S. Cahn

From: Stokes, W. L., et. al., 1964, Geologic Map of Utah

Quaternary

Q = Quaternary undivided

Tertiary

Tu = Uinta Fm

Tgu = Green River Fm undivided

Tw = Wasatch Fm

Tc = Colton Fm

Cretaceous & Tertiary undifferentiated

TK = North Horn Fm and Tuscher Fm

Cretaceous

Ky = Late Cretaceous undivided

Km = Mancos Shale

Kmf = Ferron Sandstone member of Mancos Shale

Kd = Dakota Sandstone

Jurassic

Ju = Jurassic undivided. Morrison Fm through Navajo Sandstone

Triassic?

JR = Kayenta Sandstone and Glen Canyon Group

Triassic

Tu = Triassic undivided. Includes Chinle Fm and Moenkopi Fm.

Paleozoic

Pu = Paleozoic undivided

Precambrian

pC = Precambrian undivided

CISCO-WESTWATER, GRAND CO., UTAH
BOOK CLIFFS - GREEN RIVER DESERT

FRUITA - GRAND JUNCTION, COLORADO
COLORADO NATIONAL MONUMENT

| PALEOCENE-Eocene | | 0-2000 | oil shale | PALEO-Eocene | basalt flows | 0-1000 | Pliocene | | | |
|------------------|--------------------------|-----------------------|--------------------------------|--|---------------------|-----------------------|----------------|------------------------------|------------------------|--------------|
| PALEOCENE-E | Green River Formation | | | Green River Fm | Evacuation Creek M. | | oil shale | | | |
| | | | | | Parachute Creek M. | 0-2000 | oil shale | | | |
| PALEOCENE-E | Colton Fm ("Wasatch" Fm) | 1000 | varicolored mudstone and shale | Wasatch Fm | Garden Gulch M. | | oil shale | | | |
| | Ohio Creek Conglomerate | 6-700 | red + black chert pebbles | | Douglas Creek M. | | oil shale | | | |
| | Tuscher Fm | 270 | mostly light colored ss | | Shire M. | | oil shale | | | |
| | MESAVEURDE GROUP | Price River Fm | Farrer Memb | 470 | | Molina M. | 600 | maroon, green and gray shale | | |
| | | | Neslen Memb | 300 | coal coal | Atwell Gulch M. | | maroon, green and gray shale | | |
| Sego Ss M | | | 170 | | Ohio Creek Cg | 100 | mammal fossils | | | |
| Buck Sh Tong | | | 200 | Mancos tongue | "MESAVEURDE GROUP" | Price River Formation | Farrer facies | Undivided | 1000 | |
| Castlegate Ss | | | 100 | Upper Blackhawk tongue | | | | Undivided | 1000 | |
| Desert Ss | | | 50 | | | | | Cameo M. | 1000 | "Cameo" coal |
| | | | Cozzette M. | 1000 | | | | "Rollins" Ss at base | | |
| | | | Corcoran M. | | | | | Viviparus | | |
| | | | Upper Sego Ss | 50 | | | | coal | | |
| CRETACEOUS | Mancos Shale | Early Pierre fauna | | Lingula | Mancos Shale | Early Pierre fauna | | coar Ophiomorpha coal | | |
| | | | | Inoceramus sandstone beds | | | Anchor Mine T | 50-100 | coal | |
| | | | | | | | Lower Sego Ss | 100 | Baculites Scotti | |
| | | | | | | | | | Serpula | |
| | | | | | | | | | Lingula | |
| | | | | | | | | | Baculites obtusus | |
| | | | | | | | | | Scaphites pulcherrimus | |
| | | | | | | | | | | |
| | | | | | | | | | Inoceramus sagensis | |
| | | | | | | | | | Ostrea | |
| CRETACEOUS | Mancos Shale | Telegraph Creek fauna | 3100 | Inoceramus lobatus | Mancos Shale | Telegraph Creek fauna | 4000 | Baculites | | |
| | | Niobrara fauna | | Inoceramus | | | Niobrara fauna | | Scaphites hippocrepis | |
| | | | | Baculites | | | | | Inoceramus lobatus | |
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| | | | | | | | | | Ostrea | |
| | | | | | | | | | Ferron Ss M. | |
| JURASSIC | Mancos Shale | Ferron Ss M | 50 | cuesta former | Mancos Shale | Telegraph Creek fauna | | Inoceramus | | |
| | | Tununk Sh Member | 350 | | | | Niobrara fauna | | Ostrea | |
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| JURASSIC | Mancos Shale | Dakota Ss | 100 | Gryphaea newberryi | Mancos Shale | Telegraph Creek fauna | | Inoceramus | | |
| | | Cedar Mtn Fm | 120 | oil producer at Crows and Agate fields | | | Niobrara fauna | | Ostrea | |
| | | | | dinosaurs | | | | | Ferron Ss M. | |
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| JURASSIC | Mancos Shale | Brushy Basin M | 275 | | Mancos Shale | Telegraph Creek fauna | | Inoceramus | | |
| | | Salt Wash M | 300 | | | | Niobrara fauna | | Ostrea | |
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| JURASSIC | Mancos Shale | Morrison Fm | | | Mancos Shale | Telegraph Creek fauna | | Inoceramus | | |
| | | Summerville Fm | 20 | | | | Niobrara fauna | | Ostrea | |
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| JURASSIC | Mancos Shale | Moab Memb | 100 | white ss | Mancos Shale | Telegraph Creek fauna | | Inoceramus | | |
| | | Entrada Sandstone | 100-400 | Archers Nat'l Mon | | | Niobrara fauna | | Ostrea | |
| | | | | Dewey Bridge Memb | | | | | Ferron Ss M. | |
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| | | Kayenta | 100 | | | | Niobrara fauna | | Ostrea | |
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| | | Chinle Shale | 100 | | | | Niobrara fauna | | Ostrea | |
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| JURASSIC | Mancos Shale | Precambrian | | | | | | | | |

FROM:

FELTIS, R. D., 1966, Water from bedrock in the Colorado Plateau
of Utah:

Utah State Engineer, Tech. Pub. No. 15,

pp. 82.

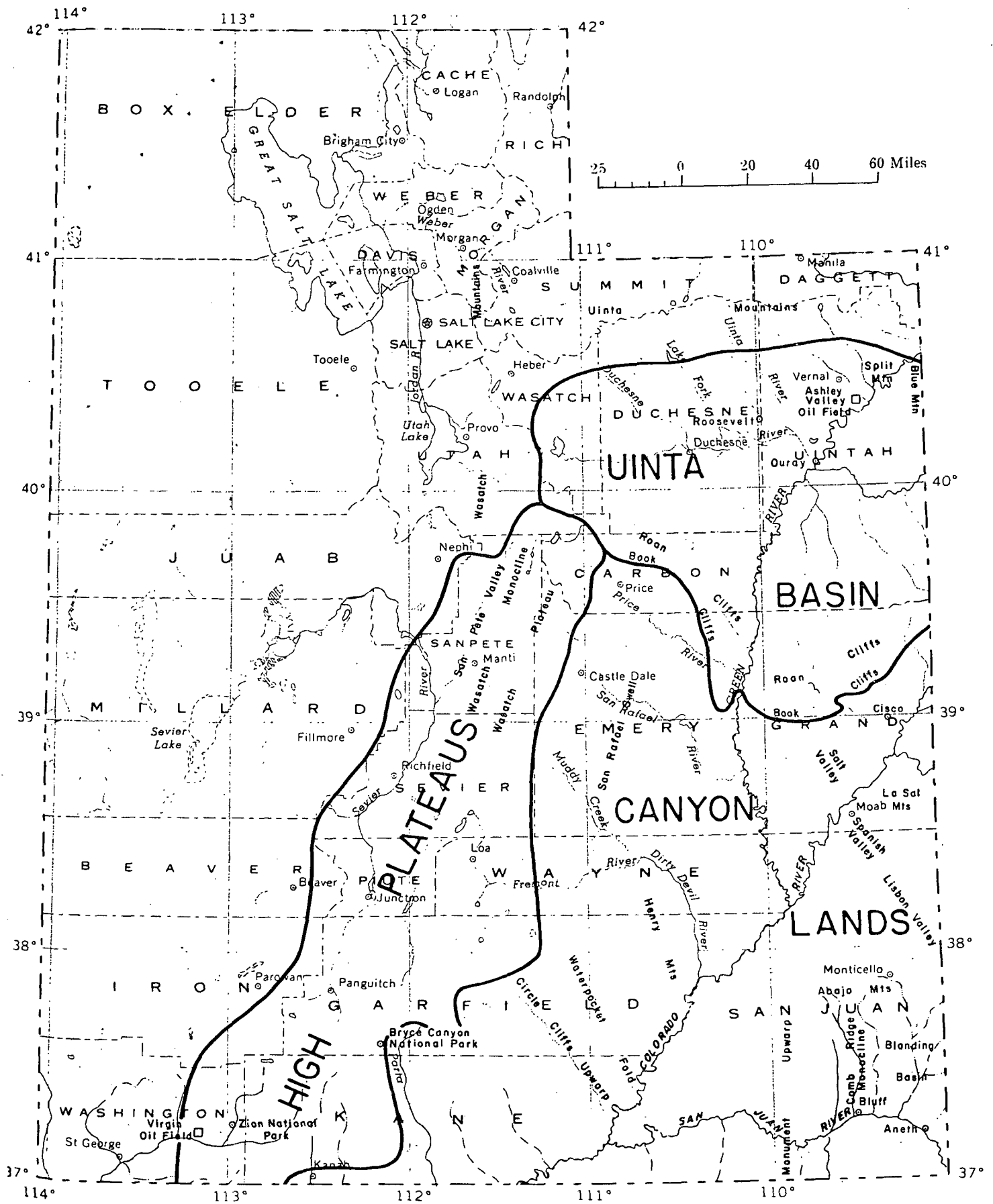


Figure 1. — Index map of the Colorado Plateau in Utah.

The chemical quality of water in the Uinta Formation is determined principally by the lithology of the formation and local recharge conditions. In the central part of the basin, the formation is composed predominantly of fine-grained lake deposits that contain large quantities of soluble salts; but it yields fresh and slightly saline water where local precipitation or runoff from the Uinta Mountains recharges the formation. In the eastern part of the basin, where there is little precipitation, wells may yield fresh or slightly saline water from coarse-grained fluvial deposits that contain few soluble salts (Picard, 1957, p. 128).

Duchesne River Formation

Sandstone beds in the Duchesne River Formation are a source of fresh water for the city of Roosevelt and for private domestic wells. Data from five water wells indicate a range in dissolved solids from 234 to 528 ppm (fig. 6 and table 2) and a range in yield from about 60 to 340 bwpd (2 to 10 gpm). The source of water in the formation is from recharge by surface streams that cross the area of outcrop and by precipitation directly on the area of outcrop along the north flank of the basin. The formation dips southward, and artesian conditions occur where water wells tap the aquifer in T. 2 S., R. 1 W. (USM). Water wells penetrate the Duchesne River to a maximum known depth of 810 feet; however, logs of oil wells show the formation to be as much as 4,000 feet thick. The electrical log of the well in sec. 5, T. 1 N., R. 2 W. (USM) in figure 4 indicates that the base of the slightly saline water in the Duchesne River may be as much as 3,460 feet deep.

WATER FROM BEDROCK IN THE CANYON LANDS SECTION

The Canyon Lands section is the most structurally complex part of the Colorado Plateau in Utah. Three upwarps—the San Rafael Swell and Circle Cliffs and Monument Upwarps—are the major structural elements in the section. The upwarps and adjacent basins are modified by numerous subsidiary folds and faults and by the intrusives that formed the Abajo and Henry Mountains. In the northeastern part of the Canyon Lands section is a northwest-trending belt of faulted anticlines, including Salt, Spanish, and Lisbon Valleys. Near the center of this area is the La Sal Mountains, also formed by an intrusive. Sedimentary rock of Cambrian and Devonian through Cretaceous age are exposed in the Canyon Lands section or have been identified in oil wells. Table 1, columns 6, 7, 8, and 9, show the stratigraphic section for the Canyon Lands.

Chemical analyses of water from water wells, oil and gas wells, and springs show that fresh water is in the Hermosa Group, the Rico and Cutler Formations, the Cedar Mesa Sandstone Member, Organ Rock Tongue, and De Chelly Sandstone Member of the Cutler Formation, Chinle Formation, Shinarump Member of the Chinle Formation, Wingate Sandstone, Kayenta Formation, Navajo Sandstone, Carmel Formation, Entrada and Bluff Sandstones, Morrison and Burro Canyon Formations, and the Dakota Sandstone. Many of the analyses are for water from scattered springs and stock wells that are the only source of ground water for hundreds of square miles.

The electrical logs of oil and gas tests used in constructing figure 8 indicate that water in bedrock in the Blanding Basin ranges from fresh to saline in chemical quality.

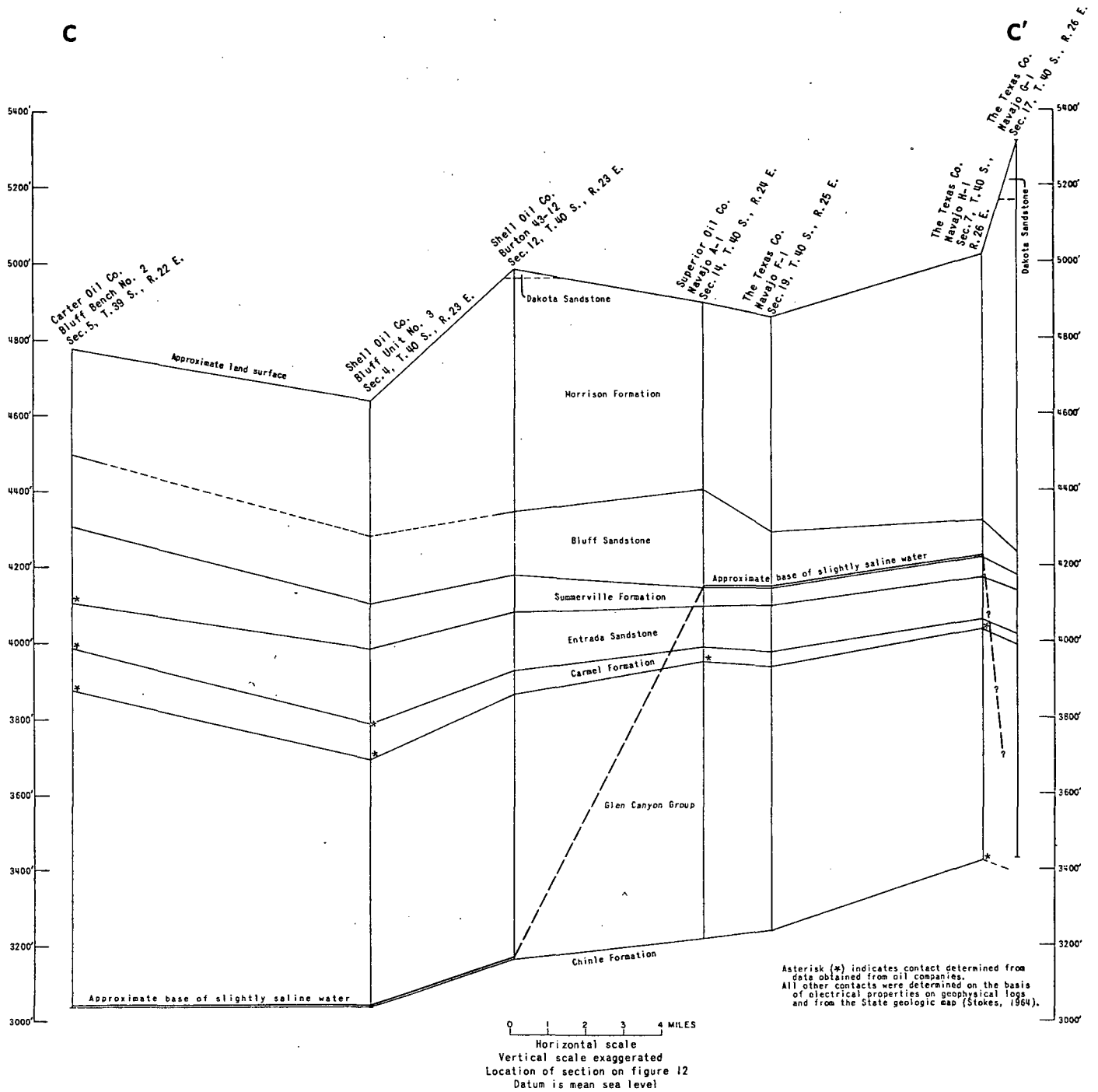


Figure 8. — Geologic section C-C' of the Blanding Basin in the Canyon Lands section.

Ground-water data are not available for many areas in the Canyon Lands, mainly because water wells have not been drilled to test the quantity or quality of water and because such data were not collected during oil and gas exploration.

Recharge to bedrock aquifers in the Canyon Lands occurs where permeable formations crop out along the flanks of the Abajo, Henry, and La Sal Mountains, along the flanks of folds such as the Comb Ridge Monocline, San Rafael Swell, or Waterpocket Fold, and on the wide expanse of flat-lying aquifers that are exposed between the major structural elements. Except near the mountains, however, the amount of recharge is generally small because of the low normal annual precipitation (fig. 2).

The area of greatest development of ground water in the Canyon Lands section is the Blanding Basin, an artesian basin east of Comb Ridge in San Juan County. In T. 40 S., R. 21 E., wells in the Glen Canyon Group yield water having less than 500 ppm of dissolved solids. Eastward from Bluff, the Entrada and Bluff Sandstones and Morrison Formation also yield fresh and slightly saline water to wells. Near Aneth, however, the ground water has as much as 8,640 ppm of dissolved solids.

Artesian conditions have also been encountered in wells drilled in formations that crop out on the flanks of the Abajo, Henry, and La Sal Mountains. The relatively high precipitation on the mountains is a source of recharge to the formations, and in or near the area of outcrop the ground water is generally fresh or slightly saline. Few wells have been drilled near the mountains, however, and the areal extent of the fresh and slightly saline water is unknown.

Table 3 contains selected hydrogeologic data for bedrock formations in the Canyon Lands section, and the locations of the sampling sites are shown in figures 9, 10, 11, 12, 13, 14, and 15. Following is a summary of the data by formation.

Rocks of Cambrian and Devonian age

Water samples from oil wells have been collected from the Aneth and Elbert Formations, the McCracken Member of the Elbert Formation, and the Ouray Limestone of Devonian age, and from sedimentary rocks of Cambrian and Devonian age that are not differentiated.

Chemical analyses of 9 water samples collected from 8 wells in these formations indicate that 6 of the samples are briny and the other 3 are moderately or very saline (fig. 9 and table 3). The moderately saline samples were from the western part of the Canyon Lands section in T. 36 S., R. 10 E., and T. 26 S., R. 7 E. (Water samples from rocks of Devonian and Mississippian age are discussed in the next section.)

Rocks of Mississippian age

Water samples from oil wells have been collected from the Leadville, Madison, and Red-wall Limestones of Mississippian age. These formations, however, generally have not been differentiated when the samples were collected. The individual formations, therefore, are stipulated where known, but otherwise they are considered as a unit called "rocks of Mississippian age."

Chemical analyses of water from three oil wells in the Leadville Limestone in T. 29 S., R. 10 E., T. 42 S., R. 23 E., and T. 43 S., R. 21 E., showed 8,470, 84,516, and 56,500 ppm of dissolved solids (fig. 9 and table 3). In T. 40 S., R. 26 E., and T. 42 S., R. 22 E., water from

the Leadville Limestone and the Ouray Limestone of Devonian age contained 31,583 and 71,948 ppm of dissolved solids.

The Madison Limestone yielded water containing 54,624 and 8,037 ppm of dissolved solids to oil wells in T. 16 S., R. 12 E., and T. 29 S., R. 10 E. (fig. 9 and table 3).

In T. 16 S., R. 9 E., and T. 36 S., R. 10 E., oil wells in the Redwall Limestone yielded water containing 73,653 and 4,669 ppm of dissolved solids and in T. 15 S., R. 12 E., an oil well in the Redwall Limestone and Elbert Formation of Devonian age yielded water containing 67,769 ppm of dissolved solids (fig. 9 and table 3).

Chemical analyses of 52 water samples from the undifferentiated rocks of Mississippian age showed a range of from 7,172 to 327,283 ppm of dissolved solids (fig. 9 and table 3). Six of the water samples were moderately saline, 16 samples were very saline, and 30 samples were brines.

In T. 40 S., R. 7 E., rocks of Mississippian and Devonian age yielded water containing 2,339 ppm of dissolved solids; and in T. 40 S., R. 26 E., and T. 41 S., R. 21 E., rocks of Mississippian age and the Ouray Limestone of Devonian age yielded water containing 39,869 and 83,940 ppm of dissolved solids (fig. 9 and table 3).

An oil well in rocks of Mississippian age and the overlying Molas Formation in T. 35 S., R. 3 E., yielded water containing 9,378 ppm of dissolved solids (fig. 9 and table 3) at a rate of 528 bwpd (16 gpm).

Hermosa Group

Most of the water samples from the Hermosa Group for which chemical analyses are available are from oil wells in the Paradox Formation. Analyses of 34 samples show a range of 5,342 to 397,061 ppm of dissolved solids (fig. 10 and table 3); and 25 of the samples were brines containing more than 35,000 ppm of dissolved solids. A spring in the Hermosa in T. 33 S., R. 16 E., yielded water at a rate of 15,300 bwpd (450 gpm) that contained 414 ppm of dissolved solids.

Molas Formation

A water sample from the Molas Formation in an oil well in T. 39 S., R. 13 E., contained 6,035 ppm of dissolved solids (fig. 10 and table 3).

Rico Formation

Chemical analyses of water from the Rico Formation are available for water from five springs and one water well. Three springs in T. 33 S., R. 15 E., yielded water with 1,220, 3,920, and 4,770 ppm of dissolved solids at rates of about 70, 510, and 850 bwpd (2, 15, and 25 gpm) (fig. 10 and table 3). Two springs in T. 40 S., R. 17 E., and T. 41 S., R. 19 E., yielded water containing 719 and 3,070 ppm of dissolved solids, each at a rate of about 170 bwpd (5 gpm). A water well in T. 35 S., R. 15 E., yielded water containing 318 ppm of dissolved solids at a rate of 350 bwpd (10 gpm).

Coconino Sandstone

Chemical analyses of water from three oil wells in the Coconino Sandstone in T. 16 S., R. 12 E., T. 18 S., R. 14 E., and T. 27 S., R. 15 E., showed 17,249, 49,902, and 3,378 ppm of dissolved solids (fig. 10 and table 3).

Toroweap Formation

Water from an oil well in the Toroweap Formation in T. 35 S., R. 3 E., contained 7,583 ppm of dissolved solids (fig. 10 and table 3).

Kaibab Limestone

Water from four oil wells in the Kaibab Limestone in T. 29 S., R. 10 E., T. 37 S., R. 2 E., T. 18 S., R. 14 E., and T. 20 S., R. 7 E., contained 3,720, 14,179, 35,985, and 72,000 ppm of dissolved solids (fig. 10 and table 3). A spring in T. 24 S., R. 10 E., yielded water having 2,150 ppm of dissolved solids at a rate of about 170 bwpd (5 gpm). (A water sample from the Kaibab Limestone and the Sinbad Limestone Member of the Moenkopi Formation is discussed in the section on the Sinbad Limestone Member.)

Cutler Formation

A water well in the Cutler Formation in T. 25 S., R. 23 E., yielded water having 931 ppm of dissolved solids at a rate of about 6,800 bwpd (200 gpm) (fig. 10 and table 3). The Cutler probably contains fresh or slightly saline water in other areas around the flanks of the La Sal Mountains. A spring in T. 33 S., R. 16 E., yielded water containing 770 ppm of dissolved solids at a rate of 12,200 bwpd (360 gpm). In T. 29 S., R. 26 E., and T. 28 S., R. 23 E., water from two oil wells in the Cutler contained 4,957 and 16,331 ppm of dissolved solids.

Cedar Mesa Sandstone Member of Cutler Formation

Two water wells in the Cedar Mesa Sandstone Member in T. 41 S., R. 16 E., and T. 43 S., R. 14 E., yielded water of 1,890 and 656 ppm of dissolved solids at rates of about 100 and 70 bwpd (3 and 2 gpm) (fig. 10 and table 3). Seven springs (in Tps. 36, 37, and 42 S., Rs. 16-18 E.) in the sandstone in San Juan County yielded water containing 298 to 596 ppm of dissolved solids at rates generally less than 170 bwpd (5 gpm).

Organ Rock Tongue of Cutler Formation

A water sample from an oil well in the Organ Rock Tongue in T. 29 S., R. 10 E., contained 4,487 ppm of dissolved solids (fig. 10 and table 3). Two springs, one in T. 43 S., R. 16 E., and another in T. 34 S., R. 14 E., yielded water containing 944 and 375 ppm of dissolved solids. The former yielded less than 3 bwpd (0.1 gpm), but the latter flowed at a rate of about 1,000 bwpd (30 gpm).

De Chelly Sandstone Member of Cutler Formation

In T. 41 S., Rs. 24 and 25 E., the De Chelly Sandstone Member yielded water containing 17,262 and 52,187 ppm of dissolved solids from two oil wells (fig. 10 and table 3). The yield of the well in T. 41 S., R. 24 E., was 270 bwpd (8 gpm). Three springs in the sandstone in T. 43 S., Rs. 14 and 19 E., yielded fresh water at rates generally less than 140 bwpd (4 gpm).

At Chinle, Ariz., about 90 miles south of Bluff, Utah, water wells in the De Chelly yielded water containing less than 400 ppm of dissolved solids. Electrical logs of oil wells in the Blanding Basin indicate that the De Chelly contains fresh or slightly saline water along the Comb Ridge Monocline, but the water becomes more saline toward the center of the basin.

White Rim Sandstone Member of Cutler Formation

The dissolved-solids content of water from six oil wells in the White Rim Sandstone Member in the west-central Canyon Lands section ranged from 2,045 to 6,045 ppm of dissolved solids (fig. 10 and table 3). Water from two springs in the White Rim in T. 40 S., R. 10 E., yielded water containing 2,470 and 4,060 ppm of dissolved solids at rates of about 70 and 5,100 bwpd (2 and 150 gpm).

Moenkopi Formation

In T. 24 S., R. 13 E., water sampled at two depths in an oil well in the Moenkopi Formation contained 12,472 and 15,999 ppm of dissolved solids. The latter sample was obtained with a reported yield of 94 bwpd (2.8 gpm). In T. 24 S., R. 14 E., however, another oil well yielded water from the formation that contained only 4,187 ppm of dissolved solids (fig. 11 and table 3). Two springs in T. 35 S., Rs. 13 and 14 E., yielded water containing 1,700 and 1,860 ppm of dissolved solids at rates of 15,300 bwpd (450 gpm) and 1,700 to 13,700 bwpd (50 to 400 gpm). Another spring in T. 31 S., R. 14 E., yielded water containing 2,355 ppm of dissolved solids; and a spring in T. 20 S., R. 11 E., yielded water containing 2,250 ppm of dissolved solids at a rate of 680 bwpd (20 gpm).

Sinbad Limestone Member of Moenkopi Formation

In T. 16 S., R. 12 E., oil wells in the Sinbad Limestone Member yielded very saline to briny water. In T. 24 S., R. 13 E., an oil well in the Sinbad yielded water containing 18,125 ppm of dissolved solids (fig. 11 and table 3). In oil wells in T. 29 S., Rs. 10 and 12 E., the Sinbad yielded water containing 4,437 and 9,130 ppm of dissolved solids, with the latter at the rate of 432 bwpd (13 gpm). A water sample collected from the Kaibab Limestone, the Sinbad Limestone Member, and undifferentiated beds in the Moenkopi Formation in an oil well in T. 29 S., R. 11 E., contained 6,167 ppm of dissolved solids.

Chinle Formation

Water from the Chinle Formation in oil tests in T. 22 S., R. 22 E. and T. 26 S., R. 7 E., contained 20,070 and 20,797 ppm of dissolved solids (fig. 11 and table 3), with the former at the rate of 34 bwpd (1 gpm). A spring in T. 39 S., R. 14 E., yielded water containing 747 ppm of dissolved solids. The water from this spring, however, may be discharging at the top of the Chinle after percolating downward through rocks of the overlying more permeable Glen Canyon Group.

Shinarump Member of Chinle Formation

Water has been produced in oil wells, water wells, springs, mines, and test holes from the Shinarump Member of the Chinle Formation (fig. 11). The dissolved-solids content of the water from the several sources were: oil well in T. 24 S., R. 13 E., 5,750 ppm; two water wells in T. 43 S., R. 4½ W., 646 and 710 ppm, with one well yielding 15,300 bwpd (450 gpm); springs in T. 31 S., R. 14 E., 1,613 ppm; and T. 41 S., R. 12 E., 840 ppm with the latter spring yielding 100 bwpd (3 gpm); mines in T. 35 S., R. 7 E., 8,510 ppm, and T. 37 S., R. 16 E., 5,840 ppm; and test holes in T. 41 S., R. 12 E., 1,670 and 3,340 ppm (table 3).

Moss Back Member of Chinle Formation

Water from the Moss Back Member in an oil test in T. 27 S., R. 14 E., yielded water containing 4,980 ppm of dissolved solids (fig. 11 and table 3).

Glen Canyon Group

The Glen Canyon Group consists of the Wingate Sandstone, the Kayenta Formation, and the Navajo Sandstone. This widespread sequence of predominantly sandstone is one of the most important aquifers in the Canyon Lands section because it generally yields fresh water to springs, and in many areas it yields water to wells that is at least suitable for livestock (fig. 12).

In some wells, the subsurface data available are not detailed enough to identify the aquifer other than as the Glen Canyon Group. Five water wells in T. 40 S., R. 21-22 E., yielded water containing from 239 to 403 ppm of dissolved solids at rates of 750 to 3,400 bwpd (22 to 100 gpm) (table 3). A water well in T. 39 S., R. 25 E., yielded water containing 791 ppm of dissolved solids at a rate of 4,320 bwpd (130 gpm). In an oil well in T. 41 S., R. 25 E., the sandstones yield water containing 3,815 ppm of dissolved solids. An oil well in T. 16 S., R. 13 E., yielded very saline or briny water at a rate of 1,680 bwpd (50 gpm).

Wingate Sandstone

Four water wells in T. 23 S., R. 21 E., T. 30 S., R. 24 E., T. 31 S., R. 23 E., and T. 43 S., R. 24 E., yielded water from the Wingate Sandstone that contained from about 300 to 400 ppm of dissolved solids (fig. 12 and table 3). The yield of two of the wells was 70 and 140 bwpd (2 and 4 gpm). Sixteen springs in the Wingate yielded water containing from 133 to 914 ppm of dissolved solids at rates ranging from 17 to 3,840 bwpd (0.5 to 113 gpm). In T. 26 S., R. 7 E., water from an oil well in the Wingate contained 4,079 ppm of dissolved solids. Water produced from a well that taps the Wingate and also the Entrada and Navajo Sandstones is discussed in the section on the Entrada Sandstone. Recharge to the Wingate is restricted by the overlying relatively impermeable Kayenta Formation. Where fracturing and faulting extend through the Glen Canyon Group, however, water moves downward from the Navajo Sandstone through the Kayenta into the Wingate.

¹According to the Western Australia Department of Agriculture (1950), beef cattle and adult sheep will tolerate water containing 10,000 and 12,000 ppm of dissolved solids, respectively.

Kayenta Formation

The Kayenta Formation generally acts as a barrier to the vertical movement of ground water rather than as an aquifer (M. E. Cooley, written commun., 1965). Many springs in the Glen Canyon Group issue at the base of the Navajo Sandstone or near the top of the Kayenta because the more impermeable rock of the Kayenta restricts or stops the downward flow of water. Three springs in the Kayenta in T. 31 S., R. 15 E., T. 39 S., R. 11 E., and T. 42 S., R. 12 E., yielded water containing 220, 115, and 144 ppm of dissolved solids at rates of 70 bwpd (2 gpm) or less (fig. 12 and table 3).

Navajo Sandstone

Most water wells in the Glen Canyon Group draw water from the Navajo Sandstone, probably because it is the shallowest and most permeable formation in the group. Twenty-one water wells in the Navajo yielded water containing from 171 to 7,250 ppm of dissolved solids at rates ranging from 70 to 45,400 bwpd (2 to 1,335 gpm) (fig. 12 and table 3). Five of the wells in Tps. 41 and 42 S., Rs. 21 to 23 E., are in the Blanding Basin, east of Comb Ridge. These five wells in the Navajo yielded water containing from about 170 to 500 ppm of dissolved solids at rates ranging from 70 to 1,200 bwpd (2 to 35 gpm). The chemical quality deteriorates toward the east, however, and two water wells in the Navajo in T. 41 S., R. 25 E., yielded water containing 7,080 and 7,250 ppm of dissolved solids at rates of 2,000 and 2,450 bwpd (60 and 72 gpm). The recharge area for the aquifer in the Blanding Basin is in the area of outcrop of the sandstone along the length of Comb Ridge Monocline. Ten wells drilled in the Navajo in Arizona and Utah to supply water at the Glen Canyon Dam construction facility in Arizona yielded water containing from 216 to 1,814 ppm of dissolved solids at rates ranging from 1,200 to 45,400 bwpd (35 to 1,335 gpm) (Goode, 1964, p. 45 and 60).

Chemical analyses of water from 14 springs in the Navajo Sandstone showed a range of dissolved solids from 129 to 354 ppm. The yield of the springs ranges from less than 34 bwpd (1 gpm) to 1,700 bwpd (50 gpm); but most of the springs yield 340 bwpd (10 gpm) or less.

Chemical analyses are available for four water samples from the Navajo Sandstone obtained from oil wells. Two wells in T. 41 S., R. 24 E., yielded water containing 3,410 and 3,890 ppm of dissolved solids, and wells in T. 15 S., R. 11 E., and T. 26 S., R. 7 E., yielded water containing 3,607 and 320 ppm of dissolved solids. Water produced from the Navajo in wells that also tap other formations is discussed in the section on the Entrada Sandstone.

Carmel Formation

The Carmel Formation has yielded water that ranges from fresh to moderately saline. The dissolved-solids content of water from three water wells in T. 25 S., R. 12 E., and T. 27 S., R. 11 E., ranged from 2,730 to 6,360 ppm (fig. 13 and table 3). The yields of two of the wells were 100 and 580 bwpd (3 and 17 gpm). Chemical analyses of water from three springs in T. 22 S., R. 8 E., T. 24 S., R. 13 E., and T. 28 S., R. 14 E., showed 7,450, 437, and 2,390 ppm of dissolved solids. The yield of the springs ranged from 34 to 170 bwpd (1 to 5 gpm). In most areas, however, the Carmel forms an aquiclude above the Navajo Sandstone. An example of this is the Blanding Basin, where the water in the Navajo is confined under artesian pressure by the overlying Carmel.

Entrada Sandstone

The Entrada Sandstone has yielded fresh water to water wells in some areas and saline water in others. The sandstone yielded water having 360 to 801 ppm of dissolved solids from six wells in eastern San Juan County; 380 to 3,500 ppm from seven wells in Emery, Kane, and Wayne Counties; and from 9,470 to 14,300 ppm from two wells in Grand County (fig 13 and table 3). ~~Although the Entrada contained saline water in northeastern Grand County,~~ in the Grand Junction area of Colorado water from the sandstone contained from 291 to 1,210 ppm of dissolved solids (Löhman, 1965, p. 115).

Data for eight wells indicate that yields from the Entrada Sandstone range from about 85 to 40,000 bwpd (2.5 to 1,200 gpm). Five of these wells are in San Juan County, and their yields average 4,860 bwpd (143 gpm).

Chemical analyses of water from nine springs, which issue from the Entrada Sandstone at rates ranging from 17 to 170 bwpd (0.5 to 5 gpm), indicate a range in dissolved solids from about 190 to 740 ppm (fig. 13).

Several wells in the Blanding Basin produce water from the Entrada Sandstone and one or more other formations, including the Bluff, Navajo, and Wingate Sandstones. In T. 39 S., R. 26 E., the Navajo and Entrada yielded water containing 1,070 ppm of dissolved solids at a rate of 990 bwpd (29 gpm); but in T. 41 S., R. 23 E., these formations yielded water containing 6,851 ppm at a rate of 1,070 bwpd (31.5 gpm). In T. 40 S., R. 24 E., and T. 41 S., R. 23 E., wells in the Navajo, Entrada, and Bluff Sandstones yielded water containing 4,526 and 1,735 ppm of dissolved solids; and in T. 41 S., R. 25 E., water from the Entrada, Navajo, and Wingate Sandstones contained 8,640 ppm. In T. 41 S., R. 25 E., a well in the Entrada and Bluff Sandstones yielded water containing 2,180 ppm of dissolved solids at a rate of 34 bwpd (1 gpm).

Bluff Sandstone

The Bluff Sandstone in Utah is found only in southern San Juan County. Two wells in T. 40 S., R. 23 E., yielded water containing 1,850 and 7,350 ppm of dissolved solids at rates of 440 to 850 bwpd (13 to 25 gpm) (fig. 13 and table 3). Two springs in the Bluff in T. 40 S., R. 22 E., and T. 41 S., R. 21 E., yield water containing 139 and 241 ppm of dissolved solids, and the latter discharges less than 34 bwpd (1 gpm). Water produced from the Bluff in wells that also tap other formations is discussed in the sections on the Entrada Sandstone and the Morrison Formation.

Morrison Formation¹

In Grand County, water from five wells in the Morrison Formation in Tps. 19-22 S. contained from 2,090 to 25,700 ppm of dissolved solids (~~fig. 13 and table 3~~). A sixth well in T. 22 S., R. 22 E., yielded water containing only 517 ppm, and this probably indicates that recharge to the formation is at or near the well site. Yields from three of the wells were 70 bwpd (2 gpm) or less. In San Juan County, in T. 36 S., R. 21 E., and T. 40 S., R. 25 E., the Morrison yielded water containing 844 and 1,460 ppm of dissolved solids, the latter at a rate of 70 bwpd (2 gpm).

¹In this discussion, data for wells and springs in all members of the Morrison Formation are treated as a unit. In figure 13 and table 3, however, the specific member is identified when possible.

Eight springs in the Morrison Formation in southeastern San Juan County yielded water containing from 216 to 712 ppm of dissolved solids. Seven of the springs yielded less than 10 bwpd (less than 1 gpm), and the other yielded 120 bwpd (3.5 gpm). A spring in Emery County in T. 19 S., R. 10 E., yielded water containing 768 ppm of dissolved solids at a rate of 34 bwpd (1 gpm).

In Grand and San Juan Counties, in ~~T. 22 S., R. 22 E., T. 23 S., R. 22 E.~~, and T. 37 S., R. 21 E., water from three mines in the Morrison Formation contained 1,430, 759, and 1,400 ppm of dissolved solids.

In T. 39 S., Rs. 24 and 25 E., and T. 40 S., Rs. 23 and 24 E., five water wells in the Bluff Sandstone and Morrison Formation yielded water containing 354, 450, 362, 438, and 2,035 ppm of dissolved solids at known rates of 1,000, 170, 5,100, 5,100, and 370 bwpd (30, 5, 150, 150, and 11 gpm). Two wells in the Morrison Formation, the Dakota Sandstone, and the Burro Canyon Formation in T. 33 S., R. 24 E., yielded water containing 292 and 414 ppm of dissolved solids at rates of 750 and 510 bwpd (22 and 15 gpm).

Dakota Sandstone

The Dakota Sandstone has yielded fresh to slightly saline water to springs and wells. Four springs in T. 34 S., R. 11 E., T. 39 S., R. 26 E. (two springs), and T. 41 S., R. 6 E., yielded water containing 199, 1,760, 1,220, and 186 ppm of dissolved solids (fig. 14 and table 3). The spring in T. 34 S., R. 11 E., flowed 510 bwpd (15 gpm), whereas the other three yielded 34 bwpd (1 gpm) or less.

Eight water wells east of Monticello penetrate the Dakota Sandstone and the Burro Canyon Formation, and two of the wells were drilled down into the Morrison Formation. For the six wells penetrating the Dakota and Burro Canyon, the dissolved-solids content of the water ranged from 290 to 453 ppm and the yields ranged from 750 to 4,250 bwpd (22 to 125 gpm). The two wells drilled to the Morrison produced water containing 292 and 414 ppm of dissolved solids at rates of 750 and 510 bwpd (22 and 15 gpm).

The Dakota Sandstone is not differentiated from the Cedar Mountain Formation in logs of oil wells along the north edge of the Canyon Lands section. The combined formational unit is reported to contain "salty" or "brackish" water.

Burro Canyon Formation

The Burro Canyon Formation has yielded fresh to slightly saline water to springs and wells. Six springs in San Juan and Garfield Counties yield water that ranges from 324 to 2,890 ppm of dissolved solids (fig. 14 and table 3) at known rates of 34 bwpd (1 gpm) or less.

Water produced from the Burro Canyon Formation in wells that also tap other formations is discussed in the section on the Dakota Sandstone.

Mancos Shale

The preponderance of fine-grained sediments and water soluble salts in the Mancos Shale suggests that this formation generally is not a fresh-water aquifer. Water wells in T. 15 S., R. 12 E., and ~~T. 18 S., R. 14 E.~~ yielded water containing 6,280 and 4,710 ppm of dissolved solids (fig. 14 and table 3).

Ferron Sandstone Member of Mancos Shale

Two water samples were collected while drilling an oil well with air through the Ferron Sandstone in T. 14 S., R. 9 E. (fig. 15). Chemical analyses of water showed a dissolved-solids content of 37,860 and 51,950 ppm (table 3). A gas well in T. 20 S., R. 7 E., yielded water containing 21,534 ppm of dissolved solids. The Ferron yielded water containing 3,454 ppm of dissolved solids in a coal mine in T. 22 S., R. 6 E.

Tununk Shale Member of Mancos Shale

Two water samples were collected while drilling an oil well with air through the Tununk Shale in T. 14 S., R. 9 E. (fig. 14). Chemical analyses of the water showed a dissolved-solids content of 11,117 and 12,093 ppm (table 3).

WATER FROM BEDROCK IN THE HIGH PLATEAUS SECTION

The High Plateaus section is divided into three longitudinal strips, each consisting of two to four plateaus that generally are separated by escarpments or valleys. The variations in relief generally are controlled by faults, but a few escarpments were formed solely by erosion. Except where distorted locally along faults, the rocks generally are horizontal or gently dipping, as indicated by the attitude of the tops of the individual plateaus. An exception is along the west edge of the Wasatch Plateau where for 50 miles strata of the Wasatch monocline plunge downward from the top of the plateau into Sanpete Valley.

Rocks exposed in the High Plateaus section range from Permian to Tertiary in age, and oil and gas wells have penetrated rocks of Cambrian, Devonian, Mississippian, and Pennsylvanian ages. The rocks include sedimentary and igneous types. Table 1, columns 10, 11, and 12, show the stratigraphic sections for the High Plateaus.

Chemical analyses of water from water wells, oil and gas wells, and springs show that fresh water is in limestones of Paleozoic age, Wingate and Navajo Sandstones, Carmel Formation, Tropic Shale, Wahweap and Straight Cliffs Sandstones, Emery Sandstone Member of the Mancos Shale, Blackhawk, Price River, Kaiparowits, and North Horn Formations, Flagstaff Limestone, Wasatch, Brian Head, Green River, and Crazy Hollow Formations, and igneous rocks of Tertiary age. The extent of fresh water in these formations is poorly known because few water wells penetrate bedrock, and oil and gas exploration has not been extensive in most of the section.

The electrical logs of oil and gas wells used in constructing figure 16 indicate that water in bedrock in the Wasatch Plateau ranges from fresh to saline in chemical quality.

Many communities in the High Plateaus section obtain their water supplies from springs that issue from bedrock. Sedimentary rocks of Tertiary age yield water to most of these springs in the northern part of the Plateaus, and igneous rocks of Tertiary age are the source of most springs in the central part of the High Plateaus. In the southern part of the High Plateaus, limestones of Tertiary age yield water to springs atop the plateaus, but along the escarpments sandstones of Mesozoic age are the principal aquifers. The numerous springs that yield large quantities of fresh water in the High Plateaus is a reflection of the great amount of precipitation on this area (fig. 2).

Table 4 contains selected hydrogeologic data from springs, water wells, and oil and gas wells in bedrock in the High Plateaus section; locations of the sampling sites are shown in figures 9, 10, 11, 12, 13, 14, 15, 17, and 18. Following is a summary of the data by formation.

Table 1. — Correlation chart of bedrock
(See fig. 12 for

format
location

| Geologic age (1) | Northwestern Uinta Basin (2) | Eastern and central Uinta Basin (3) | Book Cliffs at Green River, Utah (4) | Book Cliffs at Utah-Colorado State line (5) | Cane Creek and Big Flat (6) |
|---------------------|--------------------------------------|--|--|---|--|
| Tertiary | | Browns Park Formation | | | |
| | | Duchesne River Formation | | | |
| | | Uinta Formation | | | |
| | | Green River Formation | Green River Formation | Green River Formation | Green River Formation |
| Cretaceous | Mesaverde Group | Wasatch Formation | Wasatch Formation | Wasatch Formation | Wasatch Formation |
| | | Mancos Shale | Mancos Shale Frontier Sandstone Member Howry Shale | Mancos Shale | Mancos Shale |
| | | Dakota Sandstone | Dakota Sandstone | Dakota Sandstone Cedar Mountain Formation Buckhorn Conglomerate | Dakota Sandstone Cedar Mountain Formation |
| | | Morrison Formation | Morrison Formation | Morrison Formation | Morrison Formation |
| Jurassic | | | Summerville Formation | | |
| | | Curtis Formation | Curtis Formation | Curtis Formation | |
| | | Entrada Sandstone | Entrada Sandstone | Entrada Sandstone | Entrada Sandstone |
| | | Twin Creek Formation | Carmel Formation | Carmel Formation | Carmel Formation |
| Triassic(?) | Nugget Sandstone | Navajo Sandstone | Navajo Sandstone | Navajo Sandstone | Navajo Sandstone |
| | | | Kaventa Formation | Kaventa Formation | Kaventa Formation |
| Triassic | Chinle Formation Shinarump Member | Chinle Formation Shinarump Member | Chinle Formation Moss Back Member | Chinle Formation | Chinle Formation Moss Back Member |
| | | Ankarah Shale | Moenkopi Formation | Moenkopi Formation | Moenkopi Formation |
| Permian | Phosphoria Formation | Phosphoria Formation | Coconino Sandstone "Permian carbonate" | | Cutler Formation White Rim Sandstone Member |
| | | | | | Rico Formation |
| Pennsylvanian | Weber Sandstone | Weber Sandstone | Honaker Trail Formation | Honaker Trail Formation | Honaker Trail Formation |
| | Morgan Formation | Morgan Formation | Paradox Formation | Paradox Formation | Paradox Formation |
| Mississippian | Deseret Limestone | Deseret Limestone | Deseret Limestone | | Leadville Limestone |
| | Madison Limestone | Madison Limestone | Leadville Limestone Madison Limestone | | Madison Limestone |
| Devonian | | | Ouray Limestone | | Ouray Limestone |
| | | | Elbert Formation | | Elbert Formation |
| Silurian | | | | | McCracken Member |
| Ordovician | | | | | Aneth Formation |
| Cambrian | Ophir Formation | Lodore Formation | Lynch Dolomite | | Lynch Dolomite |
| | Tintic Quartzite | | Maxfield Limestone | | |
| Precambrian | Uinta Mountain Group | Uinta Mountain Group | Tintic Quartzite | | |
| | | | | Granite | |

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| Mesaverde Groi |
| Mancos Shale Masuk Shale Emery Sandsto Blue Gate Sha Ferron Sandst Tununk Shale |
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| Moenkopi Forma Sinbad Limest |
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Table 2. — Continued

| T | R | Section | Location | Source | Operator or owner | Name or number | Producing formation | Depth to top of formation (feet) | Depth to bottom of formation (feet) | Interval sampled (feet) | Yield (bwpd/gpm) | Method or point of collection | Date of collection | Temperature (°F) | Parts per million | | | | | | | | | | | | | Resistivity (ohm-meter at 68°F) | pH | Analysis by 2/ | Remarks | | | |
|-----|-----|-------------|----------|-----------------------------|-------------------|-----------------|---------------------|----------------------------------|-------------------------------------|-------------------------|-----------------------|-------------------------------|--------------------|------------------|----------------------------|-----------|--------------|----------------|--------|-------|---------------------------------|------------------------------|----------------------------|---------------|----------------------------|---------------------|-------------------------------|---------------------------------|--------|----------------|---|--|---|---|
| | | | | | | | | | | | | | | | Silica (SiO ₂) | Iron (Fe) | Calcium (Ca) | Magnesium (Mg) | NA + K | | Bicarbonate (HCO ₃) | Carbonate (CO ₃) | Sulfate (SO ₄) | Chloride (Cl) | Nitrate (NO ₃) | Dissolved solids 1/ | Hardness as CaCO ₃ | | | | | Noncarbonate hardness as CaCO ₃ | Percent sodium | Sodium-adsorption ratio (SAR) |
| 10S | 22E | C NE 1/4 17 | W | Bureau of Land Management | 2 | Green River Fm. | 1,100 | 4,318 | 2,311-3,405 | 340 10(M) | Flow | 11-30-64 | 3.4 | - | 0.0 | 97 | 4,070 | 2,270 | 263 | 119 | 4,840 | 8.2 | 10,500 | 399 | 0 | 96 | 89 | 16,400 | - | 8.5 | CS | Water from annulus behind 7-inch casing. | | |
| 10S | 23E | NW 1/4 2 | O | Humble Oil and Refining Co. | 1 | Wasatch Fm. | 4,252 | - | 4,592-4,614 | - | DST 3 | 11- -61 | - | - | 702 | 126 | 10,305 | 415 | - | 5,103 | 13,500 | - | 29,941 | - | - | - | - | - | 0.29 | 7.7 | CGL | DST 3 recovered 150 feet of mud and 1,553 feet of gas-cut brackish water. | | |
| 10S | 23E | NE 1/4 24 | O | Shell Oil Co. | 7 | Green River Fm. | 375 | 3,115 | 3,066 | - | Return line Swab test | 10-15-61 | - | - | 2 | 1 | 572 | 1,078 | 48 | 145 | 99 | - | 1,941 | 8 | - | - | - | - | 14/4.2 | 8.9 | SHO | | | |
| 10S | 24E | SE 1/4 28 | O | El Paso Natural Gas Co. | 5 | Mesaverde Gr. | 4,560 | - | 5,295-5,305 | - | Swab test | 6-11-59 | - | - | 1,923 | 82 | 5,194 | 19 | - | 480 | 11,250 | - | 19,536 | - | - | - | - | - | .44 | 4.8 | RME | Mud, water, and oil emulsion filtered to clear water. | | |
| 10S | 24E | C NE 1/4 32 | O | Shell Oil Co. | 8 | Wasatch Fm. | 3,306 | 4,938 | 4,390-4,497 | - | DST 2 | 1-21-62 | - | - | 21 | 11 | 3,068 | 1,220 | 72 | 620 | 3,550 | - | 8,562 | 96 | - | - | - | - | 14/85 | 8.7 | SHO | DST 2 recovered 374 feet of slightly gas-cut mud, 280 feet of heavily gas-cut and water-cut mud, 93 feet of very slightly gas-cut muddy water, and 93 feet of muddy water. Water sample collected at tool. | | |
| | | | | | | Mesaverde Gr. | 4,938 | - | 5,230-5,303 | - | DST 3 | 1-28-62 | - | - | 304 | 63 | 10,580 | 1,244 | 0 | 770 | 15,762 | - | 28,723 | 1,020 | - | - | - | - | 13/27 | 7.8 | SHO | DST 3 recovered 236 feet of gas-cut mud, 308 feet of highly gas-cut, oil-cut, and mud-cut water, and 186 feet of slightly oil-cut and slightly gas-cut muddy water. | | |
| | | | | | | do | 4,938 | - | 6,187-6,494 | - | Production water | 4-30-62 | - | - | 648 | 238 | 7,917 | 903 | 0 | 308 | 13,312 | - | 23,326 | 2,600 | - | - | - | - | 15/31 | 6.6 | SHO | | | |
| | | | | | | Mesaverde Gr. | 4,938 | - | 6,570-6,947 | - | Swab test | 3-22-62 | - | - | 1,040 | 298 | 6,323 | 464 | 0 | 470 | 11,857 | - | 20,452 | 3,825 | - | - | - | - | 10/26 | 6.2 | SHO | | | |
| 11S | 12E | NE 1/4 14 | O | King Oil Co. | 1 | Green River Fm. | 0 | - | 635-650 | 17 0.5(E) | Flow | 7-22-65 | - | 9.8 | - | 6.4 | 4.4 | 221 | 392 | 0 | 179 | 5.1 | .1 | 619 | 34 | 0 | 93 | 16 | 942 | - | 7.8 | CS | | |
| 11S | 21E | C SW 1/4 7 | O | Humble Oil and Refining Co. | 2 | Wasatch Fm. | 3,892 | 6,901 | 4,715-36 | - | DST 2 | 10- -61 | - | - | 804 | 211 | 12,457 | 329 | - | 4,827 | 17,500 | - | 35,961 | - | - | - | - | - | .23 | 7.0 | CGL | DST 2 recovered 300 feet of gas-cut muddy water and 554 feet of muddy, slightly salty water. Analysis from bottom sample. | | |
| 11S | 24E | SW 1/4 6 | O | Shamrock Oil and Gas Corp. | 5 | Green River Fm. | - | 2,677 | 5,119-47 | - | Flow | 8-26-65 | - | 12 | - | 3.2 | .5 | 438 | 644 | 0 | 334 | 19,500 | 60 | 1.6 | 1,170 | 10 | 0 | 99 | 60 | 1,800 | - | 8.2 | CS | DST 5 recovered 1,230 feet of muddy salt water. Water sample from 90 feet above tool. |
| 11S | 24E | SW 1/4 7 | O | do | 3 | do | - | 2,578 | 2,207 | - | do | 8-26-65 | - | 12 | - | 3.2 | .5 | 418 | 691 | 0 | 310 | 21 | 1.4 | 1,110 | 10 | 0 | 99 | 58 | 1,720 | - | 8.2 | CS | Report yield of 250 barrels of water per hour (175 gpm) while drilling at 1,159 feet. | |
| 11S | 24E | NE 1/4 8 | O | do | 1 | do | 0 | 2,518 | 2,396 | At 1,275 | do | 9- 6-61 | - | 13 | 0.36 | 3.6 | 1.5 | 437 | 1.6 | 606 | 12 | 422 | 4.0 | .6 | 1,200 | 15 | 0 | 98 | 49 | 1,820 | - | 8.5 | CS | Analysis includes 0.41 ppm boron, 1.8 ppm fluoride, and 0.00 ppm manganese. Sample collected when water flow was encountered while drilling well. |
| 11S | 25E | NE 1/4 22 | O | Continental Oil Co. | 22-1 | Mancos Sh. | 4,632 | - | At 6,225 | - | See Remarks | 8- 1-61 | - | - | 154 | 49 | 78 | 1,500 | 62 | 375 | - | 2,900 | 186 | - | - | - | - | - | - | 1.7 | 7.6 | CO | Sample collected from "blooie line" while drilling with air. | |
| 12S | 14E | C SW 1/4 13 | O | Carter Oil Co. | 1 | Mesaverde Gr. | 6,814 | 9,446 | 8,505-8,617 | - | DST 22 | 6-27-52 | - | - | - | 350 | 64 | 8,198 | 1,015 | - | 2,523 | 11,000 | - | 26,636 | - | - | - | - | .34 | 6.9 | CGL | DST 22 recovered 375 feet of gas-cut slightly oil-cut mud and 2,440 feet of salt water. | | |
| 13S | 23E | SE 1/4 26 | O | Skyline Oil Co. | 1 | Green River Fm. | 0 | 2,170 | 8,604-8,789 | - | - | 6- -60 | - | 40.8 | - | 10.4 | 7.1 | 261 | - | - | 423 | 17 | - | 1,086 | - | - | - | - | - | - | 7.6 | UC | DST 25 recovered 600 feet of gas-cut and slightly oil-cut mud, 450 feet of water-cut mud, and 5,970 feet of slightly mud-cut water. | |
| 14S | 20E | NW 1/4 7 | O | Phillips Petroleum Co. | 1 | Castlegate Ss. | 7,033 | 7,285 | 7,080-7,180 | - | DST 3 | 9-17-62 | - | - | - | 8 | 2 | 1,672 | 964 | 264 | 2,150 | 140 | - | 4,711 | - | - | - | - | - | 2.65 | 9.3 | CGL | DST 3 recovered 630 feet of water-cut mud (estimated to be 75 percent water). | |
| 14S | 20E | C SW 1/4 30 | O | do | 2 | Wasatch Fm. | 2,390 | 4,320 | 3,790-3,820 | - | See Remarks | 7-13-65 | - | 23 | - | 614 | 91 | 11,900 | 530 | 0 | 1,490 | 18,300 | 25 | 32,700 | 1,910 | 1,470 | 93 | 119 | 48,900 | - | 7.3 | CS | Water collected at discharge line to disposal pit after treatment to remove oil. Yield was 1 bwpd (less than 1 gpm). | |
| | | | | | | Flagstaff Ls. | 4,320 | 4,635 | 4,530-80 | - | Swab test | 12-13-62 | - | - | - | 11 | 12 | 2,897 | 598 | 360 | 4,650 | 320 | - | 8,245 | - | - | - | - | - | 1.02 | 9.4 | CGL | | |
| 14S | 20E | C NE 1/4 30 | O | do | 4 | Green River Fm. | 0 | 2,100 | 1,883-1,910 | - | do | 7-22-63 | - | - | - | 10 | 7 | 274 | 13 | 366 | 12 | 290 | 32 | - | - | - | - | - | - | 9.35 | 8.7 | CGL | Fluid level 700 feet, unable to lower with swabbing rate of 15 barrels of water per hour. | |
| 15S | 21E | C SW 1/4 22 | O | Atlantic Refining Co. | 22-2 | Wasatch Fm. | 1,610 | 3,602 | 3,134-42 | - | DST 1 | 9-26-63 | - | - | - | 20 | 36 | 664 | 149 | 12 | 2 | 1,065 | - | 1,966 | - | - | - | - | - | 1.97 | 8.4 | CL | DST 1 recovered 1,482 feet of gas-cut water. | |
| | | | | | | Castlegate Ss. | 5,518 | - | 3,466-80 | - | DST 2 | 9-28-63 | - | - | - | 80 | 36 | 3,766 | 156 | 14 | 7,579 | 355 | - | 11,986 | - | - | - | - | .66 | 8.6 | CL | DST 2 recovered 525 feet of brackish water with sulfur water. | | |
| | | | | | | Castlegate Ss. | 5,518 | - | 5,518-41 | - | DST 4 | 10-12-63 | - | - | - | 600 | 109 | 11,643 | 107 | 0 | 5,813 | 14,981 | - | 33,253 | - | - | - | - | .23 | 7.3 | CL | DST 4 recovered 150 feet of slightly gas-cut muddy water and 950 feet of slightly gas-cut brackish water. | | |
| 15S | 22E | W 1/4 36 | O | Texaco, Inc. | 1 | Entrada Ss. | 9,194 | 9,360 | 9,232-9,349 | 100(R) 3 | Swab test | 4- -60 | - | - | - | 5,115 | 534 | 28,237 | 190 | - | 72 | 54,000 | - | 88,052 | - | - | - | - | - | .10 | 7.3 | CGL | Swabbed 4 1/2 barrels of water per hour from 8,800 feet with fluid level standing at 8,000 feet. | |
| 15S | 23E | SE 1/4 36 | S | - | PR Spring | Green River Fm. | 0 | - | - | 34 1(M) | Flow | 9-17-64 | 47 | 17 | - | 65 | 36 | 17 | 302 | 0 | 94 | 2.8 | .5 | 381 | 312 | 64 | 11 | .4 | 606 | - | 7.7 | GS | | |
| 15S | 23E | NE 1/4 33 | O | Texaco, Inc. | 3 | Morrison Fm. | 8,100 | 8,706 | 8,630-8,714 | - | - | 9- -61 | - | - | - | 5,789 | 454 | 34,077 | 207 | - | 16 | 64,000 | - | 104,438 | - | - | - | - | - | - | .09 | 6.3 | CGL | Report of analysis lists the Entrada Sandstone as the water-bearing formation. |
| 16S | 17E | SW 1/4 3 | S | - | Camel Rock Spring | Wasatch Fm. | 0 | - | - | 7,700 225(R) | - | 9-25-48 | - | 26 | - | 70 | 41 | 73 | 321 | 0 | 220 | 64,000 | 7 | .7 | 596 | 343 | 80 | 32 | 1.7 | 842 | - | - | GS | |
| 17S | 17E | SW 1/4 20 | S | - | - | Mesaverde Gr. | 0 | - | - | - | - | 9-25-48 | - | 18 | - | 10 | 5.7 | 250 | 492 | 0 | 176 | 5 | .1 | 707 | 48 | 0 | 92 | 16 | 1,060 | - | - | GS | | |
| 17S | 24E | NE 1/4 9 | O | Trend Oil Co. | 6-A | Entrada Ss. | 5,240 | - | 5,247-90 | - | DST 1 | 11-21-60 | - | - | - | 2,570 | - | 30,200 | 244 | - | 2,112 | 51,500 | - | 86,626 | - | - | - | - | .08 | 6.8 | RME | DST 1 recovered 40 feet of drilling mud and 1,460 feet of slightly gas-cut salt water. | | |
| 17S | 24E | NW 1/4 12 | O | do | 5-A | do | 5,070 | - | At 5,160 | - | See Remarks | 11- 2-60 | - | - | - | 2,304 | - | 20,200 | 13 | - | 2,352 | 33,500 | - | 58,369 | - | - | - | .14 | 6.0 | RME | Drilled with air from 930 to 5,161 feet; encountered water at 5,100 feet and the water rose 300 feet. | | | |
| 20S | 20E | 17 | S | - | Thompson Spring | Mesaverde Gr. | 0 | - | - | - | - | 10-20-33 | - | - | .10 | 55 | 64 | 104 | 552 | - | 156 | 8.0 | 1.2 | 660 | 400 | - | - | - | - | - | - | GS | | |
| 20S | 20E | 27 | S | Chesterfield Coal Co. | Sego Spring | do | 0 | - | - | - | - | 2-24-41 | - | 11 | - | 44 | 79 | 198 | 664 | - | 323 | 26 | .0 | 1,090 | 432 | - | - | - | - | - | 7.5 | DH | Analysis includes 0.1 ppm fluoride | |

1/ Dissolved solids calculated from determined constituents except as noted.
 2/ Analysis by: CaO, Carter Oil Co.
 CGL, Chemical and Geological Laboratories, Caspiter, Wyo.
 CL, Core Laboratories, Inc., Dallas, Tex.
 CO, Continental Oil Co.
 GS, U.S. Geological Survey
 DH, Utah State Department of Health
 PA, Pan American Petroleum Corp.
 RME, Rocky Mountain Engineering Co., Grand Junction, Colo.
 SHO, Shell Oil Co.
 SOG, Stanolind Oil and Gas Co.
 UC, Utah State Chemist

3/ Uinta Special Meridian.
 4/ Trace.
 5/ In solution at time of analysis.
 6/ Analysis supplied by Carter Oil Co.
 7/ Total iron.
 8/ Resistivity at 72°F.
 9/ Residue at 180°C.

Owner: Name of operator or owner at time water sample was collected for chemical analysis.
 Producing formation: Fm., Formation; Gr., Group; Ls., Limestone; Mbr., Member; sed., sedimentary; Sh, Shale; Ss., Sandstone. Many formation names were reported in records of oil and gas companies and State and Federal agencies do not necessarily agree with the identification.

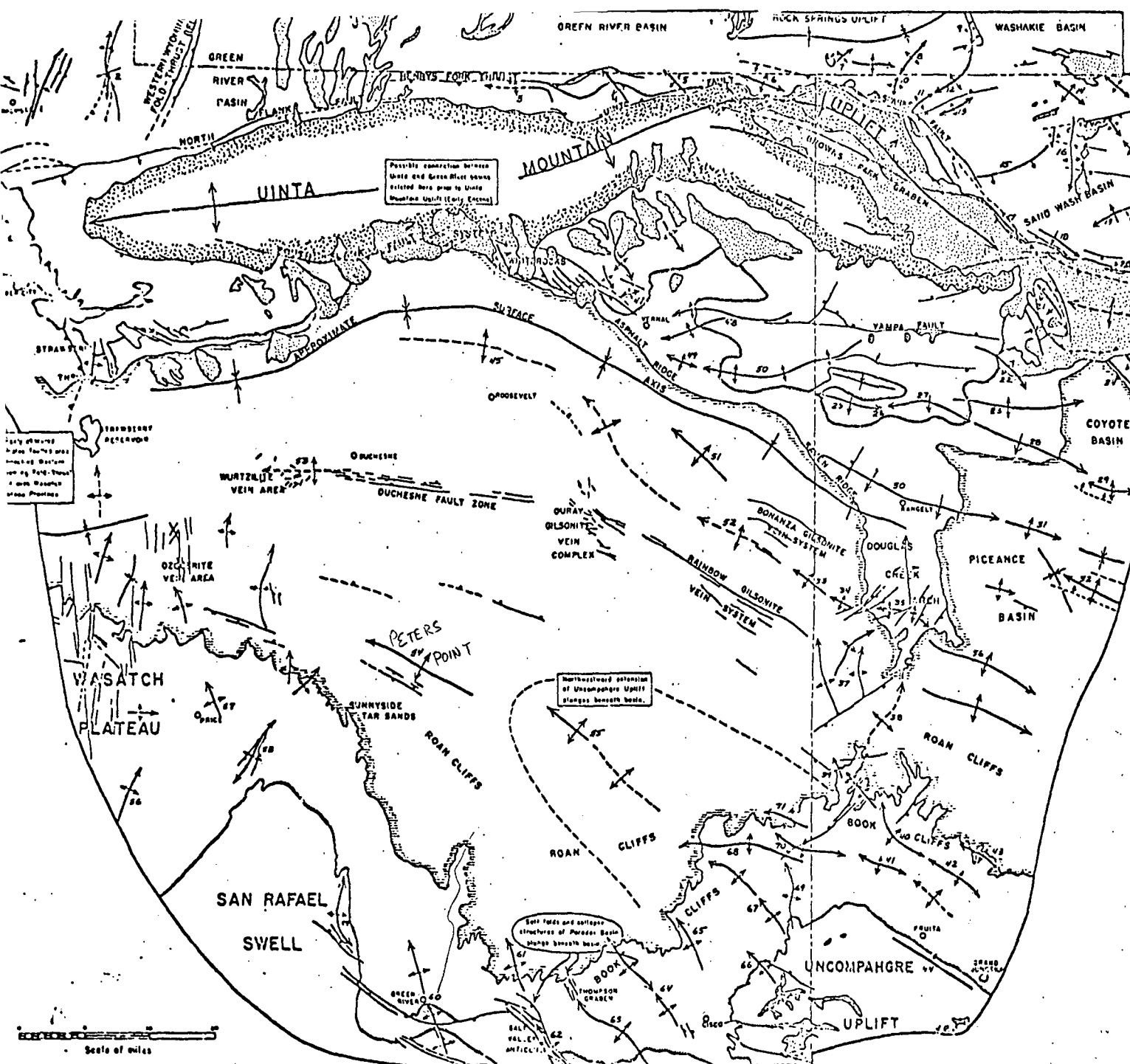
Yield: bwpd, barrels of water per day; gpm, gallons per minute; (E), estimated; (M), measured; (R), reported at time water sample was collected for chemical analysis.
 The (E), (M), or (R) is beside the given unit. The other unit is calculated on the basis of 1 gpm equals 34 bwpd and 1 bwpd equals 0.03 gpm.
 Method or point of collection: Flow, indicates collection at a spring or flowing well; DST, drill-stem test for oil or gas.
 Remarks: DST, drill-stem test data reported by oil or gas company.

| T | R | Section | Source | Operator or owner | Name or number | Producing formation | Depth to top of formation (feet) | Depth to bottom of formation (feet) | Interval sampled (feet) | Yield (bwpd/gpm) | Method or point of collection | Date of collection | Temperature (°F) | Parts per million | | | | | Sulfate (SO ₄) | Chloride (Cl) | Nitrate (NO ₃) | Dissolving solids | Hardness as CaCO ₃ | Noncarbonate hardness as CaCO ₃ | Percent sodium | Sodium-adsorption ratio (SAR) | Specific conductance (microhm/cm at 25°C) | Resistivity (ohm-meter at 68°F) | pH | Analysis by | Remarks | | |
|-----|-----|-------------|--------|---------------------------------|----------------|---------------------------------|----------------------------------|-------------------------------------|-------------------------|------------------|-------------------------------|--------------------|------------------|----------------------------|---------------|--------------|----------------|---------------------------------|----------------------------|---------------|----------------------------|-------------------|-------------------------------|--|----------------|-------------------------------|---|---------------------------------|------|-------------|---------|---|---|
| | | | | | | | | | | | | | | Silica (SiO ₂) | Iron (Fe) | Calcium (Ca) | Magnesium (Mg) | Bicarbonate (HCO ₃) | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | Sodium (Na) | Potassium (K) | Sulfur (S) | Phosphorus (P) | Fluorine (F) | | | | | | | | | | | | | | | |
| 43S | 4W | SESESESE 31 | W | F. Hamblin | 1 | Shinarump Mbr. of Chinle Fm. | 217 | 269 | 217-269 | See Remarks | Flow | 8-13-57 | 8.4 | 0.24 | 14 | 1.0 | 215 | 226 | 0 | 272 | 26 | 0.1 | 646 | 38 | 0 | 92 | 15 | 1,020 | - | 6.9 | GS | Reported yield on 7-17-56 was 450 gpm (15,300 bwpd). Analysis includes 0.8 ppm fluoride. | |
| 43S | 4W | NWSESESE 33 | W | Richard Von Hake | 1 | do | - | - | 28-79 | - | Pumped | 8-13-57 | - | .24 | 119 | 21 | 28 | 6 | 0 | 490 | 22 | .4 | 710 | 384 | 384 | 14 | .6 | 962 | - | 3.9 | GS | Analysis includes 0.5 ppm fluoride. | |
| 14S | 9E | SWNESESE 29 | O | Amerada Petroleum Co. | 1 | Ferron Ss. Mbr. of Mancos Sh. | 2,664 | 3,023 | At 2,756 | - | Flowline | 12- -62 | - | 0 | 320 | 24 | 19,978 | 488 | 144 | 40 | 30,956 | - | 51,950 | - | - | - | - | - | 0.14 | 7.0 | CL | Sample collected while drilling with air. | |
| 15S | 10E | C NESESE 26 | O | Shell Oil Co. | 1 | Tununk Sh. Mbr. of Mancos Sh. | 3,023 | 3,416 | At 3,054 | - | do | 12- -62 | - | 0 | 280 | 24 | 14,975 | 3,514 | 240 | 40 | 21,300 | - | 37,860 | - | - | - | - | - | .18 | 8.0 | CL | Do. | |
| 15S | 11E | NESESESE 12 | O | Carbon Dioxide and Chemical Co. | 2 | Mississippian sed. rocks | 8,950 | 10,763 | At 3,325 | - | DST 3 | 5-13-58 | - | - | 80 | 24 | 6,537 | 1,220 | 336 | 40 | 2,840 | - | 11,117 | - | - | - | - | - | .62 | 8.0 | CL | Do. | |
| 15S | 12E | SWSESESE 7 | O | Pan American Petroleum Corp. | 1 | Navajo Ss. | 3,095 | 3,114 | 10,058-10,165 | - | See Remarks | 1-21-39 | - | (5) | 874 | 61 | 422 | 3,070 | 0 | 2,825 | 11,600 | - | 3,607 | - | - | - | - | - | - | - | GS | Carbon dioxide well. Water sample bailed from hole at 2,320 feet under pressure by using temperature observation machine. | |
| 15S | 12E | SESESESE 8 | O | Shell Oil Co. | 1-A | Mississippian sed. rocks | 7,042 | 8,154 | 7,433-7,986 | - | DST 1 | 4- -63 | - | - | 1,144 | 311 | 10,956 | 2,269 | - | 8,400 | 13,100 | - | 35,778 | - | - | - | - | - | .26 | 7.3 | CGL | DST 1 recovered very cloudy water, dark brown organic filtrate. | |
| 15S | 12E | SESESESE 8 | O | Shell Oil Co. | 1-A | Redwall Ls. Elbert Fm. | 7,970 | 9,130 | 8,323-9,174 | - | DST 1-A | 8-18-59 | - | - | 3,496 | 716 | 21,583 | 2,147 | - | 2,346 | 38,571 | - | 67,769 | - | - | - | - | - | .12 | 7.2 | CGL | DST 1-A recovered 6,750 feet of slightly gassy, slightly muddy salt water with trace of oil and sulfurous odor. | |
| 15S | 12E | SESESESE 15 | W | Pure Oil Co. | 1-A | Mancos Sh. | 0 | 0 | 0-30 | - | - | 8- 8-58 | 11 | - | 481 | 502 | 743 | 486 | 0 | 3,530 | 305 | 466 | 6,280 | 3,260 | 2,870 | 39 | 5.7 | 6,580 | - | 7.5 | GS | Dug well, 30 feet deep. Analysis includes 0.2 ppm fluoride. | |
| 16S | 9E | SWNESESE 12 | O | Pure Oil Co. | 1-A | Redwall Ls. | 9,800 | 11,125 | 10,117-10,259 | - | DST 2 | 3- 9-62 | - | 3,013 | 3,680 | 462 | 22,050 | 3,221 | 0 | 1,640 | 42,600 | - | 73,653 | - | - | - | - | - | .14 | 6.5 | CL | DST 2 recovered 450 feet of heavy gas-cut mud (carbon dioxide) and 360 feet of salt water. | |
| 16S | 12E | C NESESE 1 | O | Cities Service Oil Co. | 1 | Sinbad Ls. Mbr. of Moenkopi Fm. | 4,014 | - | 4,014-83 | - | DST 3 | 1- -53 | - | - | - | - | - | - | - | - | 9,700 | - | - | - | - | - | - | - | - | - | (7) | DST 3 recovered 80 feet of slightly sulfur gas-cut mud, 90 feet of sulfur water-cut mud, and 450 feet of sulfur water. | |
| 16S | 12E | C NESESE 4 | O | Equity Oil Co. | 2 | Mississippian sed. rocks | 6,372 | - | 7,831-7,930 | - | DST 5 | 5- -53 | - | - | - | - | - | - | - | - | 44,000 | - | - | - | - | - | - | - | - | - | (7) | DST 5 recovered 270 feet of gas (carbon dioxide) and salt water-cut mud and 1,910 feet of gas-cut (carbon dioxide) salt water from Desert(?) Formation | |
| 16S | 12E | C NESESE 4 | O | Equity Oil Co. | 2 | Sinbad Ls. Mbr. of Moenkopi Fm. | 4,141 | - | 4,138-75 | - | - | 1- -53 | - | - | - | - | - | - | - | - | - | - | - | 29,200 | - | - | - | - | - | - | 6.5 | PL | Analysis includes 2,410 ppm magnesium as magnesium carbonate and 180 ppm free carbon dioxide. |
| 16S | 12E | C NESESE 4 | O | Equity Oil Co. | 2 | Sinbad Ls. Mbr. of Moenkopi Fm. | 4,141 | - | 4,138-75 | - | - | 1- -53 | - | - | - | - | - | - | - | - | - | - | - | 38,400 | - | - | - | - | - | - | 6.7 | PL | Analysis includes 2,680 ppm magnesium as magnesium carbonate and 210 ppm free carbon dioxide. |
| 16S | 12E | C NESESE 4 | O | Equity Oil Co. | 2 | Sinbad Ls. Mbr. of Moenkopi Fm. | 4,141 | - | 4,138-75 | - | - | 1- -53 | - | - | - | - | - | - | - | - | - | - | - | 51,320 | - | - | - | - | - | - | 6.4 | PL | Analysis includes 3,620 ppm magnesium as magnesium carbonate and 430 ppm free carbon dioxide. |
| 16S | 12E | C NESESE 27 | O | Carter Oil Co. | 1 | Coconino Ss. Madison Ls. | 3,975 | 4,830 | 4,442-58 | - | DST 2 | 1-14-57 | - | - | 1,355 | 377 | 4,749 | 2,490 | 0 | 642 | 8,900 | - | 17,249 | - | - | - | - | - | .40 | 7.9 | CGL | DST 2 recovered 30 feet of water-cut mud and 360 feet of water. | |
| 16S | 12E | C NESESE 27 | O | Carter Oil Co. | 1 | Coconino Ss. Madison Ls. | 6,585 | - | 6,998-7,133 | - | DST 5 | 2- -57 | - | - | 1,936 | 454 | 18,537 | 4,030 | 0 | 2,712 | 29,000 | - | 54,624 | - | - | - | - | - | .16 | 6.8 | CGL | DST 5 recovered 140 feet of mud and 840 feet of salt water. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (50 gpm) was produced from the Navajo Ss. below 1,784 feet. The analysis includes 10,000 ppm sodium chloride. | |
| 16S | 13E | SESESESE 21 | O | Reserve Oil and Gas Co. | 1 | Glen Canyon Gr. | 1,777 | 2,644 | At 2,400 | 3,680(R) | See Remarks | 5- -63 | - | - | 480 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | (8) | While drilling with air an estimated flow of 70 barrels of water per hour (| |

| T | R | Section | Location | Source | Operator or owner | Name or number | Producing formation | Depth to top of formation (feet) | Depth to bottom of formation (feet) | Interval sampled (feet) | Yield (bwpd/gpm) | Method or point of collection | Date of collection | Temperature (°F) | Parts per million | | | | | | | | | | Remarks | | | | | | | | | | | | |
|-----|-----|---------|-----------|--------|--------------------------------|----------------|---------------------------------------|----------------------------------|-------------------------------------|-------------------------|------------------|-------------------------------|--------------------|------------------|----------------------------|-----------|--------------|----------------|--------|-------|-------------|----------------------------|---------------|----------------------------|---------|------------------|-------------------------------|--|----------------|-------------------------------|---|--------------------------------|----|-------------|--|--|--|
| | | | | | | | | | | | | | | | Silica (SiO ₂) | Iron (Fe) | Calcium (Ca) | Magnesium (Mg) | Na + K | | Bicarbonate | Sulfate (SO ₄) | Chloride (Cl) | Nitrate (NO ₃) | | Dissolved solids | Hardness as CaCO ₃ | Noncarbonate hardness as CaCO ₃ | Percent sodium | Sodium-adsorption ratio (SAR) | Specific conductance (microhm/cm at 25°C) | Resistivity (ohmmeter at 68°F) | pH | Analysis by | | | |
| 225 | 16E | SEBWSW | 2 | O | Amerada Petroleum Co. | 1 | Paradox Fm. | 5,100 | - | At 5,250 | - | Flow | 10-48 | 16 | - | 68,459 | 9,090 | 55,950 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CTL | Analysis includes 1,891 ppm borate, 73 ppm hydroxide, and 76 ppm iron and aluminum oxide. | |
| 225 | 16E | NEBWSW | 2 | O | do | 2 | do | 5,054 | - | 5,792-5,896 | See Remarks | do | 7-49 | 10 | - | 76,176 | 9,484 | 58,301 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CTL | Analysis includes 2,362 ppm borate and 160 ppm iron and aluminum oxide. Flowed salt water at 1,000 to 5,000 bwpd (30 to 150 gpm) from July 3 to 17, 1949, from a depth of 5,792 to 5,896 feet. | |
| 225 | 17E | ESEBWS | 34 | O | Superior Oil Co. | 22-34 | Mississippian sed. rocks | 10,020 | - | 10,053-10,173 | - | DST 3 | 8-58 | - | - | 9,757 | 1,441 | 66,729 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | SO | DST 3 recovered 500 feet of muddy salt water and 2,670 feet of salt water. Analysis includes 0.0 ppm sulfide and 348 ppm iron and aluminum oxide. | | |
| 225 | 19E | NWSEBWS | 16 | O | Potash Co. of America | 1 | Morrison Fm. | 703 | 1,363 | 1,118-55 | - | Bailed | 8-12-43 | - | (5) | 329 | 175 | 4,913 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | | | |
| 225 | 22E | NWSEBWS | 33 | M | Cactus Rat Mine | | Salt Wash Ss. Mbr. of Morrison Fm. | 0 | - | - | 17 0.5(E) | - | 6-29-50 | 56 | 10 | 0.03 | 101 | 15 | 343 | 3.4 | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | Analysis includes 0.02 ppm boron, 0.3 ppm fluoride, and 0.00 ppm manganese. | | |
| 225 | 22E | SEBWSW | 33 | O | Utah Southern Oil Co. | 1 | Morrison Fm. | 0 | - | 298-319 | 70 2(E) | Pumped | 12-29-35 | - | - | - | - | 205 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | | | |
| | | | | | | | Chinle Fm. | 1,100 | - | 1,109-40 | 34 1(E) | Bailed | 11-18-35 | - | - | 474 | 137 | 6,993 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | | | |
| 235 | 10E | | 8 | S | - | | Cliff Dweller Spring | 0 | - | - | 34 1(E) | Flow | 10-31-58 | 7.5 | - | 127 | 112 | 39 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | Analysis includes 0.2 ppm fluoride. | | |
| 235 | 15E | CNEBWS | 21 | O | Shell Oil Co. | | Mississippian sed. rocks | 7,452 | - | 7,500-7,702 | - | DST 1 | 8-31-59 | - | - | 1,444 | 208 | 7,283 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | DST 1 recovered 3,240 feet (34 barrels) of salt water. | | |
| 235 | 16E | NEBWSW | 3 | O | Mobil Oil Co. | 12-3 | do | 8,355 | 9,042 | 8,530-8,715 | - | DST 1 | 8-61 | - | - | 9,588 | 1,265 | 55,921 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | DST 1 recovered 1,150 feet of mud-cut salt water and 7,000 feet of salt water. | | |
| 235 | 16E | NEBWSW | 15 | O | do | 34-15 | White Rim Ss. Mbr. of Cutler Fm. | 2,540 | 2,860 | See Remarks | See Remarks | Flow | 9-61 | - | - | 474 | 86 | 681 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | Estimated water flow of 200 gallons per hour (3 gpm or 100 bwpd) encountered while drilling between 2,530 and 2,570 feet. | | |
| | | | | | | | Mississippian sed. rocks | 8,028 | - | 8,210-8,440 | - | DST 1 | 10-61 | - | - | 5,092 | 2,916 | 65,021 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | DST 1 recovered 651 feet of mud and 6,929 feet of salt water. | | |
| 23E | 17E | CNEBWS | 15 | O | Pan American Petroleum Corp. | 1 | do | 8,422 | 8,988 | 8,678-8,766 | - | DST 3 | 3-61 | - | - | 3,469 | 752 | 84,656 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | DST 3 recovered 668 feet of heavy gas-cut mud, 704 feet of amber colored gas-cut emulsion, 1,858 feet of oil, and 610 feet of salt water. | | |
| 235 | 17E | CSEBWS | 17 | O | Texaco, Inc. | 1 | do | 8,458 | - | 8,732-38 | - | - | 12-62 | - | - | 6,302 | 1,002 | 56,175 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | | | |
| 235 | 17E | CNEBWS | 17 | O | do | 2 | do | 8,447 | - | 8,709-16 | - | Swab test | 12-62 | - | - | 5,781 | 1,453 | 56,854 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | | |
| 235 | 21E | SEBWSW | 27 | W | National Park Service | 1 | Wingate Ss. | 765 | - | 790-900 | 140 4(E) | Well head | 10-31-62 | 61 | 5.0 | 28 | 18 | 54 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | | | |
| 235 | 22E | NW | 6 | M | - | | Telluride No. 18 | 0 | - | - | See Remarks | Pumped | 6-29-50 | 50 | 11 | 14/20 | 89 | 20 | 129 | 6.1 | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | Water pumped from mine sump at rate of 300 gallons per day (0.2 gpm or 76 bwpd). Analysis includes 0.04 ppm boron, 0.4 ppm fluoride, and 0.00 ppm manganese. | | |
| 235 | 23E | | 8 | S | - | | Squaw Park Spring | 0 | - | - | 34 1(E) | Flow | 6-5-59 | 33 | - | 51 | 4.9 | 9.1 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | Analysis includes 0.10 ppm boron and 0.4 ppm fluoride. | | |
| 235 | 24E | NWSEBWS | 8 | S | - | | Dewey Bridge Spring | 0 | - | - | See Remarks | do | 4-24-59 | 56 | 10 | - | 13 | 2.4 | 147 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | | | |
| 24S | 10E | SEBWS | 4 | S | - | | Tan Seep | 0 | - | - | See Remarks | do | 10-30-58 | 44 | 11 | - | 257 | 224 | 88 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | | | |
| 24S | 13E | NWSEBWS | 2 | O | Superior Oil Co. | 23-2 | Shinarump Mbr. of Chinle Fm. | 1,527 | 1,562 | 1,527-47 | - | DST 1 | 8-58 | - | - | 76 | 89 | 275 | 4.0 | 270 | 526 | - | - | - | - | - | - | - | - | - | - | - | - | - | SO | DST 1 recovered 110 feet of 8.9 pound water-cut mud. Analysis includes 0.0 ppm sulfide and 90 ppm iron and aluminum oxide. | |
| | | | | | | | Moenkopi Fm. | 1,562 | 2,200 | 1,942-82 | - | DST 4 | 9-58 | - | - | 294 | 3.6 | 4,289 | 0 | 2,029 | 5,374 | - | - | - | - | - | - | - | - | - | - | - | - | - | SO | DST 4 recovered 280 feet of mud and 1,542 feet of black sulfur water. Analysis includes 0.0 ppm sulfide and 14 ppm iron and aluminum oxide. | |
| | | | | | | | do | 1,562 | 2,200 | 1,800-85 | 94(E) 2.8 | Pumped | 11-9-58 | - | - | 358 | 36 | 5,149 | 4.0 | 324 | 6,079 | - | - | - | - | - | - | - | - | - | - | - | - | - | SO | Well pumped at rate of 36 3/4 barrels of water in 1 1/2 hours. Analysis includes 5.0 ppm sulfide and 13 ppm iron and aluminum oxide. | |
| | | | | | | | Sinbad Ls. Mbr. of Moenkopi Fm. | 2,038 | - | 2,041-65 | - | DST 5 | 9-58 | - | - | 239 | 3.6 | 5,910 | 5.0 | 325 | 6,137 | - | - | - | - | - | - | - | - | - | - | - | - | - | SO | DST 5 recovered 85 feet of mud and 1,225 feet of black sulfur water. Analysis includes a trace of sulfide and 63 ppm iron and aluminum oxide. | |
| 24S | 13E | NW | 29 | S | - | | Red Rock Spring | 0 | - | - | 70 2(E) | Flow | 10-28-58 | 62 | 9.8 | 54 | 50 | 35 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | pH at point of collection was 7.5. Analysis includes 0.2 ppm fluoride. | | |
| 24S | 14E | NEBWSW | 21 | O | Carter Oil Co. | 1 | Moenkopi Fm. | 1,688 | 2,375 | 2,114-2,340 | - | DST 2 | 10-58 | - | .0 | 400 | 97 | 729 | 1.0 | 1,620 | 341 | - | - | - | - | - | - | - | - | - | - | - | - | - | CL | DST 2 recovered 180 feet of mud, 630 feet of mud-cut water, and 740 feet of brackish water. | |
| 24S | 16E | CSEBWS | 19 | O | Shell Oil Co. | 1 | Mississippian sed. rocks | 7,570 | 8,263 | 7,968-8,067 | - | DST 2 | 11-12-58 | - | - | 1,957 | 384 | 54,697 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | DST 2 recovered 6,900 feet (95.3 barrels) of salt water with hydrogen sulfide odor. | |
| 24S | 20E | SWNEBWS | 20 | S | - | | Courthouse Spring | 0 | - | - | - | - | 10-16-33 | - | .42 | 44 | 35 | 12 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | | |
| 24S | 22E | | 6 | S | - | | Turnbow Cabin Spring | 0 | - | - | 170 5(E) | - | 8-1-62 | - | 14/00 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | Spring is series of seeps in stream bed. Analysis includes 0.3 ppm fluoride. | |
| 24S | 24E | | 22 and 23 | S | - | | Onion Creek Spring | 0 | - | - | - | - | 9-27 | - | - | 965 | 132 | 4,490 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | | |
| 25S | 12E | SW | 14 | W | J. Marsing | | Temple Junction | - | - | - | - | - | 10-30-58 | 62 | 13 | 481 | 642 | 339 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | pH of water at point of collection was 7.0. Analysis includes 0.2 ppm fluoride. | | |
| 25S | 12E | SEBWSW | 34 | W | Bureau of Land Management | | Gilson Butte | 0 | 298 | See Remarks | See Remarks | - | 10-30-58 | 58 | 9.6 | 240 | 372 | 105 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | GS | Depth of well is 290 feet with casing perforated from 230 to 290 feet. Reported yield in March 1953 was 360 bwpd (11 gpm). pH of water at point of collection was 7.0. Analysis includes 1.4 ppm fluoride. | | |
| 25S | 15E | CNEBWS | 15 | O | Superior Oil Co. | 31-15 | Hermosa Gr. Ismay Zone of Paradox Fm. | 4,018 | 6,196 | 4,819-55 | - | DST 1 | 7-63 | - | .0 | 9,680 | 5,637 | 68,749 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CL | DST 1 recovered 290 feet of water. | |
| | | | | | | | do | 4,840 | 5,070 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 25S | 15E | CSEBWS | 22 | O | Continental Oil Co. | 2 | Hermosa Gr. Paradox Fm. | 3,283 | 5,916 | 4,345-67 | - | DST 6 | 6-58 | - | - | 801 | 460 | 7,192 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | DST 6 recovered 3,570 feet of mud-cut salt water and salt water. |
| | | | | | | | do | 4,955 | 5,916 | 4,950-5,062 | - | DST 2 | 6-58 | - | - | 876 | 444 | 7,183 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | DST 2 recovered 60 feet of mud-cut sulfur water and 750 feet of slightly gas-cut sulfur water. Sample was clear reddish-brown water from lower part of column. |
| | | | | | | | Mississippian sed. rocks | 5,916 | - | 6,085-6,220 | - | DST 5 | 7-58 | - | - | 1,382 | 234 | 9,689 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | DST 5 recovered 5,460 feet of mud-cut sulfur water and sulfur water. Sample was clear water. | |
| 25S | 15E | NWSEBWS | 32 | W | Standard Oil Co. of California | 1 | Navajo Ss. | 250 | - | 680-720 | - | Pumped | 7-11-56 | - | - | 125 | 86 | 28 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | Well is 720 feet deep and perforated from 680 to 720 feet. Reported depth to water was 650 feet in 1956. | |
| 25S | 16E | CNEBWS | 10 | O | Shell Oil Co. | 2 | Mississippian sed. rocks | 6,707 | 7,365 | 6,898-7,092 | - | DST 1 | 3-2-59 | - | - | 2,227 | 750 | 4,251 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | CG | DST 1 recovered 1,470 feet of muddy salt water and 4,395 feet of salt water. |
| 25S | 16E | CSEBWS | 29 | O | Standard Oil Co. of California | 1 | do | 6,359 | - | 6,480-6,594 | - | DST 3 | 10-21-57 | - | - | 1,623 | 41 | 13,742 | - | - | | | | | | | | | | | | | | | | | |

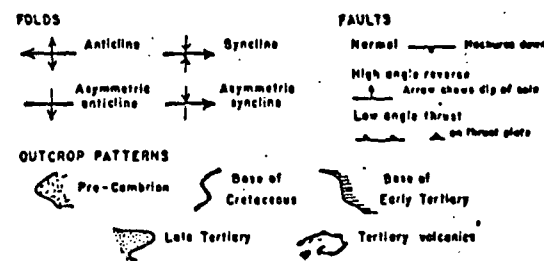
Table 3. — Continued

| Location | | | Source | Operator or owner | Name or number | Producing formation | Depth to top of formation | Remarks |
|----------|-----|------------------|--------|----------------------------------|--------------------|----------------------------------|---------------------------|--|
| T | R | Section | | | | | | |
| 255 | 19E | C NW 1/4 S 27 | 0 | Pure Oil Co. | 5 | Mississippian sed. rocks | 7,39 | 240 feet of slightly salty black sulfur water. |
| 255 | 20E | 4 S | 0 | - | Seeping Spring | Wingate Ss. | | |
| 255 | 21E | SE 1/4 NE 1/4 20 | W | National Park Service | 2 | Navajo Ss. | | |
| 255 | 21E | SE 1/4 26 | S | - | Moab Bridge Spring | Wingate Ss. | | |
| 255 | 21E | NE 1/4 NE 1/4 35 | S | D. Patriot | - | do | | |
| 255 | 21E | SW 1/4 SE 1/4 36 | S | M. R. Fish | - | do | | ed by a tunnel that was driven 116 feet into sandstone. |
| 255 | 23E | NE 1/4 NE 1/4 8 | W | A. Sarten | - | Cutler Fm. | | 0.06 ppm boron, 0.2 ppm fluoride, and 0.00 ppm manganese. |
| 265 | 7E | C NW 1/4 19 | 0 | Shell Oil Co. | 1 | Mississippian sed. rocks | 5,0 | 2.0 ppm ammonium and 2 ppm boron. DST 3 recovered 3,890 feet (54 |
| | | | | | | Devonian sed. rocks | 6,2 | -cut mud, mud-cut sulfurous water, and sulfurous water with ppm sodium chloride. |
| | | | | | | Cambrian sed. rocks | 6,0 | 1 ppm ammonium and 1 ppm boron. DST 2 recovered 4,540 feet (60 |
| 265 | 7E | C NE 1/4 20 | 0 | Shumway Uranium Mining Corp. | 1 | Navajo Ss. | 1,1 | cut water with a salinity of 1,320 ppm sodium chloride. |
| | | | | | | Wingate Ss. | 1,1 | 235 ppm of alkalinity as calcium carbonate. |
| | | | | | | Chinle Fm. | 1,1 | 1,875 ppm of alkalinity as calcium carbonate. |
| 265 | 13E | NW 1/4 SW 1/4 19 | W | - | Jeffery Well | Entrada(?) Ss. | 1,1 | 410 ppm of alkalinity as calcium carbonate. |
| | | | | | | | 1,1 | 50.9 ppm fluoride. |
| 265 | 14E | C NW 1/4 7 | 0 | Odessa Natural Gas Co. | 1 | Mississippian sed. rocks | 5,1 | 0 feet of mud-cut sulfur water and 2,595 feet of sulfur water. |
| 265 | 14E | C SW 1/4 30 | 0 | Humble Oil and Refining Co. | 7 | do | 5,1 | 528 feet of slightly mud-cut water. |
| 265 | 17E | SW 1/4 SW 1/4 5 | 0 | Superior Oil Co. | 14-5 | do | 6,1 | Gas immediately increasing to strong in 2 minutes, fluid to |
| | | | | | | | 6,1 | 65--90 percent water, 10 percent mud and asphaltic residue. |
| | | | | | | | 6,1 | changed to small spray of sulfur water. |
| | | | | | | | 6,1 | 0 feet of water. |
| | | | | | | | 6,1 | Gas immediately increasing through test. Fluid to surface in |
| 265 | 18E | S 1/4 SE 1/4 7 | 0 | Pure Oil Co. | 1 | do | 6,1 | 340 feet of sulfur water; sample from bottom of fluid column. |
| 265 | 20E | SE 1/4 NE 1/4 9 | 0 | Southern Natural Gas Co. | 1 | See Remarks | 7,1 | and middle of fluid column contained 39,876 and 22,242 ppm of |
| | | | | | | | 7,1 | respectively. |
| | | | | | | | 7,1 | 0 feet of muddy water and 5,600 feet of slightly salty sulfur |
| | | | | | | | 7,1 | reported to be "Cane Creek Member" of Paradox Formation. |
| 265 | 22E | NW 1/4 SW 1/4 15 | S | J. Westwood | - | Navajo Ss. | | 0.07 ppm boron and 0.1 ppm fluoride. |
| 275 | 11E | NE 1/4 SE 1/4 34 | W | Civil Aeronautics Administration | 1 | Carmel Fm. | | 18-46 was 17 gpm (580 bwpd). |
| 275 | 11E | NW 1/4 SE 1/4 34 | W | do | 1 | do | | |
| 275 | 12E | SW 1/4 NE 1/4 9 | 0 | Carter Oil Co. | 1 | Mississippian sed. rocks | 5,1 | feet of water-cut mud and 4,920 feet of slightly brackish water. |
| 275 | 13E | NE 1/4 4 | W | Bureau of Land Management | 91 | Entrada Ss. | | 5 to depth of 795 feet, cased to 456 feet; depth of water in |
| | | | | | | | 7,1 | 720 feet. |
| 275 | 13E | C NW 1/4 30 | 0 | Superior Oil Co. | 31-30 | Mississippian sed. rocks | 6,1 | feet of mud and water-cut water and 5,000 feet of brackish |
| 275 | 13E | C SE 1/4 36 | 0 | Continental Oil Co. | 1 | do | 6,1 | feet of salty sulfur water. |
| 275 | 14E | NE 1/4 NE 1/4 5 | W | G. H. Franz | 1 | Navajo Ss. | | 0.5 ppm fluoride. |
| 275 | 14E | NE 1/4 NW 1/4 5 | 0 | Carter Oil Co. | 1 | Mossback Mbr. of Chinle Fm. | | 142 feet in Chinle Formation; however, Mossback Member of Chinle |
| | | | | | | | | bed producing formation. DST 1 recovered 510 feet of mud-cut |
| 275 | 14E | C SW 1/4 17 | 0 | Amerada Petroleum Corp. | 5 | White Rim Ss. Mbr. of Cutler Fm. | | 55 feet of muddy fresh water. |
| 275 | 15E | C SE 1/4 32 | 0 | Texaco, Inc. | 6 | Coconino Ss. | | from 2,330 feet in Moenkopi Formation to 2,366 feet in Coconino |
| | | | | | | | | the latter formation was the reported producing formation. |
| | | | | | | | | 50 feet of muddy fresh water. |
| | | | | | | | | 100 feet of water and 100 feet of mud. |
| 275 | 15E | C SW 1/4 35 | 0 | Carter Oil Co. | 2 | do | | feet of drilling fluid and 3,085 feet of brackish water with |
| | | | | | | | | last 290 feet. |
| 275 | 16E | NW 1/4 NE 1/4 33 | 0 | Superior Oil Co. | 32-33 | do | | feet of brackish muddy water and 3,653 feet of brackish water. |
| | | | | | | | | end middle of recovery column contained 203,592 and 72,949 ppm of |
| | | | | | | | | respectively. |
| 275 | 18E | NE 1/4 NE 1/4 26 | 0 | Husky Oil Co. | 1 | do | | From 6,260 feet in Pennsylvanian rock to 6,400 feet in |
| | | | | | | | | however, the latter rock was the reported producing formation. |
| 275 | 21E | SW 1/4 SW 1/4 3 | 0 | Humble Oil and Refining Co. | 3 | do | | 27 feet of black salty sulfur water. |
| | | | | | | | | feet of slightly gas-cut drilling mud, 270 feet of highly water- |
| | | | | | | | | and 4,980 feet of salt water with sulfur odor; sampled just above |
| 275 | 22E | NW 1/4 SE 1/4 17 | 0 | do | 1 | do | | 11 feet of black salty sulfur water: |



- NUMERICAL KEY TO STRUCTURAL FEATURES**
(Anticlines and domes unless otherwise indicated)
- | | | |
|------------------------|-----------------------|---|
| 1 Coalville | 24 Grand Highback | 48 Split Mountain |
| 2 Percupine Mountain | Manoche | 49 Ashley Valley |
| 3 Ladyspole | 25 Willow Creek | 50 Section Ridge |
| 4 Linwood | 26 Blue Mountain | 51 Red Wash |
| 5 Spring Creek | 27 Skull Creek | 52 Chapin Walls |
| 6 (Duch John) | 28 Massadonna | 53 Ducheno |
| 6 Clay Basin | 29 White River | 54 Peters Point |
| 7 Middle Mountain | 30 Bangaly | 55 Hill Creek |
| 8 Canyon Creek | 31 Yellow Creek | 56 Huntington |
| 9 Altus Creek | 32 Piceance | 57 Price |
| 10 Haymower | 33 Hill Hole | 58 Farnham |
| 11 Sugarloaf | 34 West Douglas Creek | 59 Woodside |
| 12 Houghton | 35 Douglas Creek | 60 Green River |
| 13 Skull Creek | 36 East Douglas Creek | 61 Northwest Salt Valley |
| 14 Powder Wash | 37 Urado | 62 Salt Valley |
| 15 Sand Wash Monocline | 38 Twin Buttes | 63 Thompson |
| 16 Yallowast | 39 Carbonera | 64 Circa |
| 17 Dry Mountain | 40 Garmosa | 65 Cottonwood Creek |
| 18 Two Bar | 41 Highline Canal | 66-67-68-69-70-71-72-73-74-75-76-77-78-79-80-81-82-83-84-85-86-87-88-89-90-91-92-93-94-95-96-97-98-99-100 |
| 19 Mine Mile Hill | 42 Ashby Creek | |
| 20 Maybell Monocline | 43 Hunter Canyon | |
| 21 Cross Mountain | 44 Hunter Monocline | |
| 22 Ill Springs | 45 Roswell | |
| 23 Pinyon Ridge | 46 Whitetracks | |
| (Coyote Basin) | 47 Neal | |

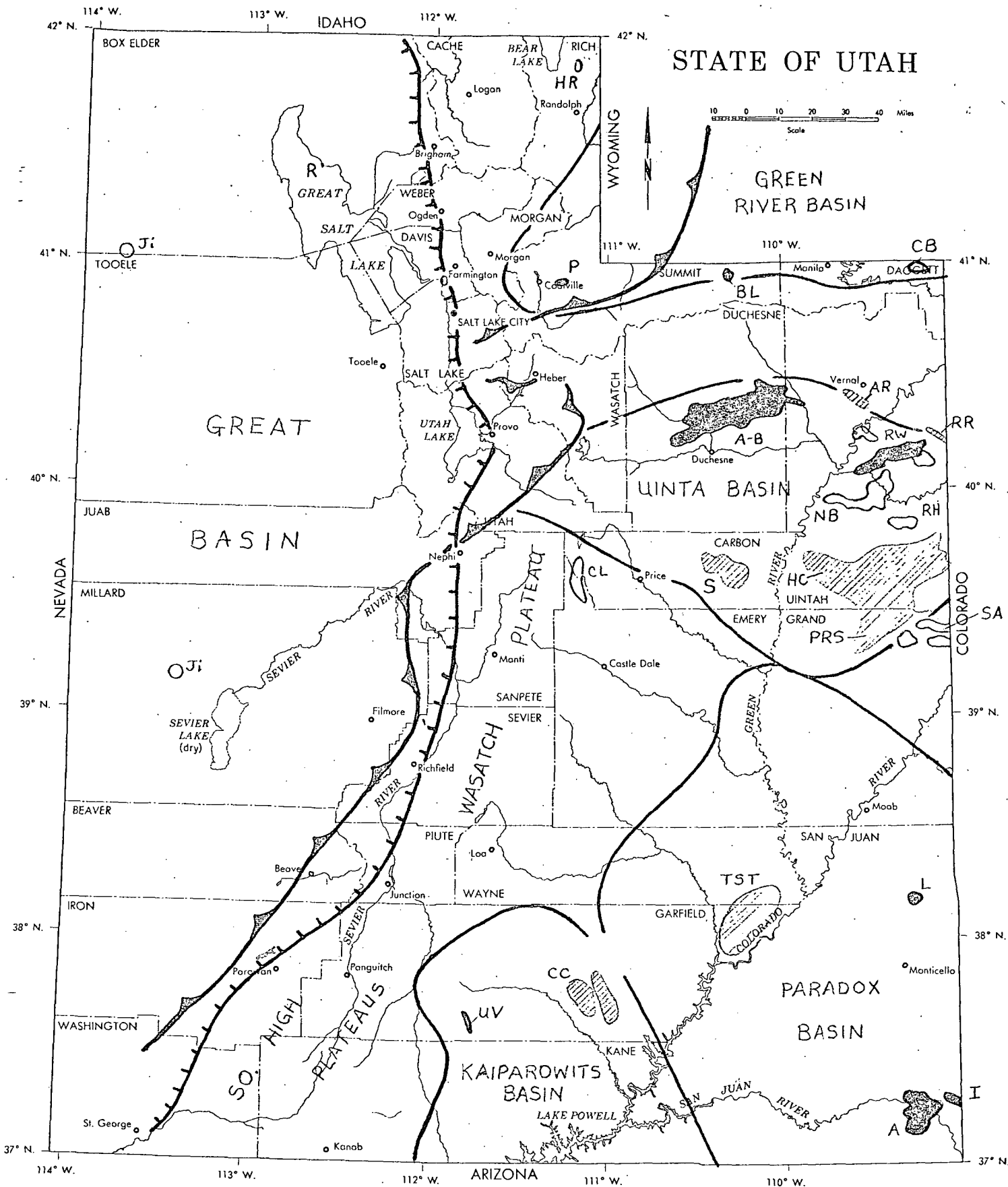
- ALPHABETICAL KEY TO STRUCTURAL FEATURES**
(Anticlines and domes unless otherwise indicated)
- | | | |
|-----------------------------|--------------------------------|--------------------------|
| Ahali Creek 9 | Green River 60 | Burgaly 30 |
| Ashby Creek 42 | Harley 47 | Red Wash 51 |
| Ashley Valley 49 | Haymower 10 | Roswell 45 |
| Bar 30 | Hells Hole 33 | Salt Valley 62 |
| Bitter Creek 49 | Hiawatha 12 | San Arroyo 71 |
| Blue Mountain 36 | Highline Canal 41 | Sand Wash Monocline 13 |
| Canyon Creek 8 | Hill Creek 55 | Section Ridge 50 |
| Carbonera 39 | Hunter Canyon 43 | Seiber 60 |
| Chapin Walls 52 | Huntington 36 | Shell Creek 13 |
| Circa 64 | Linwood 4 | Skull Creek 37 |
| Cottonwood Creek 63 | Ladyspole 3 | Split Mountain 41 |
| Cross Mountain 21 | Coalville 1 | Spring Creek (Duch John) |
| Douglas Creek 33 | Cottonwood Creek 63 | Sugarloaf 11 |
| Dry Mountain 17 | Ducheno 33 | Thompson 63 |
| Ducheno 33 | East Douglas Creek 36 | Twin Buttes 38 |
| East Douglas Creek 36 | Ill Springs 22 | Two Bar 18 |
| Farnham 58 | Fruite Ridge (Coyote Basin) 23 | Urado 37 |
| Fruite Monocline 44 | Garmosa 40 | West Douglas Creek 34 |
| Garmosa 40 | Grand Highback Monocline 24 | Peters Point 54 |
| Grand Highback Monocline 24 | | Westmore Creek 48 |
| | | White River 79 |
| | | Whitetracks 46 |
| | | Willow Creek 25 |
| | | Woodside 59 |
| | | Yallowast 16 |
| | | Yellow Creek 31 |



TECTONIC MAP
UINTA BASIN, NORTHEAST UTAH
AND ADJOINING PORTIONS OF NORTHWEST COLORADO
AND SOUTHWEST WYOMING
 PREPARED FROM ALL AVAILABLE SOURCES
 FOR I.A.P.G. GUIDEBOOK, JUNE 1937






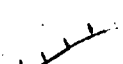
HOWARD R. RITZMA
 CONSULTING GEOLOGIST

DENVER, COLORADO
 MAY 1, 1957



J. A. CAMPBELL 1977

STRUCTURAL PROVINCES OF UTAH
WITH MAJOR PETROLEUM ACCUMULATIONS

-  OIL FIELD
-  GAS FIELD
-  OIL-IMPREGNATED ROCK DEPOSIT
-  APPROXIMATE STRUCTURAL BOUNDARY
-  EASTERN LIMIT OF THE FOLD AND THRUST BELT
-  EASTERN LIMIT OF THE BASIN-RANGE PROVINCE

OIL AND GAS FIELDS

A Aneth
A-B Altamont
BL Bridger Lake
CB Clay Basin
CL Clear Creek
I Ismay
L Lisbon
NB Natural Buttes
P Pineview
R Rozel
RW Red Wash
SA San Arroyo
UV Upper Valley

OIL-IMPREGNATED ROCKS

AR Asphalt Ridge
CC Circle Cliffs
HC Hill Creek
PRS P.R. Spring
RR Raven Ridge
S Sunnyside
TST Tar Sand Triangle

FROM

HOOD, JAMES W., 1976,

CHARACTERISTICS OF
AQUIFERS IN THE NORTHERN
UINTA BASIN AREA, UTAH
AND COLORADO:

STATE OF UTAH DEPT. OF
NATURAL RESOURCES,
TECHNICAL PUB. No. 53,
71 pages

Table 1.--Description of major lithologic units that crop out in the northern Uinta Basin area

[Location of data sites cited are shown on plate 1. Interpretations of chemical quality of water are based on analyses given in Hood, Mundorff, and Price (1976).]

| Stratigraphic System | Geologic unit | | Character of material | Hydrologic characteristics |
|----------------------|--|--------------------------|--|--|
| | Western part of basin | Eastern part of basin | | |
| Holocene | Younger alluvium, gravel surfaces, landslide and talus deposits, and dune sand and wind-blown deposits | | Surficial deposits of clay, silt, sand, gravel, and large angular blocks. Along stream valleys, younger alluvium is often well sorted, but rarely is more than about 15 ft (4.6 m) thick. Gravel surfaces are the upper parts of terrace deposits and appear in many places to be separated from deeper older gravels by a layer of clay or material of low permeability and are generally less than 10-20 ft (3.0-6.1 m) thick. Landslide and talus deposits found only in higher mountain areas; largest landslides are associated with outcrop areas of the Manning Canyon(?) Formation and consist of a chaotic mixture of soils, shale flowage, blocks of rocks, and other materials of indeterminate thickness. Talus deposits are accumulations of angular blocks at the base of cliffs and steep slopes. Dune sand generally is a well-sorted thin veneer that accumulates near sandstone outcrops. | Low to very high permeability. In many areas these deposits are above the water table; but in stream valleys and on some terraces, the younger alluvium is part of the deposits that yield water to shallow wells (dug wells in particular) and are less permeable than the underlying glacial outwash. Landslide deposits, because of poor sorting, have low permeability but locally yield water to springs. Talus deposits generally are above the water table but are good recharge areas for other formations. Dune sand also is a good recharge medium but only locally stores ground water. Chemical quality of water in most of these deposits is variable, depending on the sources of debris making up the deposit. In most areas, the water is fresh, but where the water table is shallow the water may be saline. |
| | Terrace deposits | | Alluvial deposits ranging in grain size from silt to boulders 1 ft (0.3 m) or more in diameter. Generally are part of caps of upland areas (fig. 4), locally called benches. Locally cemented; lie partly upon and also grade laterally from deposits of glacial origin. For purposes of hydrologic discussion in this report these deposits are lumped with glacial deposits and other coarse-grained unconsolidated deposits. | Low to very high permeability. Sources of much of the water yielded by shallow wells on benches around Roosevelt-Hyton-Duchesne part of basin. The water generally is fresh. |
| Quaternary | Glacial deposits and alluvium | | Glacial outwash, moraines, and undifferentiated deposits of glacial origin (include glaciated ground). Outwash is generally coarse grained (fig. 5), and consists of sand, gravel, cobbles, and boulders that underlie and grade into terrace deposits in upland areas. Thickness ranges from a few feet on edges of terraces to about 200 ft (60 m) near the mouths of major river canyons. These deposits and terrace deposits are discontinuous with those on adjacent benches and stream valleys (fig. 6). Beneath stream valleys, outwash forms the basal section of the unconsolidated valley fill; thicknesses there rarely exceed 50 ft (15 m). Other glacial deposits are found mainly in canyons (fig. 7), or on the mountains, where they are generally poorly sorted veneers on glaciated rock surfaces. | Low to very high permeability. Glacial outwash and related coarse-grained deposits comprise the most prolific aquifer in the northern Uinta Basin area in localities where the outwash is sufficiently thick to store and transmit water. Water is generally under unconfined conditions but locally may be confined or partly confined. It comprises the main aquifer in Ashley Valley, on upland slopes and outwash plains (as around Neola and Altamont), beneath the flood plains of the streams (such as the Duchesne and Uinta Rivers), and beneath the floors of the mountain canyons (near their mouths). Values for <i>K</i> are estimated to be in the range of 2 to 1,800 ft/d (0.61 to 550 m/d) (table 6). Wells near Neola yield as much as 3 ft ³ /s (0.0085 m ³ /s). The water in the outwash is fresh except where the outwash receives inflow from older rocks, as in the Duchesne River valley below Bridgeland. The other glacial deposits have lower permeability, but locally their permeability may approach that of the outwash. These less-permeable deposits generally act as a recharge medium, but locally they yield some water to springs and act as a transfer medium for water from underlying older rocks. The water in these other glacial deposits generally is fresh. |
| | Older terrace deposits | | Similar to overlying terrace deposits and lumped for hydrologic discussion with the other coarse-grained deposits. Position in section here based on old gravel surfaces given in Stokes (1964) | |
| CENOZOIC | Pliocene(?) | Browns Park Formation | Includes both rocks of the type present in far northeastern Utah and those sometimes referred to the Bishop Conglomerate (Kinney, 1951). Extremely variable deposits of sandstone, tuffaceous rocks, and conglomerate; present in irregular areas along south flank of Uinta Mountains. Thickness is less than 1 to about 800 ft (0.3 to 240 m). | Very low to moderate permeability. Not thoroughly explored by water-well drilling. Yields small quantities of freshwater to springs and stock wells in Brush Creek-Diamond Mountain area north and northeast of Vernal. Probable source of some springs in slopes of central Uinta Mountains. |
| | | Extrusive igneous rock | Chiefly andesitic pyroclastics. May be the Keetley Volcanics, or equivalent. Erosional remnants on highest hills near Wolf Creek Pass. Thickness unknown, but estimated to be generally less than 100 ft (30 m) in study area. | Yields water to some small springs. Baker (1970, table 1) estimated transmissivity to be 270 ft ² /d (25 m ² /d) for area to west, where formation is thicker; there, also, he states most springs were observed along fractures or contacts. |
| Tertiary | Oligocene(?) | Duchesne River Formation | Shale, mainly red, but including green and other pale colors, siltstone, sandstone, and conglomerate, unconformably underlying younger rocks from near the Colorado State line to near Strawberry Reservoir. (See Warner, 1966, and Andersen and Picard, 1972, for most recent descriptions). Coarsest grain sizes (fig. 8) found near basin margins where the formation interfingers with other formations. In central part of basin, formation grades up from underlying Uinta Formation and consists of interbedded sandstone and shale (fig. 9). Sandstone most abundant in lower part and, with conglomerate, in upper part. Sandstones are of two basic types--a light-colored (generally yellow) channel deposit (fig. 10) and a darker, more compact, better cemented interchannel(?) lenticular deposit. A few thin beds of sandstone are loose to friable. Formation in most areas is slightly to strongly fractured. Fractures locally contain secondary deposits of calcium sulfate, as near the Roosevelt-Bluebell road east of Dry Gulch. Maximum thickness is more than 3,000 ft (910 m). | Very low to very high permeability. The horizontal hydraulic conductivity of 19 sandstone samples ranged from 0.000033 to 3.28 ft/d (0.00001 to 1.0 m/d) (table 3). Total porosity ranged from 7 to 32 percent. However aquifer permeability is enhanced by fracturing, and yields to wells and springs range from less than 1 to more than 300 gal/min (0.06-19 l/s), generally with large drawdown (table 6). Highest permeabilities generally are near edges of outcrops west of Roosevelt in the central basin, and lowest are in areas north and east of Fort Duchesne. Water movement may be impeded locally by gilsonite dikes. Near recharge areas, and where the formation is fractured or moderately permeable, the water generally is fresh. At greater depths where the formation is of very low permeability, the water is slightly saline to briny. Confined conditions are common; in the lower parts of the basin such as near Roosevelt) in artesian heads may exceed 100 ft (30 m) above land surface, but in higher areas of the basin, water levels are below land surface. |
| | | Uinta Formation | Calcareous shale, some limestone, claystone, siltstone, and sandstone. Fluvial facies in eastern and western ends of basin interfinger with rocks similar in appearance to Duchesne River Formation and with other formations. Grades laterally into thinner bedded calcareous lake deposits in center of basin (Jones, 1957, p. 32). Maximum thickness is nearly 4,000 ft (1,220 m) near center of basin axis. | Very low to very high permeability. Highest primary permeability of the sandstone seems to approximate that of the median for sandstone in the Duchesne River Formation (table 3). Bulk of formation, however, is finer grained than the Duchesne River Formation. Permeability is enhanced by fracturing (fig. 11), which is evident in many areas; for example, Stinking Spring area along Strawberry River in secs. 14 and 15, T. 4 S., R. 7 W., Uintah meridian, where the Uinta Formation discharges water from the underlying Green River Formation. In most of the area, the formation yields only a few gallons per minute of saline water to wells |

Table 1.--Description of major lithologic units that crop out in the northern Uinta Basin area--Continued

| Erethm System | Geologic unit | | Character of material | Hydrologic characteristics | | |
|---------------|---|--|---|--|---|--|
| | Western part of basin | Eastern part of basin | | | | |
| MESOZOIC | Jurassic | Entrada Sandstone (Preuss Sandstone of Stokes, 1964) | Entrada Sandstone | In the west, 700-800 ft (213-244 m) of silty and sandy shale, thin-bedded, nonresistant siltstone, and fine- to medium-grained sandstone, with lenticular beds of white sandstone in upper part. Mostly red-colored. Redbeds appear to grade eastward into white sandstone. Section thins eastward, and in eastern part of basin consists of 100-160 ft (30-49 m) of massive crossbedded, fine- to medium-grained friable sandstone. Probably strongly fractured in areas of faulting and sharp folding. | Low to moderate permeability. Yields water to wells and springs in eastern end of basin. Yields freshwater of calcium bicarbonate type to wells and springs near Dinosaur National Monument bone quarry in eastern part of basin. Two samples from oil tests show the formation contains fresh to slightly saline calcium bicarbonate water 2,000-2,300 ft (610-701 m) below the Ashley Valley oil-field area. Chemical quality of water elsewhere in the northern Uinta Basin area unknown, but it could be expected to be good in and near outcrop areas. | |
| | | Twin Creek Limestone | Carmel Formation | In western part of Uinta Basin, section consists of 700-800 ft (213-244 m) of limestone, shale, and sandy shale with a few redbeds near top; section thins eastward in center of basin and includes gypsum and more redbeds. Near Vernal, section is 125-170 ft (38-52 m) of limy shale, siltstone, and fine-grained silty sandstone. The formation thins eastward. | Very low to moderate permeability. Limestone should have very low permeability where undisturbed and moderate to high permeability where fractured. The water should be saline where deeply buried and where gypsum is present. | |
| | Triassic(?) and Jurassic(?) | Upper Triassic(?) | Nugget Sandstone | Glen Canyon Sandstone (formerly called Navajo Sandstone in this area) | In the west, formation is about 1,100 ft (335 m) of light-orange fine- to medium-grained sandstone; massive with large-scale crossbedding, and generally is friable in the outcrop. Thickens eastward slightly and an increasing part of section becomes white. In eastern part of basin, section thins to 700 to about 900 ft (213-274 m) of white to gray, massive, crossbedded sandstone, generally friable at the outcrop. Some cliff outcrops have near-surface "case-hardening" and a desert varnish on surface. Strongly jointed at places, fractured where flexed and, on basis of a well in Dry Fork canyon, probably strongly fractured. | Very low to moderate permeability. Samples give <i>K</i> values ranging from 0.002 to 1.44 ft/d (0.00061 to 0.44 m/d) with total porosity above 20 percent. Yields water to wells and springs in eastern part of basin north of Lapoint, near Vernal, and eastward into northwestern Colorado. Water probably is confined in most areas. At and near outcrop, water is a fresh calcium bicarbonate type. Deeper within basin, water at a depth of about 6,000 ft (1,830 m) in well (D-4-21)16ccc-1 was a slightly saline sodium sulfate type; and in well (D-9-20)22cbb-1, near Ouray, a drill-stem sample was a briny sodium chloride type at 17,350 ft (5,290 m). |
| | | | Chinle Formation | | In the west, 300-380 ft (91-116 m) of variegated mudstone and siltstone, mainly thin-bedded. Appears to thicken toward center of basin and to thin toward east near Vernal, where it consists of about 260 ft (79 m) of variegated shale with the upper one-third red ripple-marked sandstone and thin beds of red shale. Contains a basal conglomerate member (see below). | Very low to low permeability. Probably yields only small quantities of saline water. |
| | Upper Triassic | | Gartra Grit Member of Chinle Formation (formerly called Shinarump Conglomerate) | | In west, consists of a few feet to about 40 ft (12 m) of massive, crossbedded, coarse-grained arkosic sandstone and conglomerate. Thickens slightly toward middle of basin and then thins toward the east, where it consists of from less than 1 in to 60 ft (2.5 cm to 18 m) of crossbedded, medium- to coarse-grained sandstone with streaks of quartzite pebbles. Locally, occupies channels cut 20-25 ft (6.1-7.6 m) into the underlying Moenkopi Formation. | Low to moderate permeability. Largest yields to wells probably would be where it is thickest and fractured. Wells have modest yields of calcium bicarbonate and sodium bicarbonate sulfate-type waters |
| | | Middle(?) Triassic | Mahogany Formation (Ankareh Formation of Stokes, 1964) | | The Mahogany Formation consists of red to purple thin-bedded shale and siltstone. Thickness is about 700 ft (213 m). Partly equivalent to the Moenkopi Formation. | Low permeability. Little known about aquifer properties, but the formation probably will yield small quantities of saline water to wells. |
| | Thaynes Formation (or Group) | | | Upper member of the Thaynes Formation is 350-400 ft (107-122 m) of partly variegated shale and siltstone. Lower member is 75-200 ft (23-60 m) of fine-grained silty sandstone interbedded with thin-bedded limestone. Gypsum veins and salt casts are present locally. Lower member thickens westward. Partly equivalent to the Moenkopi Formation. | Do. | |
| | Woodside Formation (Woodside Shale of Stokes, 1964) | | | The Woodside Formation consists of thin-bedded red-brown siltstone and shale. Thickness is 700-1,000 ft (213-305 m) and thins westward across upper Duchesne River area. Partly equivalent to the Moenkopi Formation. | Low permeability. Little known about aquifer, but yields may be enhanced by fracturing. Spring U(B-1-8)27cda-S1 yields freshwater of the calcium bicarbonate type. | |
| | Lower Triassic | | Moenkopi Formation | | The Moenkopi Formation is the eastern facies of the three formations listed above. Near Vernal, section consists of about 175 ft (53 m) of thin-bedded siltstone and very fine grained sandstone, overlain by 570 ft (174 m) of thin-bedded red shale, red siltstone, and fine-grained sandstone. A few thin beds of gypsum in a narrow stratigraphic zone near the middle of the section appear to be the local facies equivalent of the Thaynes Formation. The lower light-colored part of the Moenkopi is gradational with the underlying Park City Formation and appears to thicken eastward. Total thickness is about 700 to about 1,100 ft (213-335 m). | Very low to low permeability. Most water from the formation probably would be saline. |
| | | Paleozoic | Permian | Park City Formation (or Group)--partly(?) equivalent to Phosphoria Formation | | In western part of the Uinta Basin, consists of three members. Lower member is about 270 ft (82 m) of brecciated, very fine grained, friable, porous sandstone and dolomitic, locally brecciated, silty to sandy thin-bedded sandstone. The middle member is about 40 ft (12 m) of black phosphatic shale interbedded with gray shale and thin bedded limestone. The upper member is 100-150 ft (30-46 m) of thin-bedded to massive, silty and sandy, cherty, dolomitic limestone. Total thickness is 400-425 ft (122-130 m). In eastern part of basin, the formation is 24-28 ft (7.3-8.5 m) of phosphatic shale and phosphate rock overlain by about 100 ft (30 m) of thin-bedded cherty and sandy dolomitic limestone interbedded with shale and fine-grained sandstone (Brush Creek section). Formation in general area is about 120-340 ft (37-104 m) thick, and it thins eastward. |

Table 1.--Description of major lithologic units that crop out in the northern Uinta Basin area--Continued

| Estratum | System | Series | Geologic unit | | Character of material | Hydrologic characteristics | | |
|-------------|---------------------------------|-------------------------|--|--|--------------------------------|---|--|---|
| | | | Western part of basin | Eastern part of basin | | | | |
| PALEOZOIC | Pennsylvanian | Permian | Lower Permian | Kirkman Limestone | Diamond Creek Sandstone | <p>Weber Quartzite (or Sandstone or Formation)</p> <p>In western part of basin, 1,400-1,600 ft (427-488 m) of very fine grained, medium-bedded, partly crossbedded sandstone, with chert and, locally, thin-bedded, cherty limestone, mainly near top. Also reported as locally massive and friable. Strongly fractured, especially near faults and folds (fig. 14). In eastern part of basin, about 1,200 ft (366 m) of massive, fine- to coarse-grained sandstone with well-developed crossbedding locally, especially in upper part. In vicinity of Dinosaur National Monument, Untermann and Untermann (1954, p. 46) describe the formation as poorly cemented, friable, and jointed. Some cores show deeply buried formation as dense, very fine grained sandstone. (See discussion by Bissell, 1964, p. 67-91.)</p> | <p>Very low to very high permeability. Primary permeability is very low to moderate, depending on location in the basin and the section. Samples had K of 0.000021 to 0.28 ft/d (0.0000064 to 0.085 m/d), with total porosity in the range of 11 to 19 percent (table 3). Moderate to very high K is inferred from the existence of large-yield springs that discharge from the formation in areas that are strongly faulted and fractured. Water is under confined conditions in most areas. Most wells and springs that discharge water from this formation yield freshwater. Yields fresh to slightly saline water at depths of 4,000-5,000 ft (1,220-1,520 m) in the Ashley Valley oil field and near well U(B-2-2)22dcd-1, where water circulates through faults and fractures. Yields very saline to briny water at depths of 7,500 ft (2,286 m) at well S(B-2-102)32bcd-1 and at 18,500 ft (5,640 m) at well (D-7-24)21dda-1.</p> | |
| | | | | | | <p>North of Strawberry Reservoir, the easternmost tip of a thrust plate includes several thousand feet of rocks assigned by Bissell (1952, p. 581-589) to the Oquirrh Formation through the Diamond Creek Sandstone. The section is not included in the composite section for the basin because Sadlick (1959, p. 82-89) equates the Oquirrh-Diamond Creek section with the locally derived thinner Madison-Weber section in the Uinta Mountains.</p> | <p>Little known about aquifer properties. Locally a source of springs in adjacent drainage basin.</p> | |
| | | <p>Morgan Formation</p> | <p>In west, consists of a lower member of about 260 ft (73 m) of cherty limestone with some interbedded shale and an upper member of about 200 ft (60 m) mainly of red very fine grained sandstone interbedded with some mudstone and siltstone. In east, it also consists of two members --a lower member of thick-bedded cherty limestone and an upper member of red sandy shale, crossbedded sandstone, and a few thin beds of limestone. Total thickness is about 1,100-1,400 ft (335-427 m). This formation, like all the Paleozoic section, is locally strongly faulted and fractured.</p> | <p>Very low to very high permeability. Primary or intergranular permeability is judged to be very low to low. Fracturing and possibly cavernous zones in limestone locally cause high permeability. Acts mainly as a transfer medium for water from underlying rocks. The formation is involved in the movement of water to large springs such as Big Brush Creek Spring, (D-2-21) 24cbb-51, and it is the source of about 30 ft³/s (0.85 m³/s) of water from fractures associated with faulting at the Jones Hole Spring area, (D-3-25)1b. Water from sources in edge of the outcrop area is fresh and generally contains less than 200 mg/l of dissolved solids.</p> | | | | |
| PALEOZOIC | Mississippian and Pennsylvanian | Mississippian | Upper Mississippian | Lower Mississippian | Mississippian rocks, undivided | <p>Manning Canyon(?) Formation (of Stokes, 1964)</p> | <p>This, the "black shale unit" of previous investigators, consists of black shale interbedded with a few thin beds of limestone, siltstone, and sandstone. Thickness ranges from 350 to 400 ft (107 to 122 m) in the western Uinta Basin and is about 300 ft (91 m) in Whitecliffs Canyon. The formation thins eastward from about 100 ft (30 m) north of Vernal to 25 ft (7.6 m) or less in the far eastern part of the basin.</p> | <p>Very low(?) to low permeability. Little is known about aquifer properties, but it is estimated to act mainly as a deterrent to ground-water movement. Based on lithology, water from the formation would be saline.</p> |
| | | | | | | <p>Upper Mississippian rocks, undivided</p> | <p>In the western basin, Huddle and McCann (1947) divided these rocks (in descending order) into the Humberg Formation (Upper Mississippian), Deseret Limestone (Upper? and Lower Mississippian), and the Madison Limestone (Lower Mississippian). Stokes (1964) lumped the rocks only by age. The Humberg consists of 350-400 ft (107-122 m) of limestone breccia, sandstone breccia, and limestone. The Deseret is 600-650 ft (183-198 m) of thin-bedded to massive limestone and dolomitic limestone. The Madison is about 250 ft (76 m) of thin-bedded limestone with locally abundant chert and shaly partings. The sequence appears to be about 1,200 ft (366 m) thick in the center of the Uinta Mountains, but it thins toward the east, where Kinney (1951) describes a 960-ft (293-m) section of limestone, partly cherty and dolomitic, that has interbedded fine- to medium-grained sandstone in the upper part.</p> | <p>Very low to very high permeability. The predominantly limestone section in its undisturbed state has a very low permeability. The extensively fractured sections, however, have been dissolved locally to provide extremely permeable zones, which in some cases contain large active caves (figs. 15 and 16). Section is extensively faulted, fractured, and riddled locally with cavernous zones. Much of the uplands outcrop areas, from the Soapstone Basin west of the upper Duchesne River to the heights above Rock Creek, have a karst topography that is developed mostly in the lower part of the Humberg Formation and the Deseret Limestone. Intake of water in these areas provides the water discharged from springs such as Big Spring, U(B-1-8)17cbb-51, on the upper Duchesne River and U(B-2-7)25cab-51 and 36-51 on Rock Creek. Less is known about the outcrop area between Rock Creek and the Uinta River, but karst development is certain, and the large spring, U(B-2-2)5dbb-51, is associated with an outcrop of Mississippian rocks on the Uinta River. In the Pole Creek-Dry Fork-Brush Creek area, karst development and movement of water into the cave system has been described by Maxwell, Bridges, Barker, and Moore (1971). In general, almost all water associated with these rocks in the south slope of the Uinta Mountains is fresh and of the calcium bicarbonate type. However, where the rocks are deeply buried, they seem to be tight because the water is briny. For example, in well (D-9-20)22cbb-1 near Ouray, a drill-stem sample of brine was obtained from the Madison Limestone at a depth of about 20,000 ft (7,000 m) (Hood and others, 1976, table 9).</p> |
| | | | | | | <p>Lower Mississippian rocks, undivided</p> | <p>In the western Uinta Basin, the Tintic Quartzite (Lower and Middle Cambrian) is about 400-500 ft (122-152 m) of quartzitic sandstone of wide range in grain size with some shale partings (Lockman-Balk, 1959, p. 42-43). This and disappears eastward. In the east, the Lodore Formation (Upper Cambrian) near Diamond Mountain area is 155 ft (47 m) of thick-bedded coarse-grained sandstone that thins westward.</p> | <p>Very low to high permeability. Little is known about aquifer properties, but it can be inferred that intergranular permeability is low and fracturing locally produces high permeability. In the recharge area, water should be fresh.</p> |
| PRECAMBRIAN | Upper Precambrian | Uinta Mountain Group | | | | <p>Tintic Quartzite</p> | <p>In the western Uinta Basin, the Tintic Quartzite (Lower and Middle Cambrian) is about 400-500 ft (122-152 m) of quartzitic sandstone of wide range in grain size with some shale partings (Lockman-Balk, 1959, p. 42-43). This and disappears eastward. In the east, the Lodore Formation (Upper Cambrian) near Diamond Mountain area is 155 ft (47 m) of thick-bedded coarse-grained sandstone that thins westward.</p> | <p>Very low to high permeability. Little is known about aquifer properties, but it can be inferred that intergranular permeability is low and fracturing locally produces high permeability. In the recharge area, water should be fresh.</p> |
| | | | | | | <p>Red Pine Shale</p> | <p>In the western end of the basin, about 1,700-3,000 ft (518-914 m) of dark sericitic shale interbedded with thin beds of dark arkosic sandstone. Probably fractured near major fault zones. This eastward, and only a few hundred feet, may be present in eastern part of basin.</p> | <p>Very low(?) to low permeability. Probably impedes ground-water movement in most areas but may transmit water in fractures. Erosional derivatives from this formation appear to be mixed with stream-valley fill in the Duchesne River valley above West Fork, resulting in a degradation of the chemical quality of water in the valley fill.</p> |
| PRECAMBRIAN | Upper Precambrian | Uinta Mountain Group | | | | <p>Unnamed quartzite unit (Mutual Formation of Stokes, 1964)</p> | <p>Chiefly a purple to dark reddish-brown quartzite, but includes white to red quartzitic sandstone. Some of formation retains original(?) bedding(?) and at a distance looks very much like an unaltered sedimentary formation. (See fig. 17.) Strongly faulted and has numerous shattered zones associated with the faulting. Thickness in western end of basin is about 4,000 ft (1,220 m) (Cohenour, 1959, p. 36).</p> | <p>Very low to moderate permeability. Most of formation where deeply buried probably has very low permeability, but near-surface effects of weathering and jointing probably cause moderate permeability. A specimen from a road cut near the drainage divide on State Road 44 north of Vernal had visible pores, apparently due to leaching. Wells and springs in this zone have water with a low concentration of dissolved solids--19 to 88 mg/l. Well (D-1-20)12dca-1 yielded an acidic water with a high iron concentration. Where the formation is fractured, local high yields are possible, as at</p> |

Table 1.--Description of major lithologic units that crop out in the northern Uinta Basin area--Continued

| Eraschem | System | Series | Geologic unit | | Character of material | Hydrologic characteristics |
|-------------|-------------------|----------------------|--|-----------------------|---|---|
| | | | Western part of basin | Eastern part of basin | | |
| PRECAMBRIAN | Upper Precambrian | Uinta Mountain Group | Unnamed quartzite unit (Mutual Formation of Stokes, 1964)--Continued | | | the Smoky Springs area, U(B-3-2)19cbd, in the east wall of the Uinta River canyon where the springs discharge 3-5 ft ³ /s (0.08-0.14 m ³ /s) of water that contains less than 100 mg/l of dissolved solids. |
| | | | Lower part of the Uinta Mountain Group, undivided | | Chiefly quartzite. Character probably similar to the Mutual Formation of Stokes (1964). Exposed only in highest parts of the west-central Uinta Mountains. Aggregate thickness of the Uinta Mountain Group estimated by Cohenour (1959, p. 36) to be about 12,000-15,000 ft (3,660-4,570 m) in the western mountains and about 21,000 ft (6,400 m) in the eastern part. | Not known but probably similar to Mutual Formation. |

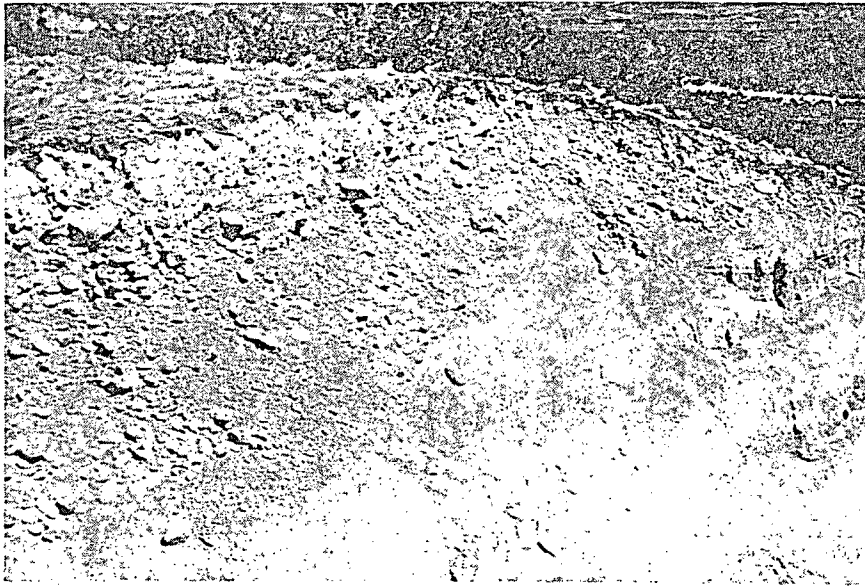
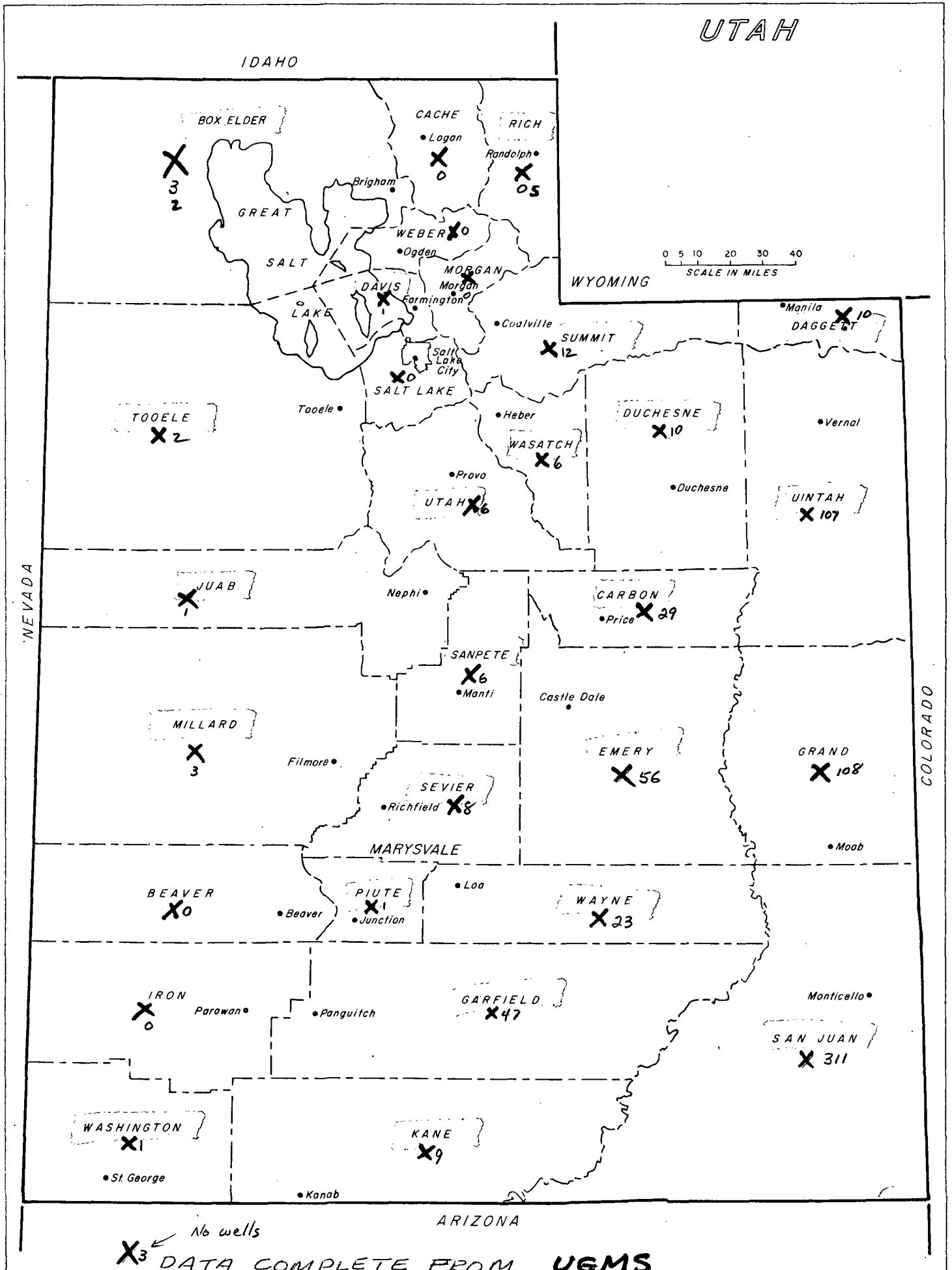


Figure 4.—Coarse-grained terrace deposits (possibly glacial outwash) overlying eroded Duchesne River Formation in canal cut above west side of Hancock Cove at U(C-1-2)6bad.



Grand C.

for climate
(not ch. ch. on map)

ALL 51° AMBIENT ^{STONY} P

| °/min | Sec | T | R | DEPTH | T °F | | | |
|-------|-------|----|-----|-------|------|------|------|------|
| 31.9 | ✓ 1. | 17 | 18S | 25E | 2799 | 100 | 19.6 | |
| 35.5 | ✓ 2. | 29 | 18S | 25E | 1490 | 20.1 | 80 | 23.5 |
| 34.7 | ✓ 3. | 9 | 19S | 21E | 2155 | 19.8 | 92 | 21.8 |
| | | | | | 2754 | 89 | ✓ | 15.9 |
| | | | | | 6800 | 142 | ✓ | |
| 39.9 | ✓ 4. | 4 | 19S | 22E | 1690 | 22.5 | 88 | 25.4 |
| | | | | | 5213 | 147 | ✓ | 19.6 |
| 45.6 | ✓ 5. | 36 | 19S | 18E | 2200 | 25.4 | 106 | 27.7 |
| 15.3 | ✓ 6. | 12 | SES | 22E | 4658 | 90 | ✓ | 9.7 |
| | ✓ 7. | 19 | 20S | 24 | 1057 | 26.4 | 78 | 31.2 |
| | ✓ 8. | 19 | 20S | 24E | 1075 | 32.5 | 85 | 37.2 |
| | ✓ 9. | 14 | 19S | 24E | 2604 | 96 | ✓ | 19.5 |
| | ✓ 10. | 35 | 19S | 24E | 1598 | 19.3 | 81 | 22.5 |
| | ✓ 11. | 35 | NE | 24E | 2134 | 20.1 | 93 | 22.5 |
| | ✓ 12. | 16 | 20S | 21E | 2719 | 19.8 | 104 | 21.7 |
| | | | | | 3409 | 109 | ✓ | 18.7 |
| | ✓ 13. | 23 | 20S | 21E | 4744 | 118 | ✓ | 15.3 |
| | ✓ 14. | 36 | 20 | 21E | 2524 | 25.8 | 115 | 27.7 |
| | ✓ 15. | 15 | 20S | 23E | 1552 | 32.2 | 100 | 35.4 |
| | | | | | 2590 | 23.9 | 112 | 25.9 |
| | ✓ 16. | 2 | CNE | 20E | 1371 | 35.0 | 98 | 38.6 |
| | ✓ 17. | 3 | 20S | 24E | 1648 | 21.2 | 85 | 24.2 |
| | ✓ 18. | 5 | NW | 24E | 1678 | 80 | ✓ | 20.8 |
| | ✓ 19. | 8 | 20S | 24E | 1370 | 23.4 | 82 | 27.0 |
| | | | | | 1610 | 23.0 | 87 | 26.1 |
| | ✓ 20. | 9 | 20S | 24 | 1670 | 22.2 | 87 | 25.1 |

Grand Co p 2

Amber

| | Sec | T | R | DEPTH | °F | |
|------|-------|-----|-----|-------|------|----------|
| ✓ 21 | 15 NW | 20S | 24E | 1344 | 25.3 | 84 |
| ✓ 22 | 19 | 20S | 2EE | 1505 | 22.6 | 84 |
| ✓ 23 | 19 NW | 20S | 24E | 1200 | 20.8 | 75 |
| ✓ 24 | 20 SW | 20S | 24 | 1024 | 22.3 | 80 |
| ✓ 25 | 23 | 21S | 18E | 3028 | 105 | 19.8 |
| | | | | 3587 | 110 | ✓ |
| ✓ 26 | 7 | 21S | 19E | 3294 | 100 | ✓ |
| | | | | 4136 | 111 | ✓ |
| ✓ 27 | 7 | 21 | 19 | 3169 | 96 | ✓ |
| ✓ 28 | 6 | 21S | 22E | 3097 | 100 | ✓ |
| ✓ 29 | 3 SE | 21S | 23E | 1425 | 22.4 | 82 26.0 |
| ✓ 30 | 3 | 21S | 23E | 1414 | 31.8 | 95 |
| ✓ 31 | 10 SW | 21S | 23E | 1136 | 30.8 | 85 |
| ✓ 32 | 20 CN | 21S | 23E | 3808 | 123 | 20.5 |
| ✓ 33 | 34 SW | 21S | 24E | 1454 | 29.5 | 93 |
| ✓ 34 | 2 NW | 22S | 16E | 4983 | 121 | ✓ |
| ✓ 35 | 2 NW | 22S | 16E | 4848 | 130 | ✓ |
| ✓ 36 | 34 NW | 22S | 17E | 5182 | 109 | 11.2 |
| | | | | 5577 | 115 | 11.5 |
| | | | | 10172 | 170 | 11.7 |
| | | | | 10291 | 175 | 12.0 |
| ✓ 37 | 22 NW | 22S | 19E | 10280 | 176 | 12.1 |
| | | | | 2921 | 21.9 | 114 23.6 |
| ✓ 38 | 10 | 22S | 21E | 525 | 64.8 | 84 74.3 |
| | | | | 1439 | 30.5 | 94 |
| ✓ 39 | 15 | 23S | 17E | 9084 | 146 | 10.4 |
| | | | | 9523 | 148 | 10.2 |

Grand p 3

| Sec | T | R | DEPTH | °F | | |
|------|-------|------|-------|-------|--------|--------------|
| ✓ 40 | 15 SW | 23S | 17E | 5121 | 118 ✓ | 13.0 |
| | | | | 9520 | 140 ✓ | |
| ✓ 41 | 16 | 23 | 17 | 8902 | 142 ✓ | |
| ✓ 42 | 16 SW | 23 | 17 | 8777 | 143 ✓ | |
| ✓ 43 | 16 NW | 23 | 17 | 8908 | 138 ✓ | |
| ✓ 44 | 17 NE | 23 | 17 | 8829 | 141 ✓ | |
| ✓ 45 | 17 | 23 | 17 | 8679 | 130 ✓ | |
| ✓ 46 | 20 NE | 23 | 19 | 6615 | 137 ✓ | |
| ✓ 47 | 36 SE | 23 | 19 | 6138 | 135 ✓ | |
| ✓ 48 | 2 NW | 23 | 20 | 3037 | 100 ✓ | |
| ✓ 49 | 5 SE | 23 | 21 | 9262 | 138 ✓ | |
| ✓ 50 | 12 | 24 | 20 | 5603 | 96 ✓ | |
| ✓ 51 | 10 | 25 | 18 | 4191 | 20.8 ✓ | 137 ✓ ✓ 22.0 |
| ✓ 52 | 27 SE | 25 | 19 | 6654 | 131 ✓ | 12.0 |
| | | | | 7238 | 140 ✓ | |
| ✓ 53 | 18 SW | 25 S | 21E | 4145 | 105 ✓ | |
| | | | | 9417 | 140 ✓ | |
| ✓ 54 | 16 NE | 25 S | 23 | 6493 | 118 ✓ | |
| ✓ 55 | 9 | 26 | 20 | 7498 | 113 ✓ | |
| | | | | 7884 | 118 ✓ | |
| | | | | 8131 | 120 ✓ | |
| ✓ 56 | 14 | 26 | 20 | 5636 | 120 ✓ | |
| ✓ 57 | 29 | 26 | 20 | 8450 | 125 ✓ | |
| | | | | 8592 | 136 ✓ | |
| ✓ 58 | 31 | 26 | 20E | 4043 | 105 ✓ | |
| ✓ 59 | 12 | 26 | 25 | 7019 | 115 ✓ | |
| | | | | 12719 | 168 ✓ | |
| | | | | 14563 | 180 ✓ | |
| | | | | 15878 | 205 ✓ | |

Grand p 4

| | Sec | T | R | DEPTH | °F | |
|-----|-------|----------|-----------|-------|-----|------------|
| ✓60 | 31 SW | 15S | 25E | 7804 | 160 | |
| | | | | 4102 | 100 | |
| ✓61 | 33 SE | 15 1/2 S | 23E | 8608 | 219 | 20.2 T LOG |
| | | | SONIC LOG | 8740 | 182 | |
| | | | | 4650 | 125 | |
| ✓62 | 15 | 16S | 21E | 6275 | 122 | |
| ✓63 | 22 NW | 16 | 21E | 6150 | 118 | |
| ✓64 | 36 | 16 | 22E | 3867 | 118 | 17.326 |
| | | | | 8364 | 176 | |
| ✓65 | 14 | 16S | 23E | 4699 | 116 | 13.8 |
| | | | | 8772 | 174 | |
| ✓66 | 12 SE | 16S | 24E | 5907 | 157 | 18.9 |
| ✓67 | 13 | 16S | 24E | 6040 | 155 | |
| ✓68 | 24 | 16S | 24E | 6270 | 170 | 19.9 |
| ✓69 | 29 | 16S | 24E | 2259 | 92 | NO |
| | | | | 6602 | 145 | |
| | | | | 6032 | 184 | 22.2 23.0 |
| ✓70 | 2 | 16S | 25E | 6643 | 162 | |
| ✓71 | 8 | 16S | 25 | 5940 | 127 | |
| ✓72 | 11 NE | 16S | 25E | 5803 | 148 | |
| ✓73 | 13 | 16S | 25E | 1540 | 112 | 40.2 43.5 |
| ✓74 | 17 | 16S | 25E | 6886 | 140 | |
| ✓75 | 21 | 16S | 25E | 6574 | 143 | |
| ✓76 | 21 NE | 16S | 25E | 6530 | 145 | |
| ✓77 | 21 SW | 16S | 25E | 6497 | 146 | |
| ✓78 | 22 | 16 | 25 | 6019 | 124 | 12.0 |
| | | | | 6831 | 160 | |

Grand Co p. 5

| | Sec | T | R | DEPTH | °F |
|------|-------|-----|--------|---------------|-------------|
| ✓ 79 | 22 NE | 16S | 25E | 5199 | 130 ✓ |
| ✓ 80 | 23 NW | 16S | 25E | 5544 (19.5) ✓ | 158 ✓ 20.38 |
| ✓ 81 | 23 SW | 16 | 25 | 5132 | 137 ✓ |
| ✓ 82 | 24 | 16 | 25 | 4953 (20.8) ✓ | 153 ✓ 21.8 |
| ✓ 83 | 25 | 16 | 25 | 4937 (21.8) ✓ | 158 ✓ 22.9 |
| ✓ 84 | 26 | 16 | 25 | 4048 | 122 ✓ |
| | | | | 5106 | 140 ✓ |
| | | | | 5806 (21.0) ✓ | 172 ✓ 21.9 |
| ✓ 85 | 27 | 16 | 25 | 4692 (21.9) ✓ | 126 ✓ 21.9 |
| | | | | 5892 | 139 ✓ |
| ✓ 86 | 30 | 16 | 26E(?) | 4760 | 133 ✓ |
| ✓ 87 | 35 | 16 | 25 | 4543 | 122 ✓ |
| ✓ 88 | 9 | 17 | 21 | 6245 | 130 ✓ |
| ✓ 89 | 14 NW | 17 | 22 | 3368 (✓) | 110 19.3 |
| ✓ 90 | 25 | 17 | 22 | 2935 | 93 ✓ |
| ✓ 91 | 13 | 17 | 23 | 5166 (19.4) ✓ | 150 ✓ 20.3 |
| ✓ 92 | 6 | 17 | 24 | 5596 | 142 ✓ |
| ✓ 93 | 7 SE | 17 | 24 | 864 (39.4) ✓ | 84 45.1 |
| | | | | 5282 (21.6) ✓ | 164 ✓ 22.5 |
| ✓ 94 | 12 SW | 17 | 25 | 2997 (22.4) ✓ | 117 24.0 |
| | | | | 3735 (✓) | 118 19.5 |
| ✓ 95 | 15 | 17 | 25 | 3814 (19.4) ✓ | 125 ✓ 21.0 |
| ✓ 96 | 21 NW | 17 | 25 | 4094 | 122 ✓ 18.8 |
| ✓ 97 | 7 NE | 17 | 26 | 3723 (22.5) ✓ | 133 ✓ 23.5 |
| ✓ 98 | 8 NE | 17 | 26 | 3849 | 116 ✓ |
| ✓ 99 | 17 NE | 17 | 26 | 3633 | 105 ✓ |

Grand #6

| Sec | T | R | DEPTH | OF |
|-------|-------|---------|-------|------------------|
| ✓ 100 | 18 | 17S 26E | 3600 | 116 19.7 |
| ✓ 101 | 19 NE | 17 26 | 3281 | 100 ✓ |
| ✓ 102 | 4 | 18 22 | 5436 | 144 ✓ |
| ✓ 103 | 29 | 18 22 | 5597 | 145 ✓ |
| ✓ 104 | 33 NE | 18 22 | 1802 | 23.3 92 |
| | | | 5386 | 126 ✓ |
| ✓ 105 | 3 | 18S 23E | 6010 | 147 ✓ |
| ✓ 106 | 16 | 18S 24E | 3282 | 108 ✓ close |
| ✓ 107 | 21 | 18S 24E | 2900 | 100 ✓ |
| | | | 4500 | 19.3 1737 ✓ 20.4 |
| ✓ 108 | 21 | 18 24 | 2884 | 19.4 106 21.2 |

end
plotted

GRAND CO

P.I.

No

72.7°/hr

X 104 ▼

✓ 145 ○

✓ 146 ○

✓ 147 ▼

✓ 149 ○

✓ 151 ○

UGMS

No

✓ 1 ▼

X 2 ▼

35.5°/hr

✓ 3 ▼

X 4 ▼

39.9°/hr

X 5 ▼

45.6°/hr

✓ 6 ○

X 7 ▼

46.5°/hr

X 8 ▼

57.6

✓ 9 ▼

✓ 10 ▼

X 11 ▼

35.9

✓ 12 ▼

35.5

✓ 13 ○

X 14 ▼

46.2

X 15 ▼

57.5

X 16 ▼

62.5

X 17 ▼

37.6

✓ 18 ▼

36 ○

35 ○

34 ○

X 33 ▼ 52.6

32 ○

X 31 ▼ 54.6

X 30 ▼

56.7

X 29 ▼

39.6

✓ 28 ▼

✓ 27 ▼

✓ 26 ○

✓ 25 ▼

X 24 ▼ 51.6

X 23 ▼

36.5

X 22 ▼

40.0

X 21 ▼

44.8

X 20 ▼

39.3

X 19 ▼

41.2

Not in Subfile !

United Energy Corp.

SW SW Sec 29, T20S

R22E

Willard Peace - Contr.

163° F BHT (log) @ 2944'

28-42 GPM

~ 160-180 °F water

Shand Co.

GRAND Co. Cont.
UGMS

| No. | No. | No. |
|-----------------------------|-------------------------------|----------------------------|
| X 37 Δ 39.3 | ✓ 64 \circ | ✓ 91 \circ |
| X 38 \blacktriangle 114.6 | ✓ 65 \circ | ✓ 92 \circ |
| ✓ 39 \circ | ✓ 66 \circ | X 93 \blacktriangle 69.6 |
| ✓ 40 \circ | ✓ 67 \circ | X 94 Δ 40.1 |
| ✓ 41 \circ | ✓ 68 \circ | X 95 \circ 35.4 |
| ✓ 42 \circ | X ✓ 69 \bullet \circ 40.7 | ✓ 96 \circ |
| ✓ 43 \circ | ✓ 70 \circ | X ✓ 97 \circ 40.1 |
| ✓ 44 \circ | ✓ 71 \circ | ✓ 98 \circ |
| ✓ 45 \circ | ✓ 72 \circ | ✓ 99 \circ |
| ✓ 46 \circ | X ✓ 73 \blacktriangle 72.2 | ✓ 100 \circ |
| ✓ 47 \circ | ✓ 74 \circ | ✓ 101 \blacktriangle |
| ✓ 48 \circ | ✓ 75 \circ | 102 \circ |
| ✓ 49 \circ | ✓ 76 \circ | 103 \circ |
| ✓ 50 \circ | ✓ 77 \circ | ✓ 104 Δ 41.5 |
| X ✓ 51 \circ 37.3 | ✓ 78 \circ | 105 \circ |
| ✓ 52 \circ | ✓ 79 \circ | 106 \circ |
| ✓ 53 \circ | X 80 \circ 35.2 | 107 \circ |
| ✓ 54 \circ | ✓ 81 \circ | ✓ 108 Δ |
| ✓ 55 \circ | X ✓ 82 \circ 37.5 | |
| ✓ 56 \circ | X 83 \circ 39.5 use 39. | |
| ✓ 57 \circ | ✓ 84 \circ GREEN 37.9 | |
| ✓ 58 \circ | ✓ 85 \circ | |
| ✓ 59 \circ | ✓ 86 \circ | |
| ✓ 60 \circ | ✓ 87 \circ | |
| X ✓ 61 \circ 35.6 | ✓ 88 \circ | |
| ✓ 62 \circ | ✓ 89 \circ | |
| ✓ 63 \circ | ✓ 90 \circ | |

✓ +163° @ 2944
FROM CAMPBELL
 \blacktriangle 69.3 °C / *pm*

ANOM WELLS
GRAND CO.

TOTAL ALL WELLS: 115

" ANOMALOUS " : 38

| See | T | R | depth (m) | °C | °C/m | Amb |
|-----|-----|-----|--------------|------|------|------|
| 29 | 20S | 22E | 897 | 72.8 | 69 | 10.6 |
| 2 | 16S | 24E | 986 | 82.2 | 73 | |
| 29 | 18S | 25E | 454 | 26.7 | 35 | |
| 4 | 19S | 22E | 515 | 31.1 | 40 | |
| 36 | 19S | 18E | 670 | 41.1 | 46 | |
| 19 | 20S | 24E | 322 | 25.6 | 46 | |
| 35 | 19S | 24E | 650 | 33.9 | 36 | |
| 19 | 20S | 24E | 327 | 29.4 | 58 | |
| 16 | 20S | 21E | 829 | 40.0 | 36 | |
| 36 | 20S | 21E | 769 | 46.1 | 46 | |
| 15 | 20S | 23E | 473 | 37.8 | 58 | |
| 2 | 20S | 20E | 418 | 36.7 | 62 | |
| 3 | 20S | 24E | 492 | 29.4 | 38 | |
| 8 | 20S | 24E | 418 | 27.8 | 41 | |
| 9 | 20S | 24E | 509 | 30.6 | 39 | |
| 15 | 20S | 24E | 410 | 28.9 | 45 | |
| 19 | 20S | 24E | 459 | 28.9 | 40 | |
| 19 | 20S | 24E | 366 | 23.9 | 36 | |
| 20 | 20S | 24E | 312 | 26.7 | 52 | |
| 3 | 21S | 23E | 434 | 27.8 | 40 | |
| 3 | 21S | 23E | 431 | 35.0 | 57 | |
| 10 | 21S | 23E | 345 | 29.4 | 55 | |
| 34 | 21S | 24E | 443 | 33.9 | 53 | |
| 22 | 22S | 19E | 890 | 45.6 | 39 | |
| 10 | 22S | 21E | 160 | 29.0 | 115 | |

ANNUAL LOGS W L 55
GRAND CO., CONT.

| See | T | R | d (m) | °C | °C/ftm | Amb |
|-----|----------|-----|----------|-------|--------|------|
| 10 | 25S | 18E | 1277 | 58.3 | 37 | 10.6 |
| 33 | 15 1/2 S | 23E | 2624 | 103.9 | 36 | |
| 29 | 16S | 24E | 1838 | 84.4 | 40 | |
| 13 | 16S | 25E | 469 | 44.4 | 72 | |
| 23 | 16S | 25E | 1690 | 70.0 | 35 | |
| 24 | 16S | 25E | 1510 | 67.2 | 38 | |
| 25 | 16S | 25E | 1505 | 70.0 | 39 | |
| 26 | 16S | 25E | 1770 | 77.8 | 38 | |
| 7 | 17S | 24E | 263 | 28.9 | 70 | |
| 12 | 17S | 25E | 913 | 47.2 | 40 | |
| 15 | 17S | 25E | 1162 | 51.7 | 35 | |
| 7 | 17S | 26E | 1135 | 56.1 | 40 | |
| 33 | 18S | 22E | 549 | 33.3 | 41 | |

GRAND CO, CISCO

| # | elev. on map (ft) * | depth to 50°C (m) | elev. of 50°C (m) | |
|-------------|---------------------|-------------------|-------------------|---|
| 3 | 7400 ± 500 | 1139 | 1117 | • |
| 4 | 6000 | 990 | 839 | • |
| 5 | 6400 | 866 | 1085 | • |
| SE SW 6 | 5400 | 2592 | -946 B.S.L. | |
| 7 | 4550 | 845 | 542 | • |
| 8 | 4550 | 688 | 699 | • |
| 9 | 4800 | 1251 | 212 | |
| 10 | 4600 | 1155 | 247 | |
| NE SW SE 11 | 4600 | 1101 | 301 | • |
| 12 | 5300 | 1110 | 505 | • |
| 13 | 5100 | 1533 | 21 | |
| 14 | 4950 | 853 | 656 | • |
| 15 | 4700 | 685 | 748 | • |
| NE NW 16 | 7100 | 631 | 1533 | • |
| 17 | 4550 | 1053 | 334 | • |
| NW SE SE 18 | 4650 | 1251 | 166 | |
| 19 | 4640 | 959 | 455 | • |
| 20 | 4600 | 1003 | 399 | • |
| NW NW NW 21 | 4600 | 883 | 519 | • |
| 22 | 4550 | 987 | 400 | • |
| WSW SE 23 | 4535 | 1095 | 297 | • |
| WSW SW 24 | 4550 | 764 | 623 | • |
| SW 33 | 4300 | 749 | 562 | • |
| 38 | 4720 | 344 | 1095 | • |
| → 41 | 4900 | 569 | 925 | • |
| 28 | 4950 | 1308 | 141 | |
| 29 | 5200 | 995 | 590 | • |
| 30 | 4400 | 696 | 645 | • |

> 1000 —
 750-1000 —
 500-750 —
 250-500 —
 0-250 —

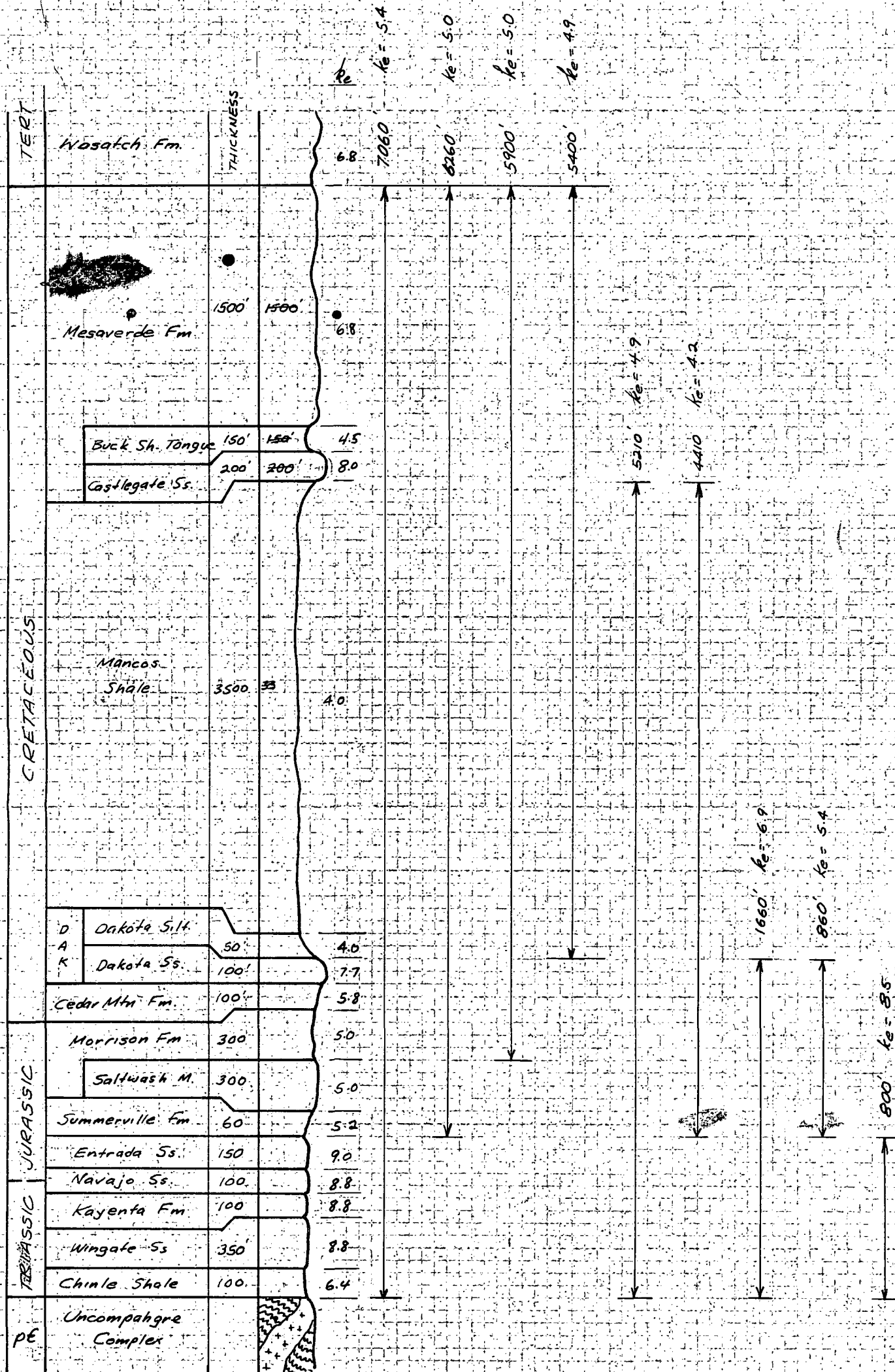
* - Large variation in elevation in section

| | | | | |
|------------|-------|------|------|---|
| SWSW NE 31 | 4400 | 726 | 615 | 0 |
| ENWSW 32 | 4500 | 1145 | 227 | 0 |
| 1 | 5045 | 1235 | 303 | 0 |
| 2 | 4900 | 1110 | 384 | 0 |
| SW 60 | 8200 | 1551 | 948 | 0 |
| SE 61 | 7800 | 1107 | 1270 | 0 |
| 62 | 7600 | 1913 | 403 | 0 |
| NW 63 | 7800 | 1990 | 387 | 0 |
| 64 | 7000 | 1247 | 887 | 0 |
| 65 | 8000 | 1545 | 893 | 0 |
| SE 66 | 7000 | 1265 | 929 | 0 |
| 67 | 6800 | 1259 | 814 | 0 |
| 68 | 7000 | 1139 | 995 | 0 |
| 69 | 7400 | 980 | 1276 | 0 |
| 70 | 8000* | 1296 | 1142 | 0 |
| 71 | 8000* | 1691 | 747 | 0 |
| NE 72 | 7600* | 1296 | 1020 | 0 |
| 73 | 6200* | 546 | 1344 | 0 |
| 74 | 7500* | 1677 | 609 | 0 |
| 75 | 7400* | 1545 | 711 | 0 |
| NE 76 | 7600 | 1504 | 812 | 0 |
| SW 77 | 7000 | 1481 | 653 | 0 |
| 78 | 7000* | 1359 | 775 | 0 |
| NE 79 | 6480 | 1428 | 523 | 0 |
| NW 80 | 6800 | 1123 | 950 | 0 |
| SW 81 | 6400 | 1292 | 659 | 0 |
| 82 | 6300* | 1051 | 869 | 0 |
| 83 | 6000 | 997 | 832 | 0 |

| | | | | | |
|--------|--------|-------|------|------|---|
| | 84 | 6300* | 1037 | 883 | o |
| SE/WNW | PI 70 | 8400 | 543 | 2017 | o |
| | 85 | 6300* | 1354 | 566 | o |
| | 86 | 6000 | 1254 | 575 | o |
| | 87 | 5800 | 1387 | 381 | o |
| | 88 | 8400 | 1713 | 647 | o |
| NW | 89 | 7000 | 1235 | 899 | o |
| | 90 | 7000 | 1510 | 624 | o |
| | 91 | 6600 | 1129 | 883 | o |
| | 92 | 7000 | 1331 | 803 | o |
| SE | 93 | 6600* | 566 | 1446 | o |
| SW | 94 | 5300 | 983 | 632 | o |
| | 95 | 5350 | 1113 | 518 | o |
| NW | 96 | 5300 | 1247 | 368 | o |
| | NE 97 | 5260 | 983 | 620 | o |
| | NE 98 | 5280 | 1279 | 330 | o |
| | NE 99 | 5235 | 1454 | 142 | |
| | 100 | 5200 | 1198 | 387 | o |
| | NE 101 | 5100 | 1449 | 105 | |
| | 102 | 7000* | 1267 | 867 | o |
| | 103 | 6600* | 1288 | 724 | o |
| | NE 104 | 6400 | 954 | 997 | o |
| | 105 | 6000 | 1354 | 475 | o |
| | 106 | 5100 | 1247 | 307 | o |
| | 107 | 5100 | 1132 | 422 | o |
| | 108 | 5100 | 1135 | 419 | o |

GRAND CO UT.

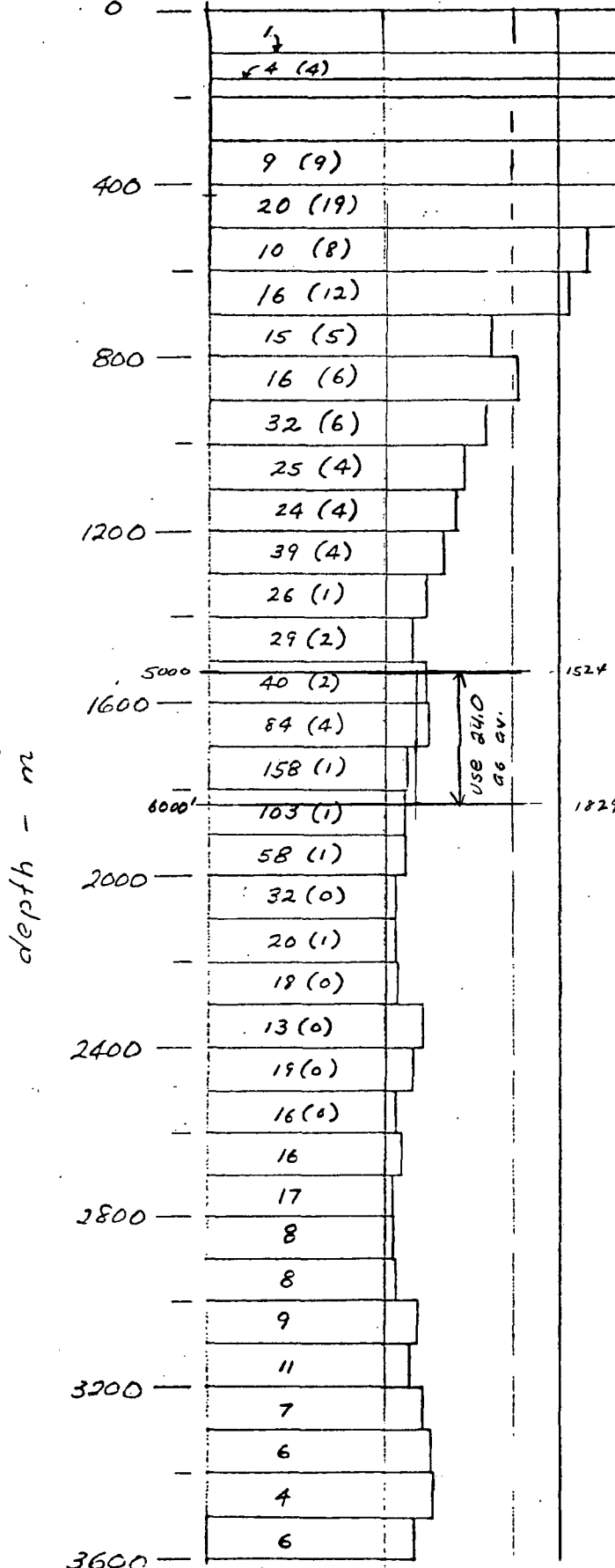
| UGMS WELL | °C/ ft | depth to 50°C (m) | WELL # | °C/ ft | depth to 50°C |
|--------------|-----------|-------------------------|-----------|-----------|------------------|
| 1 | 31.9 | 1235 | 34 | 25.6 | 1539 |
| 2 | 35.5 | 1110 | 35 | 29.7 | 1326 |
| 3 | 34.7 | 1135 | 36 | 22.0 | 1790 |
| 4 | 39.9 | 987 | 37 | 39.3 | 1002 |
| 5 | 45.6 | 868 | 38 | 114.6 | 343 |
| 6 | 15.3 | 2575 | 39 | 23.8 | 1655 |
| 7 | 46.5 | 847 | 40 | | |
| 8 | 57.6 | 684 | 41 | 18.6 | |
| 9 | 31.5 | 1257 | 42 | 19.1 | |
| 10 | 34.2 | 1152 | 43 | 17.8 | |
| 11 | 35.9 | 1097 | 44 | 18.6 | |
| 12 | 35.5 | 1110 | 45 | 16.6 | |
| 13 | 25.7 | 1533 | 46 | 23.7 | |
| 14 | 46.2 | 853 | 47 | 24.9 | |
| 15 | 57.5 | 685 | 48 | 29.4 | |
| 16 | 62.5 | 630 | 49 | 17.1 | |
| 17 | 37.6 | 1048 | 50 | 14.6 | |
| 18 | 31.5 | 1251 | 51 | 37.3 | |
| 19 | 41.2 | 956 | 52 | 22.4 | |
| 20 | 39.3 | 1002 | 53 | 23.7 | |
| 21 | 44.8 | 879 | 54 | 18.8 | |
| 22 | 40.0 | 985 | 55 | 15.5 | |
| 23 | 36.5 | 1079 | 56 | 22.3 | |
| 24 | 51.6 | 764 | 57 | 18.0 | |
| 25 | 32.5 | 1219 | 58 | 24.3 | |
| 26 | 27.1 | 1454 | 59 | 17.7 | |
| 27 | 25.9 | 1521 | 60 | 25.4 | |
| 28 | 28.8 | 1368 | 61 | 35.6 | |
| 29 | 39.6 | 995 | 62 | 20.6 | |
| 30 | 56.7 | 695 | 63 | 19.8 | |
| 31 | 54.6 | 722 | 64 | 27.2 | |
| 32 | 34.5 | 1142 | 65 | 25.6 | |
| 33 | 52.6 | 749 | 66 | 32.7 | |



CISCO - BAR-X AREA, GRAND CO.
 SECTION AS TYPICALLY RECORDED IN WELLS
 AND ESTIMATED THERMAL CONDUCTIVITIES
 IN $\frac{\text{mCal}}{\text{cm sec } ^\circ\text{C}}$

GRADIENT $^{\circ}\text{C}/\text{km}$

20 35 40 60 80 100 120



UTAH -
GRADIENTS TO SURFACE -
AVERAGES OVER DISCRETE INTERVALS
(USUALLY 100 m)

| | |
|-------|---|
| 15-16 | $25.1 \times \frac{76}{30} \times 30 = 753.0$ |
| 16-17 | $25.3 \times 84 = 2125.2$ |
| 17-18 | $23.0 \times 158 = 3634.0$ |
| 18-19 | $22.5 \times \frac{30}{30} \times 30 = 675$ |
| | 302 7187.2 |

} 5000'-6000'
mean $\bar{P} = 23.8$

| (ft.) depth int | Av grad |
|--------------------|---------|
| 1400-1600 | 47.7 |
| 1600-1800 | 44.9 |
| 1800-2000 | 43.0 |
| 2000-2200 | 41.3 |
| 2200-2500 | 35.6 |

No. of GRADIENTS $\geq 35^{\circ}\text{C}/\text{km}$
 No. OF SAMPLES

2nd Calc. of ke's for BHT's
 using air (chart) ~~the~~ from 0-2810
 93 surface Green River
 began logging at 2810

0-2140' watches (assumed) ke=7.0
 2140-2810 watches (assumed) ke=5.8
 2810-5030 watches-top castlegate (meas) ke=7.0

BHT ① 110 @ 4713

| | | | |
|------|-------|-------|--------|
| 2140 | @ 7.0 | 14980 | |
| 670 | @ 5.8 | 3886 | 6.8 |
| 1903 | @ 7.0 | 13321 | 7.6 |
| 4713 | | 32187 | 4.1 |
| | | | ke=6.8 |

Castlegate (meas)
 Mancos (meas)

(300) 5030-5330
 (3490) 5330-8820

BHT ② 110°F @ 5447

| | | | |
|------|-------|-------|--|
| 2140 | @ 7.0 | 14980 | |
| 670 | @ 5.8 | 3886 | |
| 2220 | @ 7.0 | 15540 | |
| 300 | @ 7.6 | 2280 | |
| 117 | @ 4.1 | 480 | |
| 5447 | | 371 | |

(190) 8820-9010
 (632) 9010-9642
 (58) 9642-9700
 (130) 9700-9830
 9830-9920

ke=7.0
 Dakota
 Morrison (incl. S. section)
 Summerville
 Entrada
 Navajo

BHT ③ 173° @ 9869

Continued

BHT (3) 1730 @ 9869

$k_e = 5.8$

| | | | |
|-------------|---|-----|-------|
| 5330 | @ | 6.9 | 36777 |
| 3490 | @ | 4.1 | 14309 |
| 190 | @ | 7.0 | 133.0 |
| 632 | @ | 5.2 | 3286 |
| 58 | @ | 6.4 | 371 |
| Entrada 130 | @ | 8.2 | 1066 |
| 39 | @ | 8.8 | 343 |
| <hr/> | | | |
| 9869 | | | 57482 |

(65) 9920 - 9985 unidentified $k_e = 7.0$

(118) 9985 - 10103 Kayenta $k_e = 8.8$

(466) 10103 - 10568 wingate $k_e = 8.8$

(95) 10568 - 10663 Chance $k_e = 6.4$

124 | 10663 - 10787 PE $k_e = 7.0$

BHT (4) 176 @ 10787

$k_e = 6.0$

| | | | |
|-------|---|-----|-------|
| 9830 | @ | 5.8 | 57014 |
| 90 | @ | 8.8 | 792 |
| 65 | @ | 7.0 | 455 |
| 118 | @ | 8.8 | 1038 |
| 465 | @ | 8.8 | 4092 |
| 95 | @ | 6.4 | 608 |
| 124 | @ | 7.0 | 868 |
| <hr/> | | | |
| 10787 | | | 64857 |

Schlumberger

SIMULTANEOUS
**COMPENSATED NEUTRON-
 FORMATION DENSITY**

3

COMPANY THE ANSCHUTZ CORP

WELL STATE 411-2

FIELD WILDCAT

COUNTY GRAND STATE UTAH

GRAND WILDCAT SW/NE STATE 411-2 ANSCHUTZ

| | | | |
|----------------|-------|------|-------|
| LOCATION | SW/NE | | |
| API SERIAL NO. | SEC. | TWP. | RANGE |
| | 23 | 18S | 20E |

Other Services: **93**
 DIL, BHC-GR
 TAPING, CNL

Permanent Datum: GL; Elev.: 8934
 Log Measured From KB, 18 Ft. Above Perm. Datum
 Drilling Measured From KB

Elev.: K.B. 8952
 D.F. -
 G.L. 8934

| Date | 10-19-78 | 10-31-78 | 12-5-6-78 | 12-19-20-78 |
|---------------------|-----------------------|------------------------|-----------------------|-----------------------|
| Run No. | ONE | TWO | THREE | FOUR |
| Depth-Driller | 4705 | 5453 | 9870 | 10786 |
| Depth-Logger | 4714 | 5449 | 9871 | 10789 ²¹¹ |
| Btm. Log Interval | 4713 228 | 5447 197 | 9869 225 | 10787 5453 |
| Top Log Interval | 80 | 3418 | 5453 | 9770 647 |
| Casing-Driller | 20" @ 68 | 20 @ 58 | 13 3/8 @ 5452 | 13 3/8 @ 5452 |
| Casing-Logger | 80 | 80 | 5453 | 5453 5453 |
| Bit Size | 17 1/2 | 17 1/2 | 12 1/4 | SEE REMARKS |
| Type Fluid in Hole | FRESH MUD | FGM | KCL AQUAGEL | FGM |
| Dens. | 8.9 | 60 | 9.3 | 9.0 |
| Visc. | | | 38 | 56 |
| pH | 8.2 | 9.0 | 10 | 10 |
| Fluid Loss | | 10ml | 6-8ml | 6.4ml |
| Source of Sample | PIT | TANK | TANK | TANK |
| Rm @ Meas. Temp. | 2.90 @ 76°F | 2.47 @ 65F | .434 @ ~58°F | .84 @ 56°F |
| Rmf @ Meas. Temp. | 2.47 @ 69°F | 1.74 @ 60F | .369 @ ~58°F | .386 @ 59F |
| Rmc @ Meas. Temp. | - @ °F | 3.70 @ 65F | - @ °F | 1.26 @ 56F |
| Source: Rmf Rmc | MEAS - | M C | MEAS CALC | M C |
| Rm @ BHT | 2.4 @ 110F | 1.55 @ 110F | .16 @ 173F | - @ 176F |
| Circulation Stopped | 0030 | 1030 | 0500 | 830 |
| Logger on Bottom | 1900 | 1930 | 1730 | 2330 |
| Max. Rec. Temp. | 110F | 110F | 173F | 176F |
| Equip. Location | 5768 FARM | 7759 G.J. | 7759 G.J. | 7759 G.J. |
| Recorded By | BRAAF | KRABACHER | KRABACHER | OLSON/KRAB. |
| Witnessed By Mr. | HELMKE | HELMKE | HELMKE | HELMKE |

The well name, location and borehole reference data were furnished by the customer.

ECU 93

| | | | | $\frac{^{\circ}F}{1000}$ |
|---|---------------|---|------------------|--------------------------|
| ① | 4713 110° | $T_2 = \frac{7}{7} (110 - 51) + 51$ | $= 110^{\circ}F$ | 12.5 |
| ② | 5447 110° | $T_2 = \frac{6.9}{7.0} (110 - 51) + 51$ | $= 109^{\circ}$ | 10.6 |
| ③ | 9869 173° | $T_2 = \frac{5.9}{7} (173 - 51) + 51$ | $= 154^{\circ}$ | 10.4 |
| ④ | 10787 176° | $T_2 = \frac{6.1}{7.0} (176 - 51) + 51$ | $= 160^{\circ}$ | 10.1 |

5447
 5330
 117

ECU 93

| | | | |
|-----|-------------------|------------------|----------------|
| (1) | 110 at 4713 | above castlegate | <u>7.0</u> |
| (2) | 110 at 5447 | 5030' | 7.0 = 35210 |
| | Cast to 1600 = -1 | 300' castlegate | 7.6 = 2280 |
| | | 117' mancon | 4.1 = 479.7 |
| | 5447 | | <u>37969.7</u> |
| | | | <u>6.9</u> |

| | | | | |
|-----|-------------|-----------|------------|--------------|
| (3) | 173 at 9869 | 5030 | 7.0 | 35210 |
| | | 300 | 7.6 | 2280 |
| | | 3490 | 4.1 | 14309 |
| | | 190 | 7.0 | 1330 |
| | | 325 | 5.2 | 1690 |
| | | 307 | 5.2 | 1596 |
| | | 58 | 6.4 | 371 |
| | | 130 | 8.2 | 1066 |
| | | 39 mancon | 8.8 | 343 |
| | 9869 | | <u>5.9</u> | <u>58195</u> |

9869
 9830
 39

127
 at 1600

Cast to 1600 = -46

| | | | | |
|-----|--------------|------|------------|--------------|
| (4) | 176 at 10787 | 5030 | 7.0 | 35210 |
| | | 300 | 7.6 | 2280 |
| | | 3490 | 4.1 | 14309 |
| | | 190 | 7.0 | 1330 |
| | | 325 | 5.2 | 1690 |
| | | 307 | 5.2 | 1596 |
| | | 58 | 6.4 | 371 |
| | | 130 | 8.2 | 1066 |
| | | 90 | 8.8 | 792 |
| | | 118 | 8.8 | 1038 |
| | | 465 | 8.8 | 4092 |
| | | 95 | 6.4 | 608 |
| | pl 124 | | 8.0 | 992 |
| | 10787 | | <u>6.1</u> | <u>65374</u> |

10787
 10663
 124

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

SUBMIT IN DUPLICATE

(See other instructions on reverse side)

Form approved.
Budget Bureau No. 42-R355.6.

WELL COMPLETION OR RECOMPLETION REPORT AND LOG *

1a. TYPE OF WELL: OIL WELL GAS WELL DRY Other _____

b. TYPE OF COMPLETION: NEW WELL WORK OVER DEEP-EN PLUG BACK DIFF. RESVR. Other _____

2. NAME OF OPERATOR
The Anschutz Corporation

3. ADDRESS OF OPERATOR
2400 Anaconda Tower, Denver, Colorado 80202

4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements)*
At surface
At top prod. interval reported below
At total depth
802' FWL + 1572' FNL

14. PERMIT NO. _____ DATE ISSUED _____

5. LEASE DESIGNATION AND SERIAL NO.

State 27411

6. IF INDIAN, ALLOTTEE OR TRIBE NAME

7. UNIT AGREEMENT NAME

Queant

8. FARM OR LEASE NAME

State 411

9. WELL NO.

2

10. FIELD AND POOL, OR WILDCAT

Wildcat

11. SEC., T., R., M., OR BLOCK AND SURVEY OR AREA

Sec. 23, T. 18S-R. 20E

12. COUNTY OR PARISH

13. STATE

Grand

Utah

15. DATE SPUNDED
9-10-79

16. DATE T.D. REACHED
12-19-79

17. RATE OF COMPL. (Ready to prod.)
124%
FEB 7 1979

18. ELEVATIONS (DF, RKB, RT, GR, ETC.)*
8934 GR

19. ELEV. CASING HEAD
8904' EST

20. TOTAL DEPTH, MD & TVD
10,786

21. PLUG, BACK T.D., MD & TVD
Surface

22. IF MULTIPLE HOW MANY*
1079

23. INTERVALS DRILLED BY
ROTARY TOOLS
0-10,786

CABLE TOOLS
-0-

24. PRODUCING INTERVAL(S), OF THIS COMPLETION—TOP, BOTTOM, NAME (MD AND TVD)*

25. WAS DIRECTIONAL SURVEY MADE
Yes

26. TYPE ELECTRIC AND OTHER LOGS RUN

FDC-CNL-GR, CNL, BHC-GR. DIL

27. WAS WELL CORED
No

28. CASING RECORD (Report all strings set in well)

| CASING SIZE | WEIGHT, LB./FT. | DEPTH SET (MD) | HOLE SIZE | CEMENTING RECORD | AMOUNT PULLED |
|-------------|-----------------|----------------|-----------|------------------|---------------|
| 20" | 94 | 61 | 30" | 250 SX | -0- |
| 13-3/8" | 54.5 | 5452 | 17 1/2" | 635 SX | -0- |

29. LINER RECORD

| SIZE | TOP (MD) | BOTTOM (MD) | SACKS CEMENT* | SCREEN (MD) |
|------|----------|-------------|---------------|-------------|
| | | | | |

30. TUBING RECORD

| SIZE | DEPTH SET (MD) | PACKER SET (MD) |
|------|----------------|-----------------|
| | | |

31. PERFORATION RECORD (Interval, size and number)

5280-5300 - 2 SPF
5040-5050 - 2 SPF
5054-5066 - 2 SPF
5072-5082 - 2 SPF
4" casing
gun

32. ACID, SHOT, FRACTURE, CEMENT SQUEEZE, ETC.

| DEPTH INTERVAL (MD) | AMOUNT AND KIND OF MATERIAL USED |
|---------------------|----------------------------------|
| | |

33.* PRODUCTION

DATE FIRST PRODUCTION _____ PRODUCTION METHOD (Flowing, gas lift, pumping—size and type of pump) _____ WELL STATUS (Producing or shut-in) _____

| DATE OF TEST | HOURS TESTED | CHOKE SIZE | PROD'N. FOR TEST PERIOD | OIL—BBL. | GAS—MCF. | WATER—BBL. | GAS-OIL RATIO |
|--------------|--------------|------------|-------------------------|----------|----------|------------|---------------|
| | | | | | | | |

34. DISPOSITION OF GAS (Sold, used for fuel, vented, etc.) _____ TEST WITNESSED BY _____

35. LIST OF ATTACHMENTS

36. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records

SIGNED Peter B. Doty (MGE) TITLE Operations Coordinator DATE February 5, 1979

*(See Instructions and Spaces for Additional Data on Reverse Side)

INSTRUCTIONS

General: This form is designed for submitting a complete and correct well completion report and log on all types of lands and leases to either a Federal agency or a State agency, or both, pursuant to applicable Federal and/or State laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from, the local Federal and/or State office. See instructions on items 22 and 24, and 33, below regarding separate reports for separate completions.

If not filed prior to the time this summary record is submitted, copies of all currently available logs (drillers, geologists, sample and core analysis, all types electric, etc.), formation and pressure tests, and directional surveys, should be attached hereto, to the extent required by applicable Federal and/or State laws and regulations. All attachments should be listed on this form, see item 35.

Item 4: If there are no applicable State requirements, locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local State or Federal office for specific instructions.

Item 18: Indicate which elevation is used as reference (where not otherwise shown) for depth measurements given in other spaces on this form and in any attachments.

Items 22 and 24: If this well is completed for separate production from more than one interval zone (multiple completion), so state in item 22, and in item 24 show the producing interval, or intervals, top(s), bottom(s) and name(s) (if any) for only the interval reported in item 33. Submit a separate report (page) on this form, adequately identified, for each additional interval to be separately produced, showing the additional data pertinent to such interval.

Item 29: "Sacks Cement": Attached supplemental records for this well should show the details of any multiple stage cementing and the location of the cementing tool.

Item 33: Submit a separate completion report on this form for each interval to be separately produced. (See instruction for items 22 and 24 above.)

37. SUMMARY OF POROUS ZONES:

SHOW ALL IMPORTANT ZONES OF POROSITY AND CONTENTS THEREOF; CORED INTERVALS; AND ALL DRILL-STEM TESTS, INCLUDING DEPTH INTERVAL TESTED, CUSHION USED, TIME TOOL OPEN, FLOWING AND SHUT-IN PRESSURES, AND RECOVERIES

| FORMATION | TOP | BOTTOM | DESCRIPTION, CONTENTS, ETC. |
|-------------|--------|----------|-----------------------------|
| Castlegate | 5030 | 5330 | Wet |
| Dakota | 8820 | 9010 | Wet |
| Morrison | 9010 ✓ | 9335 | Wet |
| Salt Wash | 9335 ✓ | 9642 | Wet |
| Summerville | 9642 ✓ | 9700 | Tite |
| Entrada | 9700 ✓ | 9830 | Wet |
| Navajo | 9830 | 9920 | Wet |
| Keyenta | 9985 | 10,103 | Tite |
| Wingate | 10103 | 10,568 ✓ | Wet |
| Chinle | 10568 | 10,663 ✓ | Tite |

38.

GEOLOGIC MARKERS

| NAME | TOP | |
|-------------|-------------|------------------|
| | MEAS. DEPTH | TRUE VERT. DEPTH |
| Castlegate | 5030 | |
| Dakota | 8820 | |
| Morrison | 9010 | |
| Salt Wash | 9335 | |
| Summerville | 9642 | |
| Entrada | 9700 | |
| Navajo | 9830 | |
| Kayenta | 9985 | |
| Wingate | 10103 | |
| Chinle | 10568 | |
| Granite | 10663 | |

ECU - FROM LITHO LOGS

ESTIMATED COMPOSITIONS

WELL ECU-93, Sec 23, T18S-R 20E

LOG BY ROCKY MTN. GEO-ENGINEERING CO.

Surface - Green River

| | THICKNESS | % sh | % ss | % carb | GYP | k_e |
|--------------------------------------|-----------|------|------|--------|-----|-------|
| (Tertiary) BOTTOM WASATCH | 330 | | | | | 6.8 |
| MESQUITE SURFACE TO CASTLEGATE | 5030 | 50 | 50 | | | 7.0 |
| (BUT NO MATTER) CASTLEGATE TOO THICK | 1890 | | | | | |
| CASTLEGATE | 300' | 40 | 60 | | | 7.6 |
| MANCOS | 3490' | 98 | 2 | | | 4.1 |
| DAKOTA | 190' | 48 | 48 | 4 | ✓ | 7.0 |
| MORRISON | 325' | 80 | 20 | | | 5.2 |
| SALT WASH | 307' | 80 | 20 | | | 5.2 |
| JUMMERSVILLE | 58' | 60 | 40 | | | 6.4 |
| ENTRADA | 130' | 30 | 70 | | ✓ | 8.2 |
| NAVAJO | 90' | 20 | 80 | | | 8.8 |
| KAYENTA | 118' | 20 | 80 | | | 8.8 |
| WINGATE | 465' | 20 | 80 | | | 8.8 |
| CHINLE | 95' | 60 | 40 | | | 6.4 |

BOTTOM IN pE 10663' - 10786'

k_e = thermal conductivity in $\frac{\text{milliwatt}}{\text{cm sec } ^\circ\text{C}}$

estimated from:

100% shale = 4.0

100% sand = 10.0

k_e = 7.0

BHT's

- 1 110°F @ 4713' $k_e = 6.8$ 7.0 $k_e = 7.0$
- 2 110°F @ 5447' $k_e = 6.8$ 6.9
- 3 173°F @ 9869' $k_e = 5.8$ 5.9
- 4 176°F @ 10787' (TD) $k_e = 6.0$ 6.1

wtd from surface

INDEPENDENT
CALCULATION

surface Green River

log begins at 2810 in Wasatch

| | | |
|---------------|-------------|------|
| above Green R | 0 - 2140 | 2140 |
| wasatch | 2140 - 3140 | 1000 |
| Mesa Verde | 3140 - 5030 | 1890 |
| Castlegate | 5030 - 5100 | 70 |
| Moncos | 5100 - 8600 | 3500 |
| Dakota | 8820 | |

96

began logging surface in watch

| | | |
|-------------|-----|--------------|
| 375 | 5.5 | 2062 |
| 1000 | 6.7 | 6700 |
| 959 | 5.6 | 5370 |
| 230 | 4.0 | 4920 |
| 182 | 5.4 | 983 |
| 3444 | 4.0 | 13776 |
| 166 | 8.9 | 1477 |
| 75 | 6.1 | 458 |
| 197 | 5.2 | 1024 |
| 266 | 4.6 | 1224 |
| 62 | 5.2 | 322 |
| 74 | 8.8 | 651 |
| <u>7030</u> | | <u>38967</u> |

BHT 183° @ 7023

Re = 5.5

ECU 96

SEC. 15, T18S-R 22 E

✓

EST. COMPOSITIONS - LITHO BY POWELL & COLLINS

| | THICKNESS | % [*] sh | % ss | % ^{**} CARB. | GYP | ke | |
|-------------------|-----------------|-------------------|------|-----------------------|-----|-----|--------------------|
| SURFACE - WASATCH | BOTTOM 375 | 69 | 20 | 11 | | 5.5 | |
| MESAVERDE | 1/2 TOP 1959 | 55 | 45 | | | 6.7 | TOP 1/2 |
| | 1/2 BOT | 74 | 26 | | | 5.6 | BOTTOM 1/2 |
| BUCK TONGUE | 230 | 100 | 0 | | | 4.0 | |
| CASTLE GATE | 182 | 77 | 23 | | ✓ | 5.4 | 6.7 5.6 12/3 |
| MANCOS | 3416 | 100 | 0 | ✓ | | 4.0 | |
| B/DAKOTA SILT | 28 | 100 | 0 | | | 4.0 | |
| DAKOTA | 166 | 18 | 82 | | | 8.9 | |
| CEDAR MTN. | 75 | 65 | 35 | | | 6.1 | |
| MORRISON ? | 197 | 80 | 20 | | | 5.2 | |
| SALT WASH ? | 266 | 90 | 10 | | | 4.6 | |
| SUMMERVILLE ? | 62 | 80 | 20 | | | 5.2 | |
| ENTRADA ? | TOP - 74' | 20 | 80 | | | 8.8 | |

BOTTOM IN ENTRADA AT 7030

* Siltstone & sh

** includes quartzite

est. therm. conductivity

ke in milli cal
cm sec °C

sh = 4.0

ss = 10.0

ls = 7.0

~~BHTS~~
T18S

96

Anschutz

Fed 078 #1

sec 15, T18S-R22E

Grand

Drilling application

Estimated imp. geol. on where

was at surface

Castle gate 1740

Mason 1805

Dehola 5265

Cedar netn 5338

Jim 5418

Salt Wash 5725

Summersville 6011

Je 6070

Est TD 6200

Duplicate

try to get actual

Est depth of ant. water, oil, gas

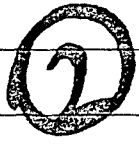
Dakota 5265 gas and/or oil H₂O

Jim 5418 gas or H₂O

Je 6070 gas

Schlumberger

**SIMULTANEOUS
COMPENSATED NEUTRON
FORMATION DENSITY**



COMPANY THE ANSCHUTZ CORP

WELL NO. 1 FEDERAL 078

FIELD DIAMOND CANYON UNIT

COUNTY GRAND STATE UTAH

| | | | |
|----------|----------------|------|------|
| LOCATION | 3850FWL 730FSL | | |
| | API SERIAL NO. | SEC. | TWP. |
| | 15 | 18S | 22E |

| | |
|-----------------|----|
| Other Services: | |
| DIL | 96 |
| CDR | |

COUNTY GRAND
FIELD DIAMOND CANYON UNIT
LOCATION 3850FWL 730FSL
WELL NO. 1 FEDERAL 078
COMPANY THE ANSCHUTZ CORP

Permanent Datum: GL; Elev.: 6055
Log Measured From: KB, 10 Ft. Above Perm. Datum
Drilling Measured From: KB

Elev.: K.B. 6065
D.F. --
G.I. 6055

| | | | | | |
|---------------------|----------------------|----------------|------|------|------|
| Date | 6-8-78 | | | | |
| Run No. | ONE | | | | |
| Depth-Driller | 7030 | | | | |
| Depth-Logger | 7025 | | | | |
| 3ft. Log Interval | 7023 34.7 | | | | |
| Top Log Interval | 112 | | | | |
| Casing-Driller | 7" | @ 2760 | @ | @ | @ |
| Casing-Logger | -- | | | | |
| Bit Size | 6 1/2 | | | | |
| Type Fluid in Hole | FGM | | | | |
| Dens. | 9.2 | 44 | | | |
| Visc. | | | | | |
| pH | 7.6 | 10.6ml | ml | ml | ml |
| Fluid Loss | | | | | |
| Source of Sample | MUDTANK | | | | |
| Rm @ Meas. Temp. | .554 @ | 71°F | @ °F | @ °F | @ °F |
| Rmf @ Meas. Temp. | .482 @ | 71°F | @ °F | @ °F | @ °F |
| Rmc @ Meas. Temp. | -- @ | --°F | @ °F | @ °F | @ °F |
| Source: Rmf | M | -- | | | |
| Rmc | | | | | |
| Rm @ BHT | .21 @ | 483 | @ °F | @ °F | @ °F |
| Circulation Stopped | ~2000 | 6-8 | | | |
| Logger on Bottom | 0530 | 6-9 | | | |
| Max. Rec. Temp. | | 183°F | °F | °F | °F |
| Equip. | 7759 | G.J. | | | |
| Location | | | | | |
| Recorded By | GRTAYLOR | | | | |
| Witnessed By Mr. | ALLRED/COLLINS | | | | |

The well name, location and borehole reference data were furnished by the customer.

FOLD HERE

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

SUBMIT IN DUPLICATE
(See other instructions on reverse side)

Form approved.
Budget Bureau No. 42-R355.5.

96 15

WELL COMPLETION OR RECOMPLETION REPORT AND LOG *

1a. TYPE OF WELL: OIL WELL GAS WELL DRY Other

b. TYPE OF COMPLETION: NEW WELL WORK OVER DEEP-EN PLUG BACK DIFF. RESVR. Other

2. NAME OF OPERATOR
The Anschutz Corporation

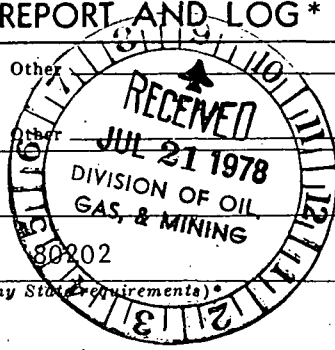
3. ADDRESS OF OPERATOR
1110 Denver Club Bldg., Denver, Colorado 80202

4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements)*
At surface

At top prod. interval reported below 3850' FWL + 730' FSL

At total depth

14. API NO. 43-019-30371 DATE ISSUED 6-15-77



5. LEASE DESIGNATION AND SERIAL NO.
U-14078

6. IF INDIAN, ALLOTTEE OR TRIBE NAME

7. UNIT AGREEMENT NAME
Diamond Canyon

8. FARM OR LEASE NAME
Federal 078

9. WELL NO.
1

10. FIELD AND POOL, OR WILDCAT
Wildcat

11. SEC., T., R., M., OR BLOCK AND SURVEY OR AREA
SW 1/4 SE 1/4 Sec. 15T 18S R22E

12. COUNTY OR PARISH Grand 13. STATE Utah

15. DATE SPUNDED 5-8-78 16. DATE T.D. REACHED 6-9-78 17. DATE COMPL. (Ready to prod.) P&A 6-9-78 18. ELEVATIONS (DF, RKB, RT, GR, ETC.)* 6055 GL 6064 KB 19. ELEV. CASINGHEAD 6055

20. TOTAL DEPTH, MD & TVD 7030 21. PLUG, BACK T.D., MD & TVD 22. IF MULTIPLE COMPL., HOW MANY* 23. INTERVALS DRILLED BY Surface-TD 24. PRODUCING INTERVAL(S), OF THIS COMPLETION—TOP, BOTTOM, NAME (MD AND TVD)* NONE 25. WAS DIRECTIONAL SURVEY MADE Yes

26. TYPE ELECTRIC AND OTHER LOGS RUN DIL - GR, CNL-FDC-GR 27. WAS WELL CORED No

28. CASING RECORD (Report all strings set in well)

| CASING SIZE | WEIGHT, LB./FT. | DEPTH SET (MD) | HOLE SIZE | CEMENTING RECORD | AMOUNT PULLED |
|-------------|-----------------|----------------|-----------|----------------------|---------------|
| 9-5/8 | 36 | 112 | 12 1/2 | 65sks circulated | None |
| 7 | 23 | 2760 | 8-3/4 | 75sks est. top 2100' | 1056' |

29. LINER RECORD 30. TUBING RECORD

| SIZE | TOP (MD) | BOTTOM (MD) | SACKS CEMENT* | SCREEN (MD) | SIZE | DEPTH SET (MD) | PACKER SET (MD) |
|------|----------|-------------|---------------|-------------|------|----------------|-----------------|
| | | | | | | | |

31. PERFORATION RECORD (Interval, size and number) 32. ACID, SHOT, FRACTURE, CEMENT SQUEEZE, ETC.

| DEPTH INTERVAL (MD) | AMOUNT AND KIND OF MATERIAL USED |
|---------------------|----------------------------------|
| | |

33.* PRODUCTION

DATE FIRST PRODUCTION PRODUCTION METHOD (Flowing, gas lift, pumping—size and type of pump) WELL STATUS (Producing or shut-in)

| DATE OF TEST | HOURS TESTED | CHOKE SIZE | PROD'N. FOR TEST PERIOD | OIL—BBL. | GAS—MCF. | WATER—BBL. | GAS-OIL RATIO |
|--------------|--------------|------------|-------------------------|----------|----------|------------|---------------|
| | | | | | | | |

34. DISPOSITION OF GAS (Sold, used for fuel, vented, etc.) TEST WITNESSED BY

35. LIST OF ATTACHMENTS
Logs

36. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records.

SIGNED Peter B. Doty TITLE Operations Coordinator DATE 7-19-78

*(See Instructions and Spaces for Additional Data on Reverse Side)

INSTRUCTIONS

General: This form is designed for submitting a complete and correct well completion report and log on all types of lands and leases to either a Federal agency or a State agency or both, pursuant to applicable Federal and/or State laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from, the local Federal and/or State office. See instructions on Items 22 and 24, and 33, below regarding separate reports for separate completions.

If not filed prior to the time this summary record is submitted, copies of all currently available logs (drillers, geologists, sample and core analysis, all types electric, etc.), formation and pressure tests, and directional surveys, should be attached hereto, to the extent required by applicable Federal and/or State laws and regulations. All attachments should be listed on this form, see item 35.

Item 4: If there are no applicable State requirements, locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local State or Federal office for specific instructions.

Item 18: Indicate which elevation is used as reference (where not otherwise shown) for depth measurements given in other spaces on this form and in any attachments.

Items 22 and 24: If this well is completed for separate production from more than one interval zone (multiple completion), so state in item 22, and in item 24 show the producing interval, or intervals, top(s), bottom(s) and name(s) (if any) for only the interval reported in item 33. Submit a separate report (page) on this form, adequately identified, for each additional interval to be separately produced, showing the additional data pertinent to such interval.

Item 29: "Sacks Cement": Attached supplemental records for this well should show the details of any multiple stage cementing and the location of the cementing tool.

Item 33: Submit a separate completion report on this form for each interval to be separately produced. (See instruction for items 22 and 24 above.)

37. SUMMARY OF POROUS ZONES:

SHOW ALL IMPORTANT ZONES OF POROSITY AND CONTENTS THEREOF; CORED INTERVALS; AND ALL DRILL-STEM TESTS, INCLUDING DEPTH INTERVAL TESTED, CUSHION USED, TIME TOOL OPEN, FLOWING AND SHUT-IN PRESSURES, AND RECOVERIES

| FORMATION | TOP | BOTTOM | DESCRIPTION, CONTENTS, ETC. |
|-----------|------|--------|-----------------------------|
| Dakota | 6192 | 6342 | Sand + Shale - Wet |
| Morrison | 6342 | 6628 | Tite Sands + Shale |
| Salt Wash | 6628 | 6950 | Tite Sands + Shale |
| Entrada | 6950 | TD | Wet |

38.

GEOLOGIC MARKERS

| NAME | TOP | |
|-----------|-------------|------------------|
| | MEAS. DEPTH | TRUE VERT. DEPTH |
| Wasatch | Sur | +6055 |
| Mesaverde | 350 | +5705 |
| Mancos | 2710 Est. | +3345 |
| Dakota | 6192 | - 137 |
| Morrison | 6342 | - 287 |
| Salt Wash | 6628 | - 573 |
| Entrada | 6950 | - 895 |
| TD | 7030 | - 975 |

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

SUBMIT IN DUPLICATE

(See other instructions on reverse side)

Form approved.
Budget Bureau No. 42-R355.6

121

WELL COMPLETION OR RECOMPLETION REPORT AND LOG *

1a. TYPE OF WELL: OIL WELL GAS WELL DRY Other _____

b. TYPE OF COMPLETION: NEW WELL WORK OVER DEEP-EN PLUG BACK DIFF. RESVR. Other _____

2. NAME OF OPERATOR
The Anschutz Corporation

3. ADDRESS OF OPERATOR
1110 Denver Club Building, Denver, Colorado 80202

4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements)*
At surface 1630' FWL, 1490' FSL
At top prod. interval reported below
At total depth

5. LEASE DESIGNATION AND SERIAL NO.
U-0149769

6. IF INDIAN, ALLOTTEE OR TRIBE NAME

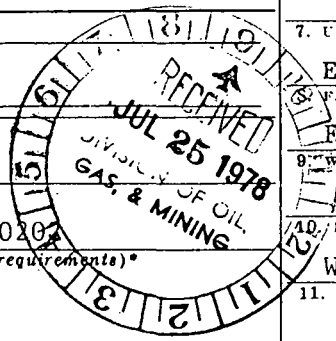
7. UNIT AGREEMENT NAME
East Willow Creek

8. FARM OR LEASE NAME
Federal 769

9. WELL NO.
1

10. FIELD AND POOL, OR WILDCAT
Wildcat

11. SEC., T., R., M., OR BLOCK AND SURVEY OR AREA
Sec. 19, T.19S-R.21E.



14. PERMIT NO. API 43-019-30352 DATE ISSUED 4-19-77

12. COUNTY OR PARISH Grand 13. STATE Utah

15. DATE SPUDDED 4-7-78 16. DATE T.D. REACHED 5-2-78 17. DATE COMPL. (Ready to prod.) P & A 5-3-78 18. ELEVATIONS (DF, RKB, RT, GR, ETC.)* 6514 GL, 6523 KB 19. ELEV. CASINGHEAD 6514'

20. TOTAL DEPTH, MD & TVD 5400' 21. PLUG, BACK T.D., MD & TVD 22. IF MULTIPLE COMPL., HOW MANY* 23. INTERVALS DRILLED BY Surface-TD 24. ROTARY TOOLS 25. CABLE TOOLS None

24. PRODUCING INTERVAL(S), OF THIS COMPLETION—TOP, BOTTOM, NAME (MD AND TVD)* None 25. WAS DIRECTIONAL SURVEY MADE Yes

26. TYPE ELECTRIC AND OTHER LOGS RUN DIL, CNL/FDL, BGT 27. WAS WELL CORED No

23. CASING RECORD (Report all strings set in well)

| CASINO SIZE | WEIGHT, LB./FT. | DEPTH SET (MD) | HOLE SIZE | CEMENTING RECORD | AMOUNT PULLED |
|-------------|-----------------|----------------|-----------|-----------------------|---------------|
| 8-5/8" | 24# | 1600 | | Circulated to surface | |

29. LINER RECORD

| SIZE | TOP (MD) | BOTTOM (MD) | SACKS CEMENT* | SCREEN (MD) |
|------|----------|-------------|---------------|-------------|
| | | | | |

30. TUBING RECORD

| SIZE | DEPTH SET (MD) | PACKER SET (MD) |
|------|----------------|-----------------|
| | | |

31. PERFORATION RECORD (Interval, size and number)

| DEPTH INTERVAL (MD) | AMOUNT AND KIND OF MATERIAL USED |
|---------------------|----------------------------------|
| | |

33.* PRODUCTION

DATE FIRST PRODUCTION _____ PRODUCTION METHOD (Flowing, gas lift, pumping—size and type of pump) _____ WELL STATUS (Producing or shut-in) _____

| DATE OF TEST | HOURS TESTED | CHOKE SIZE | PROD'N. FOR TEST PERIOD | OIL—BBL. | GAS—MCF. | WATER—BBL. | GAS-OIL RATIO |
|--------------|--------------|------------|-------------------------|----------|----------|------------|---------------|
| | | | | | | | |

| FLOW. TUBING PRESS. | CASING PRESSURE | CALCULATED 24-HOUR RATE | OIL—BBL. | GAS—MCF. | WATER—BBL. | OIL GRAVITY-API (CORR.) |
|---------------------|-----------------|-------------------------|----------|----------|------------|-------------------------|
| | | | | | | |

34. DISPOSITION OF GAS (Sold, used for fuel, vented, etc.) _____ TEST WITNESSED BY _____

35. LIST OF ATTACHMENTS

LOGS

36. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records

SIGNED R B D TITLE OPERATIONS COORDINATOR DATE 7-18-78

*(See Instructions and Spaces for Additional Data on Reverse Side)

INSTRUCTIONS

General: This form is designed for submitting a complete and correct well completion report and log on all types of lands and leases to either a Federal agency or a State agency, or both, pursuant to applicable Federal and/or State laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from, the local Federal and/or State office. See instructions on items 22 and 24, and 33, below regarding separate reports for separate completions.

If not filed prior to the time this summary record is submitted, copies of all currently available logs (drillers, geologists, sample and core analysis, all types electric, etc.), formation and pressure tests, and directional surveys, should be attached hereto, to the extent required by applicable Federal and/or State laws and regulations. All attachments should be listed on this form, see item 35.

Item 4: If there are no applicable State requirements, locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local State or Federal office for specific instructions.

Item 18: Indicate which elevation is used as reference (where not otherwise shown) for depth measurements given in other spaces on this form and in any attachments.

Items 22 and 24: If this well is completed for separate production from more than one interval zone (multiple completion), so state in item 22, and in item 24 show the producing interval, or intervals, top(s), bottom(s) and name(s) (if any) for only the interval reported in item 33. Submit a separate report (page) on this form, adequately identified, for each additional interval to be separately produced, showing the additional data pertinent to such interval.

Item 29: "Sacks Cement": Attached supplemental records for this well should show the details of any multiple stage cementing and the location of the cementing tool.

Item 33: Submit a separate completion report on this form for each interval to be separately produced. (See instruction for items 22 and 24 above.)

37. SUMMARY OF POROUS ZONES:

SHOW ALL IMPORTANT ZONES OF POROSITY AND CONTENTS THEREOF; CORED INTERVALS; AND ALL DRILL-STEM TESTS, INCLUDING DEPTH INTERVAL TESTED, CUSHION USED, TIME TOOL OPEN, FLOWING AND SHUT-IN PRESSURES, AND RECOVERIES

| FORMATION | TOP | BOTTOM | DESCRIPTION, CONTENTS, ETC. |
|-----------|-----|--------|-----------------------------|
| | | | |
| | | | |
| | | | |
| | | | |

38.

GEOLOGIC MARKERS

| NAME | TOP | |
|-------------------|-------------|------------------|
| | MEAS. DEPTH | TRUE VERT. DEPTH |
| Mesa Verde | Surface | Subsea |
| Mancos | Surface | +6514 <i>GL</i> |
| Dakota | 4571 | +1943 |
| Morrison | 4694 | +1820 |
| Salt Wash | 4846 | +1668 |
| Entrada | 5326 | +1188 |
| T.D. | 5400 | +1114 |

Schlumberger

**COMPENSATED NEUTRON-
FORMATION DENSITY**

COMPANY THE ANSCHUTZ CORP

WELL FEDERAL 769-1

FIELD WILDCAT

COUNTY GRAND STATE UTAH

COUNTY GRAND
FIELD WILDCAT
LOCATION NESW 1630FWL 1490FSL
WELL FEDERAL 769-1
COMPANY THE ANSCHUTZ CORP

| | | | |
|----------------|-----------------|------|-------|
| LOCATION | NE SW | | |
| | 1630FWL 1490FSL | | |
| API SERIAL NO. | SEC. | TWP. | RANGE |
| | 19 | 19S | 21E |

Other Services:
DIL 121

Permanent Datum: GL; Elev.: 6514
Log Measured From KB, 9 Ft. Above Perm. Datum
Drilling Measured From KB

Elev.: K.B. 6523
D.F. --
G.L. 6514

| | | | | | |
|---------------------|-----------------|-------------|--------|----|----|
| Date | 5-1-78 | | | | |
| Run No. | ONE | | | | |
| Depth-Driller | 5400 | | | | |
| Depth-Logger | 5399 | | | | |
| Btm. Log Interval | <u>5398</u> | <u>28.4</u> | | | |
| Top Log Interval | 50 | | | | |
| Casing-Driller | 8 5/8 @ 1600 | | @ | @ | @ |
| Casing-Logger | -- | | | | |
| Bit Size | 7 7/8 | | | | |
| Type Fluid in Hole | FGM | | | | |
| Dens. | Visc. | 9.0 | 39 | | |
| pH | Fluid Loss | 11.0 | 9.8 ml | ml | ml |
| Source of Sample | MUDTANK | | | | |
| Rm @ Meas. Temp. | .547 @ 70°F | @ | °F | @ | °F |
| Rmf @ Meas. Temp. | .299 @ 70°F | @ | °F | @ | °F |
| Rmc @ Meas. Temp. | -- @ --°F | @ | °F | @ | °F |
| Source: Rmf | Rmc | M | | | |
| Rm @ BHT | .28 @ <u>35</u> | @ | °F | @ | °F |
| Circulation Stopped | 1400 | 5-01 | | | |
| Logger on Bottom | 2100 | 5-01 | | | |
| Max. Rec. Temp. | | <u>35</u> | °F | °F | °F |
| Equip. | Location | 7759 | G.J. | | |
| Recorded By | GRTAYLOR | | | | |
| Witnessed By Mr. | ALLRED/POWELL | | | | |

The well name, location and borehole reference data were furnished by the customer.

121

log begins surface in Km

BHT 135° @ 5398 in Entada $k_e = 5.0$

| | | |
|------|-----|-------|
| 874 | 6.7 | 5856 |
| 122 | 5.3 | 647 |
| 286 | 8.3 | 2374 |
| 3259 | 4.1 | 13362 |
| 30 | 4.0 | 120 |
| 104 | 7.1 | 738 |
| 19 | 6.2 | 118 |
| 152 | 4.6 | 699 |
| 404 | 5.4 | 2182 |
| 72 | 4.7 | 338 |
| 78 | 9.7 | 757 |

5400

27191

503

ECL 121

Sec. 19, T19S - R21E

EST. COMP. - LITHO LOG BY WAYNE POWELL

| | THICKNESS | % silt | % ss | % CARB | % GYP | k_e | |
|---------------------|---------------|--------|------|--------|-------|-------|------------|
| SURFACE - MESAVERDE | BOTTOM 874 | 54.5 | 45.5 | | | 6.7 | lower 874' |
| BLACK TONGUE | 122 | 79 | 21 | | | 5.3 | |
| CASTLEGATE | 286 | 29 | 71 | | | 8.3 | |
| MANCOS | 3259 | 98 | 2 | | | 4.1 | |
| B/DAKOTA SILT | 30 | 100 | 0 | | | 4.0 | |
| DAKOTA | 104 | 49 | 51 | | | 7.1 | |
| CEDAR MTN | 19 | 63 | 37 | | | 6.2 | |
| MORRISON | 152 | 90 | 10 | | | 4.6 | |
| SALT WASH | 404 | 74 | 22 | 4 | | 5.4 | |
| SUMMERVILLE | 72 | 89 | 11 | | | 4.7 | |
| ENTRADA | TOP 78 | 5 | 95 | | | 9.7 | upper 78' |

BOTTOM IN ENTRADA AT 5400

k_e in $\frac{\text{millial}}{\text{cm sec}^2}$

sh = 4.0

SS = 10.0

LS = 7.0

121 Anschutz Fed 796-1
sec 19, T19S-R21E

Actual

| | | |
|-----------------------|--------------------|-----------------|
| Mesa Verde | surface | NO (Mesa Verde) |
| Kd | 4571 | OK |
| dm | 4694 | |
| Salt Wash | 4846 | |
| Te | 5326 | |
| TD | 5400 | |

USGS ^{H₂O} evaluation (prior to drilling)

USGS H₂O evaluation

| | |
|------------------|-----------------------|
| Unit | Qual H ₂ O |
| Mesa Verde group | fresh/saline |
| Km | saline |
| Kd | saline |
| dm | saline/brine |
| Te | brine |

No H₂O wells vicinity
prev. oil tests found brackish
or saline water at depths greater
than 300ft Useable water for
stock (sheep) may be found
as deep as 500'

**UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY**

SUBMIT IN DUPLICATE*

(See other instructions on reverse side)

Form approved.
Budget Bureau No. 42-R355.5.

150 2

WELL COMPLETION OR RECOMPLETION REPORT AND LOG *

a. TYPE OF WELL: OIL WELL GAS WELL DRY Other _____

b. TYPE OF COMPLETION: NEW WELL WORK OVER DEEP-EN PLUG BACK DIFF. RESVR. Other _____

2. NAME OF OPERATOR
The Anschutz Corporation

3. ADDRESS OF OPERATOR
2400 Anaconda Tower, Denver, Colorado 80202

4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements)*
At surface 768' FNL, 1520' FEL

At top prod. interval reported below

At total depth

14. PERMIT NO. _____ DATE ISSUED _____

5. LEASE DESIGNATION AND SERIAL NO.

U-15104

6. IF INDIAN, ALLOTTEE OR TRIBE NAME

7. UNIT AGREEMENT NAME

8. FARM OR LEASE NAME

Federal 104

9. WELL NO.

1

10. FIELD AND POOL, OR WILDCAT

Wildcat

11. SEC., T., R., M., OR BLOCK AND SURVEY OR AREA

Sec. 4, T. 20S-R. 21E

12. COUNTY OR PARISH

Grand

13. STATE

Utah

15. DATE SPUDDED 4-29-78 16. DATE T.D. REACHED 5-10-78 17. DATE COMPL. (Ready to prod.) 6-22-78 18. ELEVATIONS (DF, REB, RT, GR, ETC.)* 6159 GR 6205 KB 19. ELEV. CASINGHEAD 6195

20. TOTAL DEPTH, MD & TVD 4300' 21. PLUG, BACK T.D., MD & TVD 3920' 22. IF MULTIPLE COMPL., HOW MANY* _____ 23. INTERVALS DRILLED BY _____ ROTARY TOOLS _____ CABLE TOOLS _____

24. PRODUCING INTERVAL(S), OF THIS COMPLETION—TOP, BOTTOM, NAME (MD AND TVD)*
Dakota 3520'-3526' MD
3549'-3555' MD

25. WAS DIRECTIONAL SURVEY MADE

Yes

26. TYPE ELECTRIC AND OTHER LOGS RUN
DILL-GR, FDC-CNL-GR, Geologic Report, Geologic Well Log

27. WAS WELL CORED

No

28. CASING RECORD (Report all strings set in well)

| CASING SIZE | WEIGHT, LB./FT. | DEPTH SET (MD) | HOLE SIZE | CEMENTING RECORD | AMOUNT PULLED |
|-------------|-----------------|----------------|-----------|------------------|---------------|
| 8-5/8" | 24# | 319 | 12 1/4" | 230 sx | None |
| 4 1/2" | 10.5# | 4119' | 7-7/8" | 300 sx | None |

29. LINER RECORD

| SIZE | TOP (MD) | BOTTOM (MD) | SACKS CEMENT* | SCREEN (MD) |
|------|----------|-------------|---------------|-------------|
| | | | | |

30. TUBING RECORD

| SIZE | DEPTH SET (MD) | PACKER SET (MD) |
|-------|----------------|-----------------|
| 2.375 | 3565' | |

31. PERFORATION RECORD (Interval, size and number)

3520-26 3/8" holes 2 SPF
3549-55 3/8" holes 2 SPF

32. ACID, SHOT, FRACTURE, CEMENT SQUEEZE, ETC.

| DEPTH INTERVAL (MD) | AMOUNT AND KIND OF MATERIAL USED |
|---------------------|----------------------------------|
| | |

33.* PRODUCTION

| DATE FIRST PRODUCTION | PRODUCTION METHOD (Flowing, gas lift, pumping—size and type of pump) | WELL STATUS (Producing or shut-in) |
|-----------------------|--|------------------------------------|
| | <u>Flowing</u> | <u>S.I. W.O. PL Connection</u> |

| DATE OF TEST | HOURS TESTED | CHOKE SIZE | PROD'N. FOR TEST PERIOD | OIL—BBL. | GAS—MCF. | WATER—BBL. | GAS-OIL RATIO |
|----------------|--------------|--------------|-------------------------|----------|-------------|------------|---------------|
| <u>7/20/78</u> | <u>18</u> | <u>28/64</u> | <u>→</u> | <u>0</u> | <u>3600</u> | <u>0</u> | <u>-----</u> |

| FLOW. TUBING PRESS. | CASING PRESSURE | CALCULATED 24-HOUR RATE | OIL—BBL. | GAS—MCF. | WATER—BBL. | OIL GRAVITY-API (CORR.) |
|---------------------|-----------------|-------------------------|----------|-------------|------------|-------------------------|
| <u>343</u> | <u>600</u> | <u>→</u> | <u>0</u> | <u>4800</u> | <u>0</u> | <u>-----</u> |

34. DISPOSITION OF GAS (Sold, used for fuel, vented, etc.)
Flared

TEST WITNESSED BY
J. N. Burkhalter

35. LIST OF ATTACHMENTS

36. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records

SIGNED R.B.R. TITLE Production Coordinator DATE 12-4-78

* (See Instructions and Spaces for Additional Data on Reverse Side)

INSTRUCTIONS

General: This form is designed for submitting a complete and correct well completion report and log on all types of lands and leases to either a Federal agency or a State agency, or both, pursuant to applicable Federal and/or State laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from, the local Federal and/or State office. See instructions on items 22 and 24, and 33, below regarding separate reports for separate completions.

If not filed prior to the time this summary record is submitted, copies of all currently available logs (drillers, geologists, sample and core analysis, all types electric, etc.), information and pressure tests, and directional surveys, should be attached hereto, to the extent required by applicable Federal and/or State laws and regulations. All attachments should be listed on this form, see item 35.

Item 4: If there are no applicable State requirements, locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local State or Federal office for specific instructions.

Item 18: Indicate which elevation is used as reference (where not otherwise shown) for depth measurements given in other spaces on this form and in any attachments.

Items 22 and 24: If this well is completed for separate production from more than one interval zone (multiple completion), so state in item 22, and in item 24 show the producing interval, or intervals, top(s), bottom(s) and name(s) (if any) for only the interval reported in item 33. Submit a separate report (page) on this form, adequately identified, for each additional interval to be separately produced, showing the additional data pertinent to such interval.

Item 29: "Sacks Cement": Attached supplemental records for this well should show the details of any multiple stage cementing and the location of the cementing tool.

Item 33: Submit a separate completion report on this form for each interval to be separately produced. (See instruction for items 22 and 24 above.)

37. SUMMARY OF POROUS ZONES:

SHOW ALL IMPORTANT ZONES OF POROSITY AND CONTENTS THEREOF; CORED INTERVALS; AND ALL DRILL-STEM TESTS, INCLUDING DEPTH INTERVAL TESTED, CUSHION USED, TIME TOOL OPEN, FLOWING AND SHUT-IN PRESSURES, AND RECOVERIES

| FORMATION | TOP | BOTTOM | DESCRIPTION, CONTENTS, ETC. |
|-----------|---------|-------------|-----------------------------|
| Dakota | 3522' ✓ | 3706' ✓ | Sandstone - Gas |
| Morrison | 3706' ✓ | 3889' ✓ | Wet - Tite |
| Salt Wash | 3889' | 4266' | Wet - Tite |
| Entrada | 4266' | Not Reached | Wet - Tite |

38.

GEOLOGIC MARKERS

| NAME | TOP | |
|-----------|-------------|------------------|
| | MEAS. DEPTH | TRUE VERT. DEPTH |
| Dakota | 3522' | 3522' |
| Morrison | 3706' | 3706' |
| Salt Wash | 3889' | 3889' |
| Entrada | 4266' | 4266' |

ECU 150

Sec 4, T20S-R21E

EST. COMP. LITHO BY A.W. POWELL

logged only below 3,000'

log begins here →

| | THICKNESS | % sh | % ss | % carb | gyp | Re | |
|--------------------|-------------------------------|------|------|--------|-----|------|-------------|
| SURFACE-BUCKTONGUE | — | | | | | | |
| CASTLEGATE | 72 | | | | | | |
| MANCOS | 3326 BOTTOM 326 | 100 | 0 | | | 4.0 | BOTTOM 522' |
| B/DAKOTA SILT | 50 | 100 | 0 | | | 4.0 | |
| DAKOTA | 102 | N | E | S | | | |
| CEDAR MTN. | 82 | 75 | 25 | | | 5.5 | |
| MORRISON | 183 | 90 | 10 | | ✓ | 4.6 | |
| SALT WASH | 315 | 83 | 17 | | | 5.0 | |
| SUMMERVILLE | 60 | 90 | 10 | | | 4.6 | |
| ENTRADA | TOP 65 | 0 | 100 | | | 10.0 | TOP 65' |

BOTTOM IN ENTRADA AT 4329'

BHTs

120°F @ 4323 (TD)

Schlumberger

**DUAL INDUCTION - LATERO LOG
WITH LINEAR CORRELATION LOG**

12

COMPANY THE ANSCHUTZ CORP

WELL FEDERAL 104-1

FIELD WILDCAT

COUNTY GRAND STATE UTAH

Location: 500FNL API Serial No. 1400FEL
Sec. 4 Twp. 20S Rge. 21E 2

Other Services:
FDC-CNL-GR
150

COUNTY GRAND
FIELD or LOCATION WILDCAT
WELL FEDERAL 104-1
COMPANY ANSCHUTZ CORP

Permanent Datum: GL; Elev.: 6159
Log Measured From KB 10 Ft. Above Perm. Datum
Drilling Measured From KB

Elev.: K.B. 6169
D.F. --
G.L. 6159

| | | | | | | |
|-------------------------------|-----------------|-------|-------|----|----|----|
| Date | 5-10-78 | | | | | |
| Run No. | ONE | | | | | |
| Depth-Driller | 4320 | | | | | |
| Depth-Logger | 4329 | | | | | |
| Bit Log Interval | 4323 | 27.1 | | | | |
| Top Log Interval | 322 | | | | | |
| Casing-Driller | 8 5/8 | 319 | @ | @ | @ | @ |
| Casing-Logger | 322 | | | | | |
| Bit Size | 7 7/8 | | | | | |
| Type Fluid in Hole | FGM | | | | | |
| Fluid Level | FULL | | | | | |
| Dens. | Visc. | -- | -- | | | |
| pH | Fluid Loss | -- | -- ml | ml | ml | ml |
| Source of Sample | CIRCULATED | | | | | |
| R _m @ Meas. Temp. | 1.06 @ | 67°F | @ | °F | @ | °F |
| R _{mf} @ Meas. Temp. | .822 @ | 67°F | @ | °F | @ | °F |
| R _{mc} @ Meas. Temp. | 1.59 @ | 67°F | @ | °F | @ | °F |
| Source: R _{mf} | R _{mc} | M | C | | | |
| R _{tr} @ BHT | 0.60 @ | 120°F | @ | °F | @ | °F |
| Time Since Circ. | 3 HOURS | | | | | |
| Max. Rec. Temp. | 120°F | | | °F | | °F |
| Equip. | Location | 5642 | G.J. | | | |
| Recorded By | LAUDE | | | | | |
| Witnessed By | POWELL | | | | | |

150

log begins at 3000'
surface in meaverde

| | | | |
|-----------------|--------------|------|-------|
| (74) 0-74 | Buck Tongues | 5.3 | 392 |
| (72) 74-146 | Castlegate | 8.0 | 576 |
| (3326) 146-3472 | Marcos | 4.0 | 13304 |
| 50' | B/Dak silt | 4.0 | 200 |
| 102' | Dakota | 7.7 | 785 |
| 82 | Cedar Mtn | 5.5 | 451 |
| 183 | monson | 4.6 | 842 |
| 315 | saltwash | 5.0 | 1575 |
| 60 | summeville | 4.6 | 276 |
| 65 | Entrada | 10.0 | 650 |
| <hr/> | | | |
| 4329 | | | 19051 |

BHT 120° F @ 4323 $k_e = 4.4$

SCHLUMBERGER

GAMMA RAY - NEUTRON

COUNTY
FIELD or
LOCATION
WELL
COMPANY

COMPANY Shell Oil Company

①

WELL Federal 1-26

FIELD Wildcat

COUNTY Grand STATE Utah

Location: 2050' SLY. & 800' WLY.
From NE Corner

Other Services:

234

7

Sec. 26 Twp. 21S Rge. 17E

Permanent Datum: G.L.; Elev.: 4439
Log Measured From K.B., 13 Ft. Above Perm. Datum
Drilling Measured From K.B.

Elev.: K.B. 4452
D.F. _____
G.L. 4439


| | |
|------------------------|-------------------------------|
| Date | <u>7-7-69</u> |
| Run No. | <u>3</u> |
| Type Log | <u>GRN</u> |
| Depth—Driller | <u>11,895</u> |
| Depth—Logger | <u>11,886</u> |
| Bottom logged interval | <u>11,885</u> 21.7 |
| Top logged interval | <u>10,786</u> |
| Type fluid in hole | <u>S B M</u> |
| Salinity, PPM Cl. | <u>> 200,000</u> |
| Density | <u>17.2</u> |
| Level | <u>Full</u> |
| Max rec. temp., deg F. | <u>79.0</u> @ <u>7-7-1800</u> |
| Operating rig time | <u>2 hr</u> |
| Recorded by | <u>Thomas</u> |
| Witnessed by | <u>McLehaney</u> |

| BORE-HOLE RECORD | | | | CASING RECORD | | | |
|------------------|--------------|------------|------------|---------------|----------|--------------|-------------|
| Run No. | Bit | From | To | Size | Wgt. | From | To |
| <u>3</u> | <u>6 1/4</u> | <u>CSG</u> | <u>T.D</u> | <u>7</u> | <u>-</u> | <u>Surf.</u> | <u>8271</u> |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |

SCHLUMBERGER

BOHNERDLE COMPENSATED
SONIC LOG GAMMA RAY

COUNTY FIELD or LOCATION WELL COMPANY
 S7-1-2152

COMPANY Shell Oil Company 

WELL Federal 1-26

FIELD Wildcat

COUNTY Grand STATE Utah

LOCATION 2050'sly - 800' wly fr N.E. Cor

Other Services:
IES
ST 234

Sec. 26 Twp. 21S Rge. 17E

Permanent Datum: KL, Elev. 4439

Log Measured From K.B., 13 Ft. Above Perm. Datum

Drilling Measured From K.B.

Elev.: K.B. 4452
D.F. _____
G.L. 4439

| | | | | | | |
|---|---------------------|--------|--|------|------|------|
| Date | 3-21-69 | | | | | |
| Run No. | 1 | | | | | |
| Depth—Driller | 1780 | | | ① | | |
| Depth—Logger | 1780 | | | | | |
| tm. Log Interval | 1777 564 | | | | | |
| op Log Interval | 1222 | | | | | |
| casing—Driller | 13 3/8 @ 1223 | | | @ | @ | @ |
| casing—Logger | 1222 | | | | | |
| bit Size | 9" | | | | | |
| type Fluid in Hole | FGM | | | | | |
| Dens. | 9.5 | 72 | | | | |
| Visc. | | | | | | |
| pH | 9.5 | 6.4 ml | | ml | ml | ml |
| Fluid Loss | | | | | | |
| Source of Sample | C.R. | | | | | |
| R _m @ Meas. Temp. | 2.00 @ 61 °F | | | @ °F | @ °F | @ °F |
| R _{mf} @ Meas. Temp. | 1.48 @ 61 °F | | | @ °F | @ °F | @ °F |
| R _{mc} @ Meas. Temp. | 1.2 @ 61 °F | | | @ °F | @ °F | @ °F |
| Source: R _{mf} R _{mc} | M | C | | | | |
| R _m @ BHT | 0.81 @ 105 °F | | | @ °F | @ °F | @ °F |
| Time Since Circ. | 3 hr | | | | | |
| Max. Rec. Temp. | 105 °F | | | °F | °F | °F |
| Equip. Location | 4529 | 4316 | | | | |
| Recorded By | B. Thomas | | | | | |
| Witnessed By | Koenig & Rauch | | | | | |

SCHLUMBERGER

INDUCTION ELECTRICAL LOG

S7-1-2152

COUNTY
FIELD or
LOCATION
WELL
COMPANY

COMPANY Shell Oil Company



WELL Federal 1-26

FIELD Wildcat

COUNTY Grand STATE Utah

LOCATION 2050' sly - 800' wly fr
N.E. Cor. 9
Sec. 26 Twp. 21S Rge. 17E

Other Services:
BHC/GR
DIL 21 **234**

Permanent Datum: G.L., Elev. 4439
Log Measured From K.B., 13 Ft. Above Perm. Datum
Drilling Measured From K.B.

Elev.: K.B. 4452
D.F.
G.L. 4439

| | | | | | | | |
|-------------------------------|-----------------------|-------------|--------|-----|----|---|----|
| Date | 4-30-69 | | | | | | |
| Run No. | 1 | | | | | | |
| Depth—Driller | 7560 | | | | | | |
| Depth—Logger | 7560 | | | | | | |
| Btm. Log Interval | 7559 22 ft | | | (2) | | | |
| Top Log Interval | 1400 | | | | | | |
| Casing—Driller | 1 3/8 @ 1220 | | | @ | @ | @ | @ |
| Casing—Logger | 1222 | | | | | | |
| Bit Size | 9" | | | | | | |
| Type Fluid in Hole | FGM | | | | | | |
| Dens. | Visc. | 9.7 | 62 | | | | |
| pH | Fluid Loss | 11.0 | 9.0 ml | | ml | | ml |
| Source of Sample | | Circ. | | | | | |
| R _m @ Meas. Temp. | 1.03 @ 76 °F | @ | °F | @ | °F | @ | °F |
| R _{mf} @ Meas. Temp. | 0.54 @ 76 °F | @ | °F | @ | °F | @ | °F |
| R _{mc} @ Meas. Temp. | 0.90 @ 76 °F | @ | °F | @ | °F | @ | °F |
| Source: R _{mf} | M | C | | | | | |
| R _m @ BHT | 0.51 @ 141 °F | @ | °F | @ | °F | @ | °F |
| Time Since Circ. | 14 hr | | | | | | |
| Max. Rec. Temp. | 146 °F | | | | °F | | °F |
| Equip. | Location | 4529 Jernol | | | | | |
| Recorded By | B. Thomas | | | | | | |
| Witnessed By | E. Knepprich | | | | | | |



SIDEWALL NEUTRON POROSITY LOG

57-1-2152

COUNTY FIELD or LOCATION WELL COMPANY

COMPANY SHELL OIL COMPANY

WELL FEDERAL #1-26



FIELD WILDCAT

COUNTY GRAND STATE UTAH

Location: 2050' SLY. & 800' WLY. FROM NE CORNER

Other Services:
LL, MLL,
BHC-GR,
FDC-GR
234

Sec. 26 Twp. 21S Rge. 17E

Permanent Datum: GL; Elev.: 4439
Log Measured From KB, 13 Ft. Above Perm. Datum
Drilling Measured From KB

Elev.: K.B. 4495
D.F.
G.L. 442

| | |
|------------------------|-----------------------------|
| Date | <u>5-11-69</u> |
| Run No. | <u>ONE</u> |
| Type Log | <u>EPITHERMAL-NEUTRON</u> |
| Depth—Driller | <u>8271</u> |
| Depth—Logger | <u>8270</u> |
| Bottom logged interval | <u>8268</u> ^{22.5} |
| Top logged interval | <u>SURFACE</u> |
| Type fluid in hole | <u>SBM</u> |
| Salinity, PPM Cl. | <u>85,000</u> |
| Density | <u>13.0</u> |
| Level | <u>FULL</u> |
| Max rec. temp., deg F. | <u>153.0</u> |
| Operating rig time | <u>6 HR</u> |
| Recorded by | <u>PROBST</u> |
| Witnessed by | <u>KOEPERICH</u> |

~~TIGHT HOLE~~

| BORE-HOLE RECORD | | | | CASING RECORD | | | |
|------------------|-----------|------------|-----------|---------------|-----------|----------------|-------------|
| Run No. | Bit | From | To | Size | Wgt. | From | To |
| <u>1</u> | <u>9"</u> | <u>C56</u> | <u>TD</u> | <u>13 3/8</u> | <u>34</u> | <u>SURFACE</u> | <u>1220</u> |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |

SCHLUMBERGER

SONIC LOG - GAMMA RAY

S7-1-2152

COUNTY
FIELD or
LOCATION
WELL
COMPANY

COMPANY Shell Oil Company

WELL Federal No. 1-26

2

FIELD Wildcat

COUNTY Grand STATE Utah

LOCATION 2050' SLY + 800' WLY
From NE Corner

Other Services:
ICS
GRN 234

Sec. 26 Twp. 21S Rge. 17E

Permanent Datum: GL, Elev. 4439
Log Measured From KB, 13 Ft. Above Perm. Datum
Drilling Measured From KB

Elev.: K.B. 445
D.F. —
G.L. 443

| | | | | | |
|---|--------------------------------|--------------|----|----|------|
| Date | <u>6-6-69</u> | | | | |
| Run No. | <u>4</u> | | | | |
| Depth—Driller | <u>9653</u> | | | | |
| Depth—Logger | <u>8470</u> | | | | |
| Btm. Log Interval | <u>8468</u> ^{123.7} | | | | |
| Top Log Interval | <u>7800</u> | | | | |
| Casing—Driller | <u>7" @ 8271</u> | @ | @ | @ | @ |
| Casing—Logger | <u>8273</u> | | | | |
| Bit Size | <u>6 1/4"</u> | (4) | | | |
| Type Fluid in Hole | <u>SBM</u> | | | | |
| Dens. | <u>17.1</u> | <u>100</u> | | | |
| Visc. | | | | | |
| pH | <u>9.5</u> | <u>5.2ml</u> | | | |
| Fluid Loss | | | ml | | ml |
| Source of Sample | <u>Flow Line</u> | | | | |
| R _m @ Meas. Temp. | <u>0.34 @ 72°F</u> | @ | °F | @ | °F @ |
| R _{mf} @ Meas. Temp. | <u>0.14 @ 72°F</u> | @ | °F | @ | °F @ |
| R _{mc} @ Meas. Temp. | <u>0.16 @ 72°F</u> | @ | °F | @ | °F @ |
| Source: R _{mf} R _{mc} | <u>M</u> | <u>M</u> | | | |
| R _m @ BHT | <u>0.15 @ 167°F</u> | @ | °F | @ | °F @ |
| Time Since Circ. | <u>4 HR</u> | | | | |
| Max. Rec. Temp. | <u>76</u> | °F | | °F | °F |
| Equip. | <u>4529</u> | <u>Verna</u> | | | |
| Location | | | | | |
| Recorded By | <u>Godfrey</u> | | | | |
| Witnessed By | <u>Koepferich</u> | | | | |

ECU 234

SEC 26, T81S-R17E

EST. COMP. - LITHO LOG BY UNDERWOOD

log begins 45'

| | THICKNESS | % / | | | cong GTA | ke |
|---------------------------|-----------|---------------|----|------|---------------|-----|
| | | sh silt st | ss | carb | | |
| SURFACE - MANCOS | 80 T.O.M | 100 | 0 | ✓ | | 4.0 |
| DAKOTA ? | | | | | | |
| MORRISON (INCL. SALTWASH) | 800 | 45 | 55 | | | 7.3 |
| CURTIS | 340 | 25 | 75 | | | 8.5 |
| ENTRADA | 315 | 15 | 85 | | | 9.1 |
| CARMEL | 130 | 40 | 60 | | | 7.6 |
| NAVAJO | 395 | 5 | 95 | | | 9.7 |
| KAYENTA | 95 | 10 | 90 | | | 9.4 |
| WINGATE | 455 | 10 | 90 | | | 9.4 |
| CHINLE | 273 | 90 | 10 | | | 4.6 |
| SHINARUMP | 37 | 90 | 10 | | | 4.6 |
| MOENKOPI | 748 | 72 | 14 | 11 | 3* | 5.3 |
| WHITE RIM | 202 | 10 | 90 | | | 9.4 |
| CUTLER | 230 | 49 | 48 | 3 | | 7.0 |
| ELEPHANT CAN? | 790 | 14 | 20 | 66 | | 7.2 |
| HONAKER TR | 1670 | 25 | 20 | 55 | | 6.8 |
| PARADOX | ? | 15 | | 10 | saltant 75 | 8.8 |

SALT AT 7920

TO ~~800~~ 12000' IN PENNSYLVANIAN

BITS 61° @ 1777 ①

* prob shale

146 @ 7559 ②

153 @ 8265 ③

15 = 7

161 @ 8468 ④

SS = 10

165 @ 10786 ⑤

Sh = 4

UNITED STATES DEPARTMENT OF THE INTERIOR GEOLOGICAL SURVEY

234

APPLICATION FOR PERMIT TO DRILL, DEEPEN, OR PLUG BACK

1a. TYPE OF WORK DRILL [X] DEEPEN [] PLUG BACK []

b. TYPE OF WELL OIL WELL [X] GAS WELL [] OTHER [] SINGLE ZONE [] MULTIPLE ZONE []

2. NAME OF OPERATOR Shell Oil Company

3. ADDRESS OF OPERATOR 1600 Norris Road, Bakersfield, California 93308

4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements.) At surface 820± ft. from east line and 2140± ft. from north line, Section 26, T. 21 S., R. 17 E., S.L.B. & M. (location plat to follow) At proposed prod. zone Same. SW SENE

14. DISTANCE IN MILES AND DIRECTION FROM NEAREST TOWN OR POST OFFICE*

15. DISTANCE FROM PROPOSED* LOCATION TO NEAREST PROPERTY OR LEASE LINE, FT. (Also to nearest drlg. unit line, if any) 820± ft. from east line

16. NO. OF ACRES IN LEASE 2000 Ac.

17. NO. OF ACRES ASSIGNED TO THIS WELL 80

18. DISTANCE FROM PROPOSED LOCATION* TO NEAREST WELL, DRILLING, COMPLETED, OR APPLIED FOR, ON THIS LEASE, FT.

19. PROPOSED DEPTH 12,000 Ft.

20. ROTARY OR CABLE TOOLS Rotary

21. ELEVATIONS (Show whether DF, RT, GR, etc.) 4440 Ft. ground.

22. APPROX. DATE WORK WILL START* March 1, 1969

23. PROPOSED CASING AND CEMENTING PROGRAM

Table with 4 columns: SIZE OF HOLE, SIZE OF CASING, WEIGHT PER FOOT, SETTING DEPTH. Rows: 26" hole to 40±', 17-1/2" hole to 1200±', 13-3/8" casing, 54.5#, 1200±'.

Surface formation: Mancos

- 1. Drill 26" hole to 40±' and set 20" conductor pipe.
2. Drill 17-1/2" hole to 1200±'. Run and cement 13-3/8", 54.5#, 800± sacks.
3. Install 12" Series 900 double hydraulic gate with blank and 12" Series 900 GK Hydril. Test BOPE and casing with 1000 psi for 15 min.
4. Drill 9-7/8" hole to 12,000±' (Mississippian).

This is a prospect well, and casing program will depend upon formations encountered. Please keep all information private and confidential.

IN ABOVE SPACE DESCRIBE PROPOSED PROGRAM: If proposal is to deepen or plug back, give data on present productive zone and proposed new productive zone. If proposal is to drill or deepen directionally, give pertinent data on subsurface locations and measured and true vertical depths. Give blowout preventer program, if any.

24. SIGNED Robert L. Spitzerwood

TITLE Division Exploration Eng. DATE 2/18/69

(This space for Federal or State office use)

PERMIT NO. 43-019-30029

APPROVAL DATE

APPROVED BY

TITLE

CONDITIONS OF APPROVAL, IF ANY:

Vertical text on the right side of the form, likely bleed-through from the reverse side, containing various administrative and technical notes.

OPER APPROVAL TO BUREAU OF LAND MANAGEMENT

Operator Shell Oil Co Job No. Ed Koerperich

Well No. 1-26 Located SE NW 26 Sec. 21 S Twp. 17 E

Lease No. U-7121 Well WC State OK

Unit Name and Required Depth N/A Name of Operator or Owner _____

P.D. 11,895 Size hole and No. of strings 10+

Setting Set Top of To Be String Depth _____

13 3/8" @ 1220' surface none - set 100' plug in top of 7" annulus
7" @ 8271 5475 none - set 100' plug in 7" - 13 3/8" annulus

| Formation | Base | Shore |
|---------------|------|-------|
| Morrison | 1440 | ✓ |
| Custer | 2240 | ✓ |
| Entrada | 2580 | ✓ |
| Cannel | 2895 | ✓ |
| Navajo | 3025 | ✓ |
| Nezperce | 3420 | ✓ |
| Wingate | 3515 | ✓ |
| Chile | 3970 | ✓ |
| Shinarump | 4243 | ✓ |
| Moenkopi | 4280 | ✓ |
| Whitekin | 5028 | ✓ |
| Cutter | 5230 | ✓ |
| Elephant Cave | 5460 | ✓ |
| Honader Tr. | 6250 | ✓ |
| Salt | 7920 | |
| L. Huron | ? | |

- will perforate! annulus at least 100' plug above top of Navajo

- will perforate & annulate at least 100' plug above top of Whitekin - base Moenkopi

- set CIPB topped w/300' oval in bore of 7"

11,895 11,795 if able to get loose
Prob. did not penetrate Musiniquia

No soluble salts below 8275'.
DST @ 8200-8300? showed no permeability (run on shale gas show). DST @ 6455 see salt water. No sig show of hydrocarbon. lost 3' 11,895-95' lost circulation & have been having hole problems. At TD, stuck. Will run 8 way - annulus

Approved by Rodney A. Smith Date 2/7/69 Time 9:00
Seismic shots, gravimeter & try to get loose. If

234

0-1270 Marcor (incl. Dak set) 4.1

1270-1440 Dakotas

1440-2240 Morrison (highss for Jm) 7.3

BHT ① 61 at 1770

$k_e = 5.0$

| | | | |
|-------|---|-----|------|
| 1270 | x | 4.1 | 5207 |
| 170 | x | 7.7 | 1309 |
| 330 | x | 7.3 | 2409 |
| <hr/> | | | |
| 1770 | | | 8925 |

BHT ② 146 @ 7559

$k_e = 7.2$

| | | | |
|-------|---|-----|-------|
| 1270 | x | 4.1 | 5207 |
| 170 | x | 7.7 | 1309 |
| 800 | x | 7.3 | 5840 |
| 340 | x | 8.6 | 2890 |
| 315 | x | 9.1 | 2866 |
| 130 | x | 7.6 | 988 |
| 395 | x | 9.7 | 3832 |
| 4139 | x | 7.6 | 31456 |
| <hr/> | | | |
| 7559 | | | 54390 |

$\frac{22932}{3420} = 6.7$

(use for
Glen Can → HONAKER

Jm

BHT ③ 153 @ 8268

$k_e = 7.2$

| | | | |
|-------|---|-----|-------|
| 3420 | x | 6.7 | 22914 |
| 4848 | x | 7.6 | 36845 |
| <hr/> | | | |
| 8268 | | | 59759 |

Continued

BHT (4) 161° @ 8468

$$Re = 7.3$$

$$3420 \times 6.7 = 22914$$

$$4500 \times 7.6 = 34200$$

$$\underline{548 \times 9.0} = 4932$$

$$8468 = 62046$$

BHT (5) 165 @ 10786

$$Re = 7.7$$

$$3420 \times 6.7 = 22914$$

$$4500 \times 7.6 = 34200$$

$$\underline{2866 \times 9.0} = 25794$$

$$10786 = 82908$$

50 (2) lineully Feb 104 #1

Well Well # 1-26 mus, 21.5-175

Water Encountered

6465-6615 2100' hard (30561)

NaCl 17,000 ppm

| | Depth |
|-----|-------|
| Jan | 1440 |
| Jan | 2240 |
| Jan | 2580 |
| Jan | 2895 |
| Jan | 3025 |
| Jan | 3420 |
| Jan | 3615 |
| Jan | 3970 |
| Jan | 4243 |
| Jan | 4280 |
| Jan | 5028 |
| Jan | 5230 |
| Jan | 5460 |
| Jan | 6250 |
| Jan | 7920 |

total depth 11895'

note: all most panels to Musgrave

Duplicated

log is 14' long
cannot break loose cap

100% Sh 0-1270
20% Sh 1270-1460
30% Sh 1460-2200
15% Sh 2200-3000
90% SS - 3000-3960
90% Sh - 3960-4940
95% SS - 4940-5200
50-50 Sh SS - 5200-5450
60% Sh 5450-7920
40% Sh
1920'
Salt

SCHLUMBERGER

**BOREHOLE COMPENSATED
SONIC LOG - GAMMA RAY**

57-1-2153

COUNTY
FIELD or
LOCATION
WELL
COMPANY

COMPANY SHELL OIL Co.

WELL MOUNTAIN FUEL FEDERAL 1-21

FIELD WILDCAT

COUNTY GRAND STATE UTAH

LOCATION

627 FWL, 608 FNL

Sec. 21 Twp. 23-S Rge. 18 E

Other Services:

DIL 297

Permanent Datum: GL, Elev. 4510
Log Measured From KB, 15 Ft. Above Perm. Datum
Drilling Measured From KB

Elev.: K.B. 4525
D.F. 4524
G.L. 4510

| | | | | |
|-------------------------------|---------------------------|------------------|----------------|-----|
| Date | <u>8-1-69</u> | | | |
| Run No. | <u>ONE</u> | | | |
| Depth—Driller | <u>1821</u> | | | |
| Depth—Logger | <u>1822</u> | | | |
| Btm. Log Interval | <u>1820</u> | | | |
| Top Log Interval | <u>120</u> | | | |
| Casing—Driller | <u>@</u> | | | |
| Casing—Logger | <u>32</u> | | | |
| Bit Size | <u>12 1/4</u> | | | |
| Type Fluid in Hole | <u>LIME</u> | | | |
| Dens. | Visc. | <u>9.1</u> | <u>36</u> | |
| pH | Fluid Loss | <u>11.0</u> | <u>12.4 ml</u> | |
| Source of Sample | <u>FLOW LINE</u> | | | |
| R _m @ Meas. Temp. | <u>3.07 @ 80° F</u> | @ | ° F | |
| R _{mf} @ Meas. Temp. | <u>3.13 @ 80° F</u> | @ | ° F | |
| R _{mc} @ Meas. Temp. | <u>4.10 @ 80° F</u> | @ | ° F | |
| Source: R _{mf} | R _{mc} | <u>M</u> | <u>CB</u> | |
| R _m @ BHT | <u>-</u> | @ | <u>-</u> | ° F |
| Time Since Circ. | <u>2 1/2 HRS</u> | | | |
| Max. Rec. Temp. | <u>TLTM</u> | | | ° F |
| Equip. | Location | <u>3860 FARM</u> | | |
| Recorded By | <u>WELLS & LEBACK</u> | | | |
| Witnessed By | <u>MR. McLEHANEY</u> | | | |

**TIGHT
HOLE**

FIELD PRINT

SCHLUMBERGER

BOREHOLE COMPENSATED SONIC LOG - GAMMA RAY

57-1-2153

COUNTY FIELD or LOCATION WELL No. API No. 43-019-30038 COMPANY

COMPANY Shell Oil Company

1

WELL Mountain Fuel Federal 1-21

FIELD Wildcat

COUNTY Grand STATE Utah

LOCATION 627 FWL
608 FNL

Other Services:
FDC/GR
SNP/GR
DIL **297**

Sec. 21 Twp. 23S Rge. 18E

Permanent Datum: G.L., Elev. 4510
Log Measured From K.B., 15 Ft. Above Perm. Datum
Drilling Measured From K.B.

Elev.: K.B. 4525
D.F. _____
G.L. 4510

| | | | | | | | |
|-------------------------------|----------------------------|--------------|---------------|---|----|---|----|
| Date | <u>8-24-69</u> | | | | | | |
| Run No. | <u>1</u> | | | | | | |
| Depth—Driller | <u>5732</u> | | | | | | |
| Depth—Logger | <u>5737</u> | | | | | | |
| Bfm. Log Interval | <u>5734^{25.1}</u> | | | | | | |
| Top Log Interval | <u>1823</u> | | | | | | |
| Casing—Driller | <u>9 5/8</u> | @ | <u>1821</u> | @ | @ | @ | @ |
| Casing—Logger | <u>1823</u> | | | | | | |
| Bit Size | <u>8 3/4</u> | | | | | | |
| Type Fluid in Hole | <u>Clay Base</u> | | | | | | |
| Dens. | Visc. | <u>8.9</u> | <u>40</u> | | | | |
| pH | Fluid Loss | <u>11.0</u> | <u>8.8 ml</u> | | ml | | ml |
| Source of Sample | | <u>Circ.</u> | | | | | |
| R _m @ Meas. Temp. | <u>0.816</u> | @ | <u>66 °F</u> | @ | °F | @ | °F |
| R _{mf} @ Meas. Temp. | <u>0.645</u> | @ | <u>76 °F</u> | @ | °F | @ | °F |
| R _{mc} @ Meas. Temp. | <u>0.86</u> | @ | <u>66 °F</u> | @ | °F | @ | °F |
| Source: R _{mf} | R _{mc} | <u>M</u> | <u>C</u> | | | | |
| R _m @ BHT | <u>0.414</u> | @ | <u>130 °F</u> | @ | °F | @ | °F |
| Time Since Circ. | <u>20 hr</u> | | | | | | |
| Max. Rec. Temp. | <u>130 °F</u> | | | | °F | | °F |
| Equip. | Location | <u>5616</u> | <u>4316</u> | | | | |
| Recorded By | <u>G. Thomas</u> | | | | | | |
| Witnessed By | <u>D. McLehane</u> | | | | | | |

surface probably Morrison
began logging at 30'

| | sh | ss | ls | brlyd Salt | | |
|--------------------|----|----|-----|---------------|-----|------|
| 670 30-700 | 40 | 50 | 5 | 7.0 | 7.0 | 4690 |
| 300 700-1700 | 5 | 95 | | 9.7 | 9.7 | 2910 |
| 300 1700-2000 | 60 | 20 | 20 | 5.5 | 5.8 | 1740 |
| 1000 2000-3000 | 50 | 45 | 5 | 6.0 | 6.8 | 6800 |
| 1000 3000-4000 | 45 | 40 | 15 | 6.0 | 6.8 | 6800 |
| 1000 4000-5000 | 20 | 20 | 60 | 7.0 | 7.0 | 9000 |
| BITF 735 5000-5735 | 10 | 30 | 60 | 7.6 | 7.6 | 5586 |
| 5005 265 5735-6000 | | | 40 | 60 | 8.8 | 2332 |
| 1000 6000-7000 | | | 20 | 80 | 9.4 | 9400 |
| 45 1000 7000-8000 | 15 | | | 85 | 9.1 | 9100 |
| 1000 8000-9000 | 5 | | | 95 | 9.7 | 9700 |
| 1000 9000-10000 | 15 | | 25 | 60 | 9.1 | 9100 |
| 330 10000-10330 | - | - | 100 | - | 7.0 | 2310 |
| 9600 | | | | | | |

k_e (above Paradox) = 7.1

k_e (Paradox) = 9.1

Total hole = 7.9

sh 4

ss 10

ls 7

salt
artificial 10

| | |
|-------------|-------------|
| BIT's | |
| 130 @ 5734 | $k_e = 7.1$ |
| 164 @ 10330 | $k_e = 8.1$ |

ECU 307

sec 1, 245-17E

surface in glass canyon

salt 5216 - 8600

| TD | sh | % | ls | k_e | |
|-----------|----|----|----|-------|-------|
| 0-1000' | 10 | 90 | | 9.4 | 9400 |
| 1000-2000 | 75 | 25 | | 5.5 | 5500 |
| 2000-3000 | 60 | 30 | 10 | 6.1 | 6100 |
| 3000-4000 | 25 | 15 | 55 | 6.4 | 6400 |
| 4000-5000 | 5 | 25 | 70 | 7.6 | 7600 |
| 5000-5216 | 45 | 25 | 30 | 6.4 | 1382 |
| | | | | | 36382 |

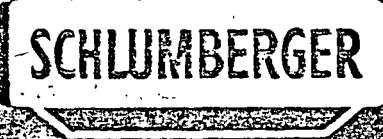
Note
7.6 on 318

BHT's

k_e
weighted from surface

| | |
|-------------|-----|
| 95° @ 1474 | 8.4 |
| 119° @ 5218 | 7.0 |
| 143° @ 9125 | 7.7 |

BOREHOLE COMPENSATED SONIC LOG - GAMMA RAY



S7-1-2160

COUNTY
FIELD or
LOCATION
WELL
COMPANY

COMPANY SHELL OIL COMPANY

WELL SHELL - QUINTANA # 1-1

FIELD WILDCAT

COUNTY GRAND STATE UTAH

LOCATION 1602'E & 1566'N
FROM SW CORNER

Sec. 1 Twp. 24S Rge. 17E

Other Services:
DIL

307

Permanent Datum: GL, Elev. 4465
 Log Measured From KB 14 Ft. Above Perm. Datum
 Drilling Measured From KB

Elev.: K.B. 4479
 D.F. _____
 G.L. 4465

| | | | | | | |
|-------------------------------|-----------------------------|------------|----------------|---------------------|----|------|
| Date | <u>10-6-69</u> | | | | | |
| Run No. | <u>ONE</u> | | API No. | <u>43-019-30042</u> | | |
| Depth—Driller | <u>1475</u> | | | | | |
| Depth—Logger | <u>1476</u> | | | | | |
| Btm. Log Interval | <u>1474 54.4</u> | | | | | |
| Top Log Interval | <u>SURFACE</u> | | | | | |
| Casing—Driller | <u>20" @ 10</u> | | @ | | @ | @ |
| Casing—Logger | <u>20</u> | | | | | |
| Bit Size | <u>12 1/4</u> | | | | | |
| Type Fluid in Hole | <u>FGM</u> | | | | | |
| Dens. | Visc. | <u>9.5</u> | <u>43</u> | | | |
| pH | Fluid Loss | <u>11</u> | <u>12.2 ml</u> | ml | ml | ml |
| Source of Sample | <u>FLOW LINE</u> | | | | | |
| R _m @ Meas. Temp. | <u>2.36 @ 66 °F</u> | @ | °F | @ | °F | @ °F |
| R _{mf} @ Meas. Temp. | <u>1.93 @ 58 °F</u> | @ | °F | @ | °F | @ °F |
| R _{mc} @ Meas. Temp. | <u>3.65 @ 63 °F</u> | @ | °F | @ | °F | @ °F |
| Source: R _{mf} | <u>M</u> | | | | | |
| R _{mc} | <u>M</u> | | | | | |
| R _m @ BHT | <u>1.65 @ 85 °F</u> | @ | °F | @ | °F | @ °F |
| Time Since Circ. | <u>3 HR</u> | | | | | |
| Max. Rec. Temp. | <u>95 °F</u> | | | °F | °F | °F |
| Equip. Location | <u>4544 VERNAL</u> | | | | | |
| Recorded By | <u>PROBST</u> | | | | | |
| Witnessed By | <u>MS LEHANEY</u> | | | | | |

SCHLUMBERGER

BOREHOLE COMPENSATED SONIC LOG - GAMMA RAY

57-1-2160

COUNTY
FIELD or
LOCATION
WELL
COMPANY

COMPANY SHELL OIL COMPANY

307

WELL QUINTANA #1-1

2

FIELD WILDCAT

COUNTY GRAND STATE UTAH

LOCATION 1602' E & 1566' N
FROM SW CORNER

Other Serv
DIL
SNP-G
FDC-G
CST

Sec. 1 Twp. 24 S Rge. 17 E

Permanent Datum: GL, Elev. 4465
Log Measured From KB, 14 Ft. Above Perm. Datum
Drilling Measured From KB

Elev.: K.B. 4
D.F. 4
G.L. 4
307

| | | | |
|---|------------------------------|---------------|---------------------|
| Date | <u>10-23-69</u> | API NO. | <u>43-019-30042</u> |
| Run No. | <u>TWO</u> | | |
| Depth—Driller | <u>5216</u> | | |
| Depth—Logger | <u>5220</u> | | |
| 3m. Log Interval | <u>5218</u> ^{23.8} | | |
| Top Log Interval | <u>1479</u> | | |
| Casing—Driller | <u>9 5/8 @ 1475</u> | @ | @ |
| Casing—Logger | <u>1479</u> | | |
| Bit Size | <u>8 3/4</u> | | |
| Type Fluid in Hole | <u>GEL</u> | | |
| Dens. | <u>9.1</u> | <u>41</u> | |
| pH | <u>11.0</u> | <u>7.8 ml</u> | ml |
| Fluid Loss | | | |
| Source of Sample | <u>FLOWLINE</u> | | |
| R _m @ Meas. Temp. | <u>1.03 @ 64 °F</u> | @ | °F |
| R _{mf} @ Meas. Temp. | <u>0.80 @ 64 °F</u> | @ | °F |
| R _{mc} @ Meas. Temp. | <u>1.24 @ 66 °F</u> | @ | °F |
| Source: R _{mf} R _{mc} | <u>M M</u> | | |
| R _m @ BHT | <u>0.55 @ 119 °F</u> | @ | °F |
| Time Since Circ. | <u>14 H</u> | | |
| Max. Rec. Temp. | <u>119 °F</u> | °F | °F |
| Equip. Location | <u>3860 FARM</u> | | |
| Recorded By | <u>WELLS</u> | | |
| Witnessed By | <u>MCLEHANEY & DOGAN</u> | | |

FIELD

PDM

SCHLUMBERGER

INDICATOR COMPENSATED
SONIC LOG - GAMMA RAY

57-1-2160

COUNTY
FIELD or
LOCATION
WELL
COMPANY

COMPANY SHELL OIL COMPANY



WELL QUINTANA # 1-1

FIELD WILDCAT

307

COUNTY GRAND

STATE UTAH

LOCATION
1672' E & 1566' N FROM
SW CORNER S
Sec. 1 Twp. 24S Rge. 17E

Other Services:

L-GR
SNP-GR
FDC-GR
CIS
PDT 307

Permanent Datum: GL, Elev. 4465
Log Measured From KB, 14 Ft. Above Perm. Datum
Drilling Measured From KB

Elev.: K.B. 4479
D.F.
G.L. 4465

| | | | | | |
|---|------------------|--------------|----|----|----|
| Date | 11-9-69 | | | | |
| Run No. | THREE | | | | |
| Depth—Driller | 9140 | | | | |
| Depth—Logger | 9134 | | | | |
| Btm. Log Interval | 9125 114 | | | | |
| Top Log Interval | 5218 | | | | |
| Casing—Driller | 9 5/8 @ 1475 | | @ | @ | @ |
| Casing—Logger | - | | | | |
| Bit Size | 8 3/4" | | | | |
| Type Fluid in Hole | SALT BASE | | | | |
| Dens. | Visc. | 10.6 38 | | | |
| pH | Fluid Loss | 11.0 92 ml | ml | ml | ml |
| Source of Sample | FLOWLINE | | | | |
| R _m @ Meas. Temp. | .057 @ 70°F | .030 @ 143°F | @ | @ | @ |
| R _{mf} @ Meas. Temp. | .051 @ 70°F | .028 @ 143°F | @ | @ | @ |
| R _{mc} @ Meas. Temp. | .080 @ 70°F | .041 @ 143°F | @ | @ | @ |
| Source: R _{mf} R _{mc} | M M | | | | |
| R _m @ BHT | .030 @ 143°F | @ °F | @ | @ | @ |
| Time Since Circ. | 19 HRS | | | | |
| Max. Rec. Temp. | 143 °F | | °F | °F | °F |
| Equip. | Location | 5625 FARM | | | |
| Recorded By | WELLS & MCBAE | | | | |
| Witnessed By | MCLFANEY & DOGAN | | | | |

FIELD
PDT

ECU 311 (new)

Sec 7, T 24S - R 21E

Began logging at 1000' in Kayenta

| | THICK | sh | ss | ls |
|------------|----------------|----|----|-----|
| Kayenta | BOTTOM 173' | 20 | 80 | 88 |
| Wingate | 397 | 35 | 65 | 7.9 |
| Chinle | 810 | 50 | 50 | 7.0 |
| Nesankopi? | ? | 80 | 20 | 5.2 |
| White Rim | TOP 155 | 45 | 55 | 7.3 |

Bottom in white Rim at 4964'

~~4802~~
755

BHTS 90° F @ 4785

94° F @ 4965

311

① $90^\circ @ 4785$ $h_e = 6.6$
 $94 @ 4964$ $h_e = 6.6$

log begins at 1000' in Kayenta
surface

| | | | | |
|------|---------|--------|-----|-------|
| wt { | Jerome | 373 @ | 8.0 | 2984 |
| | Navajo | 500 @ | 9.5 | 4750 |
| | Kayenta | 300 @ | 8.8 | 2640 |
| | Wupate | 397 @ | 7.9 | 3136 |
| | Chinle | 810 @ | 7.0 | 5670 |
| | > | 2429 @ | 5.2 | 12631 |
| | | <hr/> | | |
| | | 4809 | | 31811 |

use for both 6.6

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

SUBMIT IN DUPLICATE*

(See other In-
structions on
reverse side)

Form approved.
Budget Bureau No. 42-R355.5

WELL COMPLETION OR RECOMPLETION REPORT AND LOG*

1a. TYPE OF WELL: OIL WELL GAS WELL DRY Other _____
 b. TYPE OF COMPLETION: NEW WELL WORK OVER DEEP-EN PLUG BACK DIFF. RESVR. Other _____

2. NAME OF OPERATOR
Ferguson & Bosworth

3. ADDRESS OF OPERATOR
P.O. Bin 2427, Bakersfield, California 93303

4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements)*
At surface 660'S of N. Line & 660'W of E Line of Sec. 7
At top prod. interval reported below
At total depth

14. PERMIT NO. _____ DATE ISSUED _____

5. LEASE DESIGNATION AND SERIAL NO.
Utah #0140959

6. IF INDIAN, ALLOTTEE OR TRIBE NAME

7. UNIT AGREEMENT NAME

8. FARM OR LEASE NAME
Cullen-H.S. Pet. - Gov't

9. WELL NO.
#1

10. FIELD AND POOL, OR WILDCAT
Wildcat

11. SEC., T., R., M., OR BLOCK AND SURVEY OR AREA
Sec. 7, T.24S-R.21E SLB&M

12. COUNTY OR PARISH
Grand

13. STATE
Utah

15. DATE SPELDED 12-9-72 16. DATE T.D. REACHED 2-20-72 17. DATE COMPL. (Ready to prod.) Abd. 2-21-72 18. ELEVATIONS (DF, REB, BT, GR, ETC.)* 4855' K.B. 19. ELEV. CASINGHEAD

20. TOTAL DEPTH, MD & TVD 4964' 21. PLUG, BACK T.D., MD & TVD 22. IF MULTIPLE COMPL., HOW MANY* 23. INTERVALS DRILLED BY Rotary 24. PRODUCING INTERVAL(S), OF THIS COMPLETION—TOP, BOTTOM, NAME (MD AND TVD)* None 25. WAS DIRECTIONAL SURVEY MADE NO

26. TYPE ELECTRIC AND OTHER LOGS RUN Electric Log & Gamma-Ray Neutron 27. WAS WELL CORED NO

28. CASING RECORD (Report all strings set in well)

| CASING SIZE | WEIGHT, LB./FT. | DEPTH SET (MD) | HOLE SIZE | CEMENTING RECORD | AMOUNT PULLED |
|-------------|-----------------|----------------|-----------|-------------------|---------------|
| 9-5/8" | 32.30 | 254' | 13-3/4" | 225 Sacks Class A | None |
| | | | | | |
| | | | | | |

| 29. LINER RECORD | | | | | 30. TUBING RECORD | | |
|------------------|----------|-------------|---------------|-------------|-------------------|----------------|-----------------|
| SIZE | TOP (MD) | BOTTOM (MD) | SACKS CEMENT* | SCREEN (MD) | SIZE | DEPTH SET (MD) | PACKER SET (MD) |
| None | | | | | None | | |

| 31. PERFORATION RECORD (Interval, size and number) | | 32. ACID, SHOT, FRACTURE, CEMENT SQUEEZE, ETC. | |
|--|------|--|----------------------------------|
| Interval | Size | DEPTH INTERVAL (MD) | AMOUNT AND KIND OF MATERIAL USED |
| None | | | |
| | | | |
| | | | |

33. PRODUCTION

| DATE FIRST PRODUCTION | | PRODUCTION METHOD (Flowing, gas lift, pumping—size and type of pump) | | | | WELL STATUS (Producing or shut-in) | |
|-----------------------|--------------|--|-------------------------|----------|----------|------------------------------------|---------------|
| DATE OF TEST | HOURS TESTED | CHOSE SIZE | PROD'N. FOR TEST PERIOD | OIL—BBL. | GAS—MCF. | WATER—BBL. | GAS-OIL-RATIO |
| | | | | | | | |
| | | | | | | | |

34. DISPOSITION OF GAS (Sold, used for fuel, vented, etc.) TEST WITNESSED BY

35. LIST OF ATTACHMENTS

36. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records

SIGNED John R. Anderson TITLE Engineer DATE 4-06-73

*(See Instructions and Spaces for Additional Data on Reverse Side)

Schlumberger

GAMMA RAY-NEUTRON

COUNTY GRAND
 FIELD or LOCATION WILDCAT
 WELL CULLEN H.S., -PETRO
 -GOVERNMENT NO. 1
 COMPANY FERGUSON & BOSWORTH

COMPANY FERGUSON AND BOSWORTH

311

WELL CULLEN-H. S., PETROLEUM-GOV'T, NO. 1

FIELD WILDCAT

COUNTY GRAND STATE UTAH

Location: NE/4
 Sec. 7 Twp. 24S Rge. 21E

Other Services:
 ES
 312

Permanent Datum: GL ; Elev.: 4845
 Log Measured From KB, 10 Ft. Above Perm. Datum
 Drilling Measured From KB

Elev.: K.B. 4855
 D.F. ----
 G.L. 4845

| | | |
|------------------------|----------------------|----------------------|
| Date | 2-19-73 | 2-21-73 |
| Run No. | ONE | TWO |
| Type Log | G.R.N. | G.R.N. |
| Depth—Driller | 4785 | 4964 |
| Depth—Logger | 4786 | 4966 |
| Bottom logged interval | 4785 14.9 | 4965 15.8 |
| Top logged interval | 20 | 4500 |
| Type fluid in hole | FRESH GEL | FRESH GEL |
| Salinity, PPM Cl. | NIL | ---- |
| Density | 9.0 | 9.2 |
| Level | FULL | FULL |
| Max rec. temp., deg F. | 90 | 94 |
| Operating rig time | 5 HOURS | 6 HOURS |
| Recorded by | DANTI | YATCHAK & WILLIAMS |
| Witnessed by | AMUNDSEN & TONIETTE | AMUNDSEN & TONIETTE |

| RUN No. | BORE-HOLE RECORD | | | CASING RECORD | | | |
|---------|------------------|------|------|---------------|------|------|------|
| | Bit | From | To | Size | Wgt. | From | To |
| 1 | 8-3/4 | 250 | 2410 | 9-5/8 | 32 | SURF | 250 |
| 1 | 7-7/8 | 2410 | 2937 | | | | |
| 1 | 6-3/4 | 2937 | 4785 | | | | |
| 2 | 6-3/4 | 4500 | 4964 | 9-5/8 | --- | SURF | 4500 |

ECU 316

use values 318

Surface Glen Canyon

Paradox (sect) 4060 - 7100

TD 7850

BHTs

fe weighted from surface

| | | |
|---------|------|-----|
| 86°F @ | 2081 | 8.5 |
| 102°F @ | 4059 | 7.6 |
| 116 @ | 6165 | 8.1 |
| 120 @ | 7850 | 8.0 |

SCHLUMBERGER

WILDCAT - GRAND COUNTY - UTAH

S7-1-2154

COUNTY FIELD or LOCATION WELL COMPANY

COMPANY SHELL OIL COMPANY

316

WELL FEDERAL # 1-20

FIELD WILDCAT

COUNTY GRAND STATE UTAH

LOCATION
1430' FNL, 892' FEL
 Sec. 20 Twp. 25S Rge. 18E

Other Services:
 L-GR
 SUP-GR
 FDC-GR
 PDT, SRS

Permanent Datum: GL, Elev. 5125
 Log Measured From KB, Ft. Above Perm. Datum
 Drilling Measured From KB

Elev.: K.B. 5143
 D.F. 5142
 G.L. 5125

| | | | | | |
|---|---------------------------------|---------------|---------------------|---|----|
| Date | <u>10-25-69</u> | API No. | <u>43-519-36043</u> | | |
| Run No. | <u>TWO</u> | | | | |
| Depth—Driller | <u>7856</u> | | | | |
| Depth—Logger | <u>7852</u> | | | | |
| Btm. Log Interval | <u>7850</u> <small>11.7</small> | | | | |
| Top Log Interval | <u>6560</u> | | | | |
| Casing—Driller | <u>7" @ 6563</u> | | | | |
| Casing—Logger | <u>6560</u> | | | | |
| Bit Size | <u>6'8"</u> | | | | |
| Type Fluid in Hole | <u>SALT BASE</u> | | | | |
| Dens. | <u>10.5</u> | <u>36</u> | | | |
| Visc. | | | | | |
| pH | <u>6.4</u> | <u>6.0 ml</u> | | | |
| Fluid Loss | | | | | |
| Source of Sample | <u>FLOWLINE</u> | | | | |
| R _m @ Meas. Temp. | <u>.058 @ 69 °F</u> | @ | °F | @ | °F |
| R _{mf} @ Meas. Temp. | <u>.044 @ 75 °F</u> | @ | °F | @ | °F |
| R _{mc} @ Meas. Temp. | <u>.055 @ 75 °F</u> | @ | °F | @ | °F |
| Source: R _{mf} R _{mc} | <u>M M</u> | | | | |
| R _m @ BHT | <u>.634 @ 120 °F</u> | @ | °F | @ | °F |
| Time Since Circ. | <u>12 HRS</u> | | | | |
| Max. Rec. Temp. | <u>120 °F</u> | | °F | | °F |
| Equip. | <u>3860</u> | <u>FARM</u> | | | |
| Location | | | | | |
| Recorded By | <u>WELLS</u> | | | | |
| Witnessed By | <u>M C FURLEY</u> | | | | |

FIELD PRINT

BOREHOLE COMPENSATED SONIC LOG - GAMMA RAY

SCHLUMBERGER

57-1-2154

 COUNTY
FIELD or
LOCATION
WELL
COMPANY

 COMPANY SHELL OIL COMPANY

 WELL FEDERAL #1-20 316

 FIELD WILDCAT

 COUNTY GRAND STATE UTAH

 LOCATION
1430' FNL, 892' FEL
Sec. 20 Twp. 25-S Rge. 18 E

 Other Services:
DIL
SNP-GR
FDC-GR
316

 Permanent Datum: GL, Elev. 5125
Log Measured From: KB, 17 Ft. Above Perm. Datum
Drilling Measure From: KB

 Elev.: K.B. 5142
D.F. 5141
G.L. 5125

| | | | | | | | |
|--------------------------------------|----------------------|----------------------|---------------|-----|-----|-----|----|
| Date | <u>9-26-69</u> | | | | | | |
| Run No. | <u>ONE</u> | | | | | | |
| Depth—Driller | <u>4057</u> | | | | | | |
| Depth—Logger | <u>4062</u> | | | | | | |
| Bitm. Log Interval | <u>4059</u> | <u>22.9</u> | | | | | |
| Top Log Interval | <u>2085</u> | | | | | | |
| Casing—Driller | <u>9 5/8 @ 2085</u> | @ | | @ | | @ | |
| Casing—Logger | <u>2085</u> | | | | | | |
| Bit Size | <u>8 3/4</u> | | | | | | |
| Type Fluid in Hole | <u>FGM</u> | | | | | | |
| Dens. | Visc. | <u>9.0</u> | <u>41</u> | | | | |
| pH | Fluid Loss | <u>11.0</u> | <u>8.6 ml</u> | | ml | | ml |
| Source of Sample <u>FLOW LINE</u> | | | | | | | |
| Temp. @ Meas. Temp. | <u>0.71 @ 79° F</u> | <u>0.55 @ 102° F</u> | @ | ° F | @ | | |
| Temp. @ Meas. Temp. | <u>0.64 @ 80° F</u> | <u>0.50 @ 102° F</u> | @ | ° F | @ | | |
| Temp. @ Meas. Temp. | <u>0.55 @ 102° F</u> | @ | ° F | @ | ° F | @ | |
| | <u>M</u> | <u>C</u> | | | | | |
| | <u>0.55 @ 102° F</u> | @ | ° F | @ | ° F | @ | |
| | <u>16 HRS</u> | | | | | | |
| | <u>102</u> | ° F | ° F | ° F | ° F | ° F | |
| <u>4542 FARM</u> | | | | | | | |
| <u>RUSEN & LEBSACK</u> | | | | | | | |
| <u>MR. McLEHANEY & MR. MASON</u> | | | | | | | |

Dresser Atlas

Dual Induction Focused Log

FILE NO.

COMPANY SHELL OIL COMPANY

FIELD PRINT

WELL FEDERAL 1-20

57-1-215A

FIELD WILDCAT

COUNTY GRAND STATE UTAH

LOCATION:

SW SENE

1430' S. and 892' W. FROM N.E. CORNER
OF SLBM
SEC. 20 TWP. 25 S RGE 18 E

Other Services:
GR-BHC-AL

316

THANKS

Permanent Datum GL Elev. 5125

Elevations:
KB 5122

Log Measured from KB 17.0 Ft. Above Permanent Datum

DF -

Drilling Measured from KB

GL 5125

| | | | | | |
|-------------------------|-------------------------|--------|----|----|----|
| Date | 9-16-69 | | | | |
| Run No. | ONE | | | | |
| Depth--Driller | 2085 | | | | |
| Depth--logger | 2083 | | | | |
| Bottom Logged Interval | 2071 30.7 | | | | |
| Top Logged Interval | 31 | | | | |
| Casing--Driller | 20" @ 29 | @ | @ | @ | @ |
| Casing--Logger | 31 | | | | |
| Bit Size | 12 1/4" | | | | |
| Type Fluid in Hole | WATER GEL | | | | |
| Density and Viscosity | 9.3 | 47 | | | |
| pH and Fluid Loss | 8.8 | 9.2 cc | cc | cc | cc |
| Source of Sample | PIT | | | | |
| Rm @ Meas. Temp. | 3.84 @ 70 °F | @ | °F | @ | °F |
| Rmf @ Meas. Temp. | 3.55 @ 70 °F | @ | °F | @ | °F |
| Rmc @ Meas. Temp. | 3.90 @ 70 °F | @ | °F | @ | °F |
| Source of Rmf and Rmc | M | M | | | |
| Rm @ BHT | 3.41 @ 70 °F | @ | °F | @ | °F |
| Time Since Circ | - | | | | |
| Max. Rec. Temp. Deg. F. | 86 | °F | °F | °F | °F |
| Equip. No. and Location | 1245 | CASPER | | | |
| Recorded By | NEILL | | | | |
| Witnessed By | Mr. MASON & McLEHANEY | | | | |

ECU 316

low weight on values
very poor print of log

surface - Glen Canyon Group

began logging at 40'

| | <u>sl</u> | <u>ss</u> | <u>ls</u> | <u>sub</u> <u>total</u> | <u>ke</u> | |
|----------------------|-----------|-----------|-----------|----------------------------|-----------------------|--|
| 960 40 - 1000 | 10 | 90 | | 9.4 | 9024 | |
| 1000 1000 - 2000 | 15 | 85 | | 9.1 | 9100 | |
| 1000 2000 - 3000 | 10 | 50 | 40 | 8.2 | 8200 | |
| BHT 1060 3000 → 4060 | | 40 | 60 | 8.2 | 8692 | |
| 4020 940 4060 - 5000 | | 5 | 5 | 9.8 | 9212 ³⁵⁰¹⁶ | |
| 1000 5000 - 6000 | 2 | | 3 | 9.8 | 9800 | |
| BHT 560 6000 → 6560 | 5 | | 5 | 9.5 | 5432 | |
| 6520 440 6560 - 7000 | 10 | | 5 | 9.2 | 4048 ⁵⁹⁴⁶⁰ | |
| 850 7000 - 7850 | 10 | | 55 | 7.8 | 6630 | |
| <u>7810</u> | | | | | <u>70138</u> | |

Paradox {
Below Pdx?

weight low - log almost illegible

ke to 4060 = 8.7

ke (Paradox) = 9.7 28492
2940 ft

ke overall = 8.9

BHT'S

86°F @ 2081

~~ke = 9.2~~

102 @ 4059

~~ke = 8.7~~

116 @ 6561

~~ke = 9.1~~

120 @ 7850

ke = 8.9 ✓

bottom apparently below Paradox

ECU 317

Begun 310 feet above top wengate
cutting ss, siltstone + sh

sh ss
40% 60%

Wengate 228'

sh ss
0 100%

Chinle 310'

sh ss
81 19

Shinarump 10'

sh ss
0 100

Moenkopi 552'

sh ss
79 21

White River 210'

sh ss
5% 95%

Cutler 1226'

sh ss carb
65 19 16

HERMOSA 1260'

sh ss carb
20 20 60%

Hemlock

SALT 4106 to 6915

| SALT | sh | ss | Carb | Gyp | Anhyd |
|------|----|----|------|-----|-------|
| 70 | 15 | 0 | 15 | | ✓ |

ECU 317

SEC 21, T25S-R18E ✓

EST COMP - LOG BY B.F. LATCH

%

| | THICKNESS | sh | ss | carb | Salt | GYP Anhyd | ke |
|--------------------|-------------|----|-----|------|------|-----------|------|
| Surface to 310' | 310 | 40 | 60 | | | | 7.6 |
| WINGATE 310- | 228 | 0 | 100 | | | | 10.0 |
| CHINLE | 310 | 80 | 20 | | | | 5.2 |
| SHINARUMP | 10 | 0 | 100 | | | | 10.0 |
| MOENKOPI | 552 | 80 | 20 | | | | 5.2 |
| WHITE RIM | 210 | 5 | 95 | | | | 9.7 |
| CUTLER | 1226 | 65 | 19 | 16 | | | 5.6 |
| HERMOSA | 1260 | 20 | 20 | 60 | | | 7.0 |
| SALT TO TD (6915') | TOP 2809 | 15 | 0 | 15 | 70 | ✓ | 8.6 |

BOTTOM IN SALT AT 6915

millieal
com rec °C

sh = 4.0

ss = 10.0

carb = 7.0

Salt = 10.0

weighted
ke to surface

BHT

148°F @ 6912

7.4

OGCC-3

STATE OF UTAH
OIL & GAS CONSERVATION COMMISSION

SUBMIT IN DUPLICATE*
(See other instructions on reverse side)

WELL COMPLETION OR RECOMPLETION REPORT AND LOG*

1a. TYPE OF WELL:
NEW WELL OIL WELL GAS WELL DRY Other

b. TYPE OF COMPLETION:
NEW WELL WORK OVER DEEP-EN PLUG BACK DIFF. RESVR. Other

2. NAME OF OPERATOR
Read & Stevens, Inc.

3. ADDRESS OF OPERATOR
P. O. Box 2126, Roswell, New Mexico 88201

4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements)*
At surface 1970' FNL & 1060' FWL Sec. 21, T-25-S, R-18-E, S.L.M.
At top prod. interval reported below Same
At total depth Same

5. LEASE DESIGNATION AND SERIAL NO.
U-5949

6. IF INDIAN, ALLOTTEE OR TRIBE NAME

7. UNIT AGREEMENT NAME

8. FARM OR LEASE NAME
Shenandoah-Bowknot

9. WELL NO.
1

10. FIELD AND POOL, OR WILDCAT
Wildcat

11. SEC. T., R., M., OR BLOCK AND SURVEY OR AREA
Sec. 21, T-25-S, R-18-E, S.L.M.

12. COUNTY OR PARISH
Grand

13. STATE
Utah

15. DATE SPUEDD
8-1-73

16. DATE T.D. REACHED
8-22-73

17. DATE COMPL. (Ready to prod.)
10-9-73

DATE ISSUED

14. PERMIT NO.

18. ELEVATIONS (DF, RKB, RT, GR, ETC.)*
5161' GR - 5178' RKB

23. INTERVALS DRILLED BY
10'-6915'

19. ELEV. CASINGHEAD

25. WAS DIRECTIONAL SURVEY MADE
None

20. TOTAL DEPTH, MD & TVD
6915' RKB

21. PLUG, BACK T.D., MD & TVD

22. IF MULTIPLE COMPL., HOW MANY*

23. INTERVALS DRILLED BY

27. WAS WELL CORDED
Yes

24. PRODUCING INTERVAL(S), OF THIS COMPLETION—TOP, BOTTOM, NAME (MD AND TVD)*
None - Plugged & Abandoned
Acoustic cement Bond, Micro-Seismogram; Gamma Ray, Caliper-Comp. Density, Neutron Porosity; Compensated Density Log

26. TYPE ELECTRIC AND OTHER LOGS RUN
None - Plugged & Abandoned

| CASING SIZE | WEIGHT, LB./FT. | DEPTH SET (MD) | HOLE SIZE |
|-------------|-----------------|----------------|-----------|
| 13 3/8" | 48# & 60# | 290' RKB | 17" |
| 8 5/8" | 32# | 2790' RKB | 11" |
| 5 1/2" | 17# & 20# | 6915' RKB | 7 7/8" |

28. CASING RECORD (Report all strings set in well)

30. TUBING RECORD

| SIZE | TOP (MD) | BOTTOM (MD) | SACKS CEMENT* | SCREEN (MD) | SIZE | DEPTH SET (MD) |
|------|----------|-------------|---------------|-------------|------|----------------|
| | | | | | | |

29. LINER RECORD

32. ACID, SHOT, FRACTURE, CEMENT SQUEEZE

| 31. PERFORATION RECORD (Interval, size and number) | |
|--|----------------|
| 6845'-6855' | w/20 jet shots |
| 6830'-6838' | w/16 jet shots |
| 6818'-6825' | w/14 jet shots |
| 6804'-6812' | w/16 jet shots |
| 6785'-6795' | w/20 jet shots |
| 6595'-6600' | w/16 jet shots |
| 6312'-6326' | w/28 jet shots |
| 6186'-6200' | w/28 jet shots |

32. DEPTH INTERVAL (MD)
See attachment for description

33. PRODUCTION METHOD (Flowing, gas lift, pumping—size and type of pump)

| DATE FIRST PRODUCTION | HOURS TESTED | CHOKED SIZE | PROD'N. FOR TEST PERIOD | OIL—BBL. | GAS—MCF. |
|-----------------------|--------------|-------------|-------------------------|----------|----------|
| None | | | | | |

34. DISPOSITION OF GAS (Sold, used for fuel, vented, etc.)

35. LIST OF ATTACHMENTS
2 copies of above logs, deviation report

36. I hereby certify that the foregoing and attached information is complete and correct as determined by me.
SIGNED John L. Anderson TITLE Agent

*(See Instructions and Spaces for Additional Data on Reverse Side)

...correct well completion report and log on all types of lands and leases to either a Federal agency or a State agency, and/or State office. See instructions on items 22 and 24, and 33, below regarding separate reports for separate completions.

If not filed prior to the time this summary record is submitted, copies of all currently available logs (drillers, geologists, sample and core analysis, all types electric, etc.), formation and pressure tests, and directional surveys, should be attached hereto, to the extent required by applicable Federal and/or State laws and regulations. All attachments should be listed on this form, see item 35.

Item 4: If there are no applicable State requirements, locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local State or Federal office for specific instructions.

Item 18: Indicate which elevation is used as reference (where not otherwise shown) for depth measurements given in other spaces on this form and in any attachments.

Items 22 and 24: If this well is completed for separate production from more than one interval zone (multiple completion), so state in item 22, and in item 24 show the producing interval, or intervals, top(s), bottom(s) and name(s) (if any) for only the interval reported in item 33. Submit a separate report (page) on this form, adequately identified, for each additional interval to be separately produced, showing the additional data pertinent to such interval.

Item 29: "Sacks Cement": Attached supplemental records for this well should show the details of any multiple stage cementing and the location of the cementing tool.

Item 33: Submit a separate completion report on this form for each interval to be separately produced. (See instruction for items 22 and 24 above.)

37. SUMMARY OF POROUS ZONES:

SHOW ALL IMPORTANT ZONES OF POROSITY AND CONTENTS THEREOF; CORED INTERVALS; AND ALL DRILL-STEM TESTS, INCLUDING DEPTH INTERVAL TESTED, CUSHION USED, TIME TOOL OPEN, FLOWING AND SHUT-IN PRESSURES, AND RECOVERIES

| FORMATION | TOP | BOTTOM | DESCRIPTION, CONTENTS, ETC. |
|------------|-------|---------|---|
| | | | |
| | 0' | 310' | Gray & red sand, siltstone & shale |
| Wingate | 310' | 538' ✓ | Red sand |
| Chinle | 538' | 848' ✓ | Red siltstone, red sand, red & green shale |
| Shinarump | 848' | 858' ✓ | Gray sand |
| Moenkopi | 858' | 1410' | Red & Gray sand, red & green shale |
| White Rim | 1410' | 1620' ✓ | White sand |
| Cutler | 1620' | 2846' ✓ | Red & gray sand, red & gray shale, gry-brn. lime. |
| Hermosa | 2846' | 4106' ✓ | Gray shale, lt. & drk. gray lime, gray sand |
| Salt | 4106' | TD | Clear crystalline salt w/any., shale & dolomite inclusions. |
| Cane Creek | 6800' | 6867' | Interbedded black shale, anhydrite & dolomite. |
| Core #1 | 6804' | 6858' | See attachment for description. |
| Core #2 | 6858' | 6915' | See attachment for description. No DST's |

38.

GEOLOGIC MARKERS

| NAME | TOP | |
|-------------------|-------------|------------------|
| | MEAS. DEPTH | TRUE VERT. DEPTH |
| T/Wingate | 310' | +4868 |
| T/Chinle | 538' | +4640 |
| T/Shinarump | 848' | +4330 |
| T/Moenkopi | 858' | +4320 |
| T/White Rim | 1410' | +3768 |
| T/Cutler | 1620' | +3558 |
| T/Hermosa | 2846' | +2332 |
| T/Salt | 4106' | +1072 |
| T/Cane Creek zone | 6800' | -1622 |
| B/Cane Creek zone | 6867' | -1689 |



COMPENSATED DENSITY POROSITY
AND NEUTRON POROSITY LOG

2

COMPANY READ & STEVENS
INCORPORATED
WELL SHENANDOAH -
BOWKNOT # 1
FIELD WILDCAT
County GRAND State UTAH

COMPANY READ AND STEVENS, INCORPORATED

WELL SHENANDOAH-BOWKNOT # 1

FIELD WILDCAT

COUNTY GRAND STATE UTAH

Location
Sec. 21 Twp. 25S Rge. 18E

Other Services:
COMP. DENSITY
317

Permanent Datum GROUND LEVEL Elev. 5161'
Log Measured From KELLY BUSHING 17 Ft. Above Perm. Datum
Drilling Measured From KELLY BUSHING

Elev.: K.B. ~~5172'~~
D.F. 5177'
G.L. 5161'

| | | | | |
|--|------------------------|--------------|------|------|
| Date | 8-22-73 | | | |
| Run No. | GAMMA-GAMMA, NEUTRON | | | |
| Depth-Driller | 6915' | | | |
| Depth-Welex | 6913' | | | |
| Btm. Log Inter. | 6912.5 25.6 | | | |
| Top Log Inter. | 0' | | | |
| Casing-Driller | 13-7/8" 290' | 8-5/8" 2790' | @ | @ |
| Casing-Welex | 2792' | | | |
| Bit Size | 7-7/8" | | | |
| Type Fluid in Hole | SALT BASE MUD | | | |
| Dens. Visc. | 10.6 36 | | | |
| pH Fluid Loss | ml | ml | ml | m |
| Source of Sample | PIT. | | | |
| R _{mf} @ Meas. Temp. | .07 @ 84°F | @ °F | @ °F | @ °F |
| R _{mf} @ Meas. Temp. | .06 @ 86°F | @ °F | @ °F | @ °F |
| R _{mf} @ Meas. Temp. | .095 @ 84°F | @ °F | @ °F | @ °F |
| Source R _{mf} R _{mf} | FILTER PRESS | | | |
| R _{mf} @ BHT | .04 @ 84.8 | @ °F | @ °F | @ °F |
| Time Since Circ. | 7 HOURS | | | |
| Max. Rec. Temp. | 148°F @ TD | °F @ | °F @ | °F @ |
| Equip. Location | 7757 FARMINGTON I | | | |
| Recorded By | LEEPER | | | |
| Witnessed By | MR. LATCH | | | |

SCHLUMBERGER

BOREHOLE LOGGING SERVICES
 SONE FOR HAMMA RAY

COUNTY
 FIELD or
 LOCATION
 WELL
 COMPANY

COMPANY Shell Oil Company

WELL Federal 1-21

FIELD Wildcat

COUNTY Grand STATE Utah

LOCATION 1978' S, 735' E Fr. N.W. Cor.
S.L.B.M SW NW

Sec. 21 Twp. 25S Rge. 18E

Other Services:
 DIL
 FDC
 CST **318**

Permanent Datum: G.L., Elev. 5152
 Log Measured From D.F., 18.3 Ft. Above Perm. Datum
 Drilling Measured From D.F.

Elev.: K.B. ~~5152~~
 D.F. 5169.8
 G.L. 5152

| | | | | | | |
|---|------------------------------------|------------------------------|---------------|----------|-----------|-----------|
| Date | <u>6-26-69</u> | | | | | |
| Run No. | <u>1</u> | | | | | |
| Depth—Driller | <u>4081</u> | | | | | |
| Depth—Logger | <u>4081</u> | | | | | |
| Btm. Log Interval | 4081 <u>22.8</u> | | | | | |
| Top Log Interval | <u>848</u> | | | | | |
| Casing—Driller | <u>10³/₄</u> | <u>@ 847</u> | | <u>@</u> | | <u>@</u> |
| Casing—Logger | <u>848</u> | | | | | |
| Bit Size | <u>8³/₄</u> | | | | | |
| Type Fluid in Hole | <u>EGM</u> | | | | | |
| Dens. | Visc. | <u>2.95</u> | <u>44</u> | | | |
| pH | Fluid Loss | <u>8.5</u> | <u>6.8 ml</u> | | <u>ml</u> | <u>ml</u> |
| Source of Sample | <u>Circ</u> | | | | | |
| R _m @ Meas. Temp. | <u>1.43</u> | @ <u>76 °F</u> | | @ °F | @ °F | @ °F |
| R _{mf} @ Meas. Temp. | <u>1.17</u> | @ <u>65 °F</u> | | @ °F | @ °F | @ °F |
| R _{mc} @ Meas. Temp. | <u>1.62</u> | @ <u>71 °F</u> | | @ °F | @ °F | @ °F |
| Source: R _{mf} R _{mc} | <u>M</u> | <u>M</u> | | | | |
| R _m @ BHT | <u>1.1</u> | @ 70 <u>76</u> °F | | @ °F | @ °F | @ °F |
| Time Since Circ. | <u>7hr</u> | | | | | |
| Max. Rec. Temp. | <u>102 °F</u> | | | | °F | °F |
| Equip. | Location | <u>4529</u> | <u>Vernal</u> | | | |
| Recorded By | <u>B. Thomas</u> | | | | | |
| Witnessed By | <u>D. McLehane & Mason</u> | | | | | |

Dresser Atlas

COMPENSATED

Densilog

FILE NO.

S7-1-2159

COMPANY SHELL OIL COMPANY

WELL FEDERAL 1-21

FIELD WILOCAT

COUNTY GRAND STATE UTAH

LOCATION: 1978'S E 735'E
from NW corner

SEC 21 TWP 25 S RGE 18 S/62

Other Service
LL
BHC-A/L
SWN-GR
D. plug
318

Permanent Datum G.L. Elev. 5152

Log Measured from KB or 18.3 Ft. Above Permanent Datum

Drilling Measured from KB

Elevations:
KB 5120
DF 5169.5
GL 5152

| | | | | | |
|-------------------------|-----------------------------|----|----|----|----|
| Date | <u>7-10-69</u> | | | | |
| Run No. | <u>one</u> | | | | |
| Depth—Driller | <u>4919</u> | | | | |
| Depth—Logger | <u>4919</u> | | | | |
| Bottom Logged Interval | <u>4919 29.3</u> | | | | |
| Top Logged Interval | <u>0</u> | | | | |
| Casing—Driller | <u>10 3/4 @ 847</u> | @ | @ | @ | @ |
| Casing—Logger | <u>846</u> | | | | |
| Bit Size | <u>8 3/4</u> | | | | |
| Type Fluid in Hole | <u>SALT SAT</u> | | | | |
| Density and Viscosity | <u>11.2</u> | - | | | |
| pH and Fluid Loss | <u>-</u> | - | cc | cc | cc |
| Source of Sample | <u>P.T</u> | | | | |
| Rm @ Meas. Temp. | <u>.06 @ 84</u> | F | @ | F | @ |
| Rmf @ Meas. Temp. | <u>.013 @ 78</u> | F | @ | F | @ |
| Rmc @ Meas. Temp. | <u>.10 @ 80</u> | F | @ | F | @ |
| Source of Rmf and Rmc | <u>M M</u> | | | | |
| Rm @ BHT | <u>.036 @ 60</u> | F | @ | F | @ |
| Time Since Circ. | <u>5 hr.</u> | | | | |
| Max. Rec. Temp. Deg. F. | <u>130</u> | °F | | °F | |
| Equip. No. and Location | <u>1245 CLEAR</u> | | | | |
| Recorded By | <u>Wetter-Rall</u> | | | | |
| Witnessed By | <u>Mr. M. Lehner</u> | | | | |

ECU 318

EST. COMPOSITIONS

| depth | sh | % some anhyd. ss | ls | k_e | | Glen Canyon |
|-----------|----|---------------------------|----|---------|---------|---------------|
| | | | | surface | | |
| 0-1000 | 25 | 70 | 5 | 8.4 | 8400 | } $k_e = 7.6$ |
| 1000-2000 | 20 | 75 | 5 | 8.6 | 8600 | |
| 2000-3000 | 55 | 40 | 5 | 6.6 | 6600 | |
| 3000-4000 | 45 | 40 | 15 | 7.3 | 7300 | |
| 4000-5000 | 30 | 15 | 55 | 6.6 | 6600 | |
| 5000-5735 | 5 | 35 | 60 | 7.9 | 5806.5 | |
| | | | | | 43306.5 | |

5735 TOP PARADOX

| | sh | ss | ls | anhyd. salt | | | } $k_e = 9.0$ |
|-----------|----|----|----|----------------|-----|-------|---------------|
| 5735-6000 | 0 | 0 | 20 | 80 | 9.4 | 2491 | |
| 6000-7000 | 10 | 0 | 10 | 80 | 9.1 | 9100 | |
| 7000-8000 | 20 | 0 | 0 | 80 | 8.8 | 8800 | |
| 8000-9000 | 15 | 0 | 0 | 85 | 9.1 | 9100 | |
| 9000-9755 | 20 | 0 | ✓ | 80 | 8.8 | 6644 | |
| | | | | | | 36135 | |

9755 BOTTOM PARADOX (SALT)

| | sh | ss | ls | | | } $k_e = 7.0$ |
|-------------|----|----|-----|-----|--|---------------|
| 9755-10000 | 13 | 12 | 75 | 7.0 | | |
| 10000-10330 | 0 | 0 | 100 | 7.0 | | |

BHTS

| | | | k_e weighted to depths |
|--------|--------|-----------------------|-----------------------------|
| 115° F | @ 6850 | P _{ox} | 7.8 |
| 122° | @ 6775 | P _{ox} | 7.8 |
| 130° | @ 4916 | above P _{ox} | 7.5 |
| 102° | @ 4078 | " | 7.7 |

SCHLUMBERGER

UNRECORDED UNCOMPENSATED
SOUND LOG GAMMA RAY

57-1-2161

COUNTY
FIELD or
LOCATION
WELL
COMPANY

COMPANY SHELL OIL COMPANY

WELL QUINTANA 1-35

FIELD WILCOT

COUNTY GRAND STATE UTAH

LOCATION 1814'E & 1603'N of SW

Sec. 35 Twp. 25 S Rge. 18 E

Other Services:

OIL 319
FOC-6R
SAP-6R

Permanent Datum: 6 L, Elev. 5471
Log Measured From KB, 17 Ft. Above Perm. Datum
Drilling Measured From KB

Elev.: K.B. 548
D.F. _____
G.L. 5471

| | | | |
|---|------------|----------------------|----------------------|
| Date | | <u>11-20-69</u> | <u>API. 43-019-</u> |
| Run No. | | <u>TWO</u> | <u>30045</u> |
| Depth—Driller | | <u>4209</u> | |
| Depth—Logger | | <u>4210</u> | |
| Btm. Log Interval | | <u>4209</u> | |
| Top Log Interval | | <u>2375</u> | |
| Casing—Driller | @ | <u>95/2 @ 2375</u> | @ |
| Casing—Logger | | <u>2375</u> | |
| Bit Size | | <u>8 3/4</u> | |
| Type Fluid in Hole | | <u>F.G.H.</u> | |
| Dens. | Visc. | <u>9.2</u> | <u>39</u> |
| pH | Fluid Loss | ml <u>9.0</u> | ml <u>6.0</u> |
| Source of Sample | | <u>CIRC.</u> | |
| R _m @ Meas. Temp. | @ °F | <u>1.37 @ 69 °F</u> | @ °F |
| R _{mf} @ Meas. Temp. | @ °F | <u>1.26 @ 69 °F</u> | <u>0.85 @ 103 °F</u> |
| R _{mc} @ Meas. Temp. | @ °F | <u>0.90 @ 103 °F</u> | @ °F |
| Source: R _{mf} R _{mc} | | <u>M</u> | <u>C</u> |
| R _m @ BHT | @ °F | <u>0.93 @ 103 °F</u> | @ °F |
| Time Since Circ. | | <u>12 HRS</u> | |
| Max. Rec. Temp. | | °F <u>103</u> °F | |
| Equip. | Location | <u>5625 FARM.</u> | |
| Recorded By | | <u>RUSEN</u> | |
| Witnessed By | | <u>DOGAN</u> | |

SCHLUMBERGER

UNIVERSITY MICROFILMS
SERIALS ACQUISITION
ANN ARBOR MI 48106

S7-1-2161

COUNTY
FIELD or
LOCATION
WELL
COMPANY

COMPANY SHELL OIL COMPANY

WELL QUINTANA 1-35

FIELD WILLOCAT

COUNTY GRAND STATE UTAH

4

LOCATION 1814'E + 1603'N of SW

Sec. 35 Twp. 25 S Rge. 18 E

Other Services:
LL-3-69
SAP-69
FDC-69
31

Permanent Datum: GL, Elev. 5471

Log Measured From KB, 17 Ft. Above Perm. Datum

Drilling Measured From KB

Elev.: K.B. 5471
D.F. 548
G.L. 547

| | | | |
|---|------------------------------|----------------------|------|
| Date | <u>12-6-69</u> | <u>API-43-019-</u> | |
| Run No. | <u>3</u> | <u>30045</u> | |
| Depth—Driller | <u>8140</u> | | |
| Depth—Logger | <u>8129</u> | | |
| Btm. Log Interval | <u>812.6</u> ^{16.6} | <u>16.4</u> | |
| Top Log Interval | <u>4000</u> | | |
| Casing—Driller | <u>9 5/8 @ 2375</u> | @ | @ |
| Casing—Logger | <u>2375</u> | | |
| Bit Size | <u>2 3/4</u> | | |
| Type Fluid in Hole | <u>SALT H₂O</u> | | |
| Dens. | <u>10.4</u> | <u>39</u> | |
| Visc. | <u>6.0</u> | <u>9.2</u> ml | ml |
| pH | | | |
| Fluid Loss | | | |
| Source of Sample | <u>CIRC.</u> | | |
| R _m @ Meas. Temp. | <u>.06 @ 60 °F</u> | @ °F | @ °F |
| R _{mf} @ Meas. Temp. | <u>.05 @ 59 °F</u> | <u>.024 @ 125 °F</u> | @ °F |
| R _{mc} @ Meas. Temp. | <u>.03 @ 125 °F</u> | @ °F | @ °F |
| Source: R _{mf} R _{mc} | <u>M C</u> | | |
| R _m @ BHT | <u>.028 @ 125 °F</u> | @ °F | @ °F |
| Time Since Circ. | <u>12 HRS</u> | | |
| Max. Rec. Temp. | <u>125 °F</u> | °F | °F |
| Equip. | <u>5625</u> | <u>FARM</u> | |
| Location | | | |
| Recorded By | <u>RV SEN</u> | | |
| Witnessed By | <u>DOGAN</u> | | |

SCHLUMBERGER

UNSATURATED
SUNB LOG - GAMMA RAY

57-1-2161

COUNTY
FIELD or
LOCATION
WELL
COMPANY

COMPANY SHELL OIL COMPANY

WELL QUINTANA 1-35

FIELD WILDCAT

COUNTY GRAND STATE UTAH

LOCATION ^{NE 30}
1814'E & 1603'N of SW CORNER
Sec. 35 Twp. 255 Rge. 18E

Other Services:
DIL 319

Permanent Datum: GL, Elev. 5471
Log Measured From KB, 16 Ft. Above Perm. Datum
Drilling Measured From KB

Elev.: K.B. 5487
D.F. G. 5471

| | | | | |
|---|----------------------------|-------------------------|----|------|
| Date | <u>11-11-69</u> | <u>API-43-019-30045</u> | | |
| Run No. | <u>ONE</u> | | | |
| Depth—Driller | <u>2375</u> | | | |
| Depth—Logger | <u>2376</u> | | | |
| Btm. Log Interval | <u>2375</u> ²⁶⁴ | | | |
| Top Log Interval | | | | |
| Casing—Driller | <u>20" @ 25</u> | @ | @ | @ |
| Casing—Logger | | | | |
| Bit Size | <u>12 1/4</u> | | | |
| Type Fluid in Hole | <u>GEL-WATER</u> | | | |
| Dens. | <u>9</u> | <u>40</u> | | |
| Visc. | | | | |
| pH | <u>8</u> | <u>12.6 ml</u> | ml | ml |
| Fluid Loss | | | | |
| Source of Sample | <u>MUD PIT</u> | | | |
| R _m @ Meas. Temp. | <u>8.57 @ 67 °F</u> | @ | °F | @ °F |
| R _{mf} @ Meas. Temp. | <u>8.54 @ 67 °F</u> | @ | °F | @ °F |
| R _{mc} @ Meas. Temp. | <u>8.20 @ 63 °F</u> | @ | °F | @ °F |
| Source: R _{mf} R _{mc} | <u>M M</u> | | | |
| R _m @ BHT | <u>10.8 @ 85 °F</u> | @ | °F | @ °F |
| Time Since Circ. | <u>3 1/2 HRS</u> | | | |
| Max. Rec. Temp. | °F | °F | °F | °F |
| Equip. | <u>5625 FARM</u> | | | |
| Location | | | | |
| Recorded By | <u>WELLS</u> | | | |
| Witnessed By | <u>McFANEY</u> | | | |

FIELD
DUPNT

ECU 319

Surface Glen Canyon

Salt at 4340 - 7550

TD about 8140

| | | |
|------------------|-------|-----|
| ke above parados | 4340' | 7.6 |
| ke Parados | 3210' | 9.0 |
| ke Below Parados | 590' | 7.0 |

| BHTS | ke's (surface to BHT) weighted |
|--------------|-----------------------------------|
| 85° at 2375 | 8.2 |
| 103° at 4209 | 7.7 |
| 125° @ 8126 | 8.1 |