

UTAH
SALT LAKE 90th South
UTAH ROSES API 43-035-90001
NW SW 1980 fsl 660 fwl (approx).

1-3s-1w
WILDCAT GW

4000. El: 4350 Gr.

Contr: CRC/Colo Well Service. Spud 11/25/79. 13 3/8 @ 243, 8 5/8 @ 2244, 5 1/2 @ 3385.

5008 TD. @ 1700 ft wtr temp 94° F. Ran temp, GR, neutron, SP, resistivity logs. BHT 130° F. Perf 2080-3885. Comp 12/9/79. Pump 225 GPM. Prod Zone: Sandstone 2080-3885. Well head temp 125° F.

UT1-122680



Petroleum Information.

CORPORATION

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6101534

UTAH
SALT LAKE
UTAH ROSES
SW NW 1980 fnl 1980 fwl
(approx).

1 Bluffdale Injection
API 43-035-90002

12-4s-1w
WILDCAT GW

950 EI: 4450 Gr.
Contr: Energy Services. Spud 8/27/80. 13 3/8 @ 232, 8 5/8 @ 730, slotted
530-730.
950 TD. Ran temp logs. Comp 9/28/80. F 50 GPM (Artesian). Prod Zone:
530-730. Well head temp 182° F.

UT2-122680

 **Petroleum Information.**
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UTAH
SALT LAKE
UTAH ROSES
SW NW 1980 fnl 660 fwl
(approx).

1 Bluffdale Geothermal
API 43-035-90000

12-4s-1w
WILDCAT GW

450. El: 4450 Gr.
Contr: Energy Services. Spud 11/19/79. 12 @ 87, 8 @ 190.
410 TD. Ran temp logs. @ 410 wtr temp 85° C. F 200 GPM, P 500 GPM.
Comp 11/22/79. Pump 450 GPM. Prod Zone: 190-410 (open hole). Well head
temp 195° F.

UT3-122680



Petroleum Information.

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AREA
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GWDGROUND-WATER DISCHARGE TOWARD GREAT SALT LAKE
THROUGH VALLEY FILL IN THE JORDAN VALLEY, UTAH

By R. W. MOWER, Salt Lake City, Utah

UNIVERSITY OF UTAH
RESEARCH INSTITUTE
EARTH SCIENCE LAB.

32

*Work done in cooperation with the
Utah Department of Natural Resources, Division of Water Rights*

Abstract.—Ground water in the northern part of the Jordan Valley is principally under artesian conditions in valley fill of Quaternary age consisting of clay, silt, and sand. The water is moving generally toward the southeast shore of Great Salt Lake. The computed quantity of water discharging into Great Salt Lake from the valley fill in the northern part of the Jordan Valley is estimated to be a maximum of 7,000 acre-feet per year.

The amount of ground water that is moving toward Great Salt Lake in the northern part of the Jordan Valley was determined as a result of an investigation of the water resources of Salt Lake County, Utah. The amount of ground water could not be measured directly; but an estimate was made using Darcy's law, $Q = PIA$, where Q is the amount of water flowing through a selected cross section of the saturated aquifer, P is the average permeability of the saturated materials, I is the existing hydraulic gradient, and A is the area of the cross section.

The main aquifer in the northern part of the Jordan Valley is valley fill consisting of strata of clay, silt, and sand. The water in the valley fill is under artesian conditions, with the clay and silt acting as the confining beds. Because these confining beds themselves are slightly permeable, some water moves slowly upward, eventually arrives at the land surface, and is discharged by evapotranspiration. Most of the ground water, however, probably moves horizontally and is discharged to Great Salt Lake, although some water is pumped from wells near the west end of the Kennecott Copper Corp. tailings pond.

The section used was along a line about 15 miles long near the north end of the Jordan Valley (fig. 1). The section coincided in part with the line of a refraction seismic study that was reported by Arnow and Mattick (1968). On the basis of the seismic work and interpretation of the logs of several nearby wells, Arnow and

Mattick suggested that the valley fill is divided into units of Tertiary and Quaternary age (fig. 2). They found, also, that the seismic velocities in the Tertiary unit are characteristic of semiconsolidated sediments and that seismic velocities in the Quaternary unit are characteristic of unconsolidated water-saturated sediments. The maximum thickness of the Quaternary valley fill, computed by Arnow and Mattick, is 2,480 feet at shotpoint 9, the eastern end of their line. However, the total thickness of the valley fill may be as great as 4,000 feet east of shotpoint 9 (R. E. Mattick, written commun., 1968), and much or all of it is of Quaternary age.

The east end of the section investigated by Arnow and Mattick was extended a distance of 2.2 miles eastward from shotpoint 9 to an outcrop of Maxfield Limestone of Cambrian age (Marsell and Threet, 1960) that marks the east edge of the valley. The extension was made on the basis of a determination of the depth to bedrock by R. E. Mattick (written commun., 1968) using gravity data obtained by Cook and Berg (1961). The valley fill reaches its maximum thickness at about the point where the extrapolated trace of the seismic profile crosses the Jordan River, and from there it thins eastward toward the limestone outcrop. It is assumed that all the valley fill east of shotpoint 9 is saturated, and that it is all or mostly of Quaternary age.

The west end of the section defined by Arnow and Mattick was first extended 0.4 mile south-southwestward to Kennecott Copper Corp. well 3 that penetrated limestone (according to the driller's log)—probably a unit of the Oquirrh Formation—at 185 feet, and then extended 0.2 mile southwestward to an outcrop of limestone of the Oquirrh Formation (Tooker and Roberts, 1961). It is assumed that all the valley fill south of shotpoint 1 is saturated, and that it is mostly

ANALYSIS OF GROUND-WATER CHARACTERISTICS

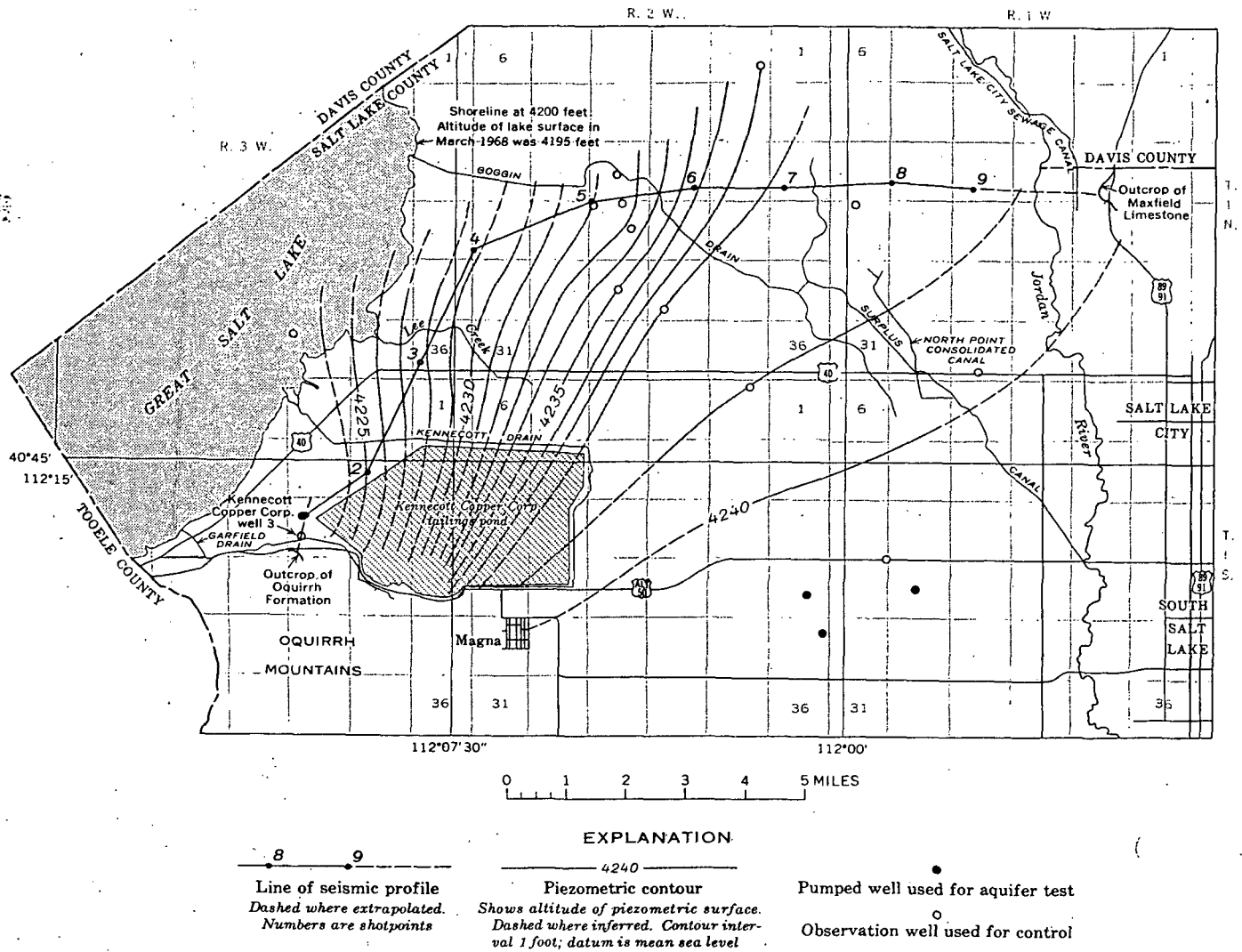


FIGURE 1.—Map of the northern part of the Jordan Valley, Utah, showing line of seismic profile, locations of observation wells, and piezometric contours, September 1967.

of Quaternary age. A small amount of water is discharged from valley fill of Tertiary age in this part of the section, where the upper part of the Tertiary fill may be as permeable as the Quaternary fill. The discharge from the Tertiary fill near the north end of the Oquirrh Mountains is lumped, in this report, with discharge from the Quaternary fill.

In order to determine the field coefficient of permeability (the amount of water in gallons per day that flows through a cross-sectional area of 1 square foot under a hydraulic gradient of 100 percent at the prevailing temperature) along the section of valley fill, aquifer tests were made by pumping four wells. The wells range in depth from 840 to 1,200 feet and tap from 400 to 600 feet of Quaternary deposits. The determined range of the coefficients of permeability is from 215 to 310 gallons per day per square foot, and

the average is 260 gallons per day per square foot. Although the aquifer tests were made about 6 miles south of the central part of the section (fig. 1), a study of gamma-ray and lithologic logs of wells in the area between the section and the aquifer-test sites indicates that the texture of the Quaternary deposits is relatively uniform. Several beds can be correlated throughout most of the area, and only slight areal variation exists in the texture of the sediments. The average coefficient of permeability, therefore, which was determined for the aquifer tests, can be applied to the entire section with little error.

The hydraulic gradient across the section was determined from a map of the piezometric surface of water in a selected bed (fig. 1). The top of the bed, which was determined from gamma-ray logs, lies between 480 and 580 feet below the land surface, and

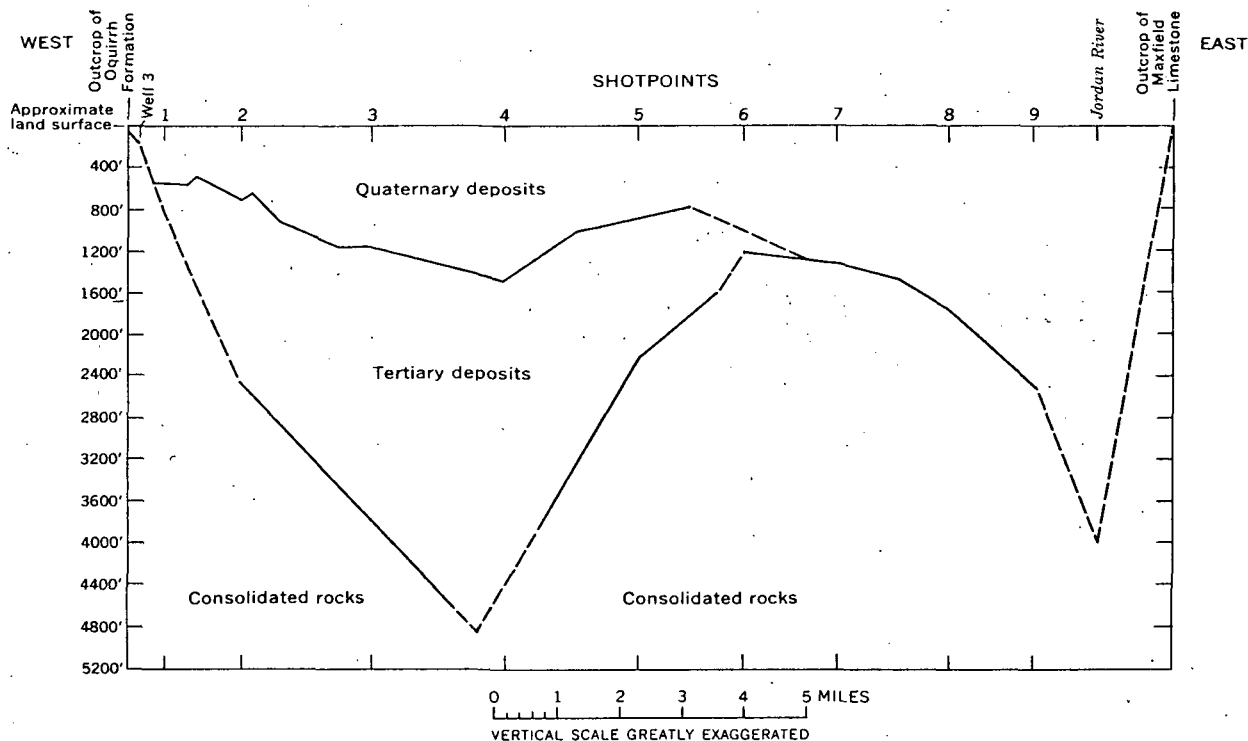


FIGURE 2.—Computed and extrapolated depth of three velocity layers along a seismic profile in the northern part of the Jordan Valley, Utah. (Section between shot points 1 and 9 after Arnow and Mattick, 1968, fig. 2.)

the bed is about 100 feet thick. The piezometric surface of the bed was from 10 to 15 feet higher than that for shallower beds, but the hydraulic gradient was about the same in all beds. The magnitude of the hydraulic gradient is independent of discharge by evapotranspiration, because evapotranspiration per unit area is similar south and north of the section.

In order to calculate the hydraulic gradient as accurately as possible, the section was divided into 10 segments. Each segment is the reach of the section between adjacent shotpoints on the seismic profile, and at the ends of the profile the segment is the reach between the end shotpoint and the nearest bedrock outcrop. The hydraulic gradient was not normal to the section for the full reach of any segment; therefore, it was necessary to compute the component of hydraulic gradient normal to the section at each segment (table 1). The component of hydraulic gradient normal to the section at individual segments ranges from 0.2 to 4.0 feet per mile, and averages 1.4 feet per mile.

Discharge was computed by applying Darcy's law to the various segments of the section and then totaling the results. As shown in table 1, the discharge across the section in the northern part of the Jordan Valley is estimated to be 8,000 acre-feet a year. Of this amount, about 1,000 acre-feet of water is flowing past the two

westernmost segments; most of this water is being diverted toward a well field near the west end of the Kennecott Copper Corp. tailings pond. Some of the remaining 7,000 acre-feet of water is discharged by evapotranspiration, but most of the water is discharged as underflow into Great Salt Lake.

TABLE 1.—Average saturated thickness, length, hydraulic gradient, and discharge by segment of a selected west-east profile across the northern part of the Jordan Valley

Segment between—	Average saturated thickness of segment (feet)	Length of segment (miles)	Component of hydraulic gradient normal to cross section by segment (feet per mile)	Discharge (acre-feet per year)
West end and shotpoint 1.	400	0.6	4.0	280
Shotpoints 1 and 2	1,700	1.2	2.4	590
2 and 3	975	2.1	2.9	1,730
3 and 4	1,325	2.1	2.5	2,030
4 and 5	1,100	2.2	1.6	1,130
5 and 6	875	1.7	1.2	520
6 and 7	1,200	1.5	1.2	630
7 and 8	1,475	1.8	.3	230
8 and 9	2,100	1.3	.2	160
Shotpoint 9 and east end.	2,600	2.2	.2	330
Total (rounded)				8,000

¹ Includes the upper 125 feet of the Tertiary deposits.

REFERENCES

- Arnow, Ted, and Mattick, R. E., 1968, Thickness of valley fill in the Jordan Valley east of Great Salt Lake, Utah, in Geological Survey Research, 1968: U.S. Geol. Survey Prof. Paper 600-B, p. B79-B82.
- Cook, K. L., and Berg, J. W., Jr., 1961, Regional gravity survey along the central and southern Wasatch Front, Utah: U.S. Geol. Survey Prof. Paper 316-E, p. 75-89.
- Marsell, R. E., and Threet, R. L., 1960, Geologic map of Salt Lake County, Utah: Utah Geol. and Mineralog. Survey Map 15.
- Tooker, E. W., and Roberts, R. J., 1961, Preliminary geologic map and sections of the north end of the Oquirrh Range (Mills Junction, Garfield, and Magna 7½-minute quadrangles), Tooele and Salt Lake Counties, Utah: U.S. Geol. Survey Mineral Inv. Map MF-240.



FACT SHEET
OFFICE BUILDING
Church of Jesus Christ of Latter-day Saints

UNIVERSITY OF UTAH
RESEARCH INSTITUTE
EARTH SCIENCE LAB.

1. 28 floor tower, plus 2 -4 floor wings.
- AREA 2. 420 feet high
- UT
- Saltlake 3. 3 levels below ground includes Cafeteria, Mail Room, Print Shop, Maintenance
- LDS Office Shop, plus parking for 1400 cars.
4. 21 elevators
5. 30,000 light fixtures
6. 3600 windows which rotate so that they might be washed from the inside.
7. 7,000 tons of steel were used in the construction of the Office Building.
8. The pyramide footing supports under the tower portion of the building are 80' below the 3rd lower level of the Parking Plaza.
9. 683,000 net square feet of office space - excluding the parking area.
10. A vertical mail conveyor system allows mail distribution through the entire building.
11. The building is constructed on a five foot module which allows light and air conditioning within each 5' area.
12. Movable partitions have been installed in all office areas to allow flexibility in office arrangements utilizing the 5' module.
13. The building is heated and cooled utilizing a heating pump system in connection with 4 water wells.
14. There is a central control room from which all electrical and mechanical functions are controlled and monitored.
15. 1600 employees occupy the building
16. The Eastern & Western hemispheres are depicted on the North and South facades of the east and west wings.
17. Construction of the Parking Plaza Oct. 1962 - Dec 1964
Construction of the Office Building July 1969 - Dec. 1972
18. A plaza with a large water pool and fountain is planned south of the building with attention focused toward the Temple - westward.

AREAS OF SPECIAL INTEREST

Employee Cafeteria - 1st Lower	335 seat auditorium - Main Floor
Church Library - Main Floor	Historical Research Library -
Genealogy Library - West Wing Main Fl.	East Wing, (2nd Floor)
25 Board and Committee Rooms on the	Meeting and Reception area - 26th Floor
22nd Floor	

CHURCH OFFICE BUILDING AIR CONDITIONING SYSTEM

I. GENERAL DESCRIPTION

- A. The Church Office Building air conditioning system operates on the heat pump principle and consists of three 750 ton liquid chilling systems operating as a single system under the overall control of a sensing center which compares chiller output to requirements and causes the various chillers to be started and stopped as required to satisfy those requirements.
- B. Each of the three primary systems (all located on the third lower level) use York equipment consisting of a turbo compressor, condenser, cooler and a liquid intercooler. Each is powered by an 800 horsepower General Dynamics squirrel cage motor using a geared speed increaser. The motors operate at 4160 volts, 100 amperes, at full load. A York pneumatic control panel associated with each unit controls the operation of that unit as directed by the Honeywell master control center located in the chiller room. These control units are discussed in the following two paragraphs and in later sections.
- C. The Honeywell Master Control Center regulates both chill and hot water outlet temperature based on outside air temperature and operating parameters (high and low limits) set into the unit. Pneumatic signals are transmitted to the individual York pneumatic control panels to activate or stop the chillers or to regulate

their level of operation by causing adjustment of the compressor vanes or the amount of hot gas being by-passed around the condenser. Pneumatic signals are also provided to initiate valve operation to permit heat exchange with well water under conditions of excess hot or cold water. Automatic changeover from heating to cooling programming (and vice versa) is also accomplished in accordance with parameters set into the control center. The degree of control provided permits the system to maintain building heating and cooling loads under design conditions.

D. The York Pneumatic Control Center associated with each individual chiller performs the following functions in response to signals from the Honeywell Master Control Center.

1. Electrical controls.

- a. Upon receiving a "start compressor" signal, starts the auxiliary oil pump to establish positive pressure before the compressor is started, starts the compressor and maintains that auxiliary oil pressure until the main oil pumps come up to speed and then stops the auxiliary pump. (Note: Other electrical interlocks insure that well water pumps, primary hot and chill water pumps, and the lubrication oil cooling pump are all in operation before the compressor can be activated.)
- b. During compressor operations, restarts the auxiliary oil pump at any time oil pressure falls below the minimum allowed during operations.

c. Upon receiving a "stop compressor" signal from the master control or when safety control settings are exceeded (low oil pressure, high oil temperature, etc.), removes power from the compressor motor and starts or continues operation of the auxiliary oil pump to maintain pressure as the compressor coasts to a stop, then stops the auxiliary oil pump.

2. Pneumatic Controls

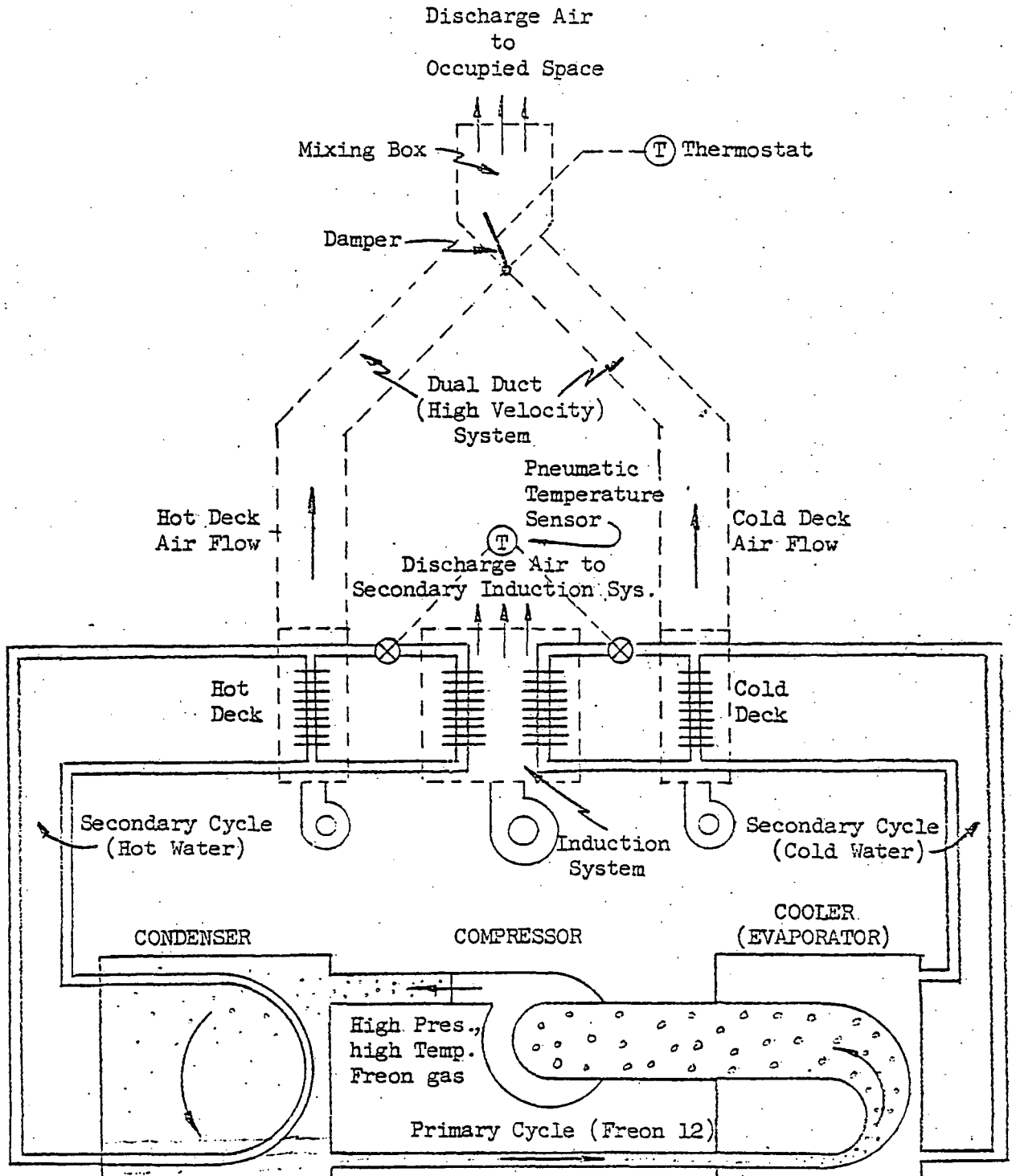
Automatically position the prerotating vanes to match load requirements at constant speed; limits opening of the vanes beyond the point where motor current would exceed the maximum load adjustment as set; and operates the pneumatic hot gas bypass valve to add a false load to the chiller as needed to maintain stability of the system under extremely low load conditions.

II. THEORY OF OPERATION

A. General

1. The heated and cooled air to meet air conditioning requirements of the building is derived from a conventional refrigeration cycle. The application of this process in a heat pump system is, however, unique.

a. In this system, (See Fig. 1) the primary refrigerant (Freon 12) cools secondary refrigerant (water) which is then circulated to heat exchangers (finned coils) in the building. Air being forced through these coils is cooled and in turn is discharged at the desired site to cool the



Gaseous Freon condenses to liquid and gives up heat to water in the secondary system.

Liquid Freon picks up heat in evaporator and boils.

Fig. 1 - Basic refrigeration cycle showing use of hot and cold water produced to condition air for building use.

conditioned space. The secondary refrigerant is warmed as the air passes through the coils and is then returned to the cooler where it releases this heat to the primary refrigerant causing it to boil and change to a gas at low pressure and temperature. The secondary refrigerant is cooled in the same process and is recirculated to the building heat coils to repeat the process.

b. The low pressure heat laden primary refrigerant gas is picked up by the rotating impellers in the compressor and is discharged, at high pressure and temperature, into the condenser, through which water from the closed circuit building heating system is circulated. This water picks up the heat from the hot refrigerant gas causing it to condense to a liquid at high pressure. The liquid refrigerant then flows through a float valve into the cooler to begin another cycle.

2. At times in the Spring and Fall production of hot and cold water in the refrigeration cycle described exactly balance building air conditioning and heating requirements. In the Summer and Winter, however, the requirement is predominantly for cooling or heating and in meeting the predominant requirement a surplus of hot or cold water is generated. At these times, Church owned wells located nearby are used as heat sinks to either absorb heat from or give heat to this excess condition to maintain balanced operation of the refrigeration cycle. The system operates in either a heating or a cooling

cycle in response to pneumatic signals from the Honeywell Master Control Center based on the operating parameters which have been set into it. The heating and cooling cycle controls are essentially separate with one or the other providing control signals. As outside air temperature rises, cooling cycle devices takes control at 60°F. When the outside air temperature falls, heating cycle programming takes control at 56°F. Operation under each of these predominant conditions is described in the following paragraphs and in the simplified diagrams referenced.

a. Heating Cycle (See Fig. 2)

The large quantity of heat energy required in the hot water system must be extracted from the chill water (secondary refrigerant) as described in operation of the basic refrigeration cycle (paragraph 1 above). This results in the chill water being brought to a lower temperature than required to support building cooling requirements. In order to prevent freeze-up, the control system automatically stops the compressors if the chill water temperature falls to 36°F. Therefore, it is necessary to impose a false cooling load to prevent interruption of hot water production. This is accomplished by routing the 40-44°F chill water through the shell of heat exchangers while 58-60°F well water is circulated through the tubes. The higher temperature well water warms the secondary refrigerant water just as if it had been used in building

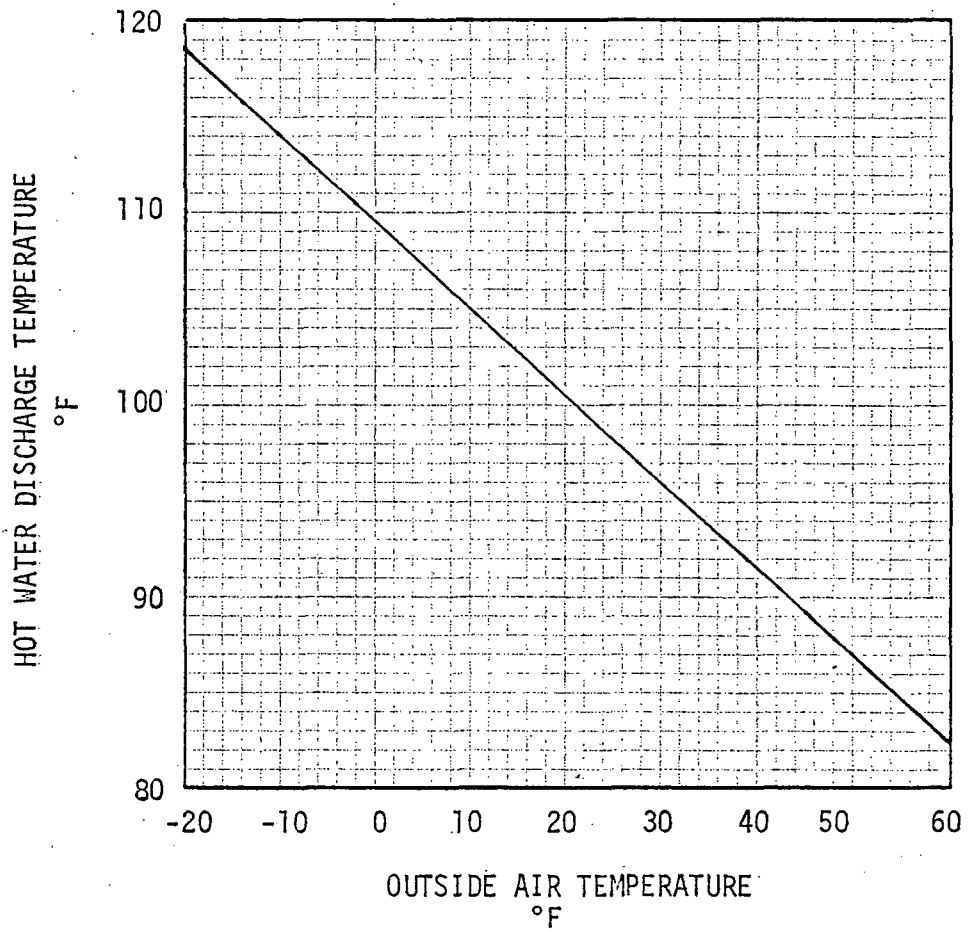


Fig. 3 - Programmed hot water discharge temperature as a function of outside air temperature.

HEAT PUMP AIR CONDITIONING SYSTEM

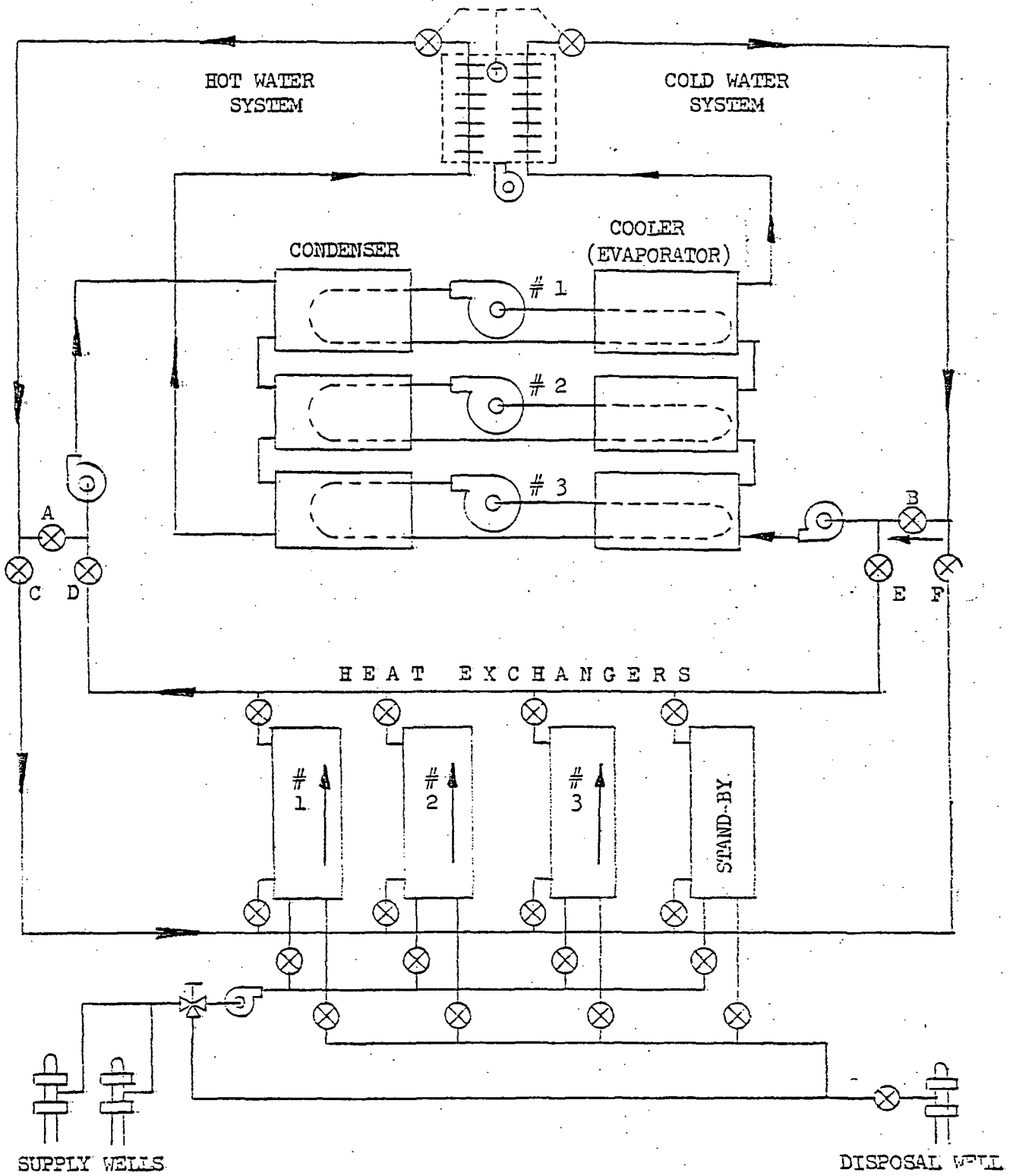


Fig. 4 - Cooling Cycle

HEAT PUMP AIR CONDITIONING SYSTEM

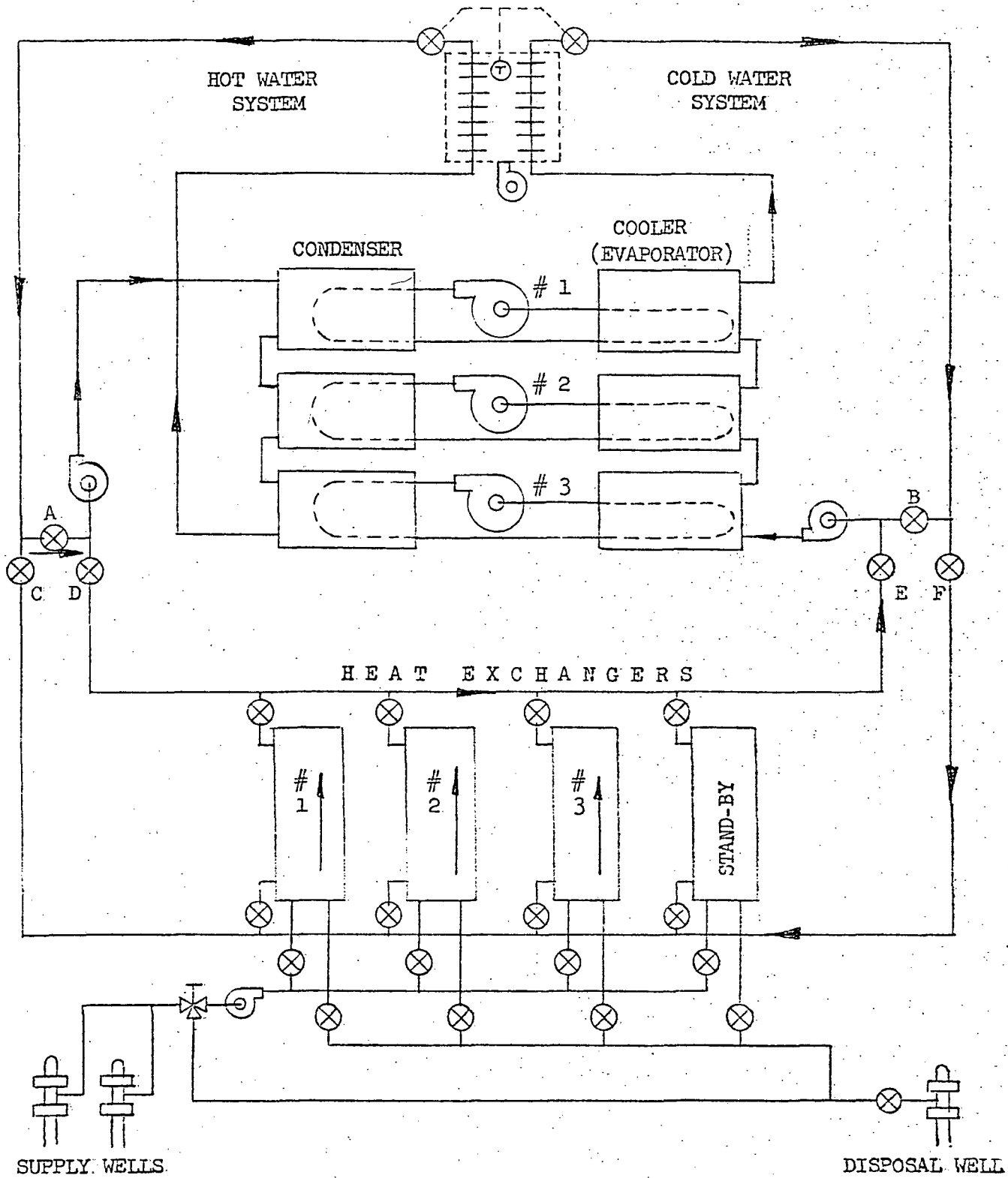


Fig. 2 - Heating Cycle

cooling and thereby maintains the necessary balanced condition in the refrigeration cycle. The well water which has been used to produce this effect is then discharged into a disposal well. This diversion to the heat exchangers is accomplished automatically by the pneumatic control system which closes valve B and opens valves E and F as necessary to achieve the required outlet water temperatures for both hot and cold water. (Control system also maintains valve A open and C and D closed to prevent cross circulation.) The hot water temperature called for is variable and is based on outside air temperature. For example, 114°F water is called for at an outside air temperature of -10°F while only 87°F water is called for at 50°F outside air temperature. (see Fig. 3)

b. Cooling Cycle (See Fig. 4)

Under summer conditions an excess of heat is generated in the refrigeration cycle and the discharge hot water temperature rises higher than required to support building heating requirements. In order to prevent continued temperature rise and accompanying high head pressures, the control system automatically stops the compressor when the temperature reaches approximately 150°F. Therefore, it is necessary to impose a false heating load to prevent interruption of the cooling function. Again, this is accomplished by routing the hot water through the shell of

the heat exchangers while 58-60°F well water is circulated through the tubes. The cooler well water removes the heat from the secondary refrigerant water just as if it had been used for building heating load and again maintains the necessary balanced operation in the refrigeration cycle. The warmed well water is then pumped into a disposal well as before. In accomplishing this, the pneumatic controls close valve A and open valves C and D as required to maintain the balanced condition (valves E and F are maintained closed and valve B open to prevent cross circulation). As in the heating cycle, discharge water temperature called for varies with outside air temperature. At an outside air temperature of 60°F the chill water discharge temperature is 53°F while at an outside air temperature of 95°F, it must be lowered to 42°F. (See Fig. 5)

3. In utilizing the hot and cold water produced in the refrigeration cycle, two main air heating and cooling systems are used. The larger "induction" system is employed around the periphery of the building to balance heat loss and gain through the windows while a dual duct "high velocity" system is used in the interior to balance the net occupancy and lighting load.
 - a. In the induction system, both hot and cold water is delivered to separate primary coils in a series arrangement in an air stream within a common enclosure. (See simplified diagram at Fig. 1) These units are located in the equipment rooms on the 13th floor and on the 4th floor of the East

CHILL WATER SUPPLY TEMPERATURE - °F

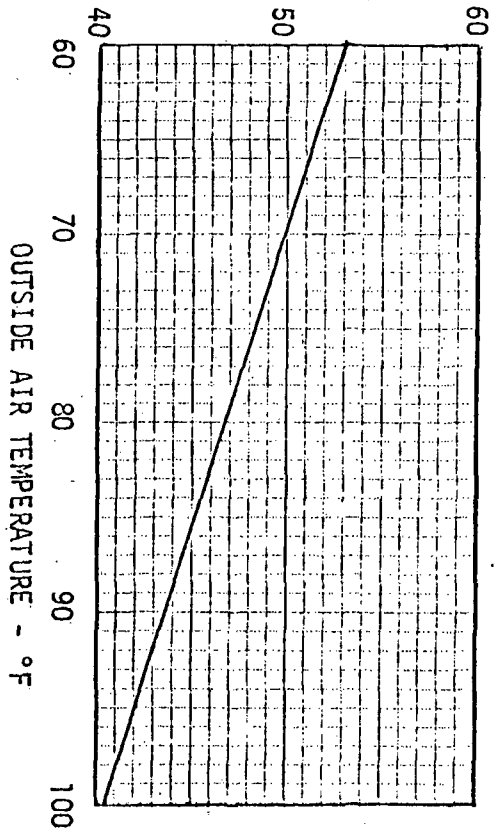


Fig. 5 - Programmed chill water temperature as a function of outside air temperature.

LEAVING AIR TEMPERATURE - °F

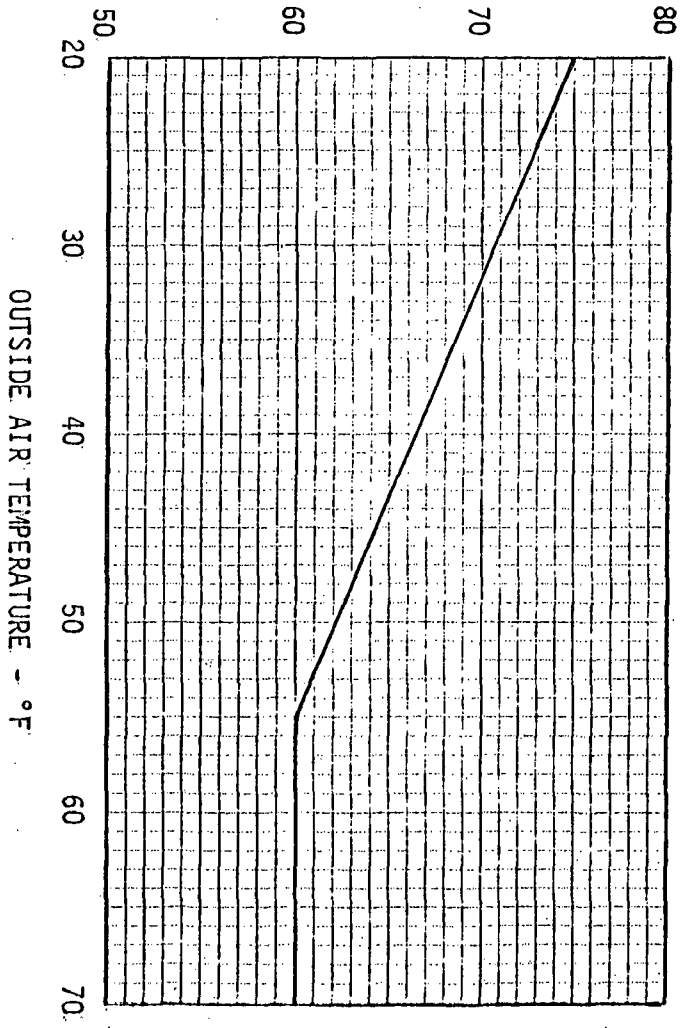


Fig. 6 - Primary induction system leaving air temperature as a function of outside air temperature.

and West wings. Fresh and return air is forced through the coils by a single fan and is heated or cooled depending upon the relative flow of hot or cold water within the coils of the unit. A pneumatic sensor regulates the flow of hot and cold water to give the desired leaving air temperature. This temperature varies between 60°F and 75°F and is based on outside air temperature. (See Fig. 6) When this air arrives at the various induction units around the periphery of the building it passes through tempering coils where additional heat is added or taken away to give the final leaving air temperature for discharge into the occupied space. (See Fig. 7) This temperature is determined by an attached controller which regulates the flow of hot and cold water to give the desired temperature, usually 72°F. The water used in these coils originates in the basic refrigeration cycle as does that used in the primary units mentioned.

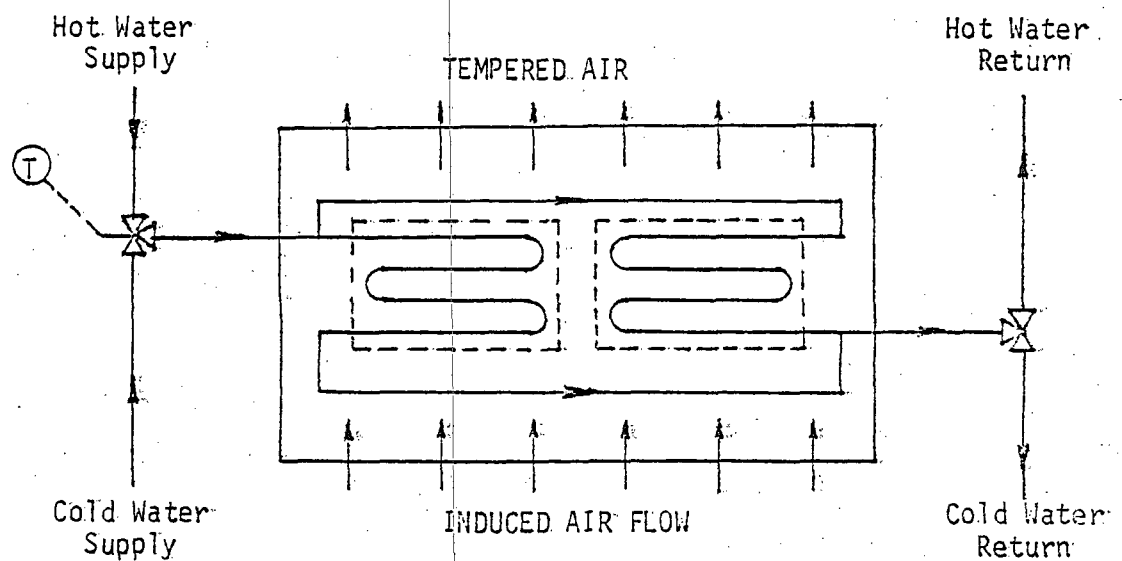


Fig. 7 - Secondary Induction Units.

b. A slightly different principle is used in the dual duct system in that separate air ducts are used to bring the hot and cold air to the occupied space. (See simplified diagram at Fig. 1) This air originates in units where fresh and return air pass through a heating and a cooling coil in separate parallel "decks". The conditioned air leaves these hot and cold decks in separate high velocity ducts and is routed to air mixing boxes located in the ceiling space of each floor. A damper in the mixing box responds to a room thermostat and moves to allow hot or cold air (or both) to enter the mixing box and be distributed to the air bar system in the ceiling at whatever temperature is selected. Hot and cold deck equipment is located in the East and West equipment rooms located on the 6th and 22nd floors, the 4th floor of the wings, the 1st lower level (serving cafeteria), and the 2d lower level storage area adjacent to the Relief Society Building. At the perimeter, care must be taken to assure that there is no more than 4°F difference in the setting of the room thermostat and the induction unit sensor controller otherwise the two systems will "fight each other" causing an out-of-control condition.

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SEISMIC-REFRACTION PROFILES ACROSS SIX CANYONS IN THE WASATCH RANGE NEAR SALT LAKE CITY, UTAH

By ROBERT E. MATTICK, Denver, Colo.

UNIVERSITY OF UTAH
RESEARCH INSTITUTE
EARTH SCIENCE LAB.

Work done in cooperation with the Utah State Engineer

Abstract.—Thickness of fill in six narrow canyons east of Salt Lake City, Utah, was determined by seismic-refraction profiling. The reciprocal method of shallow seismic-refraction interpretation proved a simple and reliable technique for depth computations where conventional seismic interpretation techniques were not applicable. A maximum fill thickness of about 250 feet and a minimum of about 5 feet were determined in Little Cottonwood and Big Cottonwood Canyons, respectively.

Investigation of the water resources of Salt Lake County, Utah, by the U.S. Geological Survey in cooperation with the Utah State Engineer involved the determination of the amount of ground water that is discharged through the unconsolidated fill material in several narrow canyons of the Wasatch Range east of Salt Lake City. To determine the thickness of the fill, seismic-refraction profiles were made across six canyons during the summer of 1965. The locations of these profiles are shown in figure 1. The steeply sloping ground surface in these narrow canyons, together with a small thickness of fill material, provides an unusual shallow seismic-refraction problem.

Figure 2 (City Creek Canyon) shows a typical seismic-refraction time-distance plot together with the computed cross section. This canyon is about 200 feet wide, and the ground surface is steeply sloping with sharp changes in slope. The unconsolidated fill material consists of boulders and stream debris. Bedrock is exposed on the northwest canyon slope and in the stream at the base of the steep southeast canyon wall.

In shooting the profile, 11 vertical seismometers were spaced between the bedrock outcrops and 1-pound dynamite charges were exploded in the stream and on the rock outcrop at the northwest end of the profile. The placement of charges directly on bedrock reasonably assures that the recorded seismic waves are refracted along the high-velocity interface and elimi-

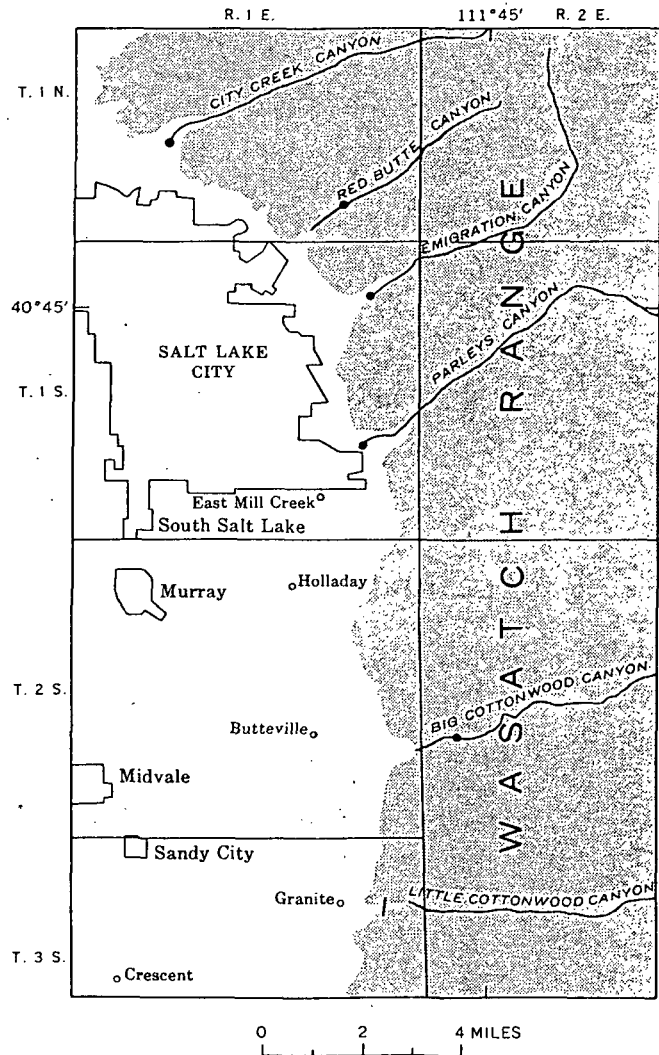


FIGURE 1.—Index map showing locations of the seismic profiles. Solid circles show the locations of seismic profiles in the five northern canyons, and a solid line shows the location of a seismic profile near the mouth of Little Cottonwood Canyon.

10/10/10

10

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10

10

10

and dividing the total by 2. It can be shown (Hawkins, 1961) that at a geophone the depth (Z) to the refracting interface, along the normal to the plane of the refractor, is given by

$$Z = tV_0 / \cos i, \quad (1)$$

where t is the time depth, V_0 is the velocity of the fill material, and i (the critical angle) is a function of V_0 and V_1 (bedrock velocity).

If the velocity of the bedrock is greater than the velocity of the fill by a factor of 5 or more, $\cos i$ will be approximately equal to 1 (error < 2) and equation 1 reduces to

$$Z = tV_0. \quad (2)$$

In such cases the true velocity of the bedrock is of little importance, and the uncertainty in depth estimation is directly related to the accuracy with which the velocity

(V_0) through the fill is measured. If a representative average velocity \bar{V}_0 is used in equation 2, the depth at a given point may be in error due to local velocity changes within the fill material, but the computed overall volume of fill will be relatively accurate.

Figure 3 shows computed sections across five additional narrow canyons in the Wasatch Range near Salt Lake City, Utah. The recording of relatively higher velocities for the fill in Little Cottonwood Canyon (fig. 3C) is attributed to its greater thickness. The higher bedrock velocity probably reflects the much greater width of this canyon, which allowed longer profiles (about 1,000 ft) and hence a deeper penetration of the seismic waves.

REFERENCE

- Hawkins, L. V., 1961, The reciprocal method of routine shallow seismic refraction investigations: *Geophysics*, v. 26, no. 6, p. 806-819.



AREA
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A DEMONSTRATION PROJECT
FOR GEOTHERMAL HEATING
OF GREENHOUSES

UNIVERSITY OF UTAH
RESEARCH INSTITUTE
EARTH SCIENCE LAB

Submitted to Energy Research and Development Administration

by

Miller Floral Company

Utah Roses, Inc.

Society of American Florists

May 20, 1977

UNIVERSITY OF UTAH
RESEARCH INSTITUTE
EARTH SCIENCE LAB.

Dr. James Bresee, Director
Division of Geothermal Energy
Energy Research & Development Administration
Washington, D. C.

Dear Sir:

It is proposed that ERDA, Miller Floral Company, of Farmington, Utah, Utah Roses, Inc., of Sandy, Utah, and the Society of American Florists, join together in a demonstration program to investigate and demonstrate the feasibility of (1) finding geothermal reservoirs of commercial value in population centers in the Rocky Mountain area, and (2) utilizing these reservoirs in competition with fossil fuels in commercial applications including the heating of greenhouses and for other space heating and other low-temperature uses.

This demonstration would be accomplished by drilling one test well in the Farmington, Utah area, and one in the Sandy, Utah area, using techniques developed by the Idaho National Engineering Laboratory in its projects at Raft River, Idaho, and at Boise, Idaho. If hot water is encountered in commercial quantities, the test wells would be completed, heat exchange and delivery equipment would be developed, and the heat from the water would be used to heat the greenhouses of Miller Floral Company and Utah Roses, Inc., and to provide heat to other commercial and residential customers in the vicinity of the two locations.

Present Geothermal Projects

Present geothermal projects in Utah and other western locations have centered on trying to find water of sufficiently high temperature to drive electric turbines of present design (400° F. water). Where lower temperatures have been

encountered, such as at Raft River, where 300° F. water is found, consideration is given to developing new designs for generators which could utilize 300° water. However, these projects, particularly Raft River and the Roosevelt Hot Springs area in Central Utah, are located in remote areas where no space heating requirement presently exists.

By contrast, a large potential market for lower temperature hot water exists in population centers, where temperatures as low as 130°-170° F. could be utilized for heating homes, commercial establishments, greenhouses, and almost any other kind of building. ERDA could provide a great impetus toward the utilization of geothermal heat as a replacement for fossil fuels by demonstrating the feasibility of using geothermal heat of relatively low temperatures for space-heating applications. This project could prove to be commercially feasible at today's fossil fuel prices, and without the need for large capital investments in electric generating plants. The heat could be used virtually in the same form as it is found, with very little processing required.

It is vital, however, that such low-temperature geothermal resources be discovered and developed where the market exists, namely, in highly populated areas.

Probability of Finding a Geothermal Reservoir

The report of the Idaho National Engineering Laboratory of ERDA on Idaho Geothermal Development Projects for the year ending February, 1976, states that the "Raft River Valley is typical of virtually every valley in the Rocky Mountain west." This refers to the presence of an occasional warm spring. The report refers

to Raft River as an "average valley geothermal setting." In the Raft River Valley, 240° water has been encountered at a depth of 2,000 feet, and 300° water at a greater depth. The size of the reservoir at 2,000 feet is unknown, but it is thought to extend for a considerable number of miles.

The Salt Lake valley would appear to have some of the same possibilities. There are warm springs at several locations along the Wasatch Front, on both sides of Farmington. Some slightly warm springs exist in Farmington. It is a general rule for this area that water temperature increases by 2° C. for every 100 feet in depth. These factors lead to the conclusion that there is good likelihood of finding hot water.

The techniques for drilling wells for hot water are different from conventional oil well drilling methods. Primarily, accurate and careful temperature monitoring is necessary, and the use of drilling mud must be carefully controlled to avoid sealing off potential hot water zones, and/or preventing geothermal flow from entering the hole and being detected. These techniques were used at Raft River and at Boise, and resulted in 100% success. By contrast, a well drilled by Utah Power & Light Company near Brigham City, Utah, used heavy drilling mud and casing, and was not carefully temperature monitored. Hot water was found at considerable depth, but it was not considered commercial because of the depth, and the temperature was not in the 400° range. Possibly with different drilling techniques, water in the 130° to 170° F. range would have been detected at shallower depths.

The Project

Two test wells will be drilled to a depth of approximately 2,000 feet, carefully monitoring temperatures and water flow. Care will be taken not to bypass

a warm water zone without detecting it.

One well will be drilled in an effort to intersect the Wasatch Fault at Farmington. The second will be drilled at Sandy, Utah, near a known area of warm springs and wells.

If no warm water is encountered, the project will be terminated, and no costs of phases II and III will be incurred.

If sufficient quantities of warm water are found, the wells will be completed, reinjection wells will be drilled, if needed, pumps and heat exchange equipment will be installed, and the geothermal heat will be used to heat the greenhouses at the locations where the successful wells have been drilled. In addition, homes and businesses in the area will be offered a supply of hot water. If feasible on an economic basis, depending on piping, right of way, and other costs, this will be offered at rates competitive to current fossil fuel heat costs.

If the initial wells are only partially successful or indicate promise, the third and fourth wells will be drilled as production wells, if indicated, and the initial wells can then be used as reinjection wells.

If only one of the sites produces hot water, then the second and third phase costs will be reduced by half, except for the engineering cost.

The microseismic data available at the University of Utah and the various information available from the USGS would be gathered and used in the selection of drilling sites. However, to minimize the legal and institutional problems and resulting delays, all drilling is proposed to be done on Miller Floral property, or on

Gov't plans to fund 50%, overall

adjacent property from which Miller could easily obtain leases and rights to drill and use water from the owners.

Because of the small value of the project wells, and the restricted area for locating the wells (piping water at \$100,000 to \$200,000 per mile makes this option impractical for more than one-half a mile), further geophysical exploration is neither economically justifiable or practical because of institutional and legal constraints on well siting. Therefore, drilling techniques to assure the cheapest wells and not inadvertently passing by the resource becomes the principal technical consideration.

Estimated Project Costs

Phase I - Exploration

Two exploratory wells to depth of ³~~2~~,000 feet 305,000
~~\$140,000~~

Phase II - Well Development

Complete exploratory wells, drill two more for rein-
(if necessary)
jection; obtain use permits (state, county, EPA) 100,000
~~80,000~~

Phase III - Utilization

Engineering	30,000
Pipelines	10,000
Heat Exchangers	75,000
Pumps	80,000
Installation and Check Out	20,000
<i>Information Gathering & Dissemination</i>	<i>10,000</i>
Contingency	80,000 20%
	\$295,000
Grand Total	\$515,000

Cost Sharing

It is proposed that ERDA fund 80% of the exploratory wells' cost. This is the area of real uncertainty in the project. No wells have been drilled in this area for geothermal heat, and relatively little information exists that would indicate the probability of success. Therefore, this phase of the project is a high-risk phase. Failure to find a useable reservoir would place a financial burden on Miller and Utah Roses which would be difficult for them to bear, and there would be no possibility of their recovering these costs. However, if this project were successful, it would be demonstrating to the general public the feasibility of finding space-heating hot water at nearly any location in the Salt Lake City area, and probably the Intermountain West, and possibly many other locations in the United States. The public would be greatly benefitted by success. Without ERDA participation, the private companies (Miller and Utah Roses) would be severely penalized by failure to find a reservoir.

It is proposed that ERDA fund 75% of the development cost. Successfully completing the wells so that they produce commercial quantities of heat, providing reinjection wells, as well as selling the basic concept to the regulatory agencies, would be time consuming and risky. The possibility of failure of the project would still be high, and no recovery could come to the private companies if the project does not succeed. Further, little is known about heat exchange with geothermal fluids, and costs of developing workable techniques could be high. Any workable methods, however, could be applied to other projects in the future.

It is proposed that ERDA fund 50% of the funds for the Utilization Phase. New equipment may need to be designed for heat exchange, and handling of the liquids could present problems of scaling and corrosion. Prototype equipment will have to be built. All of the knowledge gained in this process will benefit the general public, since it will be public knowledge.

Miller and Utah Roses will make any information desired available to any interested party and will make the premises available to anyone for inspection.

Cost Summary

	<u>ERDA</u>	<u>Miller-Utah Roses</u>	<u>Total</u>
Phase I - Exploration	\$112,000	\$ 28,000	\$140,000
Phase II - Development	60,000	20,000	80,000
Phase III - Utilization	<u>147,500</u>	<u>147,500</u>	<u>295,000</u>
	\$319,500	\$195,500	\$515,000

Miller Floral and Utah Roses can fund their Phase I and Phase II costs out of working capital.

Phase III costs can be funded from a line of credit Miller Floral has had approved with a bank for the purpose of capital improvements in the business. The loan would be repaid from revenue from the project, specifically from savings in fossil fuel use.

Economics

If sufficient quantities of water are found to heat the greenhouses, the economics would be as follows for each location:

Present heating cost: 100,000 MCF natural

gas at \$1.03/MCF	\$103,000
Standby fuel used during gas interruption	<u>7,000</u>
	\$110,000

Heating cost using geothermal heat:

Pumping cost, 100 H.P. motor, \$2.75/hr. estimated 275 days, est. 14 hrs./day av.	\$ 10,587
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Maintenance costs assumed to be equal on
boiler system or pumping system

Cash flow to amortize investment, per year, before tax	\$99,500	99,500
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Less depreciation and amortization, 15 years on \$186,750	<u>12,450</u>
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Profit before tax	\$87,050
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Federal and state tax, 48% + 6%	<u>47,007</u>
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Cash flow after tax, per year	<u>\$ 52,493</u>
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Investment by private company, assuming one of
two wells is successful:

All of private share, Phase I	\$28,000
One-half of private share, Phase II	10,000
One-half of private share, Phase III	73,750

Installation of additional heat dis-
tribution equipment in greenhouses
to use lower temperature fluids

(225⁰ steam is now used) 75,000 \$186,750

Miller Floral Company

Miller Floral Company is a grower of greenhouse roses and potted plants in Farmington, Utah, approximately fifteen miles north of Salt Lake City. It is also a wholesaler of floral products, selling cut flowers and plants grown in California, Oregon, Florida and Utah in addition to its own production. Annual sales exceed \$3,000,000. In 1976, 93,355 MCF of natural gas was used to heat the greenhouses, in addition to approximately 20,000 gallons of #2 burner fuel which was used during gas interruption.

As shown on the enclosed map, Miller's greenhouses are located within 5,000 feet of the Wasatch Fault in the Wasatch Mountains. Miller owns property within 1,600 feet of the fault.

Utah Roses, Inc.

Utah Roses, Inc. is a rose and pot plant grower located in Sandy, Utah, approximately ten miles south of Salt Lake City. Approximately 250,000 square feet of greenhouses are operated by Utah, with annual sales of over \$600,000. In 1976, 70,579 MCF of natural gas was used, plus approximately 20,000 gallons of #2 burner fuel.

Utah Roses is located somewhat in the center of the Salt Lake Valley, some ten miles from the Wasatch Mountains. It is approximately one mile east of the Jordan River. This site would give an indication of what hot water might be found further from mountains and faults, but still in an area with a sizable demand for warm water for space heating. Commercial buildings and homes are numerous in the immediate vicinity. There is indication of warm springs and wells in a large area of the Salt Lake Valley and Utah Roses is located within this area.

Personnel

Ralph M. Wright is general partner of Miller Floral Company and chairman of the board of Utah Roses. He is also serving as President of the Society of American Florists. He has a B.S. in Accounting and an M.B.A. from Harvard Business School. He has operated Miller Floral Company for thirteen years, and founded Utah Roses seven years ago. He is principal owner of both companies. He was general manager of a small independent oil refinery, Uinta Oil Refining Company, for three years.

C. Richard Wright is president of Utah Roses, Inc. He is co-founder of Utah Roses and has operated it for seven years. He is a director of Roses, Inc., the national trade association for rose growers.

Ralph M. Wright would act as program manager and be responsible for the project and, under the direction of ERDA personnel, for the proper utilization of project funds.

The Floral Industry

According to U.S. Department of Agriculture statistics, there is in excess of 137,000,000 square feet of greenhouse space in use at the present time for flower production. (See table.) Estimated fuel use is in the range of 40,000,000 MCF of natural gas or the equivalent in other fuels, primarily fuel oil.

Leaders in the flower-growing industry are seriously concerned about the future source of heat for greenhouses. The Society of American Florists Endowment, a research fund for the industry, has and is funding research programs on heat conservation in greenhouses and on solar heating. Energy costs for most greenhouses have more than doubled in the last three years, and they are expected to double again.

Solar heating for greenhouses is far from feasible now, because of the large amount of heat needed to be stored. Cost effective storage methods have yet to be devised.

Yet, the industry is ready to change. The heating methods outlined in this project could be adopted immediately, and cost effectively, by the industry. Also, it is possible that the greenhouses that might be able to utilize geothermal heat resources could serve as the nucleus for a heat-supplying company to supply heat to businesses and homes in the vicinity of the greenhouses. The funds now paying for the greenhouse heat load could serve as the source of funds that would be used to discover and develop the reservoir, and, once available, the reservoir could be used to serve other customers.

TABLE

Total Heat Load in Greenhouse Industry*

Twenty-three states:

<u>Production Area: 1976</u>	<u>Sq. Ft.</u>
Standard Carnations	28,768,000
Miniature Carnations	2,706,000
Standard Chrysanthemums	22,441,000
Pom Pon Chrysanthemums	37,412,000
Potted Chrysanthemums	17,689,000
Hybrid Tea Roses	23,420,000
Sweetheart Roses	<u>5,240,000</u>
Total square feet	137,676,000

*Source: USDA: Flowers & Foliage Plants, Production & Sales, 1975 & 1976

Sp. Cr. 6-1 (77).

Using Miller Floral as a typical case:

1976, natural gas used: 93,355 MCF for 250,000 sq. ft. = .373 MCF/sq. ft.

Projected usage for seven major crops in twenty-three major producing states:

$137,676,000 \times .373 = 51,333,148$ MCF of natural gas, or the equivalent in other fuels. (9.2 million BBI of oil.)

Information Dissemination -- Society of American Florists

SAF is the national trade association for the floral industry. There are over 6,000 direct members, including 740 growers. Also, there are 180 other trade associations in the floral industry (such as state associations) that are members of SAF. SAF publishes a monthly newspaper, and conducts a national convention annually. SAF's headquarters are in Alexandria, Virginia.

SAF could provide a vehicle to disseminate information that is gained in the project and it could interest growers in utilizing geothermal heat. SAF's national convention will be in Salt Lake City in July, 1977. Dr. Jay Kunze, manager of Geothermal Projects at Idaho National Engineering Laboratory has been invited to give a report on geothermal projects at that convention. Growers from all parts of the U.S. will be visiting Miller Floral and Utah Roses at the time of the convention.

SAF, if the project is successful, would be able to inform the leading growers throughout the United States of the potential for geothermal greenhouse heating, and could provide a conduit for technical information to the flower-growing industry.

ERDA Participation

The rationale for ERDA's participating in the program would seem to be two-fold:

1. To add to the resource base estimates of geothermal potential in one of the major metropolitan areas of the west.
2. To provide technical assistance and financial assistance for a demonstration project which at this time represents considerable risk. The size of most

non-electric space-heating projects are well below the project sizes that the major resource companies (oil companies) are interested in undertaking, therefore eliminating the major private source of exploration risk capital from the geothermal non-electric market.

In addition to the proposed financial participation, it is requested that ERDA make available the Idaho National Engineering Laboratory to assist with locating the drilling sites, selection of the drilling contractor, supervision of the contractor, monitoring the temperatures and other tests during drilling, well completion, design of heat exchange and other equipment, working with regulatory agencies to obtain necessary permits, and other areas where their experience and expertise will be valuable.

If the geothermal fluids encountered are highly saline, containing more than 5,000 ppm. dissolved solids, the project might consider the use of a fluidized bed heat exchanger, which is through a complete development stage at INEL. This would be the first application of this concept to geothermal applications. The assistance of INEL would be requested if this technology is needed because of the characteristics of the geothermal fluid.

Summary

There are good indications that low-temperature (170^o - 240^o F.) water exists underground in large quantities in the Intermountain West. This resource could be utilized now, cost effectively, if it were proved to be present and if techniques were developed to find and develop it.

The greenhouse industry could serve as a nucleus to get this resource utilized, because of its need for low-temperature heat.

Miller Floral Company and Utah Roses are situated in a location that could demonstrate the feasibility of using geothermal heat. Also, their connection with the Society of American Florists and Roses, Inc., national trade associations, and the participation of SAF in the project, would make it possible for the results of the demonstration project to be rapidly and effectively disseminated.

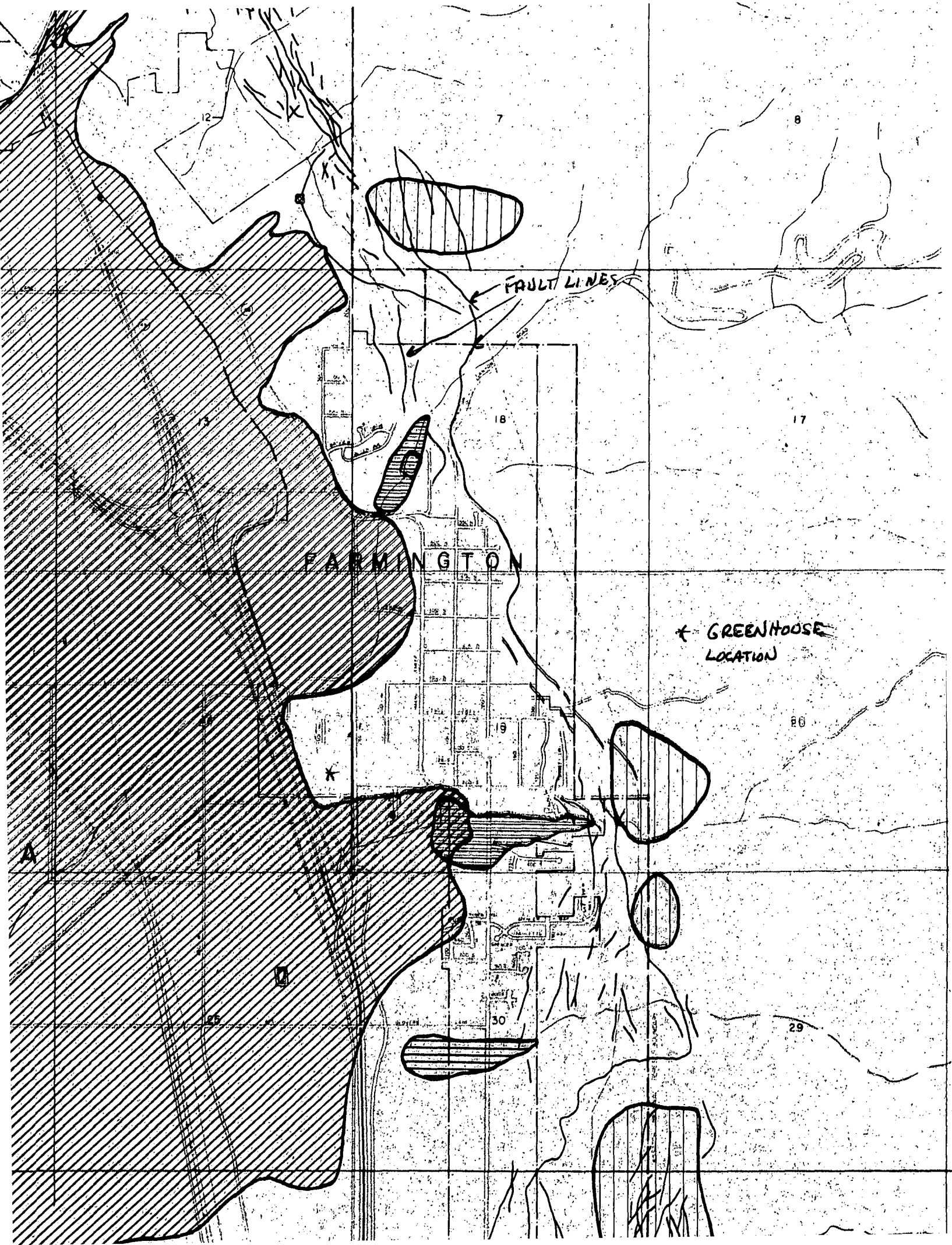
Conclusion

Of the many projects being funded in geothermal development, this one could be the most likely to result in immediate benefits to the country in terms of fuel savings. The expenditure of approximately \$112,000 of ERDA funds would indicate the likelihood of success in finding commercially feasible reservoirs of hot water. The total expenditure of \$319,500 would provide the public with a proved method of space heating that could reduce the consumption of fossil fuels by as much as one-third in specific areas, (the amount of fuel used for space heating in the Utah area.) This project should be undertaken immediately.

It is hoped that ERDA will give its early approval to this project.

If further information is desired, I will be pleased to try to provide it.

RALPH M. WRIGHT
General Partner
Miller Floral Company
Farmington, Utah



Geological Investigation

Idaho National Engineering Laboratory has looked into the geological situation involved in this proposal, and their report is enclosed.

GENERAL GEOTHERMAL RESOURCE
EVALUATION OF THE SALT LAKE VALLEY,
UTAH AREA

ABSTRACT

SUMMARY

ROUGH DRAFT

- 1.0 INTRODUCTION
- 2.0 ECONOMIC POTENTIAL
- 3.0 GENERAL TOPOGRAPHY AND HYDROLOGY
- 4.0 GENERAL GROUND-WATER
- 5.0 GENERAL GEOLOGY
- 6.0 GEOTHERMAL RESOURCE POTENTIAL
 - 6.1 TEMPERATURE OF GROUND WATER
 - 6.2 THERMAL SPRINGS
 - 6.3 GEOTHERMAL RESOURCE SETTING
 - 6.4 POTENTIAL GEOTHERMAL EXPLORATION DRILLING SITES
- 7.0 CONCLUSIONS AND RECOMMENDATIONS
- 8.0 REFERENCES

Prepared by
Geothermal Programs
Idaho National Engineering Lab.

ABSTRACT

This report is a preliminary evaluation of the geothermal resource potential of the low temperature (space heating range of 120° to 200°F)/ Salt Lake Valley (Wasatch Front) area. This assessment was undertaken as part of the Idaho National Engineering Laboratory's responsibility to evaluate and stimulate direct uses of geothermal energy for the commercial and non-federal entities. The brief study was specifically directed toward evaluating the geothermal potential of the area for use in the space heating of greenhouse complexes.

The opinions and recommendations presented are based on an area reconnaissance field study and a review of the most accessible literature written about the area. Area well drillers, well owners and greenhouse operators were contacted and information gathered from them.

The major references cited in this report are two Utah Geological and Mineralogical Survey - Water Resources Bulletins. The first is "Geology and Ground Water Resources of the Jordan Valley" (Water Resources Bulletin 7) by A. W. Marine and D. Price, USGS. The second is "Major Thermal Springs of Utah" (Water Resources Bulletin 13) by J. C. Mundorff, USGS.

SUMMARY

The Salt Lake Valley has numerous hot and warm springs that indicate the presence of a geothermal resource at depth. However, little use of these springs have been made other than for bathing purposes. This report focuses on the evaluation of the geothermal potential for space heating in the area.

If a geothermal reservoir producing water of 120°F or higher can be tapped in the immediate vicinity of a user, geothermal water could be fed directly from wells to a central heating plant. From there, hot water or heated air could be distributed to the areas to be served. The limited data available indicates that it is unlikely that geothermal water can be tapped at shallow depths at locations other than faults. Wells that do not intersect faults at depth may have to be drilled as deep as 3,000 feet or more.

However, if a geothermal reservoir producing water of only 90°F can be found close by, this temperature of water can be upgraded to the desired 150°F to 180°F by the use of heat pumps. The use of heat pumps extracting heat from water is a technique economically practical even on cool water (50°F) wells. It is being used for heating several large office buildings in Salt Lake City and will be used for the library at Idaho State University.

The conclusions and recommendations give a hopeful, but by no means a certain outlook for economic use of geothermal energy in the Salt Lake Valley. Considerable time, money and effort can be expended doing a detailed geological and geophysical survey of an area to fully evaluate the geothermal potential. However, wells are eventually required in the area to confirm the geological and geophysical interpretation of the structure beneath ground elevation.

The geothermal resource hypotheses based on the available data, can be tested fairly rapidly by drilling several exploratory wells in the area of the Wasatch Fault Zone.

1.0 INTRODUCTION

The area under immediate geological investigation lies mainly within the Jordan Valley of Utah but extends northward and includes Ogden, Utah and the southern part of Weber Valley. This cursory study was prompted by the interest expressed in the use of geothermal energy for the heating of greenhouse complexes within the study area.

Three greenhouse operations (Twentieth Century Farms, Miller Floral and Utah Roses) have expressed a desire to drill wells in the search for an adequate geothermal resource for space heating purposes. Each of these operations has about six (6) acres of greenhouses, each with annual heating bill approaching \$100,000. One greenhouse operation (Miller Floral) is at Farmington, Utah (North of Salt Lake City, but 20 miles South of Ogden). The other two greenhouses are near Sandy, Utah, at the southernmost point of interest for this particular study.

The area around Ogden, Utah, was also included in this study because of the proximity of Hill Air Force Base and the obvious benefits that geothermal space heating could have at an installation of this type.

The entire area is part of the Salt Lake Valley, elevation 4200 ft., characteristically bounded by the Wasatch Mountains by the east. These mountains rise typically 3000 to 6000 ft above the valley, and are quite active tectonically. Rainfall and spring run-off provides adequate water for irrigating and some hydroelectric power production. All of the run-off eventually drains into the closed Great Salt Lake.

2.0 ECONOMIC POTENTIAL

The Salt Lake Valley economic belt is approximately 90 miles long, only 10 miles wide, extending from Provo on the south to Brigham City on the north. The characteristics of this economic belt relevant to space heating using geothermal energy are as summarized in the following table:

SALT LAKE VALLEY

Population	950,000
Fraction of Population with 5 miles of Wasatch Fault	90%
Types of Industry	
i Heavy Industry (Copper and Steel)	
ii Light Manufacturing (Electronics)	
iii Government (State Government and DOD bases)	
Heating Requirements	~ 6,000 ⁰ F - days
Air Conditioning Req.	~ 700 ⁰ F - days
Temperature Extremes	- 15 ⁰ F to 105 ⁰ F

The area has a total space heating requirement of approximately 100×10^{12} Btu/year (0.1 Q), representing a significant contribution of which geothermal energy might conceivably contribute, someday. The proximity of all of these needs to the Wasatch Fault makes the availability of the energy at points at or very near to most potential users in the valley.

3.0 GENERAL TOPOGRAPHY & HYDROLOGY

The area of interest is within and north of the Jordan Valley, a structural valley in the Basin and Range physiographic province. The valley occupies about 400 square miles with Salt Lake City located in the north and east portion of the valley.

The valley is bounded on the east by the Wasatch Range, with peaks higher than 11,000 feet above mean sea level and a local relief of about 6,000 feet. The south is bounded by the Traverse Mountains, whose relief is about 2,000 feet. On the west are the Oquirrh Mountains with a relief of about 4,000 feet. The northern boundary is the Great Salt Lake and a low east-west salient from the Wasatch Range. The valley floor is relatively flat and gently sloping northward.

The principal source of surface water is the north flowing Jordan River and six major creeks that drains the Wasatch Range. Most of these creeks drain from about ten miles back from the mountain front and flow westward through the deep canyons. The streams flow across deposits of coarse unconsolidated material at the edges of the valley, losing part of their flow by influent seepage. This water recharges the vast ground - water basin that consists of unconsolidated deposits of gravel, sand, silt and clay. No perennial streams enter the valley from the Traverse or Oquirrh Mountains.

4.0 GENERAL GROUND-WATER

The ground water in the Jordan valley occurs in three general divisions: a shallow unconfined ground-water body, local perched water, and an artesian reservoir. Ground water is unconfined along the benches and forms a continuous body with the artesian reservoir in the central valley. Most of the recharge to the ground-water system is along the benches. The bulk of the ground-water resource is in the artesian reservoir in the lower portions of the valley.

The sediments that filled the Jordan Valley were deposited by several forces in several environments, and the complex pattern of deposition resulted in a ground-water aquifer that ranges widely from place to place in permeability and storativity. The lensy and discontinuous aquifers have been divided into six districts based on geology, water-bearing properties of the deposits, and the quality of the ground water.

The specific areas of interest, Farmington and Sandy, are similar only in the gross hydrogeologic aspect. It is necessary to discuss the areas separately for detailed hydrologic parameters.

The Farmington area can be described at depth geohydrologically as blue-gray or yellow clays with intercalated discontinuous thin lenses of gravel. Some alluvial fan deposits are present. The unconsolidated material is underlain by limestones or shales of the Tertiary age. The ground-water moves generally west and northwest, responding slowly to climatic changes. Most wells in the area are less than 6-inches in diameter and 300 feet in depth, with under flowing or near-flowing artesian conditions. Specific capacities range from 0.9 to 15 gpm/ft (gallons per minute per foot of drawdown) with an average of 4 gpm/ft.

The Sandy area can be described at depth geohydrologically as large thicknesses of well-sorted gravels interbedded with lake-bottom clays. There are also numerous channel gravels of ancient perennial streams. The ground-water moves generally northwest, responding irregularly to climatic changes. There exist many large diameter wells with hand dug wells common. Most wells are less than 150 feet in depth and under flowing artesian conditions. Specific capacities range from 6-200 gpm/ft with an average of 45 gpm/ft.

Thermal and non-thermal springs are associated with both areas. Those springs close to the Wasatch Range probably derive flow from mountain sources. Many cool and 100% of the hot springs are associated with the fault scarp.

5.0 GENERAL GEOLOGY

The area included in this report lies at the eastern edge of the Basin and Range physiographic province, bounded on the east by the Wasatch Range and on the south and west by the Traverse and Oquirrh Mountains. The area includes the Jordan Valley and the southern portion of the Weber Valley. The valleys are grabens and the surrounding mountains have been uplifted relative to the valleys. The boundaries between the valleys and mountains are most often marked by faults. In addition to the boundary faults separating the Jordan Valley from the adjacent mountains, other faults, more or less in the middle of the valley, define an inner graben which contains a considerable thickness of sediment derived from the adjacent mountains.

The Wasatch fault zone separates the Wasatch Range from the valleys and is the predominate feature in the area. The fault zone is a typical Basin and Range normal fault zone. It consists of a series of individual faults with a braided or branching pattern. Most of the faults in the valleys and on the east side strike N-S and dip 55° to 75° to the west. Those on the west side of the valleys strike N-S and dip to the east rather steeply (approximately 60°). Some of the major faults included in or associated with the Wasatch Fault zone are the Warm Springs, the Lime Kiln and the East Bench faults.

The Wasatch Fault zone and associated faults are currently active and movement along them have resulted in 53 strong earthquakes from 1850 to 1949. Generally, however, the majority of the disturbances have been relatively minor in nature and undetectable to the general populace. It would appear that the movements began in late Tertiary and have continued intermittently to the present time. The latest movement on the Wasatch Fault is that of normal upthrusting and the mountain block has been uplifted, carrying sediments of the Lake Bonneville group and younger alluvial fans upward from 60 to 200 feet.

The total vertical displacement along the Wasatch Fault zone is difficult to estimate because of the amount of sedimentation that has accumulated in the valleys and the covering of many of the fault lines. Several faults have been inferred from gravity surveys, but their displacement can only be estimated. There are few deep wells in the area and generally wells do not exceed 800 feet in depth. However, the vertical displacement would appear to be at least 750 feet and probably 3,000 feet or more.

The mountains that surround the area are composed of rocks that range in age from Precambrian to Recent. In the Wasatch Range to the east of the valley, the rocks include thick sequences of sedimentary rocks of Precambrian, Paleozoic, Mesozoic, and Cenozoic age intruded by granitic rocks of Late Cretaceous or early Tertiary age. The Traverse Mountains to the south consist principally of rocks of the Oquirrh Formation of Pennsylvanian and Permian age and of sedimentary and volcanic rocks of Tertiary age. The part of the Oquirrh Mountains that borders the Jordan Valley to the west is composed of Paleozoic rocks, principally of the Oquirrh Formation, but including Mississippian rocks, and sedimentary, intrusive, and extrusive rocks of Tertiary age.

Among the most impressive aspects of the landscape of the area are the deposits and erosional features of Lake Bonneville. Tremendous embankment deposits of gravel and sand are at the mouths of many canyons and at the Jordan Narrows. Sharp shorelines of Lake Bonneville are etched in bedrock and in pre-Lake Bonneville alluvial fans alike all around the valley. The most prominent shorelines are the Bonneville, ranging from about 5,135-5,180 feet, and the Provo at about 4,800 feet.

Alluvial deposits were laid down in the valley both before and after Lake Bonneville. On the west side of the valley the Tertiary deposits that have been pedimented by later erosion are principally stream or mudflow deposits. All over the valley minor stream activity since Lake Bonneville time has scarred or obscured older deposits.

The earth movements that originally formed the valley have continued into comparatively recent times and have formed scarps in the unconsolidated deposits of the valley. The most prominent of the faults showing late movement is the East Bench fault which is marked by a scarp that reaches a height of 80 feet in the unconsolidated deposits in the northeastern part of the Jordan Valley. The west-facing scarp of the East Bench fault, together with the east-facing scarps of the Jordan Valley fault zone delineate an inner graben within the Jordan Valley.

6.0 GEOHERMAL RESOURCE POTENTIAL

6.1 TEMPERATURE OF GROUND WATER

The temperature of ground water as measured and reported in the Jordan Valley ranges from 46⁰ to 139⁰F. The temperature of the water in most wells and springs, however, range from 52⁰ to 60⁰F.

The temperature of the ground water exceeds 60⁰F in two principle areas of the valley. The smaller of the two areas is just south of Sandy and west of Draper. The highest temperature recorded in this area is 139⁰F at Crystal Hot Springs, with the ground water temperature apparently decreasing away from the springs. The higher temperatures are probably caused by hot water moving upward along a fault zone at or near the spring.

The larger area of high temperature ground water occupies much of the northern part of the Jordan Valley. The eastern margin of this area is marked by several hot springs which rise along the Warm Springs Fault. The warmest temperature measured during this study was 130⁰F at Beck's Hot Springs. Most of the wells west of Beck's Hot Springs yield water warmer than 60⁰F. The principle source of heat for this area is not known. Warm water may be rising along a fault zone or heat may result from exothermic sections in the organic clays of the area.

6.2 THERMAL SPRINGS

Temperatures of the reported thermal springs in Utah range from 68⁰ to 189⁰F. Nearly all thermal springs are near or in fault zones. Very few of these springs issue from volcanic rocks, but a few are close to volcanics.

Total dissolved solids contents of Utah thermal springs range from 214 to 45,000 ppm (parts per million). Most springs are of the sodium chloride type (greater than 3,000 ppm NaCL).

Thermal springs within the area of interest number nine, mostly associated with the Wasatch Front. All of the springs, appear to be

associated with a fault zone. (See Figure 1.) Table 1 describes the location and some of the geochemical properties of these springs. Note that there appears to be a trend of degrading water quality of the thermal springs from south to north.

TABLE I

	Ave Est Discharge (gpm)	Ave Temp °F	Ave Silica SiO ₂	Ave Calcium Ca	Ave Magnesium Mg	Ave Sodium Na	Ave Potassium K	Ave Sulfate So ₄	Ave Chloride cL	Ave TDS Calculated	Ave pH
Crystal Hot Springs		137	55	114	28	336	55	140	541	1480	7.4
Wasatch Hot Springs		106	31	608	94	2001	195	1089	3531	7163	8.0
Becks Hot Springs	255	131	33	707	129	4953	249	884	7432	13,500	7.5
Como Warm Spring	9000	77	19	109	31	34	8.4	231	28	586	7.4
Utah Hot Spring		136	36	1071	50	7052	922	211	13,330	22,260	7.3
Saratoga Hot Spring		111	25	169	51	244	--	420	356	1017	7.8
Hooper Hot Springs		132	33	522	99	2417	246	41	4920	8848	7.6
Southwest Hooper Warm Springs		90	48	536	458	8290	803	219	14,400	27,800	--
Ogden Hot Springs	75	135	48	342	18	2790	371	107	5017	8700	7.6

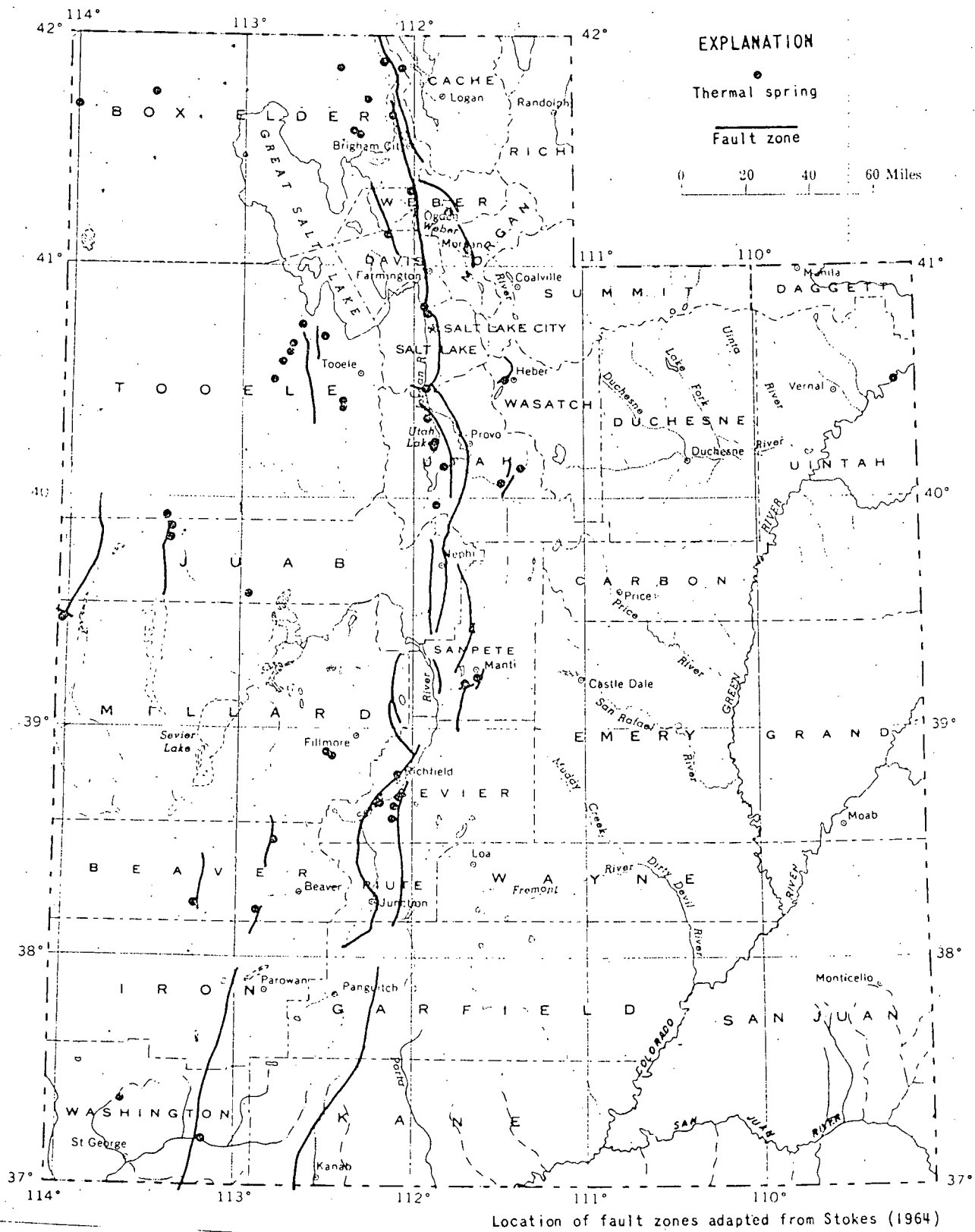


Fig. 1 Map showing locations of major thermal springs and major fault zones in Utah.
 (Taken from Utah Geological and Mineralogical Survey Water-Resources Bulletin 13, 1970)

6.3 GEOTHERMAL RESOURCE SETTINGS

Increasing attention is being directed toward thermal springs as indications of areas in which the use of geothermal energy might be economically feasible. Although thermal springs in an area indicate the existence of the geothermal resource at some depth, they do not indicate the economic feasibility of development of the resource, the depth and magnitude of the source of heat, or the optimum location for subsurface exploration and possible development of the geothermal resource. A thorough understanding of the structural geology of the area and of the movement of the geothermal water at depth is necessary in order to answer those important questions.

The detailed information and data is not available concerning the movement of the geothermal water at depth in the study area. The structural geology is only generally understood as inferred from the evidence exposed on the surface. However, several facts are known concerning the geothermal resource that can be used to evaluate the resource potential.

The majority of the hot or warm springs are associated with or occur along faults. See Figure 1. The dissolved chemicals in the water coming to the surface are a key to the temperature of the reservoir from which that water originated. The silica geothermometer indicates that the hot and warm springs waters have been at a temperature of at least 160^oF (Saratoga Hot Springs) to 215^oF (Crystal Hot Springs) somewhere at depth. See Table II.

Most of the water temperatures observed are probably the result of the normal geothermal gradient ($\sim 1^{\circ}\text{F}/100$ feet). Considering the base temperature of 160^o - 215^oF, this would necessitate at most a migration depth of approximately 15,000 feet below the source area. If the source area in the Wasatch Mountains ($\sim 8,000$ feet elevation) the water would need to percolate to about 7,000 feet below the valley floor. If cold water mixing occurred during the upward movement of the geothermal water (which seems likely) due to the presence of cold springs then the observed discharge temperatures at the springs would result.

There is little direct evidence of a geothermal resource in the vicinity of Sandy of Farmington but there is a hot well in the northeast

section of Ogden that brights the prospects in that area. It appears that the development of geothermal resources within the study area will depend first on the correct selection of faults that provide a conduit for the geothermal water from depth. Second, the exploration well must be offset downdip of the surface expression of the fault to intersect the fault at a reasonable depth (<2,000 feet) in order to minimize drilling costs. Third, the well must encounter water temperatures in the 150-180°F range and be a very productive well (>400 gpm).

6.4 POTENTIAL GEOTHERMAL EXPLORATION DRILLING SITES

There are very few deep (>800 feet) wells in the study area to serve as guides for geothermal resource drilling. The greatest potential for tapping the resource would appear to be along the surface expressions of the major faults comprising the Wasatch Fault zone. These faults dip approximately 65° in the westerly direction. The drill rig should be offset approximately 850 feet west of the surface fault line and drilled as straight down as possible. This should result in intersecting the fault at about the 1200 foot depth if the fault does indeed dip at 65°.

TABLE II

INPUT DATA FOR GEOTHERMOMETER CALCULATIONS AND RESULTS OF GEOTHERMOMETRY CALCULATIONS

Name	SiO ₂	Na/K/Ca	Mixing Model Temperature	Fraction in Cold Water	Date of Water Analysis	SiO ₂	Na (PPM)	K (PPM)	Ca (PPM)
Becks Hot Springs	355.24 180°F	396.47	393°K 120°C 248°F	0.60	7-26-67	32	4250	156	746
Utah Hot Springs	357.79 184°F	525.83	393°K 120°C 248°F	0.56	5-18-67	34	6870	932	1040
Crystal Hot Springs	374.96 215°F	**	448°K 175°C 347°F	0.76	5-27-58	50	330*	--	142
Saratoga Hot Springs	345.19 162°F	**	383°K 120°C 248°F	0.70	3-24-66	25	214*	--	190

* Na plus K reported as Na

** Insufficient data available for calculation

$$^{\circ}\text{C} = ^{\circ}\text{K} - 273.16^{\circ}$$

7.0 CONCLUSIONS AND RECOMMENDATIONS

Although it appears that geothermal energy represents a potentially economically attractive space heating method for the Salt Lake Valley, there is no certainty that a geothermal resource can be found in sufficient abundance or at shallow enough depth to be economical. For the three major greenhouses, there is no certainty that a resource exists close enough (within 300 yards) or hot enough for use by the existing facilities in the area. It should be noted, however, that from the limited data available, there appears to be a good chance of tapping the resource within the area faults at reasonable depths (~1500 feet). The temperature of the water, at this depth, is unknown at present, but indications are that it could be about 180°F in properly selected locations.

The chemical nature of the water is not attractive for direct use consideration, i.e. a heat exchanger will most likely be a necessity. The high dissolved solids content (7000-22,000 ppm) and H₂S gas will also make used water disposal a problem, virtually requiring injection into disposal wells. There may be exceptions. Much purer water might be found, and even if not at 120°F (minimum) could be used for heat pump boosting as a very economical method of space heating.

Therefore, the following recommendations are made for consideration in the immediate future. No commitment is implied at this time that this laboratory or ERDA could or would be permitted to act on any of these recommendations.

1. Additional area well and geological data should be gathered and evaluated in terms of the specific geothermal considerations. Specific attention should be given to all current geophysical information and interpretation of that information to determine the detailed geological structure in the area of the Wasatch Fault zone and the valley proper.

OR

2. Drill several exploratory wells based on the available information contained in this report and then re-evaluate the data based on the acquired well information for further geothermal development.

8,0 REFERENCES

1. A. W. Mavine and D. Price (USGS), "Geology and Ground-Water Resources of the Jordan Valley, Utah," Utah Geological and Mineralogical Survey, Water-Resources Bulletin 7 (December 1964).
2. J. C. Mundorff (USGS), "Major Thermal Springs of Utah," Utah Geological and Mineralogical Survey, Water-Resources Bulletin 13 (September 1970).
3. Guidebook to the Geology of Utah, Number 8 collection of papers, "Geology of the Central Wasatch Mountains, Utah," Utah Geological and Mineralogical Survey (1952).
4. Guidebook to the Geology of Utah, Number 18, collection of papers "The Wasatch Fault Zone in North Central Utah," Utah Geological and Mineralogical Survey (1964).

March 17, 1978

Ralph M. Wright
Miller Floral Company
P.O. Drawer "M"
Farmington, Utah 84025

Dear Ralph:

Attached is a proposal which I believe came from Wayne Brown, which in turn came from you. As I recall, you and I talked over the phone regarding this last year. I am returning it for your file, since it may contain data which is proprietary and confidential to you.

I still look forward to meeting with you at some convenient time. I hope that we may get together and have lunch or some such. Best regards, and I wish you success in your operations.

Very truly,



Sidney J. Green

SJG:pam

Attachment

SIDNEY J. GREEN / PRESIDENT

UNIVERSITY RESEARCH PARK / 420 WAKARA WAY / SALT LAKE CITY, UTAH 84108 / (801) 582-2220

AREA
UT.
SaltLK
Grav

H.P. Ross
UNIVERSITY OF UTAH
RESEARCH INSTITUTE
ICE LAB.
(41 data pages)

Listing of Principal Facts of Gravity

Stations in Jordan Valley, Utah

by

Laura F. Serpa and Kenneth L. Cook

April 15, 1980

Listing of gravity data in Jordan Valley area, Utah

All of the stations listed on the following pages have been tied to the gravity base station network in Utah (Cook et al., 1967). Because the various surveys were conducted over several years and with different instruments, the accuracy of the various surveys will vary. Any station that did not appear to be accurate enough to be included in the contour map is indicated with an '*' and may represent a bad reading or possible error in input to the computer.

The following is a listing of the station prefixes used in this listing and the source of these gravity values. Where possible the estimated accuracy is also given.

<u>Prefix</u>	<u>Taken by</u>	<u>Accuracy</u>
W	Cook and Berg, 1961	0.5 mgal
H	W. Johnson, 1958	
RR	W. Johnson, 1957-58	
BL	J. Berg & L. Rauser, 1958	
A	Novotny, 1957-58	
MB	Novotny, 1957-58	
P	Parker-wide spaced, 1979	0.05 mgal
PG	Parker-tight grid, 1979	0.05 mgal
MBE	D. Mabey	2.5 mgal
78	1978 gravity class, University of Utah	1.0 mgal
F	R. C. Fox, 1979	0.05 mgal

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
W0885	40.27.000	111.40.270	6032.00	979640.52	980220.51	-12.62	-218.07	22.71	-195.36
W0887	40.26.990	111.38.910	6332.00	979629.19	980220.50	4.28	-211.39	17.68	-193.71
W0888	40.25.980	111.38.140	7260.00	979581.80	980219.00	45.68	-201.60	9.80	-191.80
W0889	40.26.130	111.37.700	7479.00	979569.10	980219.22	53.35	-201.38	6.31	-195.07
W0266	40.26.570	111.55.310	4491.00	979751.47	980219.87	-45.98	-198.94	2.00	-196.94
W0267	40.25.210	111.55.530	4705.00	979737.52	980217.85	-37.78	-198.03	1.40	-196.63
W0268	40.25.220	111.54.370	4546.00	979745.12	980217.87	-45.15	-199.99	1.24	-198.75
W0269	40.24.350	111.54.360	4521.00	979745.53	980216.58	-45.70	-199.69	1.11	-198.58
W0270	40.24.350	111.53.150	4522.00	979742.35	980216.58	-48.89	-202.91	1.10	-201.81
W0271	40.24.370	111.51.590	4578.00	979731.92	980216.61	-54.08	-210.01	1.22	-208.79
W0272	40.25.140	111.52.610	4570.00	979739.47	980217.75	-48.43	-204.08	1.33	-202.75
W0273	40.25.890	111.53.430	4627.00	979741.54	980218.86	-42.10	-199.70	1.43	-198.27
W0281	40.26.720	112. 6.400	6278.00	979656.47	980220.10	26.88	-186.95	2.87	-184.08
W0282	40.26.690	112. 6.070	6411.00	979645.56	980220.05	29.63	-188.73	2.37	-186.36
W0283	40.26.070	112. 4.130	5820.00	979680.21	980219.13	8.51	-189.72	1.89	-187.83
W0284	40.25.250	112. 3.960	5906.00	979676.71	980217.91	14.32	-186.84	1.65	-185.19
W0285	40.26.090	112. 3.040	5622.00	979693.75	980219.16	3.40	-188.09	1.66	-186.43
W0286	40.26.050	112. 2.140	5518.00	979699.33	980219.10	-.75	-188.69	1.98	-186.71
W0287	40.26.900	112. 2.390	5897.00	979673.15	980220.36	7.46	-193.39	1.65	-191.74
W0288	40.25.240	111.50.940	4769.00	979720.89	980217.90	-48.44	-210.87	1.49	-209.38
W0289	40.25.240	111.50.370	4783.00	979720.13	980217.90	-47.88	-210.79	1.59	-209.20
W0290	40.25.250	111.49.230	4801.00	979719.40	980217.91	-46.93	-210.45	1.32	-208.63
W0291	40.25.250	111.48.080	4836.00	979718.52	980217.91	-44.52	-209.23	2.22	-207.01
W0292	40.25.250	111.47.500	4866.00	979717.52	980217.91	-42.69	-208.43	2.53	-205.90
W0293	40.25.250	111.46.350	4898.00	979719.06	980217.91	-38.14	-204.97	3.66	-201.31
W0294	40.26.950	111.45.040	5044.00	979710.55	980220.44	-35.45	-207.25	13.80	-193.45
W0295	40.26.050	111.44.140	5180.00	979691.05	980219.10	-40.82	-217.25	21.82	-195.43
W0296	40.26.170	111.43.640	5283.00	979681.71	980219.28	-40.65	-220.59	27.55	-193.04
W0297	40.26.400	111.43.130	5425.00	979673.07	980219.62	-36.27	-221.05	28.60	-192.45
W0298	40.26.690	111.41.860	5755.00	979654.49	980220.05	-24.24	-220.26	26.28	-193.98
W0299	40.26.820	111.41.100	5923.00	979645.10	980220.24	-18.02	-219.76	24.57	-195.19
W0300	40.26.630	111.42.130	5659.00	979659.13	980219.96	-28.54	-221.29	27.49	-193.80
W0301	40.26.820	111.46.650	4941.00	979712.26	980220.24	-43.23	-211.52	4.36	-207.16

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE FOUGUER
W0311	40.26.760	111.48.100	4909.00	979712.37	980220.15	-46.04	-213.24	3.00	-210.24
W0312	40.26.990	111.50.700	5362.00	979688.84	980220.50	-27.31	-209.94	3.00	-206.94
W0313	40.23.430	111.49.790	4558.00	979728.42	980215.21	-58.06	-213.31	1.37	-211.94
W0314	40.23.210	111.49.260	4549.00	979728.79	980214.89	-58.22	-213.15	1.47	-211.69
W0315	40.23.430	111.48.180	4622.00	979728.06	980215.21	-52.40	-209.83	1.79	-208.04
W0316	40.23.450	111.47.390	4674.00	979726.94	980215.24	-48.66	-207.86	2.12	-205.74
W0317	40.23.510	111.46.350	4754.00	979724.23	980215.33	-43.94	-205.86	2.89	-202.97
W0318	40.23.520	111.45.190	4733.00	979727.36	980215.35	-42.80	-204.01	4.58	-199.33
W0319	40.23.530	111.44.670	4756.00	979727.00	980215.36	-41.01	-203.00	6.42	-196.58
W0320	40.24.380	111.44.950	4940.00	979717.89	980216.62	-34.07	-202.33	6.77	-195.56
W0321	40.23.200	111.43.820	5193.00	979721.90	980214.87	-4.52	-181.39	7.61	-173.78
W0322	40.22.970	111.44.340	4666.00	979731.10	980214.53	-44.55	-203.47	6.29	-197.18
W0326	40.23.400	111.50.920	4558.00	979728.68	980215.17	-57.76	-213.01	1.14	-211.87
W0327	40.23.460	111.51.970	4536.00	979733.99	980215.26	-54.61	-209.11	1.04	-208.07
W0328	40.23.230	111.52.570	4521.00	979737.49	980214.92	-52.18	-206.17	.97	-205.20
W0329	40.23.230	111.53.550	4500.00	979743.98	980214.92	-47.67	-200.94	.95	-199.99
W0330	40.23.240	111.54.920	4546.00	979750.10	980214.93	-37.23	-192.07	.97	-191.10
W0331	40.23.210	111.56.080	4679.00	979746.32	980214.89	-28.46	-187.83	1.01	-186.82
W0332	40.23.080	111.56.930	4807.00	979741.77	980214.69	-20.77	-184.50	1.00	-183.50
W0443	40.22.560	112. .620	4997.00	979734.07	980213.92	-9.83	-180.03	.94	-179.09
W0445	40.23.020	112. .480	5039.00	979729.18	980214.60	-11.45	-183.08	.98	-182.10
W0446	40.23.460	112. .510	5108.00	979725.34	980215.26	-9.46	-183.44	1.02	-182.42
W0447	40.24.110	112. .790	5185.00	979722.19	980216.22	-6.33	-182.93	1.39	-181.54
W0448	40.22.600	112. 2.600	5168.00	979720.81	980213.98	-7.07	-183.09	1.01	-182.08
W0449	40.22.610	112. 4.660	5327.00	979710.01	980214.00	-2.93	-184.37	1.75	-182.62
W0450	40.23.050	112. 4.650	5385.00	979706.77	980214.65	-1.37	-184.78	1.73	-183.05
W0451	40.24.360	112. 4.590	5492.00	979699.20	980216.59	-.81	-187.87	1.85	-186.02
W0452	40.24.850	112. 4.770	5603.00	979694.25	980217.32	3.95	-186.89	2.04	-184.85
W0453	40.24.180	112. 3.790	5466.00	979700.84	980216.32	-1.35	-187.52	1.60	-185.92
W0454	40.24.760	112. 6.680	5787.00	979685.80	980217.19	12.94	-184.17	4.45	-179.72
W0455	40.25.060	112. 7.130	5890.00	979679.42	980217.63	15.80	-184.81	5.05	-179.76
W0462	40.22.610	112. 4.660	5328.00	979709.99	980214.00	-2.86	-184.33	1.75	-182.59
W0921	40.25.900	111.50.940	4809.00	979720.53	980218.88	-46.02	-209.81	1.74	-208.07

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE FOUGUER
W0922	40.25.890	111.49.270	4825.00	979718.31	980218.86	-46.71	-211.05	2.04	-209.01
W0923	40.25.900	111.48.650	4838.00	979717.76	980218.88	-46.06	-210.84	2.26	-208.58
W0924	40.25.900	111.48.080	4858.00	979716.79	980218.88	-45.15	-210.61	2.49	-208.12
W0925	40.26.130	111.47.040	4909.00	979715.32	980219.22	-42.16	-209.36	3.34	-206.02
W0926	40.26.130	111.46.360	4946.00	979715.04	980219.22	-38.96	-207.42	4.15	-203.27
W0927	40.24.600	111.46.340	4840.00	979721.57	980216.95	-40.03	-204.88	3.40	-201.48
W0928	40.24.820	111.45.210	4979.00	979714.86	980217.27	-34.09	-203.67	6.07	-197.60
W0929	40.24.390	111.45.210	4861.00	979722.15	980216.64	-37.26	-202.83	5.82	-197.01
W0930	40.22.980	111.45.500	4632.00	979731.54	980214.54	-47.31	-205.08	3.62	-201.46
W0931	40.22.540	111.45.500	4578.00	979732.71	980213.89	-50.57	-206.50	3.30	-203.20
W0932	40.22.980	111.46.350	4629.00	979729.83	980214.54	-49.31	-206.97	2.70	-204.27
W0933	40.24.390	111.47.360	4798.00	979721.73	980216.64	-43.61	-207.03	2.38	-204.65
W0934	40.24.380	111.48.120	4777.00	979721.23	980216.62	-46.07	-208.77	2.02	-206.75
W0935	40.24.370	111.49.210	4767.00	979719.91	980216.61	-48.32	-210.68	1.80	-208.88
W0936	40.24.030	111.50.560	4596.00	979727.95	980216.10	-55.85	-212.39	1.29	-211.10
W0196	40.33.570	111.55.110	4393.00	979756.09	980230.27	-60.97	-210.60	1.34	-209.26
W0197	40.33.740	111.56.280	4477.00	979752.07	980230.52	-57.34	-209.83	1.05	-208.78
W0198	40.33.740	111.57.420	4554.00	979747.68	980230.52	-54.49	-209.60	.89	-208.71
W0200	40.32.650	111.58.560	4631.00	979739.90	980228.90	-53.41	-211.14	.86	-210.28
W0201	40.30.460	111.57.420	4511.00	979741.70	980225.65	-59.65	-213.29	1.12	-212.17
W0202	40.30.470	111.56.270	4449.00	979746.26	980225.66	-60.93	-212.46	1.21	-211.25
W0203	40.32.210	111.57.410	4503.00	979745.32	980228.25	-59.38	-212.75	1.02	-211.73
W0204	40.32.650	111.56.290	4439.00	979749.58	980228.90	-61.69	-212.88	1.10	-211.78
W0205	40.32.230	111.52.360	4478.00	979746.51	980228.28	-60.57	-213.09	2.45	-210.64
W0206	40.32.230	111.53.430	4450.00	979748.30	980228.28	-60.91	-212.48	1.80	-210.68
W0207	40.30.040	111.52.860	4462.00	979744.57	980225.02	-60.75	-212.73	2.65	-210.08
W0208	40.30.450	111.51.150	4560.00	979741.46	980225.63	-55.26	-210.57	4.47	-206.10
W0209	40.31.040	111.51.150	4520.00	979743.25	980226.51	-58.11	-212.06	4.34	-207.72
W0210	40.30.700	111.51.890	4483.00	979743.53	980226.00	-60.70	-213.39	3.29	-210.10
W0211	40.29.340	111.53.590	4526.00	979744.19	980223.99	-54.08	-208.24	2.42	-205.82
W0977	40.32.650	111.55.710	4395.00	979751.89	980228.90	-63.62	-213.31	1.21	-212.10
W0978	40.31.560	111.55.700	4407.00	979749.48	980227.28	-63.28	-213.38	1.25	-212.13
W0979	40.31.340	111.55.700	4409.00	979749.24	980226.96	-63.01	-213.18	1.26	-211.92

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE FOUGUER	T.C.	COMPLETE FOUGUER
W0980	40.30.680	111.55.700	4434.00	979747.27	980225.98	-61.65	-212.67	1.28	-211.39
W0981	40.33.080	112. 1.430	4907.00	979731.60	980229.54	-36.39	-203.52	.87	-202.65
W0523	40.31.980	112. 8.950	6083.00	979674.78	980227.91	19.04	-188.15	6.25	-181.90
W0524	40.31.630	112. 9.450	6317.00	979658.78	980227.39	25.57	-189.59	7.42	-182.17
W0525	40.31.060	112. 8.500	6554.00	979647.49	980226.54	37.42	-185.81	4.66	-181.15
W0526	40.32.560	112. 8.780	5873.00	979685.43	980228.77	9.07	-190.96	9.90	-181.06
W0527	40.33.670	112. 7.690	5970.00	979635.50	980230.42	16.62	-186.72	3.13	-183.59
W0528	40.31.070	112.14.350	5105.00	979732.56	980226.55	-13.81	-187.69	36.96	-150.73
W0529	40.30.740	112.13.630	5434.00	979713.14	980226.06	-1.80	-186.88	41.32	-145.56
W0530	40.30.420	112.12.970	5723.00	979705.93	980225.59	18.65	-176.28	33.02	-143.26
W0884	40.27.240	111.39.680	6076.00	979640.85	980220.87	-8.51	-215.46	20.92	-194.54
W0886	40.28.910	111.38.710	6356.00	979629.19	980223.35	3.69	-212.80	11.89	-200.91
W0212	40.30.460	111.58.560	4598.00	979735.54	980225.65	-57.62	-214.23	1.07	-213.16
W0213	40.30.470	111.59.510	4695.00	979730.22	980225.66	-53.83	-213.74	1.06	-212.68
W0214	40.30.470	112. 1.420	4892.00	979727.52	980225.66	-38.00	-204.62	1.19	-203.43
W0215	40.30.470	112. 2.560	5026.00	979723.36	980225.66	-29.05	-200.24	1.31	-198.93
W0217	40.32.230	112. 4.200	5175.00	979718.88	980228.28	-22.64	-198.90	1.42	-197.48
W0218	40.32.230	112. 3.150	5060.00	979724.07	980228.28	-28.27	-200.61	1.13	-199.48
W0219	40.32.210	112. 1.940	4922.00	979730.57	980228.25	-34.72	-202.36	.99	-201.37
W0220	40.32.220	112. .850	4813.00	979734.02	980228.26	-41.53	-205.46	.92	-204.54
W0221	40.32.220	111.59.520	4682.00	979736.76	980228.26	-51.11	-210.58	.90	-209.68
W0222	40.30.660	112. 3.180	5105.00	979719.76	980225.95	-26.01	-199.89	1.33	-198.56
W0223	40.30.240	112. 4.710	5366.00	979709.43	980225.32	-11.16	-193.93	2.00	-191.93
W0224	40.30.800	112. 5.020	5337.00	979713.25	980226.15	-10.90	-192.68	2.06	-190.62
W0225	40.30.910	112. 4.480	5306.00	979712.86	980226.32	-14.38	-195.10	1.54	-193.45
W0226	40.29.370	112. 7.290	5998.00	979677.02	980224.03	17.16	-187.13	5.79	-181.34
W0227	40.31.370	112. 5.620	5519.00	979704.32	980227.00	-3.56	-191.54	2.07	-189.47
W0228	40.32.040	112. 6.590	5909.00	979633.42	980227.99	11.23	-190.03	2.83	-187.20
W0229	40.32.330	112. 5.620	5444.00	979708.01	980228.43	-8.36	-193.78	1.99	-191.79
W0230	40.32.850	112. 6.390	5713.00	979696.23	980229.20	4.39	-190.19	2.34	-187.85
W0231	40.32.640	112. 4.600	5281.00	979713.35	980228.89	-18.91	-198.68	1.46	-197.22
W0232	40.33.030	112. 4.940	5352.00	979710.24	980229.47	-15.82	-198.11	1.51	-196.60
W0245	40.33.780	112. 1.120	4904.00	979732.80	980230.58	-36.51	-203.54	.81	-202.73

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE FOUGUER	T.C.	COMPLETE FOUGUER
W0246	40.33.450	111.59.850	4805.00	979736.02	980230.09	-42.11	-205.77	.94	-204.83
W0252	40.33.570	111.47.380	5117.00	979709.91	980230.27	-39.05	-213.34	22.87	-190.47*
W0253	40.32.800	111.49.810	4810.00	979725.74	980229.12	-50.95	-214.78	5.29	-209.49
W0254	40.32.240	111.51.040	4773.00	979727.71	980228.29	-51.63	-214.20	3.85	-210.35
W0255	40.30.180	111.51.150	4618.00	979738.90	980225.23	-51.96	-209.25	4.40	-204.85
W0256	40.29.240	111.55.200	4451.00	979749.01	980223.84	-56.17	-207.77	1.51	-206.26
W0257	40.29.360	111.56.360	4439.00	979746.52	980224.01	-59.96	-211.15	1.37	-209.78
W0258	40.29.370	111.56.870	4488.00	979743.50	980224.03	-58.39	-211.25	1.31	-209.94
W0259	40.28.720	111.56.860	4579.00	979739.24	980223.06	-53.12	-209.08	1.36	-207.72
W0260	40.28.720	111.58.000	4691.00	979733.23	980223.06	-48.59	-208.37	1.50	-206.87
W0261	40.29.370	111.58.550	4662.00	979732.73	980224.03	-52.79	-211.58	1.32	-210.26
W0262	40.29.800	111.59.130	4664.00	979732.20	980224.67	-53.77	-212.63	1.32	-211.31
W0263	40.29.060	112. .650	5099.00	979717.31	980223.57	-26.65	-200.32	1.62	-198.70
W0264	40.27.700	112. .250	5657.00	979685.17	980221.55	-4.28	-196.96	1.64	-195.32
W0265	40.27.320	112. 1.430	6018.00	979664.85	980220.99	9.91	-195.06	1.83	-193.23
W0274	40.28.380	111.55.750	4443.00	979749.91	980222.56	-54.74	-206.07	1.63	-204.44
W0275	40.29.800	112. 1.410	4953.00	979725.53	980224.67	-33.26	-201.96	1.49	-200.47
W0276	40.29.840	112. 2.570	5076.00	979722.97	980224.73	-24.31	-197.20	1.58	-195.62
W0277	40.29.620	112. 3.430	5174.00	979719.41	980224.40	-18.32	-194.55	1.81	-192.74
W0278	40.29.090	112. 3.300	5279.00	979713.87	980223.61	-13.20	-193.00	2.21	-190.79
W0279	40.28.500	112. 4.470	5486.00	979702.02	980222.74	-4.71	-191.56	2.80	-188.76
W0280	40.27.930	112. 5.010	5648.00	979690.45	980221.89	-.19	-192.56	3.29	-189.27
W0302	40.27.340	111.46.640	4956.00	979711.99	980221.02	-42.87	-211.67	5.02	-206.65
W0303	40.27.470	111.45.520	5052.00	979706.84	980221.21	-39.18	-211.25	8.20	-203.05
W0304	40.27.910	111.45.730	5121.00	979702.18	980221.86	-38.00	-212.42	7.66	-204.76
W0305	40.27.930	111.46.710	5055.00	979705.29	980221.89	-41.13	-213.30	5.80	-207.50
W0306	40.27.320	111.47.090	4963.00	979710.66	980220.99	-43.51	-212.55	4.37	-208.18
W0307	40.27.650	111.48.010	5156.00	979698.92	980221.43	-37.59	-213.20	3.55	-209.65
W0308	40.29.760	111.50.080	5004.00	979716.96	980224.61	-36.97	-207.41	7.77	-199.64
W0309	40.29.150	111.49.300	5859.00	979661.74	980223.70	-10.86	-210.42	3.68	-206.74
W0310	40.27.600	111.48.450	5134.00	979700.04	980221.40	-38.46	-213.32	3.34	-209.98
W0937	40.30.250	111.52.180	4478.00	979744.04	980225.34	-60.10	-212.62	3.21	-209.41
W0938	40.30.040	111.51.450	4615.00	979737.77	980225.02	-53.16	-210.35	3.98	-206.37

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
W0939	40.30.670	111.50.570	4589.00	979741.27	980225.96	-53.05	-209.35	6.74	-202.61
W0940	40.31.570	111.50.010	4702.00	979733.52	980227.30	-51.51	-211.66	8.21	-203.45
W0941	40.31.070	111.50.080	4864.00	979723.53	980226.55	-45.51	-211.18	8.26	-202.92
W0942	40.31.800	111.50.750	4656.00	979734.51	980227.64	-55.19	-213.77	4.40	-209.37
W0943	40.32.660	111.51.020	4773.00	979729.01	980228.92	-50.96	-213.53	3.59	-209.94
W0944	40.32.650	111.51.710	4575.00	979742.26	980228.90	-56.32	-212.14	2.72	-209.42
W0945	40.33.080	111.51.700	4597.00	979742.36	980229.54	-54.79	-211.36	2.62	-208.74
W0946	40.33.530	111.51.700	4598.00	979743.98	980230.21	-53.74	-210.35	2.54	-207.81
W0947	40.33.530	111.52.270	4537.00	979747.84	980230.21	-55.62	-210.15	2.20	-207.95
W0948	40.33.090	111.52.280	4548.00	979745.48	980229.55	-56.29	-211.19	2.26	-208.93
W0949	40.33.530	111.53.400	4397.00	979755.50	980230.21	-61.13	-210.89	1.79	-209.10
W0950	40.33.530	111.54.040	4382.00	979756.57	980230.21	-61.47	-210.72	1.61	-209.11
W0951	40.32.650	111.53.420	4454.00	979749.35	980228.90	-60.61	-212.31	1.78	-210.53
W0952	40.32.650	111.54.580	4398.00	979752.33	980228.90	-62.89	-212.69	1.45	-211.24
W0953	40.31.600	111.54.580	4406.00	979750.30	980227.34	-62.61	-212.68	1.49	-211.19
W0954	40.31.600	111.53.400	4421.00	979749.44	980227.34	-62.06	-212.64	1.93	-210.71
W0955	40.31.590	111.52.810	4433.00	979747.85	980227.33	-62.51	-213.50	2.33	-211.17
W0956	40.31.500	111.51.920	4488.00	979744.05	980227.19	-61.00	-213.86	3.00	-210.86
W0957	40.30.960	111.53.410	4426.00	979747.96	980226.39	-62.12	-212.87	1.99	-210.83
W0958	40.31.330	111.56.280	4435.00	979747.78	980226.94	-62.00	-213.06	1.19	-211.87
W0959	40.31.330	111.57.420	4512.00	979742.84	980226.94	-59.70	-213.38	1.05	-212.33
W0960	40.31.330	111.58.560	4603.00	979736.38	980226.94	-57.10	-213.88	.95	-212.93
W0961	40.31.330	111.59.130	4652.00	979733.85	980226.94	-55.52	-213.97	.95	-213.02
W0962	40.31.340	111.59.550	4689.00	979732.28	980226.96	-53.63	-213.34	.95	-212.39
W0963	40.30.460	111.58.080	4565.00	979737.90	980225.65	-59.37	-213.85	1.07	-212.78
W0964	40.30.460	111.56.980	4482.00	979743.99	980225.65	-60.18	-212.84	1.15	-211.69
W0132	40.40.710	111.47.380	5144.00	979739.89	980240.88	-17.15	-192.35	6.02	-185.43
W0143	40.40.010	112. 5.460	4858.00	979761.97	980239.84	-20.93	-186.39	1.56	-184.83
W0144	40.39.940	112. 5.680	4904.00	979759.59	980239.73	-18.87	-185.90	1.66	-184.24
W0145	40.39.940	112. 3.700	4814.00	979764.75	980239.73	-22.18	-186.14	1.05	-185.09
W0146	40.40.050	112. 2.600	4746.00	979769.76	980239.90	-23.73	-185.38	.91	-184.47
W0147	40.40.060	112. 1.440	4605.00	979779.24	980239.91	-27.52	-184.37	.73	-183.64
W0148	40.40.060	112. .300	4505.00	979782.98	980239.91	-33.19	-186.63	.66	-185.97

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
W0149	40.40.030	111.59.760	4474.00	979783.58	980239.87	-35.47	-187.85	.66	-187.19
W0150	40.40.020	111.53.680	4294.00	979786.88	980239.85	-49.08	-195.33	1.36	-193.97
W0151	40.40.300	111.54.570	4275.00	979789.05	980240.27	-49.11	-194.72	1.13	-193.59
W0152	40.40.400	111.55.470	4272.00	979739.51	980240.42	-49.09	-194.59	.97	-193.62
W0153	40.40.060	111.56.870	4304.00	979788.08	980239.91	-47.00	-193.59	.81	-192.78
W0154	40.40.050	111.58.000	4379.00	979785.79	980239.90	-42.22	-191.37	.71	-190.66
W0155	40.40.220	111.51.200	4328.00	979786.56	980240.15	-46.50	-193.91	2.35	-191.56
W0156	40.40.030	111.50.320	4367.00	979784.53	980239.87	-44.58	-193.32	3.00	-190.32
W0157	40.40.400	111.48.870	4598.00	979774.58	980240.42	-33.35	-189.96	4.58	-185.38
W0158	40.39.550	111.48.690	4534.00	979774.63	980239.15	-38.05	-192.48	6.62	-185.86
W0159	40.37.940	111.47.940	4843.00	979749.17	980236.76	-32.06	-197.01	7.51	-189.50
W0160	40.38.280	111.48.680	4561.00	979767.87	980237.27	-40.39	-195.74	5.92	-189.82
W0161	40.38.310	111.50.020	4434.00	979774.59	980237.31	-45.66	-196.68	3.46	-193.22
W0162	40.38.430	111.51.230	4388.00	979775.63	980237.49	-49.12	-198.58	2.45	-196.13
W0163	40.37.910	111.52.280	4396.00	979772.29	980236.72	-50.94	-200.67	1.92	-198.75
W0164	40.38.580	111.53.280	4337.00	979778.90	980237.71	-50.87	-198.59	1.60	-196.99
W0165	40.38.580	111.54.570	4320.00	979781.77	980237.71	-49.60	-196.74	1.21	-195.53
W0166	40.38.770	111.55.850	4298.00	979784.34	980237.99	-49.38	-195.77	.98	-194.79
W0167	40.38.310	111.56.850	4460.00	979772.94	980237.31	-44.86	-196.77	.86	-195.91
W0168	40.38.310	111.57.980	4563.00	979767.21	980237.31	-40.90	-196.32	.85	-195.47
W0169	40.38.310	111.59.120	4571.00	979768.02	980237.31	-39.34	-195.03	.68	-194.35
W0170	40.38.310	112. .290	4640.00	979763.75	980237.31	-37.12	-195.16	.70	-194.46
W0171	40.38.310	112. 1.430	4813.00	979754.26	980237.31	-30.34	-194.27	.78	-193.49
W0172	40.38.230	112. 2.610	4999.00	979742.46	980237.19	-24.52	-194.79	.90	-193.89
W0176	40.37.440	111.55.690	4334.00	979775.35	980236.02	-53.01	-200.63	1.10	-199.53
W0178	40.37.430	112. 1.430	4816.00	979750.06	980236.00	-32.95	-196.98	.81	-196.17
W0179	40.35.710	112. 1.410	4829.00	979743.74	980233.45	-35.49	-199.97	.82	-199.15
W0180	40.35.710	112. .270	4708.00	979750.80	980233.45	-39.82	-200.17	.77	-199.40
W0181	40.35.700	111.59.140	4597.00	979756.64	980233.43	-44.40	-200.97	.77	-200.20
W0182	40.35.920	111.58.350	4521.00	979761.12	980233.76	-47.39	-201.38	.81	-200.57
W0183	40.35.640	111.56.850	4427.00	979764.21	980233.34	-52.73	-203.51	.95	-202.56
W0184	40.35.860	111.54.300	4346.00	979768.76	980233.67	-56.13	-204.15	1.46	-202.69
W0185	40.35.250	111.54.570	4311.00	979768.71	980232.76	-58.56	-205.39	1.41	-203.98

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
W0186	40.35.700	111.53.730	4381.00	979765.42	980233.43	-55.93	-205.15	1.55	-203.60
W0187	40.35.630	111.52.270	4507.00	979757.25	980233.33	-52.15	-205.66	1.96	-203.70
W0188	40.34.390	111.52.270	4518.00	979751.37	980231.49	-55.16	-209.04	2.12	-206.92
W0189	40.34.390	111.51.410	4586.00	979747.45	980231.49	-52.68	-208.88	2.61	-206.27
W0190	40.35.700	111.51.120	4663.00	979747.00	980233.43	-47.83	-206.65	2.46	-204.19
W0191	40.35.700	111.49.990	4722.00	979743.10	980233.43	-46.18	-207.01	3.32	-203.69
W0192	40.36.130	111.49.130	4682.00	979747.14	980234.07	-46.54	-206.01	4.61	-201.40
W0193	40.37.450	111.50.000	4518.00	979766.19	980236.03	-44.88	-198.76	3.37	-195.39
W0194	40.37.280	111.51.890	4444.00	979767.62	980235.78	-50.16	-201.52	2.05	-199.47
W0195	40.33.960	111.53.990	4380.00	979758.60	980230.85	-60.27	-209.45	1.60	-207.85
W0199	40.33.960	111.59.130	4688.00	979742.07	980230.85	-47.83	-207.50	.80	-206.70
W0974	40.36.560	111.55.690	4341.00	979771.35	980234.71	-55.05	-202.90	1.16	-201.74
W0975	40.35.260	111.55.700	4364.00	979765.61	980232.78	-56.69	-205.33	1.19	-204.14
W0976	40.34.340	111.55.700	4393.00	979759.97	980231.41	-58.23	-207.86	1.16	-206.70
W0982	40.34.530	112. .840	4838.00	979739.07	980231.69	-37.56	-202.34	.78	-201.56
W0983	40.33.960	112. 2.150	4988.00	979729.14	980230.85	-32.54	-202.43	.89	-201.54
W0984	40.34.550	112. 3.650	5142.00	979720.06	980231.72	-28.00	-203.14	1.12	-202.02
W0985	40.35.270	112. 3.530	5100.00	979723.22	980232.79	-29.86	-203.57	1.12	-202.45
W0986	40.35.720	112. 2.420	4935.00	979737.13	980233.46	-32.14	-200.23	.91	-199.32
W0987	40.39.180	111.56.850	4352.00	979783.28	980238.60	-45.97	-194.20	.82	-193.38
W0988	40.39.180	111.57.980	4467.00	979776.92	980238.60	-41.51	-193.66	.75	-192.91
W0989	40.39.180	111.59.170	4558.00	979772.54	980238.60	-37.33	-192.58	.65	-191.93
W0990	40.39.180	112. .300	4637.00	979769.53	980238.60	-32.91	-190.85	.69	-190.16
W0991	40.39.180	112. 1.440	4771.00	979763.56	980238.60	-26.28	-188.78	.79	-187.99
W0992	40.39.180	112. 2.590	4948.00	979751.70	980238.60	-21.49	-190.02	.96	-189.06
W1007	40.40.460	111.52.230	4301.00	979787.04	980240.51	-48.92	-195.41	1.82	-193.59
W1008	40.39.230	111.54.570	4296.00	979786.11	980238.68	-48.49	-194.81	1.20	-193.61
W1009	40.39.360	111.53.250	4297.00	979784.37	980238.87	-49.82	-196.18	1.53	-194.65
W1010	40.38.980	111.51.920	4336.00	979780.46	980238.31	-50.01	-197.69	2.07	-195.62
W1011	40.39.430	111.51.210	4334.00	979783.55	980238.98	-47.77	-195.39	2.44	-192.95
W1012	40.39.350	111.50.050	4385.00	979781.06	980238.86	-45.35	-194.70	3.40	-191.30
W1013	40.40.480	111.48.090	4908.00	979755.66	980240.54	-23.23	-190.40	5.86	-184.54
W1077	40.36.890	111.47.730	5071.00	979730.00	980235.20	-28.22	-200.94	6.70	-194.24

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
W1078	40.36.570	111.47.730	5068.00	979726.73	980234.72	-31.29	-203.91	7.07	-196.84
W1079	40.36.570	111.48.570	4906.00	979735.21	980234.72	-38.05	-205.15	4.94	-200.21
W1080	40.37.430	111.49.440	4597.00	979761.65	980236.00	-41.96	-198.53	3.96	-194.57
W1081	40.36.780	111.49.440	4781.00	979745.03	980235.04	-40.31	-203.15	3.87	-199.23
W1082	40.36.620	111.49.020	4820.00	979741.29	980234.80	-40.14	-204.31	4.27	-200.04
W1083	40.36.830	111.48.870	4801.00	979744.59	980235.11	-38.94	-202.46	4.49	-197.97
W1084	40.37.280	111.46.310	5144.00	979717.80	980235.73	-34.14	-209.34	20.37	-188.97
W1108	40.37.410	111.48.880	4778.00	979750.39	980235.97	-36.16	-198.90	4.51	-194.39
W1109	40.37.560	111.51.230	4431.00	979770.27	980236.20	-49.15	-200.07	2.44	-197.63
W1110	40.37.240	111.52.870	4391.00	979770.02	980235.72	-52.68	-202.24	1.70	-200.54
W1112	40.38.000	111.53.340	4353.00	979775.20	980236.85	-52.21	-200.47	1.57	-198.90
W1111	40.37.890	111.54.580	4299.00	979779.39	980236.69	-52.94	-199.36	1.23	-198.13
W0517	40.39.170	112. 4.430	5034.00	979745.06	980238.59	-20.03	-191.49	1.16	-190.33
W0518	40.38.870	112. 4.130	5142.00	979736.97	980238.14	-17.51	-192.65	1.19	-191.46
W0519	40.37.960	112. 5.270	5533.00	979708.89	980236.79	-7.47	-195.92	2.01	-193.91
W0520	40.38.320	112. 3.510	5104.00	979735.69	980237.33	-21.56	-195.40	1.01	-194.39
W0521	40.36.560	112. 3.290	5031.00	979731.57	980234.71	-29.92	-201.28	1.06	-200.22
W0522	40.34.840	112. 4.040	5195.00	979718.37	980232.15	-25.14	-202.08	1.24	-200.84
W0216	40.33.970	112. 3.790	5210.00	979716.78	980230.86	-24.03	-201.48	1.17	-200.31
W0233	40.33.910	112. 6.070	5504.00	979709.10	980230.77	-3.96	-191.43	2.08	-189.35
W0234	40.34.480	112. 6.470	5784.00	979695.52	980231.62	7.94	-189.06	2.22	-186.84
W0235	40.34.880	112. 6.330	5721.00	979698.61	980232.21	4.52	-190.34	2.13	-188.21
W0236	40.35.550	112. 4.540	5271.00	979715.25	980233.21	-22.17	-201.70	1.36	-200.34
W0177	40.37.450	111.57.990	4465.00	979770.69	980236.03	-45.36	-197.44	.78	-196.66
W0237	40.34.620	112. 4.830	5349.00	979712.51	980231.83	-16.09	-198.28	1.47	-196.81
W0238	40.35.710	112. 3.440	5082.00	979725.75	980233.45	-29.69	-202.78	1.08	-201.70
W0239	40.37.380	112. 3.150	5171.00	979727.70	980235.93	-21.85	-197.97	1.06	-196.91
W0240	40.35.840	112. 6.620	5874.00	979689.23	980233.64	8.10	-191.97	2.52	-189.45
W0241	40.36.050	112. 5.880	5566.00	979706.00	980233.95	-4.41	-193.99	1.92	-192.07
W0242	40.37.160	112. 5.570	5410.00	979715.54	980235.60	-11.20	-195.46	1.76	-193.70
W0243	40.37.070	112. 5.110	5380.00	979714.96	980235.47	-14.47	-197.71	1.50	-196.21
W0244	40.36.610	112. 4.470	5154.00	979725.83	980234.78	-24.16	-199.71	1.42	-198.29
W0247	40.37.240	111.46.940	5213.00	979721.93	980235.72	-23.46	-201.01	10.44	-190.57

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE POUGUER	T.C.	COMPLETE FOUGUER
W0248	40.36.130	111.47.710	5038.00	979725.30	980234.07	-34.90	-206.49	8.03	-199.46
W0249	40.34.760	111.49.430	4858.00	979733.34	980232.04	-41.76	-207.22	4.19	-203.03
W0250	40.34.400	111.50.580	4792.00	979734.64	980231.50	-46.12	-209.34	3.07	-206.27
W0251	40.34.170	111.49.420	4943.00	979724.68	980231.16	-41.54	-209.90	4.43	-205.47
W0495	40.38.440	111.37.870	7433.00	979580.52	980237.50	42.17	-211.00	11.04	-199.96
W0504	40.35.440	111.38.050	8585.00	979505.66	980233.05	80.12	-212.29	11.35	-200.94
H52	40.37.560	111.44.460	5816.00	979672.93	980236.20	-16.22	-214.31	22.86	-191.45
H53	40.38.170	111.41.850	6709.00	979618.92	980237.10	12.87	-215.64	16.36	-199.28
H54	40.38.960	111.38.880	7268.00	979593.15	980238.28	38.50	-209.05	10.36	-199.69
H55	40.38.600	111.39.010	7412.00	979585.03	980237.74	44.46	-207.99	7.99	-200.00
H58	40.35.480	111.37.960	8697.00	979499.75	980233.11	84.68	-211.54	9.73	-201.81
H59	40.34.890	111.39.590	8142.00	979526.64	980232.23	60.25	-217.07	13.34	-203.73
H60	40.34.580	111.40.740	7704.00	979548.47	980231.77	41.34	-221.06	17.71	-203.35
H61	40.34.350	111.43.540	6493.00	979612.28	980231.43	-8.42	-229.57	32.76	-196.81
W0040	40.47.260	111.43.110	4863.00	979776.60	980250.62	-16.61	-182.24	25.57	-156.67
W0042	40.47.390	111.42.710	4668.00	979790.35	980250.81	-21.39	-180.38	33.60	-146.78
W0048	40.46.710	111.41.160	4830.00	979778.71	980249.80	-16.78	-181.29	27.86	-153.43
W0049	40.46.150	111.40.430	4830.00	979777.63	980248.97	-17.03	-181.54	33.12	-148.42
W0058	40.47.150	112. . . 930	4223.00	979831.09	980250.45	-22.14	-165.93	.37	-165.61
W0065	40.47.040	112. 8.300	4208.00	979829.13	980250.29	-25.36	-168.68	.22	-168.46
W0066	40.47.040	112. 6.030	4216.00	979824.54	980250.29	-29.19	-172.79	.23	-172.56
W0067	40.47.040	112. 4.890	4218.00	979829.13	980250.29	-24.41	-168.08	.23	-167.85
W0068	40.47.040	112. 2.890	4219.00	979834.38	980250.29	-19.07	-162.77	.27	-162.50
W0069	40.47.040	112. 2.020	4220.00	979833.65	980250.29	-19.71	-163.44	.30	-163.14
W0070	40.47.040	111.59.100	4224.00	979816.87	980250.29	-36.11	-179.93	.49	-179.49
W0072	40.47.470	111.58.020	4213.00	979813.70	980250.93	-40.96	-184.45	.62	-183.83
W0073	40.47.080	111.56.330	4215.00	979806.68	980250.35	-47.01	-190.57	.97	-189.60
W0074	40.46.820	111.55.320	4219.00	979806.05	980249.96	-47.07	-190.77	1.29	-189.43
W0075	40.46.950	111.54.460	4220.00	979812.14	980250.16	-41.09	-184.82	1.89	-182.93
W0076	40.45.260	111.52.390	4274.00	979800.75	980247.64	-44.88	-190.45	2.06	-188.39
W0077	40.45.250	111.53.250	4241.00	979800.03	980247.63	-48.69	-193.14	1.65	-191.49
W0078	40.45.120	111.54.990	4224.00	979797.90	980247.43	-52.22	-196.09	1.09	-195.00
W0079	40.45.510	111.56.300	4232.00	979799.33	980248.01	-50.62	-194.76	.82	-193.94

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE FOUGUER
W0080	40.45.070	111.57.160	4226.00	979800.12	980247.36	-49.74	-193.68	.58	-193.00
W0081	40.45.510	111.58.280	4230.00	979804.50	980248.01	-45.54	-189.61	.56	-189.05
W0082	40.45.280	111.59.390	4227.00	979809.00	980247.67	-41.08	-185.05	.54	-184.51
W0083	40.45.280	112. .310	4231.00	979814.95	980247.67	-34.75	-178.86	.63	-178.23
W0084	40.45.280	112. 1.450	4233.00	979823.08	980247.67	-26.43	-170.61	.41	-170.20
W0085	40.46.280	112. 5.060	4219.00	979825.88	980249.16	-26.44	-170.14	.29	-169.85
W0086	40.46.280	112. 6.000	4213.00	979824.73	980249.16	-28.16	-171.65	.32	-171.33
W0087	40.46.280	112. 8.920	4214.00	979830.79	980249.16	-22.00	-165.53	.31	-165.22
W0088	40.45.860	112. 9.540	4215.00	979831.76	980248.53	-20.31	-163.87	.39	-163.48
W0089	40.46.430	112.10.310	4212.00	979835.34	980249.38	-17.86	-161.32	.30	-161.02
W0090	40.45.740	112. 8.320	4214.00	979828.76	980248.36	-23.23	-166.76	.42	-166.34
W0091	40.45.040	111.50.810	4618.00	979784.01	980247.32	-28.94	-186.23	2.21	-184.02
W0092	40.45.080	111.48.710	4914.00	979769.36	980247.37	-15.80	-183.17	4.24	-178.93
W0093	40.46.040	111.45.880	5328.00	979741.32	980248.80	-6.33	-187.80	6.68	-181.12
W0100	40.43.340	111.53.880	4240.00	979792.88	980244.79	-53.10	-197.51	1.21	-196.30
W0101	40.43.540	111.55.360	4230.00	979794.48	980245.09	-52.74	-196.81	.92	-195.89
W0102	40.43.550	111.56.280	4239.00	979795.55	980245.10	-50.73	-195.11	.78	-194.33
W0103	40.43.540	111.57.450	4238.00	979798.85	980245.09	-47.61	-191.96	.66	-191.30
W0104	40.43.540	111.59.180	4245.00	979804.95	980245.09	-40.86	-185.44	.54	-184.90
W0105	40.43.540	112. .090	4241.00	979809.98	980245.09	-36.20	-180.65	.54	-180.11
W0106	40.43.540	112. 1.450	4241.00	979816.02	980245.09	-30.16	-174.61	.48	-174.13
W0107	40.43.360	112. 3.760	4229.00	979819.71	980244.82	-27.33	-171.37	.61	-170.76
W0108	40.43.610	112. 4.900	4227.00	979820.54	980245.19	-27.06	-171.03	.66	-170.37
W0109	40.43.100	112. 6.610	4238.00	979823.85	980244.43	-21.95	-166.30	1.39	-164.91
W0110	40.43.190	112. 8.950	4337.00	979822.17	980244.56	-14.45	-162.17	2.90	-159.27
W0111	40.43.600	112. 9.690	4240.00	979831.04	980245.17	-15.32	-159.73	2.29	-157.44
W0112	40.43.580	112.11.060	4248.00	979831.63	980245.14	-13.94	-158.63	2.98	-155.65
W0113	40.43.320	112.13.630	4224.00	979829.38	980244.76	-18.07	-161.94	3.01	-158.93
W0114	40.42.700	112.14.640	4243.00	979827.72	980243.84	-17.02	-161.54	4.20	-157.34
W0115	40.43.340	111.52.730	4276.00	979792.56	980244.79	-50.03	-195.67	1.50	-194.17
W0116	40.43.100	111.51.170	4415.00	979787.68	980244.43	-41.48	-191.85	1.98	-189.87
W0117	40.43.520	111.50.020	4506.00	979784.38	980245.06	-36.85	-190.32	2.65	-187.67
W0118	40.43.510	111.49.430	4618.00	979781.96	980245.04	-28.71	-186.00	3.06	-182.94

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE FOUQUER	T.C.	COMPLETE FOUQUER
W0119	40.42.850	111.48.320	4873.00	979767.66	980244.06	-18.05	-184.02	4.18	-179.84
W0120	40.43.740	111.48.880	4830.00	979772.40	980245.38	-18.67	-183.18	3.66	-179.52
W0121	40.44.580	111.49.230	4809.00	979774.27	980246.63	-20.03	-183.82	2.97	-180.85
W0122	40.44.870	111.48.310	5103.00	979756.62	980247.06	-10.45	-184.26	3.79	-180.47
W0123	40.42.570	111.47.860	4719.00	979774.12	980243.64	-25.65	-186.38	7.56	-178.82
W0124	40.42.800	111.47.200	4914.00	979757.27	980243.98	-24.50	-191.87	10.39	-181.48
W0125	40.43.220	111.46.620	4970.00	979750.76	980244.61	-26.37	-195.65	15.31	-180.34
W0126	40.41.990	111.52.570	4261.00	979791.29	980242.78	-50.70	-195.83	1.58	-194.25
W0127	40.42.000	111.51.180	4391.00	979786.87	980242.80	-42.91	-192.47	1.99	-190.48
W0128	40.41.990	111.50.000	4531.00	979782.43	980242.78	-34.16	-188.49	2.58	-185.91
W0129	40.41.990	111.48.860	4692.00	979774.17	980242.78	-27.28	-187.09	3.41	-183.68
W0130	40.41.980	111.47.650	4940.00	979759.90	980242.77	-18.21	-186.47	5.41	-181.06
W0131	40.41.340	111.47.430	4971.00	979753.93	980241.81	-20.31	-189.62	6.39	-183.23
W0133	40.41.220	111.54.630	4256.00	979790.18	980241.64	-51.14	-196.10	1.07	-195.03
W0134	40.42.240	111.56.290	4246.00	979793.00	980243.15	-50.77	-195.39	.79	-194.60
W0135	40.41.360	111.56.870	4258.00	979792.19	980241.84	-49.14	-194.17	.76	-193.41
W0136	40.41.770	111.59.180	4267.00	979800.99	980242.45	-40.11	-185.44	.62	-184.82
W0137	40.41.570	112. .310	4297.00	979803.60	980242.16	-34.38	-180.74	.62	-180.12
W0138	40.41.790	112. 1.460	4291.00	979807.42	980242.48	-31.45	-177.60	.64	-176.96
W0139	40.41.780	112. 2.600	4318.00	979807.57	980242.47	-28.75	-175.82	.70	-175.12
W0140	40.41.800	112. 3.760	4329.00	979807.77	980242.50	-27.54	-174.99	.87	-174.12
W0141	40.41.780	112. 5.450	4410.00	979806.32	980242.47	-21.35	-171.55	1.30	-170.25
W0142	40.42.210	112. 6.570	4369.00	979814.14	980243.11	-18.02	-166.83	2.05	-164.78
W0173	40.41.610	112. 7.850	4964.00	979776.61	980242.22	1.30	-167.77	3.01	-164.76
W0993	40.42.750	111.53.770	4242.00	979754.27	980243.91	-90.64	-235.12	1.23	-233.89*
W0994	40.44.490	111.51.180	4473.00	979789.90	980246.50	-35.87	-188.22	2.08	-186.14
W0995	40.44.010	111.51.180	4420.00	979789.99	980245.78	-40.04	-190.59	2.04	-188.55
W0996	40.44.020	111.50.140	4574.00	979782.98	980245.80	-32.59	-188.38	2.45	-185.93
W0997	40.44.270	111.49.800	4637.00	979732.09	980246.17	-27.92	-185.86	2.69	-183.17
W0998	40.42.760	111.50.000	4530.00	979784.18	980243.93	-33.66	-187.95	2.53	-185.42
W0999	40.42.670	111.48.860	4729.00	979773.33	980243.79	-25.65	-186.72	3.39	-183.33
W1000	40.40.940	111.46.900	5262.00	979732.00	980241.22	-14.28	-193.50	8.34	-185.16
W1001	40.41.220	111.48.280	4831.00	979762.63	980241.64	-24.61	-189.15	4.34	-184.81

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
W1002	40.41.230	111.48.850	4667.00	979772.89	980241.65	-29.78	-188.74	3.77	-184.97
W1003	40.41.220	111.49.430	4586.00	979777.65	980241.64	-32.63	-188.83	3.20	-185.63
W1004	40.40.980	111.50.010	4503.00	979731.23	980241.28	-36.50	-189.87	2.86	-187.01
W1005	40.40.910	111.51.190	4319.00	979788.63	980241.17	-46.29	-193.40	2.24	-191.16
W1006	40.41.230	111.52.230	4280.00	979789.23	980241.65	-49.84	-195.62	1.72	-193.90
W1014	40.42.760	111.51.890	4304.00	979754.94	980243.93	-84.16	-230.75	1.80	-228.95*
W1015	40.43.090	112. 4.890	4234.00	979820.02	980244.42	-26.15	-170.36	.79	-169.57
W1016	40.42.670	112. 5.460	4263.00	979818.33	980243.79	-23.98	-169.18	1.06	-168.12
W1017	40.42.660	112. 6.060	4261.00	979820.58	980243.73	-22.41	-167.54	1.35	-166.19
W1018	40.43.440	112.12.110	4236.00	979830.98	980244.94	-15.52	-159.80	4.15	-155.65
W1019	40.43.840	112.12.370	4212.00	979829.42	980245.53	-19.93	-163.39	1.99	-161.40
W1020	40.44.140	112.12.650	4209.00	979824.40	980245.98	-25.68	-169.04	1.35	-167.69
W1021	40.44.710	112.10.910	4211.00	979830.20	980246.82	-20.53	-163.96	.90	-163.06
W1022	40.44.120	112.10.260	4252.00	979829.22	980245.95	-16.79	-161.61	1.33	-160.28
W1023	40.44.990	112. 8.440	4296.00	979823.27	980247.24	-19.89	-166.21	.55	-165.66
W1024	40.44.580	112. 5.030	4278.00	979817.83	980246.63	-26.41	-172.12	.43	-171.69
W1025	40.44.280	112. 5.240	4283.00	979818.38	980246.19	-24.95	-170.83	.50	-170.33
W1026	40.43.160	112. 5.270	4286.00	979816.32	980244.52	-25.06	-171.04	.76	-170.28*
W1027	40.43.180	112. 7.140	4303.00	979821.42	980244.55	-18.39	-164.95	1.40	-163.55
W1028	40.43.730	112. 4.190	4226.00	979819.91	980245.37	-27.96	-171.90	.56	-171.34
W1029	40.43.850	112. 3.710	4223.00	979819.36	980245.55	-28.47	-172.31	.54	-171.77
W1030	40.44.320	112. 3.810	4222.00	979820.52	980246.24	-28.60	-172.40	.47	-171.93
W1031	40.44.530	112. 4.470	4223.00	979821.22	980246.56	-28.12	-171.96	.45	-171.51
W1032	40.44.430	112. 2.770	4228.00	979822.44	980246.41	-26.28	-170.29	.41	-169.88
W1033	40.44.420	112. 1.460	4232.00	979820.31	980246.39	-28.02	-172.16	.44	-171.72
W1034	40.44.420	112. .300	4239.00	979812.61	980246.39	-35.06	-179.44	.58	-178.86
W1035	40.46.290	112. 1.950	4228.00	979828.55	980249.17	-22.93	-166.94	.33	-166.61
W1036	40.46.280	112. 6.890	4213.00	979824.38	980249.16	-28.51	-172.00	.33	-171.67
W1037	40.45.440	112.10.030	4215.00	979832.60	980247.91	-18.85	-162.41	.50	-161.91
W1038	40.45.770	111.51.710	4406.00	979798.29	980248.40	-35.68	-185.75	2.45	-183.30
W1039	40.46.030	111.51.370	4514.00	979794.34	980248.79	-29.86	-183.61	2.71	-180.90
W1040	40.46.030	111.52.390	4365.00	979799.74	980248.79	-38.48	-187.15	2.25	-184.90
W1041	40.46.150	111.53.420	4327.00	979801.53	980248.97	-40.44	-187.82	1.72	-186.10

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE FOUGUER
W1042	40.46.290	111.54.950	4222.00	979803.01	980249.17	-49.04	-192.84	1.29	-191.55
W1043	40.46.300	111.56.170	4220.00	979802.39	980249.19	-49.87	-193.60	.92	-192.68
W1044	40.46.290	111.57.950	4220.00	979806.53	980249.17	-45.71	-189.44	.62	-183.82
W1045	40.47.470	111.56.320	4214.00	979809.06	980250.93	-45.50	-189.03	1.02	-188.01
W0481	40.47.480	111.42.700	5894.00	979697.00	980250.94	.45	-200.30	3.95	-196.35
RR1	40.43.390	112.13.660	4208.00	979830.03	980244.86	-19.03	-162.35	2.75	-159.60
RR2	40.43.120	112.14.080	4208.00	979829.66	980244.46	-19.00	-162.32	3.37	-158.95
RR3	40.42.860	112.14.510	4208.00	979830.39	980244.07	-17.88	-161.20	4.13	-157.07
BL2	40.43.530	112.14.100	4198.00	979825.73	980245.07	-24.48	-167.46	1.85	-165.61
H16	40.44.830	111.38.530	6666.00	979638.53	980247.00	18.63	-208.41	3.74	-204.67
H17	40.44.330	111.40.410	6133.00	979674.34	980246.26	4.95	-203.94	6.80	-197.14
H18	40.44.340	111.44.540	5316.00	979732.74	980246.27	-13.51	-194.57	8.51	-186.06
H50	40.41.950	111.43.320	5956.00	979681.26	980242.72	-1.24	-204.10	16.34	-187.76
H51	40.42.400	111.41.350	6634.00	979640.78	980243.39	21.38	-204.57	11.38	-193.19
W0025	40.50.520	111.55.730	4218.00	979819.41	980255.47	-39.31	-182.93	1.42	-181.56
W0026	40.50.320	111.57.270	4215.00	979827.04	980255.17	-31.67	-175.23	.81	-174.42
W0027	40.50.310	111.58.010	4216.00	979827.46	980255.15	-31.13	-174.73	.64	-174.09
W0028	40.50.750	111.58.860	4211.00	979831.39	980255.81	-28.03	-171.46	.51	-170.95
W0029	40.51.420	111.59.890	4211.00	979838.96	980256.81	-21.76	-165.19	.40	-164.79
W0030	40.52.050	111.58.700	4213.00	979833.57	980257.74	-27.90	-171.39	.53	-170.86
W0031	40.51.700	111.55.740	4231.00	979817.00	980257.22	-42.25	-186.36	1.23	-185.13
W0032	40.51.710	111.54.550	4283.00	979817.69	980257.24	-36.69	-182.57	1.77	-180.80
W0033	40.51.700	111.53.750	4380.00	979815.43	980257.22	-29.81	-178.99	2.25	-176.74
W0034	40.51.660	111.53.090	4531.00	979807.76	980257.16	-23.21	-177.54	2.68	-174.86
W0035	40.51.960	111.52.310	4669.00	979799.87	980257.61	-18.57	-177.60	3.31	-174.29
W0036	40.52.280	111.51.730	4804.00	979793.40	980258.09	-12.83	-176.45	3.64	-172.81
W0037	40.52.270	111.51.170	5035.00	979779.27	980258.07	-5.21	-176.70	4.01	-172.69
W0038	40.51.820	111.51.170	5196.00	979768.10	980257.40	-.56	-177.54	3.95	-173.59
W0039	40.50.510	111.54.290	4421.00	979809.06	980255.45	-30.55	-181.13	2.44	-178.69
W0041	40.51.590	112. 2.340	4205.00	979857.54	980257.06	-4.00	-147.22	.20	-147.02 *
W0043	40.48.040	111.42.320	4819.00	979777.14	980251.78	-21.36	-185.50	35.57	-149.93
W0044	40.48.360	111.41.370	5032.00	979766.15	980252.25	-12.79	-184.18	33.92	-150.26
W0045	40.48.800	111.40.080	5275.00	979752.96	980252.91	-3.78	-183.45	33.11	-150.34

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
W0046	40.49.230	111.38.710	5591.00	979733.37	980253.55	5.71	-184.72	37.37	-147.35
W0047	40.49.010	111.56.140	4212.00	979815.68	980253.22	-41.36	-184.82	1.30	-183.52
W0050	40.48.340	111.57.170	4213.00	979814.99	980252.22	-40.96	-184.45	.82	-183.63
W0051	40.49.010	111.57.180	4216.00	979817.98	980253.22	-38.68	-182.28	.83	-181.45
W0052	40.49.660	111.57.180	4217.00	979821.88	980254.19	-35.66	-179.29	.83	-178.46
W0053	40.51.420	112. 1.820	4205.00	979852.72	980256.81	-8.57	-151.79	.24	-151.55
W0054	40.50.880	112. .910	4205.00	979846.23	980256.00	-14.25	-157.47	.31	-157.16
W0055	40.50.210	112. .190	4205.00	979840.65	980255.01	-18.84	-162.06	.37	-161.69
W0056	40.51.060	111.58.250	4214.00	979830.35	980256.27	-29.05	-172.58	.60	-171.98
W0057	40.48.780	111.59.190	4216.00	979825.17	980252.88	-31.15	-174.75	.48	-174.27
W0059	40.48.300	112. 2.960	4213.00	979839.35	980252.16	-16.54	-160.03	.23	-159.80
W0060	40.48.760	112. 2.910	4213.00	979840.77	980252.85	-15.33	-159.00	.22	-158.73
W0061	40.49.570	112. 6.880	4214.00	979833.54	980254.05	-24.14	-167.67	.08	-167.59
W0062	40.48.580	112. 2.420	4217.00	979839.39	980252.58	-16.54	-160.17	.24	-159.93
W0063	40.50.810	112. 1.750	4212.00	979845.73	980255.90	-13.99	-157.45	.25	-157.20
W0064	40.49.000	112. 6.040	4208.00	979830.88	980253.21	-26.53	-169.85	.13	-169.72
W0071	40.48.120	111.58.020	4222.00	979816.17	980251.90	-38.61	-182.41	.62	-181.79
W0094	40.49.870	112. 2.080	4214.00	979844.02	980254.50	-14.11	-157.64	.24	-157.40
W0095	40.49.610	112. 1.080	4217.00	979839.58	980254.11	-17.88	-161.51	.31	-161.20
W0096	40.49.500	112. 4.260	4213.00	979842.86	980253.95	-14.82	-158.31	.15	-158.16
W0097	40.50.880	112. 3.920	4210.00	979848.55	980256.00	-11.46	-154.85	.14	-154.71
W0098	40.51.120	112. 8.820	4205.00	979849.42	980256.36	-11.42	-154.64	.02	-154.62
W0099	40.50.500	112. 8.030	4205.00	979843.58	980255.44	-16.34	-159.56	.04	-159.52
W0174	40.47.900	112. 6.020	4216.00	979826.09	980251.57	-28.92	-172.52	.18	-172.34
W0175	40.47.900	112. 4.890	4218.00	979834.28	980251.57	-20.54	-164.21	.19	-164.02
W0472	40.51.710	112.10.380	4218.00	979862.74	980257.24	2.25	-141.42	.55	-140.87
W0480	40.50.890	112.10.280	4207.00	979860.49	980256.02	.18	-143.11	.07	-143.04
W1046	40.47.900	111.55.730	4215.00	979810.33	980251.57	-44.48	-188.04	1.39	-186.65
W1047	40.50.900	111.55.730	4225.00	979818.47	980256.03	-40.16	-184.06	1.34	-182.72
W1048	40.50.700	112. .060	4212.00	979837.04	980255.73	-22.51	-165.97	.38	-165.59
W0482	40.48.640	111.43.350	6538.00	979663.69	980252.67	25.98	-196.70	5.42	-191.28
A1	40.51.670	112.10.110	4200.00	979862.70	980257.18	.57	-142.48	.29	-142.19
A2	40.51.610	112. 9.870	4200.00	979860.20	980257.09	-1.84	-144.89	.13	-144.76

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
MFE42	40.35.840	112.10.520	8470.00	979520.82	980233.63	83.87	-204.69	21.62	-183.07
MBE43	40.35.550	112. 4.530	5271.00	979711.37	980233.21	-25.75	-205.33	1.35	-203.98

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE POUGUER	T.C.	COMPLETE FOUGUER
A3	40.51.550	112. 9.640	4200.00	979857.62	980257.00	-4.33	-147.38	.08	-147.30
A4	40.51.470	112. 9.400	4200.00	979855.47	980256.88	-6.36	-149.41	.05	-149.36
A5	40.51.380	112. 9.180	4200.00	979853.17	980256.75	-8.53	-151.58	.04	-151.54
A6	40.51.230	112. 8.920	4200.00	979851.95	980256.52	-9.52	-152.57	.03	-152.54
A7	40.51.130	112. 8.650	4200.00	979850.29	980256.37	-11.03	-154.08	.03	-154.05
A8	40.50.890	112. 8.400	4200.00	979847.65	980256.02	-13.32	-156.37	.03	-156.34
A9	40.50.710	112. 8.180	4200.00	979846.18	980255.75	-14.52	-157.57	.04	-157.53
A10	40.50.510	112. 7.990	4200.00	979844.92	980255.45	-15.48	-158.53	.04	-158.49
A11	40.50.320	112. 7.800	4200.00	979842.44	980255.17	-17.68	-160.73	.07	-160.66
A12	40.50.150	112. 7.630	4200.00	979841.06	980254.92	-18.81	-161.86	.07	-161.79
A13	40.50.860	112.10.460	4200.00	979864.87	980255.97	3.95	-139.10	.07	-139.03
A14	40.50.710	112. 7.750	4200.00	979850.06	980255.75	-.64	-143.69	.06	-143.63*
A15	40.50.580	112.10.030	4200.00	979858.45	980255.56	-2.06	-145.11	.03	-145.08
A16	40.50.450	112. 8.830	4200.00	979856.53	980255.36	-3.78	-146.83	.04	-146.79
A17	40.50.320	112. 9.620	4200.00	979858.52	980255.17	-1.60	-144.65	.04	-144.61
A18	40.50.210	112. 9.440	4200.00	979852.99	980255.01	-6.97	-150.02	.05	-149.97
A19	40.50.060	112. 9.200	4200.00	979855.84	980254.78	-3.89	-146.94	.06	-146.88
A20	40.49.920	112. 9.000	4200.00	979850.00	980254.57	-9.52	-152.57	.06	-152.51
A21	40.49.790	112. 8.790	4200.00	979849.85	980254.38	-9.48	-152.53	.07	-152.46
A22	40.49.650	112. 8.600	4200.00	979848.20	980254.17	-10.92	-153.97	.07	-153.90
A23	40.49.530	112. 8.410	4200.00	979848.02	980253.99	-10.92	-153.97	.07	-153.90
A24	40.49.420	112. 8.210	4200.00	979846.54	980253.83	-12.14	-155.19	.07	-155.12
A25	40.49.310	112. 7.990	4200.00	979845.16	980253.67	-13.46	-156.51	.09	-156.42
A26	40.49.410	112. 8.960	4200.00	979846.63	980253.82	-12.14	-155.19	.07	-155.12
A27	40.49.620	112. 9.060	4200.00	979848.77	980254.13	-10.31	-153.36	.07	-153.29
A28	40.49.750	112. 9.240	4200.00	979850.23	980254.32	-9.04	-152.09	.07	-152.02
A29	40.50.050	112. 9.570	4200.00	979854.26	980254.77	-5.46	-148.51	.05	-148.46
A30	40.50.370	112.10.180	4200.00	979859.93	980255.24	-.26	-143.31	.04	-143.27
A31	40.50.510	112.10.470	4200.00	979861.18	980255.45	.78	-142.27	.04	-142.23
A32	40.50.650	112.10.400	4200.00	979861.36	980255.66	.75	-142.30	.04	-142.26
A33	40.50.790	112.10.920	4200.00	979861.57	980255.87	.85	-142.20	.07	-142.13
A34	40.50.780	112.10.210	4200.00	979861.82	980255.85	1.02	-142.03	.05	-141.98
A35	40.50.730	112. 9.990	4200.00	979860.16	980255.78	-.57	-143.62	.04	-143.58

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A36	40.50.990	112.11.120	4200.00	979858.88	980256.17	-2.24	-145.29	.13	-145.16
A71	40.52.270	112. 7.450	4200.00	979839.45	980258.07	-23.57	-166.62	.03	-166.59
A72	40.52.050	112. 6.970	4200.00	979839.75	980257.74	-22.94	-165.99	.04	-165.95
A73	40.51.800	112. 6.450	4200.00	979839.81	980257.37	-22.51	-165.56	.05	-165.51
A74	40.51.570	112. 5.980	4200.00	979841.68	980257.03	-20.30	-163.35	.06	-163.29
A75	40.51.720	112. 5.380	4200.00	979847.09	980257.25	-15.11	-158.16	.08	-158.03
A76	40.51.910	112. 2.860	4200.00	979852.70	980257.53	-9.78	-152.83	.17	-152.66
A77	40.52.120	112. 4.350	4200.00	979853.50	980257.85	-9.30	-152.35	.10	-152.25
A78	40.51.370	112. 6.380	4200.00	979833.95	980256.73	-22.73	-165.78	.05	-165.73
A79	40.51.100	112. 6.880	4200.00	979838.39	980256.33	-22.89	-165.94	.05	-165.89
A80	40.50.840	112. 7.320	4200.00	979839.39	980255.94	-21.20	-164.25	.06	-164.19
A81	40.50.500	112. 7.680	4200.00	979841.51	980255.44	-18.88	-161.93	.05	-161.88
A98	40.51.340	112.10.380	4223.00	979864.54	980256.69	5.07	-138.77	.21	-138.56
A99	40.52.450	112.10.340	4232.00	979861.29	980258.34	1.01	-143.13	.72	-142.41
A111	40.51.730	112.10.400	4222.00	979861.86	980257.27	1.71	-142.09	.61	-141.43
A151	40.51.340	112.10.380	4240.00	979864.34	980256.69	6.46	-137.95	.17	-137.78
A152	40.52.450	112.10.340	4230.00	979861.29	980258.34	.82	-143.25	.73	-142.52
A197	40.51.670	112.10.110	4200.00	979862.83	980257.18	.70	-142.35	.29	-142.06
A198	40.51.610	112. 9.870	4200.00	979860.34	980257.09	-1.70	-144.75	.13	-144.62
A199	40.51.550	112. 9.640	4200.00	979857.76	980257.00	-4.19	-147.24	.08	-147.16
A200	40.51.470	112. 9.400	4200.00	979855.60	980256.88	-6.23	-149.28	.05	-149.23
A201	40.51.380	112. 9.180	4200.00	979853.33	980256.75	-8.37	-151.42	.04	-151.38
A202	40.51.230	112. 8.920	4200.00	979852.05	980256.52	-9.42	-152.47	.03	-152.44
A203	40.51.130	112. 8.650	4200.00	979850.43	980256.37	-10.89	-153.94	.03	-153.91
A204	40.50.890	112. 8.400	4200.00	979847.94	980256.02	-13.03	-156.08	.03	-156.05
A205	40.50.710	112. 8.180	4200.00	979846.33	980255.75	-14.37	-157.42	.04	-157.38
A206	40.50.510	112. 7.990	4200.00	979845.07	980255.45	-15.33	-158.38	.04	-158.34
A207	40.50.320	112. 7.800	4200.00	979842.72	980255.17	-17.40	-160.45	.07	-160.38
A208	40.50.150	112. 7.630	4200.00	979841.13	980254.92	-18.74	-161.79	.07	-161.72
A209	40.50.860	112.10.460	4200.00	979864.90	980255.97	3.98	-139.07	.07	-139.00
A210	40.50.710	112. 7.750	4200.00	979861.86	980255.75	1.16	-141.89	.06	-141.83
A211	40.50.580	112.10.030	4200.00	979859.87	980255.56	-.64	-143.69	.03	-143.66
A212	40.50.450	112. 8.830	4200.00	979858.25	980255.36	-2.06	-145.11	.04	-145.07

STAT.	LATITUDE	LONGITUDE	ELEV.	OPSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A213	40.50.320	112. 9.620	4200.00	979856.34	980255.17	-3.78	-146.83	.04	-146.79
A214	40.50.210	112. 9.440	4200.00	979858.36	980255.01	-1.60	-144.65	.05	-144.60
A215	40.50.060	112. 9.200	4200.00	979852.76	980254.78	-6.97	-150.02	.06	-149.93
A216	40.49.920	112. 9.000	4200.00	979855.63	980254.57	-3.89	-146.94	.06	-146.88
A217	40.49.790	112. 8.790	4200.00	979849.87	980254.38	-9.46	-152.51	.07	-152.44
A218	40.49.650	112. 8.600	4200.00	979843.14	980254.17	-10.98	-154.03	.07	-153.96
A219	40.49.530	112. 8.410	4200.00	979846.32	980253.99	-12.62	-155.67	.07	-155.60
A220	40.49.420	112. 8.210	4200.00	979844.94	980253.83	-13.84	-156.89	.07	-156.82
A221	40.49.310	112. 7.990	4200.00	979843.46	980253.67	-15.16	-158.21	.09	-158.12
A256	40.52.270	112. 7.450	4200.00	979840.15	980258.07	-22.87	-165.92	.03	-165.89
A257	40.52.050	112. 6.970	4200.00	979839.55	980257.74	-23.14	-166.19	.04	-166.15
A258	40.51.800	112. 6.450	4200.00	979839.61	980257.37	-22.71	-165.76	.05	-165.71
A259	40.51.570	112. 5.980	4200.00	979841.48	980257.03	-20.50	-163.55	.06	-163.49
A260	40.51.720	112. 5.380	4200.00	979846.99	980257.25	-15.21	-158.26	.08	-158.13
A261	40.51.910	112. 2.860	4200.00	979852.50	980257.53	-9.98	-153.03	.17	-152.86
A262	40.52.120	112. 4.350	4200.00	979853.30	980257.85	-9.50	-152.55	.10	-152.45
A263	40.51.370	112. 7.380	4200.00	979838.85	980256.73	-22.83	-165.88	.04	-165.84
A264	40.51.100	112. 6.880	4200.00	979833.09	980256.33	-23.19	-166.24	.05	-166.19
A265	40.50.840	112. 7.320	4200.00	979839.69	980255.94	-21.20	-164.25	.06	-164.19
A266	40.50.500	112. 7.710	4200.00	979841.51	980255.44	-18.88	-161.93	.05	-161.88
MB	40.51.720	112.10.350	4205.00	979864.44	980257.25	2.71	-140.51	.57	-139.94
BL44	40.50.150	112. .110	4196.00	979819.13	980254.92	-41.11	-184.03	.38	-183.65*
P0101	40.32.231	111.53.444	4446.97	979747.06	980228.27	-62.93	-214.43	1.80	-212.64
P0102	40.32.240	111.53.222	4441.66	979748.37	980228.29	-62.14	-213.46	1.92	-211.54
P0103	40.32.242	111.53.009	4445.12	979748.99	980228.29	-61.19	-212.63	2.05	-210.58
P0104	40.32.229	111.52.800	4456.65	979749.11	980228.27	-59.97	-211.81	2.16	-209.65
P0105	40.32.231	111.52.580	4468.87	979747.14	980228.27	-60.79	-213.04	2.29	-210.75
P0106	40.32.227	111.52.376	4475.75	979746.99	980228.27	-60.29	-212.78	2.44	-210.34
P0107	40.32.215	111.52.162	4476.19	979747.24	980228.26	-59.99	-212.49	2.66	-209.83
P0108	40.32.211	111.51.936	4491.21	979746.42	980228.24	-59.38	-212.39	2.95	-209.54
P0109	40.32.218	111.51.727	4558.05	979741.96	980228.26	-57.57	-212.86	2.83	-210.03
P0110	40.32.217	111.51.525	4618.57	979737.76	980228.26	-56.07	-213.42	2.95	-210.48
P0111	40.32.216	111.51.291	4704.61	979732.06	980228.26	-53.68	-213.96	3.35	-210.61

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
P0112	40.32.217	111.51.069	4763.71	979728.37	980228.26	-51.81	-214.11	3.76	-210.35
P0113	40.32.219	111.50.855	4762.98	979728.21	980228.26	-52.04	-214.31	3.97	-210.34
P0114	40.32.222	111.50.631	4736.31	979729.96	980228.26	-52.80	-214.16	4.24	-209.92
P0115	40.32.220	111.50.421	4657.02	979735.48	980228.26	-54.74	-213.40	4.85	-208.55
P0116	40.32.226	111.50.210	4679.43	979734.02	980228.27	-54.11	-213.53	5.40	-208.13
P0117	40.32.223	111.49.994	4718.94	979731.46	980228.26	-52.93	-213.70	6.08	-207.62
P0118	40.32.221	111.49.770	4773.24	979728.04	980228.26	-51.25	-213.87	6.81	-207.06
P0119	40.32.217	111.49.559	4811.10	979725.55	980228.26	-50.18	-214.08	7.87	-206.22
P0120	40.32.215	111.49.351	4864.05	979722.14	980228.26	-48.61	-214.32	9.08	-205.24
P0121	40.32.214	111.49.127	4946.39	979716.88	980228.24	-46.11	-214.62	10.68	-203.94
P0122	40.32.218	111.48.874	5089.20	979707.68	980228.26	-41.89	-215.27	12.53	-202.74
P0123	40.32.215	111.48.708	5196.98	979700.04	980228.26	-39.39	-216.45	13.47	-202.98
P0201	40.31.557	111.49.719	4859.34	979723.75	980227.27	-46.45	-212.00	10.04	-201.96
P0202	40.31.565	111.49.927	4728.11	979732.08	980227.28	-50.47	-211.56	8.86	-202.70
P0203	40.31.541	111.50.173	4653.09	979736.30	980227.25	-52.78	-211.31	7.31	-204.00
P0204	40.31.542	111.50.366	4614.53	979738.95	980227.25	-54.26	-211.47	6.32	-205.15
P0205	40.31.562	111.50.604	4577.84	979740.76	980227.28	-55.93	-211.89	5.38	-206.51
P0206	40.31.546	111.50.792	4578.31	979740.02	980227.25	-56.59	-212.57	4.72	-207.85
P0207	40.31.574	111.51.021	4648.95	979734.54	980227.30	-55.48	-213.86	3.90	-209.96
P0208	40.31.587	111.51.240	4553.72	979740.87	980227.32	-58.13	-213.27	3.73	-209.54
P0209	40.31.588	111.51.456	4551.68	979740.89	980227.32	-58.30	-213.37	3.35	-210.02
P0210	40.31.609	111.51.636	4553.55	979740.53	980227.35	-58.51	-213.65	3.09	-210.56
P0211	40.31.625	111.51.851	4502.95	979743.71	980227.37	-60.11	-213.52	3.03	-210.49
P0212	40.31.607	111.52.061	4479.99	979744.99	980227.35	-60.97	-213.60	2.85	-210.75
P0213	40.31.604	111.52.297	4463.05	979745.91	980227.34	-61.63	-213.68	2.71	-210.97
P0214	40.31.609	111.52.509	4449.67	979746.61	980227.35	-62.21	-213.80	2.52	-211.28
P0215	40.31.608	111.52.721	4439.61	979747.49	980227.35	-62.27	-213.52	2.33	-211.15
P0216	40.31.610	111.52.995	4430.99	979748.65	980227.35	-61.92	-212.88	2.16	-210.72
P0217	40.31.623	111.53.847	4413.56	979750.60	980227.37	-61.63	-211.99	1.71	-210.28
P0218	40.31.596	111.54.749	4353.41	979753.70	980227.32	-64.14	-212.45	1.53	-210.92
P0219	40.31.412	111.55.278	4343.98	979753.72	980227.06	-64.75	-212.74	1.49	-211.25
P0220	40.31.362	111.55.865	4412.86	979749.45	980226.98	-62.46	-212.80	1.24	-211.56
P0221	40.31.342	111.56.588	4452.32	979746.88	980226.96	-61.30	-212.98	1.16	-211.82

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE POUGUER
P0222	40.31.343	111.57.288	4502.08	979743.70	980226.96	-59.80	-213.18	1.08	-212.10
P0301	40.31.265	111.52.417	4455.47	979745.32	980226.84	-62.44	-214.24	2.66	-211.58
P0302	40.31.167	111.52.258	4461.47	979744.60	980226.70	-62.45	-214.45	2.35	-211.60
P0303	40.31.076	111.52.067	4466.86	979744.81	980226.55	-61.59	-213.77	3.00	-210.77
P0304	40.30.953	111.51.887	4478.61	979744.31	980226.37	-60.81	-213.39	3.23	-210.16
P0305	40.30.853	111.51.721	4487.65	979744.26	980226.23	-59.86	-212.75	3.51	-209.24
P0306	40.30.769	111.51.569	4503.96	979743.82	980226.10	-58.64	-212.08	3.66	-208.42
P0307	40.30.680	111.51.382	4523.47	979743.30	980225.97	-57.19	-211.30	3.94	-207.36
P0308	40.30.590	111.51.167	4551.43	979742.29	980225.84	-55.44	-210.50	4.31	-206.19
P0309	40.30.482	111.50.983	4576.12	979741.24	980225.68	-54.01	-209.91	4.84	-205.07
P0310	40.30.383	111.50.821	4621.63	979739.27	980225.53	-51.55	-209.00	5.30	-203.70
P0311	40.30.295	111.50.662	4703.71	979734.34	980225.40	-48.13	-208.38	5.49	-202.89
P0312	40.30.175	111.50.483	4777.23	979730.86	980225.23	-45.02	-207.78	6.12	-201.66
P0313	40.30.244	111.50.200	4993.39	979717.88	980225.33	-37.77	-207.89	6.38	-201.51
P0401	40.31.366	111.52.882	4436.66	979747.16	980226.98	-62.51	-213.67	2.28	-211.39
P0402	40.31.245	111.52.762	4440.17	979746.44	980226.81	-62.73	-214.00	2.42	-211.58
P0403	40.31.082	111.52.667	4449.69	979745.26	980226.56	-62.76	-214.36	2.45	-211.91
P0404	40.30.942	111.52.542	4450.03	979744.94	980226.36	-62.84	-214.45	2.58	-211.87
P0405	40.30.801	111.52.430	4449.47	979744.86	980226.14	-62.76	-214.35	2.77	-211.58
P0406	40.30.648	111.52.338	4454.07	979744.62	980225.92	-62.35	-214.10	2.90	-211.20
P0407	40.30.489	111.52.237	4459.56	979744.50	980225.69	-61.72	-213.65	3.08	-210.57
P0408	40.30.344	111.52.132	4473.06	979744.23	980225.47	-60.50	-212.90	3.22	-209.67
P0409	40.30.228	111.52.048	4488.63	979743.79	980225.30	-59.31	-212.23	3.36	-208.87
P0410	40.30.116	111.51.980	4529.88	979741.57	980225.14	-57.49	-211.82	3.31	-208.51
P0411	40.29.930	111.51.866	4591.76	979738.20	980224.86	-54.76	-211.19	3.61	-207.58
P0412	40.29.775	111.51.768	4689.84	979733.05	980224.62	-50.45	-210.23	3.47	-206.76
P0413	40.29.639	111.51.649	4772.21	979729.09	980224.42	-46.46	-209.04	3.63	-205.41
P0414	40.29.475	111.51.579	4901.24	979721.88	980224.17	-41.28	-208.26	3.88	-204.38
P0415	40.29.346	111.51.468	5081.90	979709.88	980223.98	-36.10	-209.24	3.55	-205.69
P0416	40.29.190	111.51.369	5306.10	979695.26	980223.75	-29.40	-210.17	3.42	-206.75
P0417	40.29.064	111.51.307	5397.96	979689.81	980223.56	-26.02	-209.92	3.72	-206.20
P0501	40.28.791	111.51.774	5583.96	979678.41	980223.16	-19.52	-209.76	3.28	-206.48
P0502	40.28.907	111.51.815	5227.31	979701.15	980223.33	-30.50	-208.59	4.98	-203.61

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
P0503	40.29.185	111.52.055	5123.05	979707.67	980223.75	-34.21	-208.74	3.29	-205.45
P0504	40.29.052	111.51.954	4977.07	979716.94	980223.55	-38.46	-208.03	4.53	-203.50
P0505	40.29.335	111.52.170	4885.11	979722.50	980223.97	-41.97	-208.41	3.19	-205.22
P0506	40.29.471	111.52.251	4759.81	979729.35	980224.17	-47.11	-209.28	3.53	-205.75
P0507	40.29.608	111.52.382	4654.23	979734.50	980224.38	-52.01	-210.57	3.04	-207.53
P0508	40.29.752	111.52.484	4560.18	979740.09	980224.59	-55.57	-210.93	3.05	-207.88
P0509	40.29.902	111.52.615	4494.03	979743.73	980224.82	-58.38	-211.49	2.98	-208.51
P0510	40.30.022	111.52.739	4468.37	979744.77	980224.99	-59.93	-212.16	2.79	-209.37
P0511	40.30.180	111.52.841	4451.90	979745.28	980225.23	-61.20	-212.87	2.62	-210.25
P0512	40.30.338	111.52.941	4438.73	979745.84	980225.46	-62.11	-213.34	2.48	-210.86
P0513	40.30.466	111.53.060	4431.92	979746.20	980225.65	-62.58	-213.57	2.33	-211.24
P0514	40.30.604	111.53.171	4431.65	979746.57	980225.85	-62.44	-213.42	2.21	-211.21
P0515	40.30.759	111.53.288	4429.80	979747.18	980226.09	-62.24	-213.16	2.11	-211.05
P0516	40.30.894	111.53.389	4426.38	979747.93	980226.29	-62.01	-212.82	2.01	-210.81
P0517	40.31.038	111.53.505	4422.51	979748.71	980226.51	-61.82	-212.49	1.92	-210.57
P0518	40.31.193	111.53.607	4417.33	979749.42	980226.73	-61.81	-212.31	1.86	-210.45
P0519	40.31.344	111.53.699	4413.53	979750.04	980226.96	-61.78	-212.15	1.80	-210.35
P0601	40.31.099	111.54.413	4409.48	979750.74	980226.59	-61.19	-211.39	1.56	-209.83
P0602	40.30.952	111.54.306	4413.65	979750.59	980226.37	-60.64	-211.00	1.60	-209.41
P0603	40.30.818	111.54.179	4414.35	979750.49	980226.17	-60.47	-210.86	1.66	-209.20
P0604	40.30.671	111.54.093	4413.93	979750.38	980225.95	-60.40	-210.78	1.71	-209.07
P0605	40.30.556	111.53.964	4422.37	979749.44	980225.78	-60.37	-211.04	1.76	-209.28
P0606	40.30.415	111.53.866	4404.78	979749.85	980225.58	-61.41	-211.48	1.89	-209.59
P0607	40.30.266	111.53.746	4420.60	979748.76	980225.36	-60.80	-211.40	1.94	-209.46
P0608	40.30.135	111.53.638	4424.00	979748.31	980225.15	-60.72	-211.44	2.05	-209.39
P0609	40.29.997	111.53.539	4426.69	979747.90	980224.95	-60.67	-211.48	2.18	-209.30
P0610	40.29.847	111.53.376	4442.44	979746.94	980224.73	-59.93	-211.28	2.42	-208.86
P0611	40.29.706	111.53.278	4461.01	979746.50	980224.52	-58.42	-210.40	2.60	-207.80
P0612	40.29.545	111.53.150	4504.75	979744.39	980224.28	-56.17	-209.65	2.76	-206.89
P0613	40.29.404	111.53.036	4599.18	979739.14	980224.07	-52.33	-209.02	2.85	-206.17
P0614	40.29.285	111.52.935	4735.56	979732.48	980223.90	-45.99	-207.33	2.70	-204.63
P0615	40.29.135	111.52.842	4833.93	979727.07	980223.66	-41.91	-206.60	3.02	-203.58
P0616	40.29.006	111.52.717	4993.83	979717.16	980223.43	-36.60	-206.73	3.67	-203.06

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE POUGUER
P0617	40.28.849	111.52.609	5118.40	979709.37	980223.24	-32.43	-206.81	3.87	-202.94
P0618	40.28.530	111.52.375	5987.15	979652.25	980222.77	-7.37	-211.35	6.89	-204.46
P0619	40.28.453	111.52.300	5908.84	979659.32	980222.66	-7.55	-208.36	4.68	-204.13
P0702	40.30.610	111.54.684	4355.82	979754.79	980225.87	-61.37	-209.77	1.65	-208.12
P0703	40.30.479	111.54.547	4365.02	979753.90	980225.68	-61.21	-209.92	1.68	-208.24
P0704	40.30.332	111.54.412	4421.25	979750.11	980225.46	-59.49	-210.12	1.62	-208.50
P0705	40.30.173	111.54.352	4420.77	979750.15	980225.21	-59.24	-209.85	1.67	-208.18
P0706	40.30.024	111.54.231	4421.14	979750.01	980224.99	-59.13	-209.75	1.76	-207.99
P0707	40.29.040	111.53.496	4688.98	979738.15	980223.53	-44.34	-204.08	2.47	-201.61
P0708	40.28.895	111.53.379	4756.28	979734.97	980223.31	-40.97	-203.01	3.21	-199.80
P0709	40.28.757	111.53.269	4826.68	979729.95	980223.11	-39.16	-203.60	3.50	-200.02
P0710	40.28.617	111.53.151	5119.23	979711.38	980222.91	-30.01	-204.42	2.79	-201.63
P0711	40.28.371	111.52.913	6115.53	979642.00	980222.55	-5.32	-213.67	10.86	-202.81
P0712	40.28.272	111.52.800	5926.58	979764.73	980222.40	99.79	-102.13	6.35	-95.73*
P0812	40.27.980	111.53.419	5782.64	979669.69	980221.96	-8.36	-205.36	6.68	-198.68
P0811	40.28.159	111.53.543	5622.24	979680.50	980222.22	-12.89	-204.43	5.83	-198.60
P0810	40.28.339	111.53.636	5125.43	979713.06	980222.48	-27.33	-201.94	2.40	-199.55
P0809	40.28.554	111.53.776	4782.07	979735.48	980222.80	-37.52	-200.44	2.55	-197.89
P0808	40.28.682	111.53.893	4737.99	979738.36	980222.99	-38.98	-200.40	2.18	-198.22
P0807	40.28.814	111.54.013	4650.68	979743.58	980223.20	-42.17	-200.62	2.14	-198.48
P0806	40.29.816	111.54.759	4430.43	979749.97	980224.69	-57.99	-208.93	1.57	-207.36
P0805	40.29.954	111.54.871	4425.54	979750.12	980224.89	-58.50	-209.28	1.52	-207.76
P0804	40.30.100	111.54.960	4354.32	979754.71	980225.11	-60.83	-209.18	1.65	-207.53
P0803	40.30.245	111.55.080	4357.66	979754.11	980225.33	-61.34	-209.80	1.58	-208.22
P0802	40.30.382	111.55.153	4355.18	979753.67	980225.53	-62.21	-210.59	1.55	-209.04
P0801	40.30.520	111.55.280	4363.11	979752.80	980225.73	-62.54	-211.19	1.49	-209.70
P0912	40.27.800	111.53.941	5327.90	979701.00	980221.68	-19.54	-201.05	3.49	-197.56
P0911	40.28.070	111.54.179	5065.52	979717.18	980222.09	-28.45	-201.03	2.61	-198.42
P0910	40.28.211	111.54.185	4836.45	979732.42	980222.30	-34.96	-199.73	1.91	-197.82
P0909	40.28.365	111.54.327	4702.45	979743.01	980222.53	-37.21	-197.42	2.04	-195.33
P0908	40.28.512	111.54.446	4615.83	979746.61	980222.75	-41.97	-199.23	1.91	-197.32
P0907	40.28.637	111.54.565	4546.88	979749.79	980222.94	-45.47	-200.38	1.86	-198.52
P0906	40.29.594	111.55.308	4361.54	979753.97	980224.35	-60.14	-208.73	1.65	-207.03

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
P0905	40.29.709	111.55.394	4364.79	979753.46	980224.52	-60.51	-209.22	1.58	-207.64
P0904	40.29.854	111.55.496	4368.04	979753.06	980224.74	-60.82	-209.64	1.53	-208.11
P0903	40.29.997	111.55.614	4366.89	979753.57	980224.95	-60.63	-209.40	1.49	-207.91*
P0902	40.30.135	111.55.691	4440.77	979747.42	980225.15	-60.03	-211.32	1.32	-210.00
P0901	40.30.283	111.55.780	4437.52	979747.52	980225.38	-60.47	-211.65	1.30	-210.35
P1001	40.30.168	111.56.203	4448.62	979746.38	980225.21	-60.39	-211.95	1.24	-210.71
P1002	40.30.017	111.56.104	4449.59	979746.45	980224.98	-60.00	-211.59	1.27	-210.32
P1003	40.29.876	111.56.021	4433.66	979747.53	980224.77	-60.21	-211.26	1.31	-209.95
P1004	40.29.729	111.55.922	4392.43	979750.45	980224.55	-60.95	-210.60	1.42	-209.13
P1005	40.29.586	111.55.823	4384.29	979751.07	980224.34	-60.88	-210.25	1.47	-208.78
P1006	40.29.436	111.55.724	4374.14	979752.12	980224.12	-60.57	-209.59	1.55	-208.04
P1007	40.29.293	111.55.625	4378.59	979752.20	980223.91	-59.86	-209.04	1.58	-207.46
P1008	40.29.146	111.55.526	4462.54	979746.64	980223.70	-57.31	-209.34	1.45	-207.89
P1009	40.28.860	111.55.302	4494.48	979747.02	980223.26	-53.49	-206.61	1.49	-205.12
P1010	40.28.720	111.55.191	4493.80	979747.96	980223.05	-52.41	-205.51	1.55	-203.96
P1011	40.28.575	111.55.077	4498.70	979748.55	980222.84	-51.14	-204.40	1.62	-202.78
P1012	40.28.431	111.54.964	4521.29	979748.29	980222.63	-49.07	-203.11	1.72	-201.39
P1013	40.28.296	111.54.864	4593.82	979744.18	980222.43	-46.16	-202.66	1.65	-201.01
P1014	40.28.213	111.54.788	4617.26	979744.77	980222.30	-43.23	-200.53	1.57	-198.85
P1015	40.28.010	111.54.613	4758.16	979735.28	980222.00	-39.17	-201.27	1.66	-199.61
P1016	40.27.897	111.54.615	4856.70	979729.17	980221.83	-35.84	-201.30	1.72	-199.53
P1017	40.27.730	111.54.396	5077.41	979714.54	980221.58	-29.36	-202.34	2.47	-199.87
P1018	40.27.608	111.54.295	5126.83	979711.55	980221.41	-27.63	-202.29	2.62	-199.67
P1019	40.27.466	111.54.179	5143.23	979710.10	980221.19	-27.32	-202.54	2.96	-199.53
P1020	40.27.309	111.54.075	4849.49	979730.86	980220.95	-33.95	-199.17	1.58	-197.59
P1021	40.27.274	111.54.021	4828.20	979732.42	980220.91	-34.35	-198.85	1.67	-197.13
P1022	40.27.168	111.53.938	4813.72	979733.52	980220.75	-34.45	-198.45	1.70	-196.75
P1023	40.27.035	111.53.835	4803.02	979734.02	980220.55	-34.76	-198.39	1.76	-196.63
P1024	40.26.889	111.53.708	4822.95	979732.56	980220.34	-34.14	-198.45	1.70	-196.75
P1025	40.26.755	111.53.601	4868.89	979723.95	980220.14	-33.22	-199.10	1.71	-197.39
P1026	40.26.608	111.53.487	4859.37	979729.49	980219.92	-33.36	-198.91	1.63	-197.28
P1027	40.26.467	111.53.373	4830.95	979731.12	980219.72	-34.20	-198.78	1.61	-197.17
P1028	40.26.310	111.53.259	4788.74	979733.08	980219.43	-35.97	-199.12	1.55	-197.57

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
P1029	40.26.181	111.53.149	4765.53	979733.91	980219.30	-37.14	-199.50	1.51	-197.99
P1030	40.26.042	111.53.028	4741.94	979734.35	980219.09	-38.71	-200.26	1.51	-198.75
P1031	40.25.784	111.52.803	4678.95	979736.64	980218.71	-41.97	-201.38	1.46	-199.92
P1032	40.25.628	111.52.698	4663.63	979736.54	980218.48	-43.28	-202.16	1.41	-200.75
P1101	40.29.505	111.56.306	4441.02	979746.78	980224.22	-59.72	-211.02	1.34	-209.68
P1102	40.29.341	111.56.395	4446.61	979746.46	980223.97	-59.26	-210.75	1.36	-209.39
P1103	40.29.205	111.56.449	4473.75	979745.11	980223.78	-57.87	-210.29	1.34	-208.95
P1104	40.29.030	111.56.535	4496.96	979744.10	980223.52	-56.44	-209.65	1.36	-208.29
P1105	40.28.863	111.56.608	4519.87	979743.06	980223.27	-55.07	-209.06	1.37	-207.69
P1106	40.28.714	111.56.678	4558.50	979740.95	980223.05	-53.33	-208.64	1.37	-207.27
P1107	40.28.547	111.56.748	4589.90	979739.44	980222.80	-51.64	-208.01	1.41	-206.60
P1108	40.28.401	111.56.805	4620.92	979738.19	980222.59	-49.75	-207.18	1.42	-205.75
P1109	40.28.212	111.56.754	4632.23	979738.25	980222.30	-48.34	-206.16	1.48	-204.67
P1110	40.28.051	111.56.685	4631.53	979738.99	980222.06	-47.43	-205.22	1.60	-203.62
P1111	40.27.917	111.56.609	4632.70	979740.21	980221.86	-45.90	-203.73	1.78	-201.95
P1112	40.27.755	111.56.543	4634.96	979741.35	980221.62	-44.31	-202.22	1.90	-200.32
P1113	40.27.616	111.56.478	4638.01	979742.41	980221.42	-42.76	-200.77	1.96	-198.81
P1114	40.27.451	111.56.396	4660.60	979741.82	980221.17	-40.98	-199.76	2.10	-197.66
P1115	40.27.311	111.56.337	4684.46	979741.06	980220.97	-39.29	-198.88	2.15	-196.73
P1116	40.27.142	111.56.255	4702.86	979740.25	980220.70	-38.10	-198.32	2.03	-196.29
P1117	40.27.002	111.56.184	4721.60	979739.41	980220.50	-36.98	-197.84	1.96	-195.88
P1118	40.26.832	111.56.104	4741.42	979738.78	980220.26	-35.50	-197.03	1.98	-195.06
P1119	40.26.690	111.56.037	4758.79	979737.74	980220.04	-34.69	-196.81	1.86	-194.95
P1120	40.26.529	111.55.968	4768.96	979736.40	980219.80	-34.84	-197.31	1.65	-195.66
P1121	40.26.360	111.55.893	4772.55	979735.48	980219.57	-35.18	-197.78	1.58	-196.20
P1122	40.26.211	111.55.812	4786.15	979733.76	980219.34	-35.39	-198.45	1.45	-197.00
P1123	40.25.908	111.55.680	4837.15	979729.23	980218.90	-34.69	-199.48	1.30	-198.13
P1124	40.25.743	111.55.632	4829.26	979729.16	980218.65	-35.25	-199.78	1.30	-198.48
P1125	40.25.575	111.55.581	4751.26	979734.61	980218.41	-36.89	-198.76	1.37	-197.39
P1201	40.29.003	111.55.424	4453.19	979749.10	980223.43	-55.51	-207.23	1.50	-205.73
P1202	40.28.852	111.55.515	4451.89	979748.80	980223.26	-55.71	-207.38	1.51	-205.87
P1203	40.28.704	111.55.611	4448.29	979748.85	980223.04	-55.78	-207.33	1.54	-205.79
P1204	40.28.555	111.55.700	4445.59	979749.55	980222.80	-55.00	-206.46	1.57	-204.89

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
P1205	40.28.404	111.55.789	4434.15	979750.29	980222.59	-55.22	-206.29	1.65	-204.64
P1206	40.28.250	111.55.877	4446.55	979750.65	980222.35	-53.46	-204.95	1.68	-203.27
P1207	40.28.084	111.55.899	4445.58	979750.91	980222.11	-53.05	-204.50	1.77	-202.74
P1208	40.27.919	111.55.931	4444.86	979751.37	980221.87	-52.42	-203.85	1.92	-201.93
P1209	40.27.756	111.55.952	4447.59	979752.42	980221.62	-50.86	-202.39	2.14	-200.25
P1210	40.27.596	111.55.908	4451.10	979753.57	980221.39	-49.15	-200.80	2.16	-198.64
P1211	40.27.446	111.55.822	4455.16	979754.71	980221.16	-47.39	-199.18	2.29	-196.89
P1212	40.27.333	111.55.666	4461.24	979754.72	980221.00	-46.66	-198.65	2.19	-196.46
P1213	40.27.211	111.55.516	4468.37	979754.28	980220.81	-46.24	-198.47	2.05	-196.42
P1214	40.27.098	111.55.388	4473.45	979753.52	980220.65	-46.36	-198.76	1.96	-196.80
P1215	40.26.934	111.55.291	4480.07	979752.81	980220.40	-46.19	-198.83	1.95	-196.87
P1216	40.26.781	111.55.290	4482.09	979752.49	980220.18	-46.10	-198.81	1.99	-196.82
P1217	40.26.602	111.55.302	4492.41	979751.31	980219.91	-46.04	-199.09	1.97	-197.12
P1218	40.26.494	111.55.159	4499.42	979750.79	980219.74	-45.74	-199.03	1.94	-197.09
P1219	40.26.477	111.54.948	4501.76	979750.17	980219.73	-46.12	-199.49	1.71	-197.73
P1220	40.26.439	111.54.745	4506.58	979749.76	980219.69	-46.04	-199.57	1.65	-197.92
P1221	40.26.320	111.54.590	4512.53	979748.85	980219.51	-46.21	-199.95	1.57	-198.38
P1222	40.26.186	111.54.455	4518.44	979748.44	980219.30	-45.86	-199.80	1.52	-198.28
P1223	40.26.062	111.54.326	4528.31	979748.31	980219.12	-44.87	-199.15	1.46	-197.69
P1224	40.25.933	111.54.165	4534.05	979748.10	980218.93	-44.36	-198.83	1.44	-197.39
P1225	40.25.801	111.54.032	4539.34	979747.69	980218.74	-44.08	-198.73	1.39	-197.34
P1226	40.25.681	111.53.909	4546.25	979746.83	980218.55	-44.10	-198.98	1.36	-197.62
P1227	40.25.554	111.53.776	4549.54	979745.98	980218.36	-44.45	-199.45	1.32	-198.13
P1228	40.25.422	111.53.643	4551.26	979745.37	980218.17	-44.71	-199.77	1.32	-198.45
P1229	40.25.302	111.53.494	4549.45	979744.69	980217.99	-45.38	-200.38	1.30	-199.08
P1230	40.25.178	111.53.349	4549.58	979743.98	980217.80	-45.89	-200.89	1.26	-199.63
P1231	40.25.031	111.53.212	4548.51	979743.37	980217.59	-46.38	-201.35	1.22	-200.13
P1301	40.25.634	111.56.453	5060.00	979719.17	980218.49	-23.38	-195.77	1.49	-194.28
P1302	40.25.737	111.56.275	4943.39	979727.08	980218.64	-26.59	-195.00	1.60	-193.40
P1303	40.25.813	111.56.139	4842.75	979731.78	980218.75	-31.46	-196.45	1.84	-194.61
P1304	40.25.951	111.55.942	4810.27	979732.96	980218.96	-33.55	-197.43	1.52	-195.91
P1305	40.26.051	111.55.788	4780.47	979733.59	980219.10	-35.86	-198.73	1.44	-197.29
P1306	40.26.149	111.55.623	4693.61	979738.38	980219.25	-39.39	-199.30	1.58	-197.72

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
P1307	40.26.263	111.55.448	4685.96	979738.75	980219.42	-39.91	-199.56	1.47	-198.09
P1308	40.26.382	111.55.253	4634.65	979742.27	980219.60	-41.40	-199.29	1.42	-197.87
P1309	40.26.613	111.54.906	4650.98	979741.10	980219.92	-41.35	-199.31	1.39	-198.42
P1310	40.26.730	111.54.751	4742.09	979735.34	980220.09	-38.71	-200.27	1.82	-198.45
P1311	40.26.864	111.54.613	4766.66	979733.65	980220.30	-38.30	-200.69	1.69	-199.00
P1312	40.26.968	111.54.451	4791.72	979732.97	980220.46	-36.78	-200.03	1.53	-198.50
P1313	40.27.072	111.54.281	4844.24	979730.00	980220.60	-34.95	-199.99	1.51	-198.48
P1314	40.27.181	111.54.154	4896.04	979726.29	980220.77	-33.95	-200.76	1.53	-199.23
P1315	40.27.238	111.54.053	4990.44	979720.31	980220.95	-30.64	-200.66	1.80	-198.86
P1316	40.27.406	111.53.835	5064.18	979716.24	980221.10	-28.53	-201.06	1.97	-199.09
P1317	40.27.473	111.53.654	5132.63	979711.92	980221.20	-26.51	-201.37	2.18	-199.19
PG001	40.29.449	111.55.364	4366.26	979753.66	980224.15	-59.80	-208.55	1.67	-206.83
PG002	40.29.512	111.55.243	4371.28	979753.52	980224.23	-59.55	-208.48	1.66	-206.82
PG003	40.29.568	111.55.112	4428.24	979749.69	980224.32	-58.11	-208.98	1.52	-207.46
PG004	40.29.627	111.54.981	4432.18	979749.54	980224.41	-57.97	-208.98	1.54	-207.43
PG005	40.29.691	111.54.853	4432.35	979749.63	980224.49	-57.95	-208.96	1.56	-207.40
PG006	40.29.750	111.54.722	4431.01	979749.88	980224.59	-57.93	-208.89	1.59	-207.30
PG007	40.29.814	111.54.588	4425.37	979749.95	980224.69	-58.49	-209.25	1.65	-207.60
PG008	40.29.867	111.54.463	4456.18	979749.99	980224.76	-55.62	-207.44	1.62	-205.82
PG009	40.29.936	111.54.342	4423.67	979749.95	980224.86	-58.82	-209.53	1.73	-207.80
PG010	40.29.997	111.54.207	4420.46	979749.93	980224.95	-59.23	-209.83	1.78	-208.05
PG011	40.30.069	111.54.076	4420.92	979749.59	980225.06	-59.64	-210.26	1.82	-208.44
PG012	40.29.332	111.55.448	4371.91	979753.34	980223.97	-59.41	-208.35	1.65	-206.70
PG013	40.30.063	111.53.910	4421.02	979749.26	980225.05	-59.95	-210.57	1.92	-208.65
PG014	40.29.346	111.55.288	4397.45	979752.01	980223.98	-58.35	-208.17	1.60	-206.57
PG015	40.29.382	111.55.218	4424.27	979750.25	980224.05	-57.65	-208.38	1.53	-206.85
PG016	40.29.409	111.55.157	4435.93	979749.46	980224.07	-57.37	-208.49	1.52	-206.97
PG017	40.29.440	111.55.097	4442.70	979749.03	980224.13	-57.22	-208.58	1.51	-207.07
PG018	40.29.475	111.55.040	4436.76	979749.49	980224.17	-57.36	-208.52	1.54	-206.99
PG019	40.29.508	111.54.959	4437.73	979749.40	980224.23	-57.42	-208.61	1.55	-207.06
PG020	40.29.526	111.54.895	4437.77	979749.40	980224.25	-57.43	-208.62	1.57	-207.05
PG021	40.29.559	111.54.831	4438.08	979749.35	980224.30	-57.51	-208.71	1.59	-207.12
PG022	40.29.590	111.54.771	4436.81	979749.49	980224.35	-57.53	-208.69	1.60	-207.09

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
PG023	40.29.620	111.54.713	4436.45	979749.56	980224.39	-57.54	-208.68	1.62	-207.06
PG024	40.29.646	111.54.635	4434.44	979749.65	980224.44	-57.68	-208.76	1.65	-207.11
PG025	40.29.684	111.54.578	4433.09	979749.69	980224.48	-57.82	-208.85	1.66	-207.19
PG026	40.29.720	111.54.511	4431.82	979749.72	980224.54	-57.96	-208.95	1.69	-207.26
PG027	40.29.736	111.54.451	4430.22	979749.74	980224.57	-58.12	-209.06	1.72	-207.34
PG028	40.29.769	111.54.387	4428.55	979749.80	980224.61	-58.26	-209.14	1.74	-207.40
PG029	40.29.797	111.54.326	4427.09	979749.79	980224.66	-58.45	-209.28	1.77	-207.51
PG030	40.29.833	111.54.262	4425.45	979749.79	980224.71	-58.66	-209.43	1.81	-207.62
PG031	40.29.861	111.54.188	4423.88	979749.77	980224.76	-58.88	-209.59	1.84	-207.75
PG032	40.29.889	111.54.131	4422.50	979749.69	980224.79	-59.12	-209.79	1.86	-207.93
PG033	40.29.922	111.54.061	4421.37	979749.57	980224.84	-59.40	-210.03	1.89	-208.14
PG034	40.29.948	111.53.998	4421.02	979749.48	980224.87	-59.55	-210.17	1.91	-208.26
PG035	40.29.239	111.55.370	4378.22	979753.46	980223.83	-58.55	-207.71	1.68	-206.03
PG036	40.29.300	111.55.246	4442.58	979749.25	980223.91	-56.80	-208.15	1.50	-206.65
PG037	40.29.327	111.55.182	4441.69	979750.10	980223.95	-56.07	-207.39	1.51	-205.88
PG038	40.29.365	111.55.118	4439.35	979749.61	980224.02	-56.84	-208.08	1.53	-206.56
PG039	40.29.388	111.55.054	4439.07	979749.56	980224.05	-56.95	-208.18	1.55	-206.63
PG040	40.29.421	111.54.977	4439.40	979749.49	980224.10	-57.04	-208.29	1.57	-206.72
PG041	40.29.454	111.54.919	4440.26	979749.28	980224.15	-57.22	-208.49	1.58	-206.91
PG042	40.29.482	111.54.852	4441.19	979749.12	980224.19	-57.33	-208.64	1.60	-207.04
PG043	40.29.505	111.54.794	4441.06	979749.14	980224.22	-57.35	-208.66	1.61	-207.05
PG044	40.29.538	111.54.721	4438.75	979749.31	980224.28	-57.46	-208.69	1.63	-207.06
PG045	40.29.566	111.54.660	4437.54	979749.41	980224.30	-57.50	-208.68	1.65	-207.03
PG046	40.29.604	111.54.596	4437.05	979749.41	980224.37	-57.61	-208.77	1.67	-207.10
PG047	40.29.630	111.54.532	4435.73	979749.43	980224.41	-57.75	-208.87	1.70	-207.17
PG048	40.29.661	111.54.472	4432.78	979749.62	980224.45	-57.89	-208.91	1.72	-207.19
PG049	40.29.689	111.54.405	4431.61	979749.67	980224.49	-57.99	-208.97	1.74	-207.23
PG050	40.29.720	111.54.344	4430.57	979749.66	980224.54	-58.14	-209.08	1.78	-207.31
PG051	40.29.750	111.54.283	4429.25	979749.62	980224.59	-58.35	-209.25	1.78	-207.47
PG052	40.29.783	111.54.212	4426.89	979749.70	980224.64	-58.55	-209.37	1.85	-207.52
PG053	40.29.809	111.54.152	4425.12	979749.62	980224.67	-58.82	-209.58	1.88	-207.70
PG054	40.29.837	111.54.088	4423.63	979749.59	980224.71	-59.03	-209.74	1.90	-207.84
PG055	40.29.868	111.54.015	4423.21	979749.52	980224.76	-59.19	-209.89	1.95	-207.93

STAT.	LATITUDE	LONGITUDE	ELEV.	OPSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE FOUGUER	T.C.	COMPLETE FOUGUER
PG056	40.29.896	111.53.959	4422.50	979749.42	980224.80	-59.40	-210.07	1.96	-208.11
PG057	40.29.959	111.53.823	4422.42	979748.99	980224.91	-59.94	-210.61	2.06	-208.55
PG058	40.29.243	111.55.199	4450.74	979749.17	980223.83	-56.02	-207.65	1.51	-206.14
PG059	40.29.278	111.55.149	4445.51	979749.59	980223.88	-56.15	-207.60	1.53	-206.07
PG060	40.29.309	111.55.079	4443.71	979749.79	980223.93	-56.16	-207.56	1.55	-206.01
PG061	40.29.339	111.55.014	4443.75	979749.71	980223.97	-56.28	-207.67	1.57	-206.10
PG062	40.29.371	111.54.943	4442.50	979749.58	980224.03	-56.58	-207.94	1.59	-206.35
PG063	40.29.399	111.54.876	4439.29	979749.60	980224.06	-56.90	-208.15	1.62	-206.52
PG064	40.29.428	111.54.812	4446.42	979748.94	980224.10	-56.93	-208.42	1.62	-206.80
PG065	40.29.461	111.54.745	4446.91	979749.92	980224.16	-55.97	-207.47	1.64	-205.83
PG066	40.29.486	111.54.690	4441.13	979749.22	980224.19	-57.24	-208.54	1.67	-206.87
PG067	40.29.515	111.54.624	4439.77	979749.18	980224.23	-57.45	-208.71	1.68	-207.03
PG068	40.29.550	111.54.563	4438.45	979749.20	980224.29	-57.61	-208.82	1.70	-207.12
PG069	40.29.583	111.54.499	4437.86	979749.21	980224.34	-57.70	-208.89	1.72	-207.17
PG070	40.29.609	111.54.432	4435.51	979749.37	980224.38	-57.81	-208.92	1.75	-207.17
PG071	40.29.640	111.54.368	4434.46	979749.45	980224.42	-57.87	-208.94	1.78	-207.16
PG072	40.29.670	111.54.304	4434.60	979749.39	980224.47	-57.96	-209.04	1.81	-207.23
PG073	40.29.701	111.54.240	4431.97	979749.55	980224.51	-58.09	-209.08	1.84	-207.24
PG074	40.29.734	111.54.173	4430.40	979749.53	980224.57	-58.32	-209.26	1.88	-207.38
PG075	40.29.757	111.54.115	4427.79	979749.53	980224.60	-58.59	-209.44	1.91	-207.53
PG076	40.29.788	111.54.045	4426.99	979749.41	980224.64	-58.83	-209.65	1.95	-207.70
PG077	40.29.814	111.53.981	4425.98	979749.31	980224.69	-59.07	-209.86	1.99	-207.87
PG078	40.29.849	111.53.920	4425.11	979749.22	980224.73	-59.28	-210.04	2.01	-208.03
PG079	40.29.143	111.55.301	4452.51	979749.19	980223.68	-55.69	-207.38	1.50	-205.88
PG080	40.29.199	111.55.164	4455.67	979749.26	980223.77	-55.41	-207.21	1.52	-205.69
PG081	40.29.227	111.55.106	4451.51	979749.58	980223.81	-55.52	-207.18	1.54	-205.64
PG082	40.29.257	111.55.039	4447.09	979749.90	980223.85	-55.66	-207.17	1.57	-205.60
PG083	40.29.289	111.54.970	4446.04	979749.88	980223.90	-55.82	-207.30	1.59	-205.71
PG084	40.29.317	111.54.903	4447.67	979749.70	980223.95	-55.90	-207.42	1.61	-205.82
PG085	40.29.348	111.54.839	4449.28	979749.40	980223.98	-56.09	-207.67	1.63	-206.04
PG086	40.29.379	111.54.772	4451.12	979749.01	980224.03	-56.35	-207.99	1.65	-206.34
PG087	40.29.407	111.54.705	4451.34	979748.75	980224.07	-56.63	-208.28	1.67	-206.61
PG088	40.29.465	111.54.584	4443.41	979748.89	980224.16	-57.33	-208.71	1.73	-206.98

STAT.	LATITUDE	LONGITUDE	FLEV.	OFSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLF BOUGUER	T.C.	COMPLETE FOUGUER
PG089	40.29.498	111.54.527	4440.50	979749.02	980224.20	-57.51	-208.79	1.74	-207.05
PG090	40.29.440	111.54.654	4447.16	979748.97	980224.13	-56.86	-208.37	1.69	-206.68
PG091	40.29.529	111.54.456	4437.77	979749.05	980224.27	-57.80	-208.99	1.77	-207.22
PG092	40.29.557	111.54.392	4438.02	979749.01	980224.30	-57.86	-209.05	1.80	-207.25
PG093	40.29.590	111.54.331	4437.00	979749.14	980224.35	-57.87	-209.03	1.82	-207.21
PG094	40.29.626	111.54.264	4436.30	979749.37	980224.41	-57.76	-208.90	1.85	-207.05
PG095	40.29.649	111.54.194	4435.16	979749.36	980224.44	-57.91	-209.01	1.88	-207.13
PG096	40.29.680	111.54.137	4433.52	979749.44	980224.48	-58.03	-209.07	1.90	-207.17
PG097	40.29.713	111.54.073	4431.75	979749.44	980224.52	-58.23	-209.22	1.95	-207.27
PG098	40.29.737	111.53.996	4430.74	979749.27	980224.57	-58.55	-209.50	2.01	-207.49
PG099	40.29.764	111.53.941	4429.00	979749.22	980224.61	-58.80	-209.69	2.04	-207.65
PG100	40.29.800	111.53.877	4428.53	979749.03	980224.66	-59.08	-209.95	2.06	-207.89
PG101	40.29.862	111.53.745	4428.28	979748.61	980224.76	-59.62	-210.49	2.16	-208.33
PG102	40.29.150	111.55.134	4462.62	979749.14	980223.70	-54.80	-206.84	1.53	-205.31
PG103	40.29.182	111.55.070	4458.39	979749.54	980223.73	-54.84	-206.73	1.55	-205.13
PG104	40.29.204	111.54.988	4453.00	979750.00	980223.78	-54.93	-206.64	1.59	-205.05
PG105	40.29.242	111.54.935	4448.59	979750.22	980223.83	-55.17	-206.73	1.62	-205.11
PG106	40.29.268	111.54.863	4449.56	979750.24	980223.87	-55.10	-206.69	1.64	-205.05
PG107	40.29.296	111.54.799	4451.62	979750.00	980223.91	-55.20	-206.86	1.65	-205.21
PG108	40.29.327	111.54.736	4452.83	979749.77	980223.95	-55.35	-207.05	1.67	-205.38
PG109	40.29.362	111.54.672	4451.65	979749.71	980224.02	-55.59	-207.25	1.70	-205.55
PG110	40.29.390	111.54.611	4451.99	979749.44	980224.05	-55.85	-207.53	1.71	-205.82
PG111	40.29.419	111.54.544	4451.83	979749.07	980224.09	-56.28	-207.95	1.74	-206.21
PG112	40.29.447	111.54.470	4450.95	979748.72	980224.13	-56.76	-208.40	1.77	-206.63
PG113	40.29.485	111.54.410	4446.88	979748.78	980224.19	-57.13	-208.64	1.81	-206.83
PG114	40.29.510	111.54.355	4441.62	979748.94	980224.23	-57.52	-208.84	1.84	-207.00
PG115	40.29.541	111.54.288	4442.11	979748.35	980224.28	-57.61	-208.94	1.86	-207.08
PG116	40.29.572	111.54.224	4440.60	979749.07	980224.32	-57.57	-208.85	1.89	-206.96
PG117	40.29.602	111.54.161	4440.22	979749.14	980224.37	-57.58	-208.85	1.91	-206.94
PG118	40.29.628	111.54.100	4439.11	979749.12	980224.41	-57.74	-208.93	1.94	-207.04
PG119	40.29.659	111.54.033	4437.70	979749.09	980224.45	-57.95	-209.14	1.98	-207.16
PG120	40.29.690	111.53.967	4434.49	979749.14	980224.49	-58.24	-209.32	2.03	-207.29
PG121	40.29.715	111.53.906	4433.52	979748.33	980224.54	-58.69	-209.74	2.06	-207.68

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
PG122	40.29.750	111.53.838	4431.94	979748.84	980224.59	-58.88	-209.87	2.11	-207.76
PG123	40.29.042	111.55.219	4474.26	979748.38	980223.53	-54.30	-206.74	1.52	-205.22
PG124	40.29.103	111.55.095	4469.73	979749.06	980223.62	-54.14	-206.42	1.54	-204.88
PG125	40.29.126	111.55.033	4462.68	979749.56	980223.66	-54.24	-206.28	1.57	-204.71
PG126	40.29.155	111.54.955	4457.74	979750.10	980223.71	-54.32	-206.19	1.61	-204.58
PG127	40.29.192	111.54.893	4453.42	979750.48	980223.75	-54.38	-206.10	1.64	-204.47
PG128	40.29.219	111.54.827	4454.00	979750.47	980223.80	-54.38	-206.13	1.66	-204.47
PG129	40.29.247	111.54.750	4453.55	979750.49	980223.84	-54.45	-206.18	1.69	-204.49
PG130	40.29.262	111.54.725	4453.91	979750.51	980223.85	-54.41	-206.15	1.70	-204.45
PG131	40.29.318	111.54.587	4455.87	979750.38	980223.95	-54.45	-206.25	1.74	-204.51
PG132	40.29.334	111.54.565	4457.49	979750.23	980223.97	-54.47	-206.33	1.75	-204.58
PG133	40.29.364	111.54.501	4459.11	979749.70	980224.02	-54.89	-206.81	1.73	-205.03
PG134	40.29.395	111.54.440	4458.10	979749.23	980224.06	-55.50	-207.39	1.80	-205.59
PG135	40.29.428	111.54.370	4454.09	979748.80	980224.10	-56.35	-208.10	1.85	-206.25
PG136	40.29.449	111.54.306	4446.78	979748.93	980224.15	-56.95	-208.45	1.93	-206.52
PG137	40.29.485	111.54.235	4449.03	979748.68	980224.19	-57.03	-208.61	1.95	-206.66
PG138	40.29.508	111.54.178	4451.13	979748.61	980224.23	-56.95	-208.60	1.92	-206.68
PG139	40.29.536	111.54.108	4452.53	979748.63	980224.27	-56.83	-208.52	1.94	-206.58
PG140	40.29.569	111.54.044	4442.34	979748.94	980224.32	-57.53	-208.88	2.01	-206.87
PG141	40.29.598	111.53.979	4444.93	979748.97	980224.37	-57.31	-208.74	2.03	-206.71
PG142	40.29.628	111.53.905	4442.50	979748.35	980224.41	-57.70	-209.05	2.03	-206.97
PG143	40.29.653	111.53.847	4441.26	979748.64	980224.44	-58.05	-209.36	2.12	-207.24
PG144	40.29.686	111.53.785	4439.34	979748.52	980224.49	-58.41	-209.65	2.17	-207.48
PG145	40.29.746	111.53.654	4439.90	979747.95	980224.59	-59.02	-210.23	2.23	-208.05
PG146	40.29.052	111.55.061	4470.49	979749.37	980223.55	-53.68	-205.99	1.56	-204.43
PG147	40.29.077	111.54.982	4468.28	979749.66	980223.59	-53.65	-205.88	1.59	-204.29
PG148	40.29.111	111.54.912	4463.31	979750.10	980223.63	-53.71	-205.77	1.63	-204.14
PG149	40.29.142	111.54.855	4458.79	979750.54	980223.68	-53.75	-205.65	1.65	-204.00
PG150	40.29.167	111.54.787	4460.00	979750.43	980223.73	-53.70	-205.74	1.68	-204.06
PG151	40.29.207	111.54.723	4456.71	979750.74	980223.78	-53.84	-205.68	1.71	-203.97
PG152	40.29.231	111.54.656	4457.16	979750.87	980223.81	-53.70	-205.55	1.74	-203.81
PG153	40.29.259	111.54.592	4458.87	979750.76	980223.85	-53.69	-205.60	1.76	-203.84
PG154	40.29.292	111.54.535	4463.61	979750.34	980223.90	-53.71	-205.73	1.78	-204.00

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
PG155	40.29.323	111.54.462	4465.11	979749.89	980223.95	-54.07	-206.20	1.80	-204.40
PG156	40.29.348	111.54.401	4463.45	979749.44	980223.98	-54.71	-206.78	1.83	-204.95
PG157	40.29.377	111.54.333	4460.14	979743.70	980224.03	-55.81	-207.76	1.90	-205.86
PG158	40.29.409	111.54.273	4455.49	979748.70	980224.07	-56.29	-208.08	1.96	-206.12
PG159	40.29.435	111.54.199	4456.82	979748.50	980224.12	-56.41	-208.25	1.98	-206.27
PG160	40.29.441	111.54.119	4462.74	979748.34	980224.13	-56.03	-208.07	1.99	-206.08
PG161	40.29.464	111.54.074	4457.79	979748.67	980224.19	-56.22	-208.09	2.01	-206.08
PG162	40.29.525	111.54.011	4453.71	979749.40	980224.25	-55.93	-207.67	2.02	-205.65
PG163	40.29.551	111.53.936	4450.83	979749.07	980224.29	-56.57	-208.21	2.08	-206.13
PG164	40.29.584	111.53.872	4449.18	979748.81	980224.34	-57.04	-208.61	2.13	-206.49
PG165	40.29.604	111.53.811	4468.01	979748.55	980224.37	-55.56	-207.78	2.09	-205.69
PG166	40.29.639	111.53.746	4446.81	979743.42	980224.42	-57.74	-209.23	2.21	-207.02
PG167	40.28.941	111.55.143	4481.18	979748.59	980223.39	-53.30	-205.97	1.54	-204.43
PG168	40.29.003	111.55.013	4473.84	979749.56	980223.48	-53.11	-205.53	1.59	-203.94
PG169	40.29.028	111.54.945	4471.04	979749.96	980223.52	-53.02	-205.34	1.61	-203.73
PG170	40.29.061	111.54.875	4468.11	979750.35	980223.56	-52.94	-205.17	1.65	-203.52
PG171	40.29.094	111.54.818	4464.08	979750.81	980223.61	-52.91	-205.00	1.68	-203.32
PG172	40.29.120	111.54.750	4464.48	979750.79	980223.65	-52.93	-205.03	1.71	-203.32
PG173	40.29.153	111.54.687	4461.83	979750.87	980223.70	-53.15	-205.16	1.73	-203.43
PG174	40.29.184	111.54.610	4465.58	979750.77	980223.73	-52.93	-205.07	1.76	-203.31
PG175	40.29.209	111.54.553	4464.48	979750.91	980223.78	-52.94	-205.04	1.80	-203.24
PG176	40.29.243	111.54.495	4467.77	979750.61	980223.83	-52.98	-205.19	1.81	-203.39
PG177	40.29.271	111.54.425	4465.86	979750.42	980223.87	-53.39	-205.54	1.85	-203.69
PG178	40.29.306	111.54.364	4467.16	979749.34	980223.93	-54.41	-206.60	1.88	-204.72
PG179	40.29.332	111.54.297	4465.72	979748.78	980223.97	-55.14	-207.29	1.93	-205.36
PG180	40.29.358	111.54.229	4465.22	979748.53	980224.00	-55.47	-207.60	1.97	-205.63
PG181	40.29.391	111.54.159	4466.55	979748.24	980224.06	-55.70	-207.87	1.98	-205.89
PG182	40.29.417	111.54.099	4464.81	979748.34	980224.09	-55.79	-207.90	2.01	-205.89
PG183	40.29.452	111.54.035	4465.84	979748.31	980224.15	-55.78	-207.93	2.03	-205.90
PG184	40.29.464	111.53.965	4464.09	979748.70	980224.16	-55.57	-207.66	2.09	-205.57
PG185	40.29.499	111.53.897	4463.28	979748.50	980224.22	-55.90	-207.96	2.12	-205.84
PG186	40.29.524	111.53.833	4458.31	979748.48	980224.25	-56.42	-208.31	2.20	-206.11
PG187	40.29.559	111.53.768	4456.17	979748.37	980224.30	-56.79	-208.60	2.22	-206.39

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE FOUGJER	T.C.	COMPLETE FOUGJER
PG188	40.29.587	111.53.707	4455.95	979748.14	980224.35	-57.09	-208.90	2.24	-206.66
PG189	40.29.657	111.53.595	4455.30	979747.33	980224.45	-58.06	-209.84	2.29	-207.58
PG190	40.28.946	111.54.981	4479.38	979749.71	980223.39	-52.35	-204.96	1.61	-203.35
PG191	40.28.976	111.54.914	4472.65	979750.39	980223.43	-52.34	-204.72	1.66	-203.08
PG192	40.29.009	111.54.838	4462.95	979750.76	980223.49	-52.95	-205.00	1.71	-203.28
PG193	40.29.038	111.54.775	4467.99	979751.14	980223.53	-52.13	-204.35	1.71	-202.64
PG194	40.29.073	111.54.711	4467.36	979751.16	980223.58	-52.22	-204.42	1.74	-202.68
PG195	40.29.099	111.54.644	4467.29	979751.23	980223.62	-52.20	-204.40	1.77	-202.63
PG196	40.29.130	111.54.580	4467.12	979751.22	980223.66	-52.27	-204.46	1.77	-202.69
PG197	40.29.160	111.54.522	4469.78	979751.10	980223.71	-52.18	-204.46	1.82	-202.64
PG198	40.29.191	111.54.452	4470.89	979750.97	980223.75	-52.25	-204.57	1.85	-202.72
PG199	40.29.217	111.54.385	4472.24	979750.43	980223.80	-52.71	-205.07	1.88	-203.19
PG200	40.29.245	111.54.321	4470.64	979749.44	980223.84	-53.89	-206.21	1.94	-204.27
PG201	40.29.278	111.54.257	4470.55	979748.91	980223.88	-54.47	-206.78	1.97	-204.81
PG202	40.29.311	111.54.190	4470.29	979748.68	980223.93	-54.77	-207.07	2.01	-205.06
PG203	40.29.334	111.54.126	4470.22	979748.51	980223.97	-54.99	-207.29	2.04	-205.25
PG204	40.29.365	111.54.059	4469.74	979748.46	980224.02	-55.13	-207.41	2.07	-205.34
PG205	40.29.387	111.53.990	4471.39	979748.42	980224.05	-55.05	-207.38	2.11	-205.27
PG206	40.29.417	111.53.929	4471.66	979748.30	980224.09	-55.18	-207.53	2.15	-205.38
PG207	40.29.445	111.53.865	4473.89	979747.90	980224.13	-55.42	-207.84	2.24	-205.60
PG208	40.29.480	111.53.797	4469.55	979747.31	980224.19	-55.97	-208.24	2.29	-205.95
PG209	40.29.505	111.53.739	4468.01	979747.74	980224.22	-56.22	-208.44	2.26	-206.18
PG210	40.29.540	111.53.671	4481.16	979746.63	980224.28	-56.15	-208.82	2.22	-206.60
PG211	40.28.841	111.55.064	4491.32	979748.65	980223.24	-52.14	-205.15	1.58	-203.57
PG212	40.28.894	111.54.941	4484.90	979749.83	980223.31	-51.63	-204.43	1.64	-202.79
PG213	40.28.925	111.54.871	4479.25	979750.48	980223.36	-51.56	-204.17	1.70	-202.47
PG214	40.28.958	111.54.810	4477.57	979750.88	980223.41	-51.37	-203.91	1.73	-202.13
PG215	40.28.991	111.54.747	4473.04	979751.38	980223.46	-51.35	-203.74	1.77	-201.97
PG216	40.29.016	111.54.674	4471.12	979751.64	980223.49	-51.30	-203.62	1.79	-201.83
PG217	40.29.047	111.54.607	4471.38	979751.64	980223.55	-51.33	-203.66	1.78	-201.88
PG218	40.29.085	111.54.547	4474.66	979751.59	980223.59	-51.12	-203.55	1.81	-201.75
PG219	40.29.114	111.54.479	4473.25	979751.50	980223.63	-51.38	-203.78	1.86	-201.92
PG220	40.29.144	111.54.415	4481.36	979750.79	980223.68	-51.37	-204.05	1.88	-202.17

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
PG221	40.29.172	111.54.345	4477.87	979750.77	980223.73	-51.77	-204.33	1.94	-202.39
PG222	40.29.198	111.54.291	4481.31	979749.68	980223.77	-52.57	-205.25	1.95	-203.30
PG223	40.29.233	111.54.224	4482.10	979748.32	980223.81	-53.41	-206.11	1.99	-204.12
PG224	40.29.262	111.54.157	4479.84	979748.46	980223.85	-54.02	-206.64	2.02	-204.62
PG225	40.29.287	111.54.087	4477.70	979748.31	980223.90	-54.42	-206.97	2.09	-204.89
PG226	40.29.313	111.54.022	4477.75	979748.24	980223.95	-54.53	-207.08	2.16	-204.92
PG227	40.29.343	111.53.958	4479.12	979748.07	980223.98	-54.61	-207.21	2.17	-205.04
PG228	40.29.373	111.53.890	4480.19	979748.04	980224.03	-54.59	-207.22	2.23	-204.99
PG229	40.29.401	111.53.828	4485.49	979747.29	980224.07	-54.87	-207.69	2.27	-205.42
PG230	40.29.436	111.53.764	4486.47	979746.89	980224.12	-55.23	-208.08	2.31	-205.77
PG231	40.29.461	111.53.700	4485.74	979746.77	980224.16	-55.47	-208.29	2.34	-205.95
PG232	40.29.488	111.53.638	4484.99	979746.72	980224.19	-55.61	-208.41	2.34	-206.07
PG233	40.29.556	111.53.510	4475.62	979746.66	980224.29	-56.65	-209.13	2.39	-206.74
PG234	40.28.848	111.54.898	4489.86	979749.35	980223.24	-50.98	-203.94	1.67	-202.27
PG235	40.28.876	111.54.831	4487.00	979750.43	980223.29	-50.81	-203.68	1.72	-201.96
PG236	40.28.911	111.54.767	4484.01	979750.33	980223.34	-50.65	-203.41	1.77	-201.64
PG237	40.28.944	111.54.706	4482.42	979751.34	980223.39	-50.43	-203.15	1.80	-201.35
PG238	40.28.970	111.54.636	4480.93	979751.62	980223.43	-50.33	-202.99	1.82	-201.17
PG239	40.28.998	111.54.567	4481.29	979751.71	980223.48	-50.26	-202.93	1.84	-201.09
PG240	40.29.031	111.54.497	4481.08	979751.85	980223.52	-50.18	-202.85	1.88	-200.97
PG241	40.29.057	111.54.436	4486.10	979751.53	980223.56	-50.07	-202.91	1.89	-201.02
PG242	40.29.090	111.54.372	4497.44	979750.47	980223.61	-50.11	-203.33	1.89	-201.44
PG243	40.29.116	111.54.302	4496.87	979750.20	980223.65	-50.47	-203.68	1.93	-201.75
PG244	40.29.149	111.54.245	4497.72	979749.39	980223.70	-51.25	-204.48	1.96	-202.52
PG245	40.29.177	111.54.174	4493.53	979748.95	980223.73	-52.12	-205.21	2.02	-203.19
PG246	40.29.208	111.54.110	4492.08	979748.73	980223.78	-52.53	-205.57	2.06	-203.51
PG247	40.29.238	111.54.040	4490.20	979748.29	980223.83	-53.19	-206.17	2.14	-204.03
PG248	40.29.266	111.53.980	4488.43	979747.93	980223.87	-53.76	-206.67	2.19	-204.48
PG249	40.29.293	111.53.921	4491.11	979747.49	980223.91	-53.99	-207.00	2.22	-204.78
PG250	40.29.326	111.53.851	4493.26	979747.03	980223.95	-54.29	-207.37	2.27	-205.10
PG251	40.29.351	111.53.789	4496.42	979746.35	980224.00	-54.42	-207.60	2.32	-205.28
PG252	40.29.386	111.53.719	4498.04	979746.43	980224.05	-54.53	-207.77	2.35	-205.42
PG253	40.29.414	111.53.657	4498.79	979746.09	980224.09	-54.84	-208.11	2.37	-205.74

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
PG254	40.29.434	111.53.593	4499.95	979745.92	980224.12	-54.93	-208.24	2.41	-205.83
PG255	40.28.735	111.54.983	4494.12	979749.29	980223.09	-51.08	-204.19	1.65	-202.54
PG256	40.28.796	111.54.865	4495.43	979750.01	980223.17	-50.32	-203.48	1.70	-201.78
PG257	40.28.827	111.54.794	4494.35	979750.39	980223.21	-50.08	-203.20	1.75	-201.45
PG258	40.28.860	111.54.727	4492.78	979750.99	980223.26	-49.68	-202.74	1.78	-200.96
PG259	40.28.888	111.54.663	4492.73	979751.45	980223.30	-49.27	-202.33	1.82	-200.51
PG260	40.28.921	111.54.600	4492.37	979751.76	980223.36	-49.05	-202.10	1.85	-200.25
PG261	40.28.946	111.54.543	4492.66	979751.87	980223.39	-48.94	-202.00	1.87	-200.13
PG262	40.28.982	111.54.466	4497.15	979751.30	980223.45	-48.64	-201.86	1.91	-199.95
PG263	40.29.010	111.54.400	4504.65	979751.10	980223.49	-48.68	-202.15	1.91	-200.24
PG264	40.29.041	111.54.339	4518.36	979749.86	980223.53	-48.67	-202.61	1.89	-200.72
PG265	40.29.059	111.54.288	4518.79	979749.52	980223.56	-49.01	-202.96	1.92	-201.04
PG266	40.29.099	111.54.208	4521.03	979748.73	980223.62	-49.65	-203.67	1.95	-201.72
PG267	40.29.120	111.54.160	4518.84	979748.58	980223.65	-50.03	-203.98	1.98	-202.00
PG268	40.29.151	111.54.093	4518.31	979748.03	980223.70	-50.67	-204.61	2.03	-202.58
PG269	40.29.179	111.54.036	4519.09	979747.38	980223.73	-51.29	-205.25	2.06	-203.19
PG270	40.29.209	111.53.966	4519.44	979746.86	980223.78	-51.82	-205.80	2.11	-203.69
PG271	40.29.239	111.53.898	4516.88	979746.50	980223.83	-52.47	-206.36	2.17	-204.19
PG272	40.29.274	111.53.844	4516.87	979746.08	980223.88	-52.95	-206.83	2.22	-204.61
PG273	40.29.304	111.53.769	4516.33	979745.68	980223.93	-53.44	-207.31	2.29	-205.02
PG274	40.29.331	111.53.708	4519.65	979745.28	980223.95	-53.55	-207.53	2.31	-205.23
PG275	40.29.352	111.53.660	4524.26	979744.80	980224.00	-53.65	-207.78	2.32	-205.47
PG276	40.29.402	111.53.557	4517.32	979744.93	980224.07	-54.24	-208.14	2.41	-205.73
PG277	40.29.459	111.53.431	4513.22	979744.57	980224.16	-54.98	-208.74	2.55	-206.19
PG278	40.28.637	111.54.920	4496.02	979749.95	980222.94	-50.09	-203.27	1.72	-201.55
PG279	40.28.696	111.54.792	4497.67	979750.79	980223.02	-49.18	-202.41	1.80	-200.61
PG280	40.28.754	111.54.645	4504.99	979751.51	980223.11	-47.86	-201.34	1.88	-199.46
PG281	40.28.825	111.54.523	4521.93	979751.02	980223.21	-46.86	-200.92	1.91	-199.01
PG282	40.28.884	111.54.392	4547.07	979749.51	980223.30	-46.10	-201.01	1.90	-199.11
PG283	40.28.942	111.54.261	4568.56	979746.02	980223.39	-47.65	-203.30	1.93	-201.37
PG284	40.29.003	111.54.132	4574.60	979747.30	980223.48	-45.89	-201.74	1.96	-199.78
PG285	40.29.067	111.54.001	4579.80	979746.14	980223.58	-46.66	-202.69	2.01	-200.68
PG286	40.29.125	111.53.872	4574.34	979745.48	980223.65	-47.91	-203.75	2.13	-201.62

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
PG287	40.29.187	111.53.730	4575.69	979744.47	980223.75	-48.89	-204.78	2.20	-202.58
PG288	40.29.243	111.53.614	4582.49	979742.73	980223.83	-50.07	-206.19	2.28	-203.91
PG289	40.29.301	111.53.485	4584.29	979741.58	980223.91	-51.14	-207.32	2.37	-204.95
PG290	40.29.356	111.53.349	4579.44	979741.28	980224.00	-51.98	-208.00	2.54	-205.45
F0101	40.49.650	111.56.600	4211.15	979820.93	980254.17	-37.14	-180.61	1.05	-179.56
F0102	40.49.650	111.56.390	4210.76	979820.09	980254.17	-38.02	-181.47	1.16	-180.31
F0103	40.49.660	111.56.170	4214.33	979819.39	980254.18	-38.39	-181.97	1.28	-180.69
F0104	40.49.660	111.55.970	4213.61	979819.04	980254.18	-38.81	-182.36	1.40	-180.96
F0105	40.49.660	111.55.850	4212.06	979819.14	980254.18	-38.85	-182.35	1.52	-180.83
F0106	40.49.660	111.55.750	4217.60	979818.85	980254.18	-38.62	-182.31	1.59	-180.72
F0107	40.49.640	111.55.630	4218.36	979818.94	980254.16	-38.44	-182.15	1.72	-180.43
F0108	40.49.640	111.55.510	4218.41	979819.19	980254.16	-38.18	-181.90	1.90	-180.00
F0109	40.49.640	111.55.410	4218.30	979819.62	980254.16	-37.76	-181.48	2.07	-179.41
F0110	40.49.640	111.55.300	4218.24	979820.18	980254.16	-37.21	-180.92	2.37	-178.55
F0111	40.49.650	111.55.190	4219.94	979820.83	980254.17	-36.41	-180.18	2.66	-177.52
F0112	40.49.650	111.55.090	4230.05	979820.85	980254.17	-35.44	-179.56	2.97	-176.59
F0113	40.49.650	111.54.980	4254.59	979820.34	980254.17	-33.64	-178.59	3.26	-175.33
F0114	40.49.650	111.54.870	4276.28	979821.06	980254.17	-30.88	-176.57	3.80	-172.77
F0115	40.49.650	111.54.760	4430.05	979810.85	980254.17	-26.63	-177.56	2.95	-174.61
F0201	40.49.220	111.56.630	4210.36	979818.89	980253.53	-38.62	-182.06	1.05	-181.01
F0202	40.49.220	111.56.410	4214.61	979817.95	980253.53	-39.16	-182.74	1.14	-181.60
F0203	40.49.220	111.56.200	4210.17	979817.87	980253.53	-39.65	-183.09	1.29	-181.80
F0204	40.49.220	111.55.980	4211.15	979817.81	980253.53	-39.62	-183.09	1.45	-181.64
F0205	40.49.220	111.55.870	4210.79	979818.03	980253.53	-39.43	-182.89	1.55	-181.34
F0206	40.49.220	111.55.770	4211.19	979818.28	980253.53	-39.15	-182.62	1.68	-180.94
F0207	40.49.220	111.55.660	4212.96	979818.42	980253.53	-38.84	-182.37	1.80	-180.57
F0208	40.49.220	111.55.550	4211.03	979819.02	980253.53	-38.42	-181.89	2.01	-179.88
F0209	40.49.220	111.55.440	4212.93	979819.97	980253.53	-37.29	-180.82	2.22	-178.60
F0210	40.49.220	111.55.330	4216.49	979820.59	980253.53	-36.34	-179.99	2.54	-177.45
F0211	40.49.220	111.55.220	4217.98	979821.52	980253.53	-35.27	-178.97	2.97	-176.00
F0212	40.49.220	111.55.120	4222.90	979822.26	980253.53	-34.07	-177.93	3.50	-174.43
F0213	40.49.220	111.55.010	4255.34	979821.55	980253.53	-31.72	-176.70	4.59	-172.11
F0214	40.49.220	111.54.900	4268.84	979822.47	980253.53	-29.53	-174.97	4.76	-170.21

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
F0215	40.49.220	111.54.840	4342.03	979819.05	980253.53	-26.07	-174.00	4.47	-169.53
F0301	40.49.020	111.56.690	4209.33	979817.27	980253.23	-40.03	-183.44	1.02	-182.42
F0302	40.49.020	111.56.480	4214.04	979816.50	980253.23	-40.35	-183.93	1.09	-182.84
F2303	40.49.010	111.56.280	4212.67	979816.32	980253.22	-40.66	-184.18	1.22	-182.96
F0304	40.49.010	111.56.060	4216.42	979815.99	980253.22	-40.63	-184.28	1.34	-182.94
F0305	40.49.010	111.55.960	4216.27	979816.05	980253.22	-40.58	-184.22	1.41	-182.81
F0306	40.49.010	111.55.850	4216.32	979816.23	980253.22	-40.40	-184.05	1.53	-182.52
F0307	40.49.010	111.55.740	4216.05	979816.58	980253.22	-40.08	-183.71	1.66	-182.05
F0308	40.49.010	111.55.630	4216.15	979817.05	980253.22	-39.60	-183.24	1.78	-181.46
F0309	40.49.010	111.55.520	4216.09	979817.77	980253.22	-38.88	-182.52	1.95	-180.57
F0310	40.49.010	111.55.410	4216.49	979818.71	980253.22	-37.91	-181.56	2.21	-179.35
F0311	40.49.010	111.55.310	4217.38	979820.00	980253.22	-36.53	-180.21	2.52	-177.69
F0312	40.49.000	111.55.200	4218.28	979821.59	980253.20	-34.74	-178.45	2.80	-175.65
F0313	40.49.000	111.55.090	4231.83	979822.99	980253.20	-32.17	-176.34	3.16	-173.18
F0314	40.49.000	111.54.980	4269.47	979822.75	980253.20	-28.87	-174.32	3.49	-170.83
F0315	40.49.000	111.54.820	4498.38	979810.03	980253.20	-20.06	-173.31	2.67	-170.64
F0401	40.48.790	111.56.700	4212.00	979815.98	980252.88	-40.72	-184.22	1.01	-183.21
F0402	40.48.790	111.56.500	4212.15	979815.50	980252.88	-41.19	-184.69	1.11	-183.58
F0403	40.48.790	111.56.270	4212.16	979815.10	980252.88	-41.59	-185.09	1.23	-183.86
F0404	40.48.790	111.56.050	4209.72	979815.10	980252.88	-41.82	-185.24	1.37	-183.87
F0405	40.48.790	111.55.940	4209.70	979815.27	980252.88	-41.65	-185.07	1.46	-183.61
F0406	40.48.790	111.55.830	4210.33	979815.39	980252.88	-41.47	-184.91	1.58	-183.33
F0407	40.48.780	111.55.730	4211.39	979815.52	980252.87	-41.23	-184.71	1.69	-183.02
F0408	40.48.780	111.55.620	4208.38	979816.38	980252.87	-40.66	-184.03	1.83	-182.20
F0409	40.48.780	111.55.500	4207.93	979817.13	980252.87	-39.95	-183.31	2.14	-181.17
F0410	40.48.780	111.55.390	4208.23	979818.29	980252.87	-38.76	-182.13	2.28	-179.85
F0411	40.48.780	111.55.280	4214.34	979819.30	980252.87	-37.17	-180.75	2.63	-178.12
F0412	40.48.780	111.55.170	4219.84	979820.77	980252.87	-35.19	-178.95	2.97	-175.98
F0413	40.48.770	111.55.060	4236.69	979821.56	980252.86	-32.80	-177.14	3.55	-173.59
F0414	40.48.770	111.54.950	4237.21	979823.25	980252.86	-31.06	-175.42	4.22	-171.19
F0415	40.48.770	111.54.580	4739.43	979793.84	980252.86	-13.23	-174.70	3.20	-171.70
F0701	40.47.980	111.56.310	4211.89	979811.73	980251.68	-43.78	-187.27	1.10	-186.17
F0702	40.47.960	111.56.110	4215.77	979811.26	980251.65	-43.95	-187.48	1.17	-186.31

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE FOUGUER	T.C.	COMPLETE FOUGUER
F0703	40.47.960	111.55.900	4213.75	979811.26	980251.65	-44.04	-187.60	1.29	-186.31
F0704	40.47.960	111.55.680	4212.90	979811.29	980251.65	-44.09	-187.62	1.44	-186.18
F0705	40.47.960	111.55.570	4212.77	979811.39	980251.65	-44.01	-187.53	1.51	-186.02
F0706	40.47.960	111.55.460	4216.06	979811.51	980251.65	-43.58	-187.21	1.60	-185.61
F0707	40.47.960	111.55.350	4215.36	979811.93	980251.65	-43.22	-186.83	1.73	-185.10
F0708	40.47.960	111.55.240	4216.25	979812.45	980251.65	-42.62	-186.26	1.88	-184.38
F0709	40.47.960	111.55.110	4220.07	979813.06	980251.65	-41.65	-185.42	2.02	-183.40
F0710	40.47.970	111.55.010	4220.05	979813.32	980251.66	-40.91	-184.68	2.20	-182.48
F0711	40.47.970	111.54.900	4219.64	979814.65	980251.66	-40.11	-183.97	2.48	-181.39
F0712	40.47.970	111.54.790	4221.37	979815.41	980251.66	-39.19	-183.01	2.81	-180.20
F0713	40.47.970	111.54.680	4227.52	979816.18	980251.66	-37.84	-181.87	3.06	-178.81
F0714	40.47.970	111.54.560	4241.61	979816.33	980251.66	-36.37	-180.88	3.34	-177.54
F0715	40.47.970	111.54.450	4242.10	979817.53	980251.66	-35.13	-179.65	3.96	-175.69
F0716	40.47.970	111.54.370	4247.90	979817.61	980251.66	-34.50	-179.22	4.51	-174.71
F0717	40.47.990	111.54.000	4826.93	979783.65	980251.70	-14.03	-178.48	2.93	-175.55
F0801	40.47.710	111.56.330	4214.23	979810.36	980251.28	-44.23	-187.81	1.05	-186.75
F0802	40.47.710	111.56.070	4215.16	979810.17	980251.28	-44.63	-188.24	1.16	-187.08
F0803	40.47.710	111.55.870	4217.07	979809.95	980251.28	-44.67	-188.34	1.24	-187.10
F0804	40.47.700	111.55.650	4211.51	979810.41	980251.27	-44.72	-188.20	1.39	-186.81
F0805	40.47.700	111.55.450	4213.07	979810.53	980251.27	-44.35	-187.89	1.52	-186.37
F0806	40.47.700	111.55.330	4214.33	979810.35	980251.27	-44.02	-187.59	1.62	-185.97
F0807	40.47.700	111.55.210	4215.07	979811.21	980251.27	-43.59	-187.19	1.73	-185.46
F0808	40.47.700	111.55.080	4216.46	979811.72	980251.27	-42.95	-186.60	1.87	-184.73
F0809	40.47.700	111.54.980	4221.08	979812.03	980251.27	-42.20	-186.01	2.00	-184.01
F0810	40.47.700	111.54.870	4220.28	979812.94	980251.27	-41.47	-185.25	2.18	-183.07
F0811	40.47.700	111.54.750	4221.26	979813.53	980251.27	-40.68	-184.50	2.45	-182.05
F0812	40.47.700	111.54.650	4225.74	979813.39	980251.27	-39.90	-183.87	2.61	-181.26
F0813	40.47.700	111.54.540	4227.33	979814.72	980251.27	-38.92	-182.94	3.03	-179.91
F0814	40.47.690	111.54.410	4231.67	979815.68	980251.26	-37.55	-181.72	3.38	-178.34
F0815	40.47.690	111.54.260	4243.89	979816.57	980251.26	-35.51	-180.09	4.13	-175.96
F0816	40.47.690	111.54.140	4263.27	979816.61	980251.26	-33.64	-178.89	4.43	-174.46
F0817	40.47.710	111.54.050	4276.67	979816.07	980251.28	-32.95	-178.65	5.42	-173.23
F0818	40.47.730	111.53.660	4826.37	979784.52	980251.31	-12.82	-177.25	2.62	-174.63

STAT.	LATITUDE	LONGITUDE	ELEV.	OPSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
F0901	40.47.470	111.56.310	4212.94	979809.48	980250.92	-45.17	-188.70	1.03	-187.67
F0902	40.47.470	111.56.040	4218.36	979808.91	980250.92	-45.23	-188.95	1.11	-187.84
F0903	40.47.470	111.55.840	4217.42	979809.02	980250.92	-45.21	-188.90	1.21	-187.68
F0904	40.47.470	111.55.610	4216.94	979809.29	980250.92	-44.99	-188.65	1.31	-187.34
F0905	40.47.470	111.55.370	4217.31	979809.80	980250.92	-44.44	-188.12	1.47	-186.65
F0906	40.47.470	111.55.250	4217.29	979810.23	980250.92	-44.01	-187.69	1.55	-186.14
F0907	40.47.470	111.55.140	4216.96	979810.66	980250.92	-43.61	-187.28	1.63	-185.65
F0908	40.47.470	111.55.030	4216.49	979811.26	980250.92	-43.06	-186.71	1.73	-184.98
F0909	40.47.470	111.54.920	4221.03	979811.63	980250.92	-42.26	-186.07	1.83	-184.24
F0910	40.47.480	111.54.820	4218.71	979812.43	980250.93	-41.69	-185.42	1.99	-183.42
F0911	40.47.480	111.54.700	4221.70	979813.13	980250.93	-40.71	-184.54	2.14	-182.40
F0912	40.47.480	111.54.510	4223.17	979814.58	980250.93	-39.12	-183.00	2.46	-180.54
F0913	40.47.480	111.54.440	4222.35	979815.04	980250.93	-38.74	-182.59	2.65	-179.94
F0914	40.47.480	111.54.350	4227.64	979815.52	980250.93	-37.76	-181.79	2.90	-178.89
F0915	40.47.480	111.54.260	4239.03	979815.63	980250.93	-36.67	-181.06	3.11	-177.95
F0916	40.47.480	111.54.160	4251.50	979815.71	980250.93	-35.32	-180.17	3.25	-176.92
F0917	40.47.480	111.54.040	4266.38	979816.18	980250.93	-33.45	-178.81	3.53	-175.27
F0918	40.47.480	111.53.930	4333.46	979813.35	980250.93	-29.97	-177.61	3.51	-174.10
F0919	40.47.470	111.53.660	4833.14	979782.74	980250.92	-13.58	-178.24	3.15	-175.11
F1001	40.47.230	111.56.320	4213.69	979808.04	980250.57	-46.19	-189.75	.99	-188.76
F1002	40.47.200	111.55.960	4216.53	979807.63	980250.52	-46.29	-189.94	1.11	-188.83
F1003	40.47.200	111.55.750	4218.09	979807.65	980250.52	-46.12	-189.83	1.20	-188.63
F1004	40.47.200	111.55.550	4218.74	979808.05	980250.52	-45.66	-189.39	1.27	-188.12
F1005	40.47.200	111.55.310	4216.96	979808.34	980250.52	-45.04	-188.70	1.41	-187.29
F1006	40.47.200	111.55.170	4216.32	979809.49	980250.52	-44.45	-188.09	1.50	-186.59
F1007	40.47.200	111.55.030	4217.29	979810.14	980250.52	-43.70	-187.38	1.60	-185.78
F1008	40.47.210	111.54.920	4218.18	979810.91	980250.54	-42.97	-186.68	1.68	-185.00
F1009	40.47.210	111.54.820	4220.24	979811.30	980250.54	-42.28	-186.06	1.77	-184.29
F1010	40.47.210	111.54.690	4228.34	979811.70	980250.54	-41.12	-185.18	1.86	-183.32
F1011	40.47.200	111.54.580	4219.32	979812.92	980250.52	-40.73	-184.48	2.04	-182.44
F1012	40.47.200	111.54.500	4220.64	979813.62	980250.52	-39.91	-183.70	2.21	-181.49
F1013	40.47.200	111.54.360	4221.71	979814.26	980250.52	-39.17	-183.00	2.38	-180.62
F1014	40.47.210	111.54.250	4227.65	979814.95	980250.54	-37.94	-181.97	2.62	-179.35

STÁT.	LATITUDE	LONGITUDE	ELEV.	OPSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
F1015	40.47.210	111.54.150	4230.94	979815.65	980250.54	-36.93	-181.07	2.80	-178.27
F1016	40.47.210	111.54.040	4239.75	979815.94	980250.54	-35.81	-180.25	3.19	-177.06
F1017	40.47.220	111.53.940	4252.79	979815.92	980250.55	-34.62	-179.51	3.37	-176.14
F1018	40.47.220	111.53.830	4285.55	979814.94	980250.55	-32.52	-178.52	3.48	-175.04
F1019	40.47.210	111.53.720	4404.99	979808.25	980250.54	-27.96	-178.03	2.63	-175.40
F1020	40.47.240	111.53.450	4767.56	979735.49	980250.59	-16.66	-179.08	2.54	-176.55
F1101	40.46.820	111.56.320	4217.95	979805.59	980249.95	-47.62	-191.32	.94	-190.38
F1102	40.46.820	111.55.900	4219.45	979805.14	980249.95	-47.93	-191.68	1.06	-190.62
F1103	40.46.820	111.55.750	4218.64	979805.33	980249.95	-47.82	-191.54	1.13	-190.41
F1104	40.46.820	111.55.480	4218.16	979805.79	980249.95	-47.40	-191.11	1.22	-189.89
F1105	40.46.820	111.55.220	4217.46	979806.65	980249.95	-46.61	-190.29	1.34	-188.95
F1106	40.46.820	111.54.980	4217.03	979807.99	980249.95	-45.30	-188.98	1.45	-187.53
F1107	40.46.820	111.54.800	4217.37	979809.03	980249.95	-44.24	-187.92	1.57	-186.35
F1108	40.46.820	111.54.620	4219.15	979810.11	980249.95	-42.99	-186.73	1.68	-185.05
F1109	40.46.820	111.54.550	4221.06	979810.49	980249.95	-42.43	-186.24	1.74	-184.50
F1110	40.46.820	111.54.450	4221.46	979811.26	980249.95	-41.62	-185.44	1.82	-183.62
F1111	40.46.820	111.54.350	4222.91	979812.08	980249.95	-40.67	-184.54	1.93	-182.61
F1112	40.46.820	111.54.230	4226.11	979812.58	980249.95	-39.76	-183.75	2.07	-181.67
F1113	40.46.820	111.54.110	4232.74	979813.14	980249.95	-38.68	-182.89	2.13	-180.76
F1114	40.46.820	111.53.980	4238.80	979813.63	980249.95	-37.62	-182.03	2.29	-179.74
F1115	40.46.820	111.53.880	4245.96	979813.70	980249.95	-36.88	-181.53	2.40	-179.13
F1116	40.46.810	111.53.770	4278.40	979812.31	980249.95	-35.21	-180.97	2.37	-178.60
F1117	40.46.800	111.53.670	4311.37	979810.13	980249.93	-34.27	-181.16	2.24	-178.92
F1118	40.46.800	111.53.560	4360.71	979806.76	980249.93	-33.00	-181.57	2.12	-179.45
F1119	40.46.790	111.53.420	4481.79	979799.34	980249.91	-29.02	-181.71	1.91	-179.80
F1120	40.46.800	111.53.310	4523.64	979796.58	980249.93	-27.86	-181.97	1.94	-180.03
F1121	40.46.800	111.53.200	4577.29	979793.28	980249.93	-26.11	-182.05	2.06	-179.99
F1122	40.46.790	111.53.080	4584.10	979792.64	980249.91	-26.09	-182.27	2.03	-180.24
F1201	40.46.300	111.56.310	4220.29	979802.81	980249.19	-49.42	-193.20	.89	-192.31
F1202	40.46.300	111.55.950	4220.43	979802.42	980249.19	-49.79	-193.53	.98	-192.60
F1203	40.46.300	111.55.730	4221.22	979802.13	980249.19	-50.01	-193.82	1.05	-192.77
F1204	40.46.300	111.55.510	4223.49	979802.00	980249.19	-49.93	-193.82	1.10	-192.72
F1205	40.46.300	111.55.280	4222.19	979802.42	980249.19	-49.63	-193.47	1.18	-192.29

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
F1206	40.46.300	111.55.060	4221.82	979803.03	980249.19	-49.05	-192.89	1.25	-191.64
F1207	40.46.300	111.54.790	4222.76	979804.05	980249.19	-47.95	-191.81	1.36	-190.45
F1208	40.46.300	111.54.580	4226.58	979804.36	980249.19	-46.68	-190.67	1.44	-189.23
F1209	40.46.300	111.54.440	4232.11	979805.49	980249.19	-45.62	-189.81	1.50	-188.31
F1210	40.46.290	111.54.300	4243.74	979805.37	980249.17	-44.64	-189.22	1.53	-187.69
F1211	40.46.290	111.54.200	4250.54	979805.74	980249.17	-43.63	-188.44	1.56	-186.88
F1212	40.46.290	111.54.110	4258.64	979805.66	980249.17	-42.94	-188.03	1.59	-186.44
F1213	40.46.300	111.54.020	4269.57	979805.74	980249.19	-41.85	-187.31	1.62	-185.69
F1214	40.46.300	111.53.920	4277.95	979805.59	980249.19	-41.21	-186.96	1.65	-185.31
F1215	40.46.300	111.53.760	4295.09	979805.08	980249.19	-40.11	-186.44	1.70	-184.74
F1216	40.46.300	111.53.680	4304.12	979804.80	980249.19	-39.54	-186.18	1.72	-184.46
F1217	40.46.300	111.53.600	4312.16	979804.54	980249.19	-39.05	-185.96	1.74	-184.22
F1218	40.46.300	111.53.510	4325.25	979803.74	980249.19	-38.61	-185.97	1.78	-184.19
F1219	40.46.300	111.53.410	4337.36	979803.13	980249.19	-38.09	-185.85	1.80	-184.06
F1220	40.46.300	111.53.300	4352.72	979802.16	980249.19	-37.61	-185.90	1.83	-184.07
F1221	40.46.300	111.53.180	4369.76	979801.29	980249.19	-36.88	-185.75	1.85	-183.90
F1222	40.46.300	111.53.110	4390.48	979799.23	980249.19	-36.99	-186.57	1.84	-184.73
F1223	40.46.300	111.52.970	4436.74	979797.04	980249.19	-34.83	-185.98	1.84	-184.14
F1224	40.46.300	111.52.870	4442.20	979796.84	980249.19	-34.51	-185.85	1.89	-183.97
F1225	40.46.300	111.52.790	4429.66	979797.76	980249.19	-34.77	-185.69	1.95	-183.74
F1226	40.46.300	111.52.700	4425.58	979798.18	980249.19	-34.74	-185.51	2.03	-183.45
F1227	40.46.300	111.52.600	4426.58	979798.36	980249.19	-34.46	-185.27	2.10	-183.17
FBECK	40.48.950	111.55.060	4247.19	979823.24	980253.13	-30.40	-175.10	3.18	-171.92
FX101	40.32.180	111.29.700	5863.02	979656.45	980228.20	-20.27	-220.02	5.86	-214.16
FX102	40.32.180	111.29.560	5800.60	979659.62	980228.20	-22.97	-220.59	5.87	-214.72
FX103	40.32.190	111.29.420	5783.13	979660.59	980228.21	-23.66	-220.68	5.57	-215.11
FX104	40.32.190	111.29.280	5765.20	979661.33	980228.21	-24.61	-221.02	5.37	-215.65
FX105	40.32.190	111.29.130	5751.15	979662.01	980228.21	-25.25	-221.18	5.17	-216.01
FX106	40.32.190	111.29.000	5746.65	979662.03	980228.21	-25.65	-221.43	5.07	-216.36
FX107	40.32.190	111.28.850	5970.32	979648.03	980228.21	-18.61	-222.01	4.02	-218.00
FX108	40.32.190	111.28.710	5810.67	979658.24	980228.21	-23.42	-221.38	4.24	-217.14
FX109	40.32.190	111.28.570	5730.69	979663.02	980228.21	-26.16	-221.40	4.70	-216.70
FX110	40.32.190	111.28.430	5734.19	979662.55	980228.21	-26.30	-221.66	4.54	-217.12

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
FX111	40.32.190	111.28.280	5738.51	979662.93	980228.21	-25.52	-221.02	4.46	-216.55
FX112	40.32.190	111.28.140	5719.32	979663.74	980228.21	-26.51	-221.36	4.39	-216.97
FX113	40.32.190	111.28.000	5811.21	979657.81	980228.21	-23.80	-221.73	3.58	-218.20
FX114	40.32.190	111.27.860	6013.97	979644.74	980228.21	-17.80	-222.69	3.58	-219.11
FX201	40.31.840	111.29.820	6008.04	979649.35	980227.69	-13.22	-217.91	5.08	-212.83
FX202	40.31.800	111.29.690	5925.62	979651.92	980227.63	-18.35	-220.23	5.07	-215.16
FX203	40.31.750	111.29.570	5869.51	979654.58	980227.55	-20.89	-220.86	5.02	-215.84
FX204	40.31.760	111.29.430	5805.98	979657.22	980227.57	-24.24	-222.04	4.96	-217.08
FX205	40.31.810	111.29.200	5743.35	979661.17	980227.64	-26.25	-221.92	4.66	-217.26
FX206	40.31.800	111.29.070	5698.29	979663.40	980227.63	-28.25	-222.39	4.66	-217.73
FX207	40.31.800	111.28.920	5692.69	979663.79	980227.63	-28.39	-222.33	4.40	-217.93
FX208	40.31.800	111.28.780	5690.63	979664.09	980227.63	-28.28	-222.16	4.20	-217.96
FX209	40.31.750	111.28.660	5685.15	979664.14	980227.55	-28.67	-222.36	4.02	-218.34
FX210	40.31.750	111.28.520	5683.18	979664.21	980227.55	-28.79	-222.41	3.88	-218.52
FX211	40.31.750	111.28.380	5671.25	979664.96	980227.55	-29.16	-222.37	3.80	-218.57
FX212	40.31.750	111.28.230	5642.91	979666.92	980227.55	-29.86	-222.11	3.89	-218.22
FX213	40.31.750	111.28.090	5639.01	979667.23	980227.55	-29.92	-222.03	3.74	-218.30
FX214	40.31.750	111.27.950	5633.68	979667.68	980227.55	-29.97	-221.91	3.64	-218.26
FX215	40.31.750	111.27.810	5627.16	979668.68	980227.55	-29.58	-221.30	3.56	-217.74
FX216	40.31.730	111.27.680	5617.99	979670.23	980227.53	-28.87	-220.27	3.47	-216.80
FX217	40.31.750	111.27.530	5607.78	979670.49	980227.55	-29.60	-220.65	3.37	-217.28
FX218	40.31.760	111.27.390	5599.28	979670.57	980227.57	-30.33	-221.09	3.27	-217.82
FX301	40.31.310	111.29.850	5985.62	979646.40	980226.90	-17.49	-221.42	5.10	-216.32
FX302	40.31.310	111.29.710	5904.91	979651.53	980226.90	-19.95	-221.13	4.96	-216.17
FX303	40.31.310	111.29.570	5824.58	979655.86	980226.90	-23.18	-221.62	4.97	-216.65
FX304	40.31.310	111.29.430	5766.32	979659.31	980226.90	-25.21	-221.66	4.83	-216.83
FX305	40.31.310	111.29.280	5714.35	979661.26	980226.90	-28.15	-222.83	4.62	-218.21
FX306	40.31.310	111.29.140	5706.95	979661.44	980226.90	-28.66	-223.09	4.30	-218.79
FX307	40.31.310	111.29.000	5684.04	979662.74	980226.90	-29.52	-223.17	4.14	-219.03
FX308	40.31.310	111.28.860	5635.47	979665.77	980226.90	-31.06	-223.05	4.11	-218.94
FX309	40.31.310	111.28.720	5638.14	979665.51	980226.90	-31.07	-223.15	3.85	-219.30
FX310	40.31.310	111.28.580	5636.04	979665.52	980226.90	-31.25	-223.27	3.68	-219.59
FX311	40.31.310	111.28.430	5633.64	979665.75	980226.90	-31.25	-223.18	3.52	-219.66

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
FX312	40.31.310	111.28.290	5631.00	979665.94	980226.90	-31.31	-223.15	3.39	-219.76
FX313	40.31.310	111.28.150	5634.00	979665.66	980226.90	-31.30	-223.25	3.26	-219.99
FX314	40.31.310	111.28.010	5634.11	979665.45	980226.90	-31.50	-223.45	3.16	-220.29
FX315	40.31.310	111.27.870	5641.07	979666.41	980226.90	-29.89	-222.08	3.05	-219.02
FX316	40.31.310	111.27.730	5619.40	979668.24	980226.90	-30.10	-221.55	3.02	-218.52
FX317	40.31.310	111.27.580	5606.66	979668.74	980226.90	-30.80	-221.81	2.96	-218.85
FX318	40.31.310	111.27.440	5587.68	979669.75	980226.90	-31.57	-221.94	2.94	-219.00
FX319	40.31.310	111.27.300	5574.38	979670.48	980226.90	-32.09	-222.01	2.90	-219.11
FX401	40.30.910	111.29.430	5890.67	979652.05	980226.30	-20.18	-220.87	4.19	-216.68
FX402	40.30.920	111.29.280	5723.91	979661.72	980226.32	-26.21	-221.22	4.33	-216.89
FX403	40.30.920	111.29.130	5635.60	979665.89	980226.32	-30.35	-222.34	4.46	-217.89
FX404	40.30.920	111.28.990	5594.25	979667.91	980226.32	-32.22	-222.81	4.33	-218.48
FX405	40.30.920	111.28.850	5597.11	979667.51	980226.32	-32.35	-223.03	4.00	-219.03
FX406	40.30.920	111.28.710	5603.71	979667.11	980226.32	-32.12	-223.04	3.72	-219.32
FX407	40.30.920	111.28.570	5613.04	979666.58	980226.32	-31.78	-223.01	3.50	-219.51
FX408	40.30.930	111.28.430	5608.65	979666.92	980226.34	-31.87	-222.95	3.37	-219.58
FX409	40.30.930	111.28.280	5606.25	979667.19	980226.34	-31.83	-222.83	3.25	-219.58
FX410	40.30.930	111.28.150	5600.23	979667.38	980226.34	-31.71	-222.50	3.15	-219.35
FX411	40.30.930	111.28.000	5607.36	979668.28	980226.34	-31.29	-222.09	3.03	-219.06
FX412	40.30.930	111.27.860	5600.16	979668.85	980226.34	-30.74	-221.53	2.95	-218.58
FX413	40.30.930	111.27.720	5685.42	979663.87	980226.34	-27.70	-221.40	2.95	-218.45
FX414	40.30.930	111.27.580	5628.03	979667.81	980226.34	-29.16	-220.90	2.76	-218.14
FX415	40.30.930	111.27.430	5568.55	979671.34	980226.34	-31.23	-220.94	2.78	-218.16
FX416	40.30.930	111.27.280	5556.68	979671.55	980226.34	-32.13	-221.44	2.74	-218.70
FX501	40.30.440	111.29.140	5659.33	979666.33	980225.62	-26.97	-219.78	4.05	-215.73
FX502	40.30.440	111.29.010	5544.16	979673.32	980225.62	-30.81	-219.70	4.35	-215.35
FX503	40.30.440	111.28.870	5546.26	979672.22	980225.62	-31.72	-220.67	3.98	-216.69
FX504	40.30.440	111.28.730	5551.81	979671.29	980225.62	-32.12	-221.27	3.69	-217.58
FX505	40.30.440	111.28.580	5537.50	979671.97	980225.62	-32.79	-221.45	3.54	-217.91
FX506	40.30.440	111.28.440	5537.00	979672.34	980225.62	-32.47	-221.11	3.37	-217.74
FX507	40.30.440	111.28.300	5533.82	979672.93	980225.62	-32.18	-220.71	3.25	-217.46
FX508	40.30.440	111.28.160	5528.93	979673.29	980225.62	-32.28	-220.64	3.14	-217.50
FX509	40.30.440	111.28.020	5529.76	979673.45	980225.62	-32.04	-220.43	3.03	-217.40

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
FX510	40.30.430	111.27.880	5534.00	979673.21	980225.60	-31.86	-220.40	2.90	-217.50
FX511	40.30.430	111.27.730	5535.88	979672.67	980225.60	-32.23	-220.83	2.82	-218.01
FX512	40.30.440	111.27.590	5534.39	979672.67	980225.62	-32.38	-220.93	2.75	-218.18
FX513	40.30.440	111.27.450	5533.74	979672.74	980225.62	-32.37	-220.90	2.69	-218.21
FX514	40.30.440	111.27.310	5529.94	979672.79	980225.62	-32.68	-221.08	2.65	-218.43
FX515	40.30.440	111.27.170	5527.96	979672.74	980225.62	-32.92	-221.25	2.60	-218.65
FX516	40.30.440	111.27.030	5485.33	979675.59	980225.62	-34.08	-220.96	2.70	-218.26
FXGW1	40.31.820	111.28.850	5702.08	979663.87	980227.66	-27.45	-221.71	4.26	-217.45
FXGW2	40.32.020	111.28.400	5707.59	979663.90	980227.96	-27.20	-221.66	4.21	-217.45
FXGW4	40.30.610	111.27.500	5539.54	979672.58	980225.87	-32.24	-220.97	2.76	-218.20
UBASE	40.45.800	111.50.900	4675.00	979786.18	980248.44	-22.53	-181.80	2.46	-179.34
78401	40.36.220	111.49.950	4619.00	979753.58	980234.20	-46.16	-203.52	3.49	-200.03
78402	40.38.170	111.41.860	6709.00	979618.65	980237.10	12.60	-215.97	16.23	-199.74
78403	40.38.030	111.42.670	6490.00	979633.48	980236.90	7.03	-214.08	17.20	-196.88
78404	40.38.070	111.43.400	6213.00	979651.58	980236.95	-.98	-212.65	19.54	-193.11
78405	40.37.560	111.44.470	5816.00	979673.93	980236.20	-15.22	-213.36	22.66	-190.70
78406	40.37.390	111.44.660	5744.00	979676.98	980235.94	-18.78	-214.47	28.08	-186.39
78407	40.37.300	111.45.130	5452.00	979695.29	980235.80	-27.70	-213.44	30.12	-183.32
78408	40.37.410	111.45.710	5290.00	979706.43	980235.97	-31.96	-212.19	25.67	-186.52
78409	40.37.230	111.46.300	5120.00	979718.20	980235.70	-35.92	-210.35	21.35	-189.00
78410	40.37.110	111.46.850	4990.00	979732.05	980235.53	-34.13	-204.13	15.57	-188.56
78411	40.37.150	111.47.320	4900.00	979741.47	980235.59	-33.22	-200.16	10.48	-189.68
78412	40.37.200	111.47.610	4875.00	979746.92	980235.66	-30.29	-196.38	8.25	-188.13
78415	40.37.430	111.48.190	4830.00	979749.21	980236.01	-32.49	-197.04	5.94	-191.10
78416	40.37.440	111.48.870	4782.00	979751.62	980236.02	-34.61	-197.53	4.53	-193.00
78417	40.37.440	111.49.440	4600.00	979762.96	980236.02	-40.38	-197.10	3.96	-193.14
78418	40.37.510	111.50.540	4498.00	979768.09	980236.12	-44.96	-198.20	2.85	-195.35
78419	40.37.570	111.51.240	4430.00	979771.62	980236.21	-47.90	-198.83	2.43	-196.40
78420	40.37.900	111.51.230	4405.00	979774.34	980236.70	-48.02	-198.09	2.45	-195.64
78421	40.37.920	111.52.280	4396.00	979773.25	980236.73	-49.99	-199.76	1.92	-197.84
78422	40.37.980	111.53.830	4336.00	979777.70	980236.83	-51.29	-199.01	1.44	-197.57
78423	40.37.920	111.54.540	4321.00	979780.59	980236.73	-49.71	-196.92	1.24	-195.68 *
78424	40.37.790	111.55.700	4362.00	979776.19	980236.53	-50.05	-198.66	1.11	-197.55

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE FOUQUER	T.C.	COMPLETE FOUQUER
78101	40.43.570	111.56.620	4236.00	979805.96	980245.12	-40.72	-185.04	.74	-184.30*
78102	40.43.550	111.55.360	4230.00	979794.16	980245.09	-53.05	-197.16	.92	-196.24
78103	40.43.560	111.57.430	4233.00	979799.09	980245.10	-47.86	-192.07	.66	-191.41
78104	40.43.530	111.58.030	4239.00	979800.99	980245.06	-45.35	-189.77	.61	-189.16
78105	40.43.540	111.58.590	4239.00	979803.06	980245.08	-43.30	-187.72	.57	-187.15
78106	40.43.540	111.59.170	4245.00	979805.28	980245.08	-40.52	-185.14	.54	-184.60*
78107	40.43.550	112. . . .250	4244.00	979810.86	980245.09	-35.03	-179.62	.55	-179.07
78108	40.43.550	112. . . .980	4247.00	979813.94	980245.09	-31.67	-176.36	.48	-175.88
78109	40.43.550	112. . . .1.440	4241.00	979816.26	980245.09	-29.91	-174.40	.48	-173.92
78110	40.43.540	112. . . .2.110	4241.00	979818.51	980245.08	-27.66	-172.15	.48	-171.67
78111	40.43.230	112. . . .2.970	4240.00	979818.48	980244.61	-27.32	-171.77	.54	-171.23
78112	40.43.100	112. . . .3.750	4235.00	979819.44	980244.42	-26.64	-170.92	.64	-170.28
78113	40.43.090	112. . . .4.900	4234.00	979820.15	980244.41	-26.00	-170.25	.79	-169.46
78114	40.43.070	112. . . .6.260	4241.00	979823.66	980244.37	-21.80	-166.29	1.23	-165.06
78115	40.42.980	112. . . .7.320	4329.00	979819.44	980244.24	-17.62	-165.10	2.16	-162.94
78116	40.43.090	112. . . .5.460	4237.00	979820.83	980244.41	-25.04	-169.39	.92	-168.47
78117	40.43.360	112.13.430	4238.00	979829.87	980244.81	-16.32	-160.70	3.03	-157.67
78118	40.43.200	112. . . .8.920	4341.00	979823.46	980244.56	-12.79	-160.68	2.78	-157.90
78201	40.43.550	111.56.630	4236.00	979796.93	980245.09	-49.71	-194.03	.74	-193.29*
78202	40.43.530	111.55.380	4230.00	979794.31	980245.06	-52.88	-196.99	.92	-196.07
78203	40.43.550	111.57.450	4235.00	979799.27	980245.09	-47.47	-191.75	.66	-191.09
78204	40.43.550	111.54.480	4236.00	979793.79	980245.09	-52.85	-197.17	1.08	-196.09
78205	40.43.600	111.53.600	4241.00	979793.67	980245.16	-52.58	-197.07	1.29	-195.78
78206	40.43.450	111.53.150	4277.00	979793.08	980244.95	-49.57	-195.28	1.36	-193.92
78207	40.43.500	111.52.040	4315.00	979792.59	980245.02	-46.55	-193.56	1.73	-191.83
78208	40.43.600	111.51.330	4391.00	979790.23	980245.16	-41.91	-191.51	1.95	-189.56
78209	40.43.530	111.50.630	4472.00	979786.60	980245.06	-37.82	-190.13	2.22	-187.96
78210	40.43.430	111.49.430	4599.00	979781.96	980244.91	-30.38	-187.06	3.09	-183.97
78211	40.42.470	111.48.850	4702.00	979775.41	980243.48	-25.81	-186.00	3.40	-182.60
78213	40.42.390	111.47.690	4941.00	979761.35	980243.37	-16.77	-185.10	5.31	-179.79
78212	40.42.460	111.48.280	4821.00	979768.70	980243.47	-21.30	-185.55	4.06	-181.49
78214	40.43.000	111.47.000	4913.00	979755.57	980244.27	-26.59	-193.97	12.03	-181.94
78215	40.43.450	111.46.310	5021.00	979747.29	980244.95	-25.38	-196.44	16.77	-179.67

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE FOUGUER
78216	40.43.950	111.45.200	5213.00	979737.20	980245.69	-18.15	-195.75	14.11	-181.64
78217	40.44.550	111.47.470	5350.00	979729.13	980246.58	-14.23	-196.50	8.22	-188.29
78218	40.45.270	111.42.620	5564.00	979714.38	980247.66	-9.93	-199.49	4.39	-195.10
78301	40.34.830	111.50.580	4787.00	979736.50	980232.13	-45.27	-208.36	2.93	-205.43
78302	40.34.350	111.46.730	5350.00	979693.24	980231.42	-34.96	-217.23	19.91	-197.32
78303	40.34.300	111.46.260	5480.00	979679.28	980231.34	-36.61	-223.31	25.30	-198.01
78304	40.34.570	111.40.740	7704.00	979551.06	980231.76	43.94	-218.53	17.72	-200.81
78305	40.34.330	111.41.990	7200.00	979574.34	980231.39	20.18	-225.12	18.30	-206.82
78306	40.34.360	111.43.540	6493.00	979611.04	980231.43	-9.66	-230.87	32.48	-198.39
78307	40.34.280	111.44.510	6054.00	979635.84	980231.32	-26.04	-232.29	36.06	-196.23
78308	40.34.320	111.45.480	5740.00	979657.11	980231.37	-34.36	-229.92	29.59	-200.33
78309	40.34.330	111.45.840	5620.00	979667.24	980231.39	-35.53	-227.00	27.39	-199.61
78310	40.34.390	111.47.340	5270.00	979706.04	980231.48	-29.74	-209.28	11.56	-197.72
78311	40.34.390	111.47.860	5219.00	979711.31	980231.48	-29.26	-207.07	7.80	-199.27
78312	40.34.680	111.48.290	5138.00	979718.06	980231.91	-30.57	-205.62	6.27	-199.35
78313	40.34.570	111.49.030	5011.00	979724.20	980231.76	-36.22	-206.94	4.75	-202.19
78314	40.34.840	111.50.000	4804.00	979736.16	980232.15	-44.12	-207.79	3.44	-204.35
78315	40.34.850	111.51.150	4725.00	979739.80	980232.16	-47.93	-208.91	2.65	-206.26
78316	40.34.850	111.52.280	4520.00	979753.39	980232.16	-53.62	-207.61	2.05	-205.56
78317	40.35.280	111.53.890	4367.00	979765.36	980232.80	-56.68	-205.46	1.53	-203.93
78318	40.34.830	111.53.400	4466.00	979756.53	980232.13	-55.43	-207.58	1.64	-205.94
78319	40.34.830	111.54.280	4368.00	979763.70	980232.13	-57.58	-206.39	1.49	-204.90
78320	40.35.280	111.54.280	4357.00	979756.21	980232.80	-56.77	-205.21	1.47	-203.74
78321	40.35.260	111.55.700	4364.00	979766.01	980232.77	-56.28	-204.96	1.19	-203.77
78322	40.35.260	111.56.850	4444.00	979761.84	980232.77	-52.93	-204.33	.95	-203.39
78324	40.35.270	111.59.140	4626.00	979752.64	980232.79	-45.03	-202.63	.77	-201.86
MBE01	40.31.370	112. 5.600	5519.00	979700.75	980226.98	-7.11	-195.14	2.05	-193.09
MBE02	40.31.560	112. 6.950	7057.00	979668.87	980227.28	105.37	-135.05	16.35	-118.70
MBE03	40.31.050	112. 7.820	7150.00	979600.39	980226.52	46.69	-196.90	7.62	-189.29
MBE04	40.30.070	112. 8.220	7090.00	979608.98	980225.06	50.80	-190.75	5.29	-185.46
MBE05	40.30.610	112. 8.390	7401.00	979587.63	980225.87	57.91	-194.24	8.86	-185.38
MBE06	40.30.830	112.10.090	6990.00	979618.54	980226.19	49.83	-188.31	8.50	-179.81
MBE07	40.31.450	112. 9.700	6465.00	979648.45	980227.12	29.43	-190.83	8.59	-182.24

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
MBE08	40.31.970	112. 8.780	6083.00	979672.31	980227.89	16.58	-190.66	6.86	-183.80
MBE09	40.31.300	112. 9.000	5641.00	979683.12	980226.88	-13.17	-205.35	21.38	-183.97
MBE10	40.32.370	112. 8.850	5961.00	979677.29	980228.43	9.50	-193.58	8.95	-184.63
MBE11	40.33.780	112. 7.690	5970.00	979682.59	980230.57	13.56	-189.83	3.31	-186.52
MBE12	40.34.080	112. 8.990	6408.00	979655.21	980231.02	26.92	-191.39	5.80	-185.59
MBE13	40.34.000	112.10.320	7120.00	979615.71	980230.91	54.51	-188.06	7.73	-180.33
MBE14	40.42.870	112.11.060	4816.00	979791.08	980244.09	-.01	-164.09	3.51	-160.58
MBE15	40.39.190	112.12.040	8853.00	979505.82	980238.62	99.91	-201.70	36.45	-165.25
MBE16	40.39.590	112.12.100	9054.00	979488.00	980239.22	100.40	-208.06	43.08	-164.93
MBE17	40.40.080	112.12.100	8181.00	979564.18	980239.95	93.74	-184.98	19.34	-165.64
MBE18	40.39.280	112. 6.670	5193.00	979745.87	980238.75	-4.43	-181.35	2.44	-178.91*
MBE19	40.30.010	112.14.220	9068.00	979472.28	980224.93	100.24	-208.70	51.02	-157.68
MBE21	40.30.480	112.10.500	5977.00	979669.45	980225.68	5.97	-197.66	40.33	-157.33
MBE22	40.30.480	112.16.160	5218.00	979720.34	980225.68	-14.04	-191.81	14.12	-177.69
MBE23	40.31.340	112.16.190	5427.00	979708.50	980226.95	-7.98	-192.87	3.32	-189.25
MBE24	40.31.900	112.16.390	5191.00	979724.80	980227.77	-14.71	-191.56	3.07	-188.49
MBE25	40.32.560	112.16.400	5044.00	979736.64	980228.77	-17.69	-189.53	2.58	-186.95
MBE26	40.33.080	112.16.410	4947.00	979741.50	980229.54	-22.62	-191.16	2.30	-188.86
MBE27	40.33.060	112.17.830	4857.00	979748.77	980229.51	-23.89	-189.36	1.63	-187.73
MBE28	40.30.070	112.17.220	5451.00	979706.26	980225.06	-6.08	-191.79	6.40	-185.39
MBE29	40.30.820	112.17.800	5254.00	979720.93	980226.17	-11.05	-190.05	3.61	-186.44
MBE30	40.31.150	112.17.940	5176.00	979726.42	980226.66	-13.39	-189.73	2.65	-187.08
MBE31	40.39.170	112.14.230	5166.00	979760.11	980238.59	7.44	-168.56	7.57	-160.99
MBE32	40.39.170	112.14.820	4748.00	979735.44	980238.59	-6.55	-168.31	4.93	-163.33
MBE33	40.39.170	112.15.960	4508.00	979799.58	980238.59	-14.99	-168.57	2.52	-166.05
MBE34	40.39.200	112.16.500	4445.00	979805.46	980238.63	-15.07	-166.51	2.01	-164.50
MBE35	40.39.200	112.17.330	4283.00	979814.29	980238.63	-21.48	-167.40	1.45	-165.95
MBE36	40.38.650	112.18.510	4263.00	979808.95	980237.82	-27.89	-173.13	.98	-172.15
MBE37	40.22.490	112.18.800	4878.00	979746.80	980213.81	-8.19	-174.38	16.87	-157.51
MBE38	40.31.610	112.18.800	5002.00	979736.35	980227.35	-20.52	-190.93	1.80	-189.13
MBE39	40.36.470	112. 9.560	6466.00	979524.30	980234.58	-102.09	-322.38	21.41	-300.97*
MBE40	40.36.250	112.10.260	8609.00	979515.34	980234.25	90.85	-202.45	21.93	-180.52
MBE41	40.36.800	112.11.200	9359.00	979457.42	980235.06	102.66	-216.19	40.06	-176.13

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
F0501	40.48.540	111.56.590	4210.23	979814.78	980252.52	-41.73	-185.17	1.03	-184.14
F0502	40.48.540	111.56.380	4211.79	979814.06	980252.52	-42.30	-185.79	1.13	-184.66
F0503	40.48.540	111.56.160	4211.53	979813.90	980252.52	-42.49	-185.97	1.26	-184.71
F0504	40.48.540	111.55.940	4211.53	979813.87	980252.52	-42.52	-186.00	1.40	-184.60
F0505	40.48.530	111.55.830	4211.12	979813.95	980252.51	-42.46	-185.93	1.52	-184.41
F0506	40.48.530	111.55.730	4210.15	979814.25	980252.51	-42.25	-185.69	1.63	-184.06
F0507	40.48.530	111.55.620	4212.83	979814.33	980252.51	-41.92	-185.45	1.71	-183.74
F0508	40.48.530	111.55.510	4212.33	979815.03	980252.51	-41.27	-184.78	1.85	-182.93
F0509	40.48.530	111.55.390	4214.38	979815.82	980252.51	-40.28	-183.86	2.09	-181.77
F0510	40.48.530	111.55.290	4211.13	979816.98	980252.51	-39.43	-182.90	2.40	-180.50
F0511	40.48.530	111.55.190	4211.88	979818.47	980252.51	-37.87	-181.36	2.63	-178.73
F0512	40.48.530	111.55.080	4237.44	979818.64	980252.51	-35.29	-179.66	2.73	-176.93
F0513	40.48.530	111.54.970	4239.65	979820.13	980252.51	-33.60	-178.04	3.21	-174.83
F0514	40.48.530	111.54.860	4259.66	979819.98	980252.51	-31.86	-176.99	3.96	-173.03
F0515	40.48.520	111.54.600	4671.94	979794.51	980252.49	-18.44	-177.61	2.61	-175.00
F0601	40.48.290	111.56.390	4209.00	979813.26	980252.14	-42.98	-186.38	1.11	-185.27
F0602	40.48.290	111.56.170	4210.60	979812.90	980252.14	-43.19	-186.64	1.23	-185.41
F0603	40.48.290	111.55.930	4211.45	979812.75	980252.14	-43.26	-186.74	1.37	-185.37
F0604	40.48.290	111.55.850	4211.03	979812.80	980252.14	-43.25	-186.72	1.44	-185.28
F0605	40.48.290	111.55.730	4210.62	979812.92	980252.14	-43.17	-186.62	1.55	-185.07
F0606	40.48.290	111.55.640	4210.88	979813.11	980252.14	-42.95	-186.42	1.62	-184.80
F0607	40.48.280	111.55.530	4215.46	979813.13	980252.12	-42.49	-186.10	1.74	-184.36
F0608	40.48.280	111.55.420	4216.94	979813.53	980252.12	-41.95	-185.62	1.86	-183.76
F0609	40.48.280	111.55.310	4219.43	979814.03	980252.12	-41.22	-184.97	2.04	-182.93
F0610	40.48.280	111.55.190	4216.96	979815.73	980252.12	-39.75	-183.42	2.29	-181.12
F0611	40.48.270	111.55.080	4226.72	979816.07	980252.12	-38.48	-182.48	2.51	-179.97
F0612	40.48.270	111.54.960	4243.91	979816.27	980252.12	-36.66	-181.25	2.78	-178.47
F0613	40.48.270	111.54.890	4249.71	979816.80	980252.12	-35.59	-180.37	2.93	-177.44
F0614	40.48.280	111.54.780	4258.19	979817.72	980252.12	-33.88	-178.95	3.47	-175.48
F0615	40.48.290	111.54.640	4267.42	979818.00	980252.14	-32.75	-178.13	4.10	-174.03
F0616	40.48.240	111.54.260	4831.07	979785.13	980252.07	-12.53	-177.12	2.94	-174.18

Memo

March 7, 1980

①

To: Howard Ross

Copy for Howard Ross

Re: Open filing of principal facts of gravity data -- DOE funds.

Cooperative project: ESL, UGMS, & U. of Utah - G.G. Delta
Tentative plans

I. Phase I -- Jordan Valley -- March 1980 -- (UGMS interested)

A. Field work -- optional but desirable

Tie several base stations together - 1-2 days work only

B. Office work -- Surfa & Cook

Computers

NO terrain corrections

1st	1: 125,000	} sta. locations only
	1: 62,500	

(by mid-April)[#] Station locations + gravity values (simple Bouguer gravity values)

II. Phase II -- Wasatch Front -- April + 1st part of May 1980

continued:
(scale 1: 62,500)

A. Areas:

- 1) Utah Valley - UGMS interested
- 2) Juch Valley -- Cook "
- 3) From Salt Lake Salt to Idaho state line -- UGMS interested

B. Field work

Tie several base stations together - 1-2 days work only.

C. Office work -- Surfa & Cook

Computers

NO terrain corrections.

III. Phase III -- E $\frac{1}{4}$ of 1° x 2° sheets -- Delta, Tooele, Utah - May + early June

A. Office work -- Surfa & Cook

B. NO terrain corrections

IV. Phase IV -- June 1980 - Surfa & Cook

A. Terrain corrections of all of above data.

B. Complete (terrain-corrected) Bouguer gravity anomaly map - to be published by UGMS

Assumes Surfa full-time DOE during March 10 - 31, 1980

Funding

Scholarship - Surfs -
Student

Computers

Travel -

Administration

Technical supervision by Cook

Cook to report progress weekly to Howard Ross.

Surfs to work directly under supervision of Cook

Scheduling of Laura Surfs

(20 hrs/week)

\$8.00/hr ±

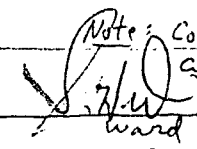

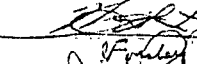
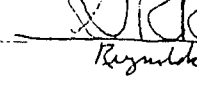
1980 Month	GG Debt 6.00/hr ±	DOE (20 hrs/week)	DMAAC #
March	yes*	Mar 10-31/80 yes	-
April	yes*	1/2-time	1/2 time ##
May	yes*	1/2-time	" ##
June	yes*	1/2-time	" ##

= Contingent on funding for Cooks from DMAAC. Would ~~cancel~~ cancel Surfs. funding ~~and~~ support requirement

* = funds available in Dept. and no funds from DMAAC

still pending for W. 3/4 of 1° x 2° sheet } Della Toole K.L. Cook

Approved

- 1)  ward
- 2)  Ross
- 3)  Ross
- 4)  Reynolds

Note: Cook may get some USGS funding for entire Brighton City 1° x 2° sheet. (still pending).

MEMORANDUM

March 27, 1981

TO: W. L. Forsberg
FROM: Kenneth L. Cook
SUBJECT: Deliverables for the UGMS project entitled:
"Gravity Data in the Wasatch Front, Utah area"

Attached herewith are three copies*(two for the UGMS and one for ESL files) of each of the following deliverables incident to the subject project:

1. Principal facts of all gravity stations in Jordan Valley, including terrain corrections.

Note: Each copy consists of three separate listings:

- a) Previous University of Utah stations, etc.1/
- b) New stations taken by Meiji Resource consultants during 1980.2/
- c) Special additional stations--repeat stations, closely gridded stations, and "bad" stations.3/

* Only one copy of the magnetic tape of the gravity data (for the UGMS) is included.

2. Worksheet maps (scale 1:62,500) of Jordan Valley containing locations of stations (represented by "x") on two separate maps for each area, on which are identified separately:

- a) Station number designations
- b) Complete Bouguer gravity anomaly values

Notes: a) A total of 4 maps in each set is included.
b) The maps are overlapped by:
7½-minute quadrangles common to each map area.

- 1/ List No. 1.
- 2/ List No. 2.
- 3/ List No. 3.

3. Complete Bouguer gravity anomaly map of Jordan Valley, Utah--professionally drafted.

Scale: 1:62,500

Contour interval: 2 milligals

4. One copy only of magnetic tape--for UGMS:

This tape includes a listing of the principal facts of all stations indicated in item 1 above.

These deliverables constitute the final task on this contract; and it is therefore understood that with the transmittal to you of these deliverables, our entire commitment on this project has therefore been fulfilled.* It should be noted that these deliverables were originally contracted for our delivery to the UGMS "by November 1, 1980," provided that the UGMS had submitted to K. L. Cook "by August 1, 1980" the listing of the principal facts of the new additional gravity stations. However, because the listing of the new additional gravity stations (actually taken by Meiji Resource Consultants) was not submitted to K. L. Cook until mid-November 1980, an extension was given us until the present time.

Kenneth L. Cook

Kenneth L. Cook

RECEIPT

This is to acknowledge safe receipt of all of the above-mentioned material.

W. L. Forsberg

W. L. Forsberg

March 27 1981

Date

* subject to the acceptance of all data by the UGMS,
constituting final acceptance of all deliverables.

KCC

Principal Facts of Gravity Stations,
Jordan Valley, Utah

by

J. I. Adhidjaja, K. L. Cook, and L. F. Serpa

March 25, 1981
Department of Geology and Geophysics
University of Utah
Salt Lake City, Utah 84112

Listing of Principal Facts of Gravity Stations,
Jordan Valley, Utah

For the reduction of the gravity data, the total elevation correction factor was taken as 0.05999 mgal/ft, which includes a free-air correction of 0.09406 mgal/ft and a Bouguer correction of 0.03407 mgal/ft for an assumed crustal density of 2.67 gm/cc. For theoretical gravity at mean sea level, the International Gravity Formula of 1930 was used. The data were tied to the values of the base stations in the gravity base station network in Utah (Cook et al., 1971). Terrain corrections were made using an assumed density of 2.67 gm/cc out to a radial distance of 100 miles (166.7 km) from each station using a computer terrain-correction program (Serpa, 1980).

Because the various surveys were conducted over several years and with different instruments, the accuracy of the various surveys will vary. However, the values of some stations have been adjusted.

The following is a listing of the station prefixes used in this listing and the sources of these gravity values. Where possible the estimated accuracy is also given. The following stations that were not used in the contouring of the gravity map are listed separately: *

(1) the stations that were repeated or tightly gridded; (2) the stations lying outside the map area (lat $40^{\circ}22'30''$ to $40^{\circ}52'30''$; and long $111^{\circ}37'30''$ to $112^{\circ}15'00''$); and (3) the "bad" stations (which may represent a bad reading or possible error in input to the computer) which are indicated in the listing with an asterisk (*).

* In List No. 3.

<u>Prefix</u>	<u>Taken by</u>	<u>Accuracy</u>
W	Cook and Berg, 1961	0.5 mgal
H	W. Johnson, 1958	
RR	W. Johnson, 1957-58	
BL	J. Berg & L. Rausher, 1958	
A	Novotny, 1957-58	
MB	Novotny, 1957-58	
P	Parker-wide spaced, 1979	0.05 mgal
PG	Parker-tight grid, 1979	0.05 mgal
MBE	D. Mabey	2.5 mgal
78	1978 gravity class, University of Utah	1.0 mgal
F	R. C. Fox, 1979	0.05 mgal
01-70	Meiji Resource Consultants, 1980	0.05 mgal

Three separate lists of principal facts of gravity stations are attached herewith:

<u>List No.</u>	<u>Data</u>
1	University of Utah data, etc.
2	Meiji Resource Consultants, 1980 data.
3	Stations <u>not</u> used in contouring the gravity map.

Listing of gravity data in the Northern Wasatch area, Utah

AREA
UT
Salt LK
Grav

All of the stations listed on the following pages have been tied to the gravity base station network in Utah (Cook et al., 1967). Because the various surveys were conducted over several years and with different instruments, the accuracy of the various surveys will vary. To aid in the determination of the accuracy, a listing of 375 repeat stations is included following the listing of the gravity data. It should be noted that the repeat readings indicate that the average error is 0.05 mgal for all of the stations read more than once.

The following is a listing of the station prefixes used in this listing and the source of the gravity values in their order of appearance in the list.

<u>Prefix</u>	<u>Taken by</u>
PTF	Data provided by Don Mabey of the USGS
PTH	Data provided by Don Mabey of the USGS
PT	Data provided by Don Mabey of the USGS
W	Cook and Berg, 1961
A	Novotny, 1957-1958
BL	J. Berg & L. Rauser, 1958
L	D. Lum, 1956-1957
TA	Tanis, 1960
SR	J. Berg & W. Johnson, 1957
SL	J. Berg & W. Dolan, 1957
BC	W. Johnson, 1957
FB	Novotny, 1957-1958
P	W. Johnson, 1957

<u>Prefix</u>	<u>Taken by</u>
MB	D. Lum, 1956-1957
BW	W. Dolan & W. Johnson, 1957
SI	W. Johnson, 1957
612, etc -- no prefix --	Best, Berg, & Cook, 1956-1958
A	Hill Field, ESL, 1979
AD	Hill Field, ESL, 1979
AB	Hill Field, ESL, 1979
1350, etc -- no prefix --	NOAA gravity data
LV	J. Berg & W. Dolan, 1957
SS2	J. Berg & W. Dolan, 1957
N	North Ogden-Parker, 1980
T	Honeyville-Parker, 1980
Q	Plymouth-Parker, 1980

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
PTF18	41.28.650	112. 2.000	4272.00	979874.27	980312.29	-36.20	-181.74	2.94	-178.80
PTF19	41.28.600	112. 1.400	4332.00	979874.69	980312.22	-30.06	-177.65	4.35	-173.30
PTF20	41.28.420	112. 3.220	4231.00	979868.07	980311.94	-45.90	-190.05	1.68	-188.37
PTF21	41.26.920	112. 3.350	4228.00	979870.87	980309.71	-41.16	-185.20	2.18	-183.02
PTF22	41.25.710	112. 2.100	4309.00	979863.97	980307.91	-33.64	-180.44	7.06	-173.38
PTF23	41.24.770	112. 2.150	4353.00	979864.64	980306.49	-32.41	-180.71	6.00	-174.71
PTF24	41.20.170	112. 4.340	4227.00	979846.16	980299.62	-55.87	-199.88	.79	-199.09
PTF25	41.21.030	112. 4.930	4215.00	979847.02	980300.91	-57.42	-201.02	.77	-200.25
PTF26	41.20.580	112. 6.500	4209.00	979849.36	980300.23	-55.97	-199.37	.39	-198.98
PTF27	41.20.650	112. 7.540	4207.00	979852.79	980300.35	-51.85	-195.18	.25	-194.93
PTF28	41.21.600	112. 7.540	4207.00	979853.26	980301.77	-52.79	-196.12	.29	-195.83
PTF29	41.22.500	112. 7.540	4205.00	979853.20	980303.11	-54.39	-197.65	.33	-197.32
PTF30	41.23.170	112. 6.850	4205.00	979850.25	980304.12	-58.35	-201.61	.48	-201.13
PTF31	41.23.980	112. 6.130	4205.00	979850.07	980305.16	-59.57	-202.83	.68	-202.15
PTF32	41.24.510	112. 5.470	4205.00	979854.16	980306.11	-56.43	-199.69	.90	-198.79
PTF33	41.25.080	112. 4.800	4206.00	979860.70	980306.95	-50.64	-193.93	1.23	-192.70
PTH52	41.59.180	112.26.370	5063.00	979890.72	980357.89	9.05	-163.44	.68	-162.76
PTH54	41.57.580	112.26.880	5160.00	979884.26	980355.50	14.11	-161.69	.37	-161.32
PTH96	41.21.090	112.25.570	4264.00	979904.57	980301.01	4.63	-140.64	2.28	-138.36
PT100	41.56.060	112.26.300	5127.00	979884.34	980353.23	13.36	-161.31	.60	-160.71
PT111	41.41.810	112.10.800	4301.00	979907.03	980331.94	-20.36	-166.89	.20	-166.69
PT112	41.41.830	112.10.190	4306.00	979905.41	980331.97	-21.54	-168.24	.25	-167.99
PT113	41.41.860	112. 9.040	4300.00	979904.39	980332.01	-23.16	-169.66	.42	-169.24
PT114	41.41.880	112. 7.880	4302.00	979897.00	980332.04	-30.39	-176.96	.65	-176.31
PT115	41.42.780	112. 7.060	4237.00	979900.42	980333.37	-34.42	-178.77	1.22	-177.55
PT116	41.42.910	112. 5.520	4339.00	979903.49	980333.59	-21.96	-169.79	3.57	-166.22
PT117	41.41.420	112. 5.350	4312.00	979896.38	980331.35	-29.38	-176.29	3.59	-172.70
PT118	41.40.010	112. 5.460	4297.00	979896.71	980329.24	-28.36	-174.75	2.35	-172.40
PT119	41.40.000	112. 6.220	4293.00	979895.00	980329.23	-30.43	-176.69	1.44	-175.25
PT120	41.38.420	112. 4.980	4271.00	979892.71	980326.87	-32.43	-177.94	2.63	-175.31
PT121	41.39.800	112. 3.370	5001.00	979858.56	980328.94	.02	-170.36	7.87	-162.49
PT122	41.39.970	112. 4.280	4651.00	979873.39	980329.18	-13.32	-171.77	4.40	-167.37
PT123	41.38.500	112. 3.600	4796.00	979865.80	980326.98	-10.08	-173.47	6.54	-166.93

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
PT124	41.37.850	112. 3.280	4866.00	979862.57	980326.02	-5.75	-171.53	8.03	-163.50
PT125	41.38.110	112. 6.210	4270.00	979883.52	980326.40	-41.24	-186.72	1.15	-185.57
PT126	41.37.950	112. 8.320	4257.00	979887.86	980326.16	-37.89	-182.92	.42	-182.50
PT127	41.37.840	112.11.280	4262.00	979906.42	980326.01	-18.71	-163.91	.12	-163.79
PT128	41.37.820	112.12.360	4264.00	979912.29	980325.98	-12.61	-157.88	.26	-157.62
PT129	41.37.820	112.13.590	4262.00	979916.13	980325.98	-8.96	-154.16	.50	-153.66
PT130	41.37.810	112.14.180	4258.00	979917.55	980325.96	-7.90	-152.97	.69	-152.28
PT131	41.41.790	112.11.950	4298.00	979910.52	980331.91	-17.11	-163.54	.24	-163.30
PT132	41.41.770	112.13.100	4294.00	979910.42	980331.87	-17.56	-163.85	.36	-163.49
PT133	41.41.720	112.14.280	4291.00	979905.84	980331.80	-22.35	-168.54	.43	-168.11
PT141	41.43.590	112.14.420	4464.00	979907.64	980334.59	-7.07	-159.15	.77	-158.38
PT142	41.43.180	112.13.550	4409.00	979909.92	980333.98	-9.35	-159.56	.42	-159.14
PT143	41.40.030	112.11.900	4270.00	979905.28	980329.27	-22.35	-167.82	.20	-167.62
PT144	41.40.020	112.12.480	4268.00	979907.15	980329.26	-20.66	-166.07	.26	-165.81
PT145	41.39.990	112.14.200	4259.00	979905.43	980329.21	-23.18	-168.28	.47	-167.81
PT146	41.40.040	112.10.740	4276.00	979902.04	980329.28	-25.04	-170.72	.17	-170.55
PT147	41.40.100	112. 9.580	4278.00	979895.86	980329.38	-31.13	-176.88	.29	-176.59
PT148	41.40.180	112. 8.390	4281.00	979891.25	980329.50	-35.58	-181.43	.49	-180.94
PT157	41.34.610	112.13.970	4261.00	979912.01	980321.18	-8.38	-153.55	.44	-153.11
PT158	41.35.240	112.12.260	4240.00	979912.33	980322.11	-10.97	-155.42	.30	-155.12
PT159	41.35.580	112.10.670	4248.00	979905.11	980322.62	-17.94	-162.67	.11	-162.56
PT160	41.33.890	112.11.820	4243.00	979905.56	980320.10	-15.45	-160.00	.03	-159.97
PT161	41.33.010	112.11.810	4233.00	979900.90	980318.79	-19.74	-163.95	.01	-163.94
PT162	41.31.220	112. 9.450	4223.00	979888.72	980316.11	-30.18	-174.05	.09	-173.96
PT163	41.31.230	112.11.220	4223.00	979890.28	980316.12	-28.63	-172.50	.00	-172.50
PT164	41.30.590	112.10.600	4225.00	979890.32	980315.18	-27.46	-171.40	.02	-171.39
PT165	41.29.500	112.10.590	4215.00	979889.29	980313.55	-27.79	-171.39	.02	-171.37
PT166	41.33.000	112.10.650	4239.00	979898.14	980318.77	-21.91	-166.33	.04	-166.29
PT167	41.33.000	112. 9.460	4239.00	979893.40	980318.77	-26.65	-171.07	.10	-170.97
PT168	41.32.980	112. 7.710	4233.00	979880.67	980318.75	-39.93	-184.14	.26	-183.88
PT169	41.32.400	112. 4.970	4228.00	979869.49	980317.87	-50.70	-194.74	.65	-194.09
PT170	41.32.030	112. 3.500	4224.00	979867.32	980317.32	-52.19	-196.10	1.04	-195.06
PT171	41.31.790	112. 2.070	4238.00	979870.99	980316.97	-47.36	-191.74	1.94	-189.80

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T. C.	COMPLETE BOUGUER
PT172	41.31.500	112. .900	4326.00	979875.02	980316.53	-34.61	-181.99	2.92	-179.07
PT173	41.29.980	111.59.200	4633.00	979860.60	980314.26	-17.88	-175.72	8.77	-166.95
PT174	41.30.080	111.56.580	5145.00	979820.74	980314.41	-9.73	-185.01	2.23	-182.78
PT175	41.30.380	112. .530	4498.00	979867.60	980314.85	-24.17	-177.41	2.56	-174.85
PT176	41.30.660	112. 2.630	4236.00	979868.44	980315.29	-48.40	-192.72	1.45	-191.27
PT177	41.30.590	112. 4.590	4218.00	979870.40	980315.18	-48.04	-191.74	.69	-191.05
PT178	41.30.580	112. 6.490	4214.00	979875.06	980315.16	-43.73	-187.30	.36	-186.94
PT179	41.29.000	112. 7.700	4209.00	979878.97	980312.80	-37.92	-181.32	.24	-181.08
PT180	41.28.760	112. 9.300	4212.00	979883.85	980312.45	-32.42	-175.92	.11	-175.81
PT181	41.28.130	112.10.720	4207.00	979883.24	980311.52	-32.56	-175.89	.03	-175.86
PT182	41.28.020	112.11.900	4207.00	979890.52	980311.34	-35.11	-178.44	-.03	-178.47
PT183	41.27.990	112.13.090	4208.00	979879.67	980311.30	-35.82	-179.18	-.06	-179.24
PT184	41.28.770	112.14.970	4209.00	979879.91	980312.47	-36.66	-180.06	-.10	-180.16
PT185	41.45.350	112. 9.730	4350.00	979911.53	980337.23	-16.44	-164.64	.49	-164.15
PT186	41.45.330	112.10.890	4479.00	979908.44	980337.20	-7.46	-160.06	.92	-159.14
PT187	41.45.360	112.11.820	4963.00	979881.09	980337.24	10.66	-158.42	1.49	-156.93
PT188	41.45.180	112.12.730	5127.00	979870.44	980336.98	15.71	-158.96	1.42	-157.54
PT189	41.45.340	112. 7.650	4346.00	979898.52	980337.21	-29.91	-177.97	.53	-177.44
PT190	41.48.880	112. 6.350	4391.00	979907.47	980342.48	-21.99	-171.59	.33	-171.26
PT191	41.48.880	112. 5.190	4469.00	979904.99	980342.48	-17.14	-169.39	.44	-168.95
PT195	41.50.200	112. 6.380	4413.00	979907.60	980344.47	-21.78	-172.13	.43	-171.70
PT196	41.51.500	112. 6.400	4499.00	979904.05	980346.41	-19.18	-172.46	.73	-171.73
PT197	41.52.380	112. 6.440	4641.00	979897.90	980347.72	-13.29	-171.40	1.08	-170.32
PT201	41.53.210	112. 7.610	4891.00	979885.93	980348.96	-2.98	-169.61	1.67	-167.94
PT202	41.53.200	112. 8.780	4738.00	979889.28	980348.95	-14.01	-175.43	1.23	-174.20
PT203	41.53.180	112. 9.970	4502.00	979907.93	980348.91	-17.52	-170.90	.97	-169.93
PT204	41.53.180	112.11.130	4396.00	979912.38	980348.91	-23.04	-172.81	.94	-171.87
PT205	41.53.580	112.12.910	4556.00	979915.11	980349.52	-5.87	-161.09	1.20	-159.89
PT206	41.53.360	112.14.100	4856.00	979898.23	980349.20	5.79	-159.65	2.50	-157.15
PT208	41.54.880	112.13.200	4480.00	979918.06	980351.47	-12.02	-164.65	1.10	-163.55
PT209	41.54.820	112.14.680	4798.00	979900.93	980351.37	.85	-162.61	1.71	-160.90
PT212	41.56.590	112.14.410	4601.00	979917.33	980354.02	-3.92	-160.67	1.22	-159.45
PT213	41.56.610	112.12.810	4372.00	979920.08	980354.05	-22.74	-171.69	1.14	-170.55

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
PT214	41.56.650	112.11.220	4374.00	979909.30	980354.10	-33.38	-182.40	1.75	-180.65
PT215	41.56.670	112.10.500	4443.00	979905.52	980354.15	-30.72	-182.09	2.72	-179.37
PT216	41.56.290	112. 8.900	5223.00	979872.40	980353.58	10.09	-167.85	6.21	-161.64
PT217	41.57.520	112.11.220	4378.00	979908.91	980355.41	-34.71	-183.86	2.25	-181.61
PT218	41.58.600	112.11.600	4411.00	979911.80	980357.03	-30.33	-180.61	2.48	-178.13
PT219	42. .080	112.12.040	4428.00	979920.19	980359.25	-22.56	-173.42	2.81	-170.61
PT220	41.57.750	112.10.870	4436.00	979911.46	980355.75	-27.04	-178.17	3.21	-174.96
PT221	41.58.590	112.12.340	4364.00	979909.34	980357.02	-36.89	-185.57	1.57	-184.00
PT222	41.58.560	112.13.250	4369.00	979914.85	980356.98	-31.18	-180.03	1.22	-178.81
PT223	41.58.540	112.14.200	4441.00	979920.29	980356.93	-18.92	-170.22	1.11	-169.11
PT226	41.46.780	112.10.670	4839.00	979888.74	980339.37	4.53	-160.33	1.64	-158.69
PT227	41.47.080	112. 9.780	4383.00	979914.84	980339.80	-12.70	-162.02	.70	-161.32
PT228	41.48.390	112. 9.820	4423.00	979910.37	980341.76	-15.36	-166.05	.60	-165.45
PT229	41.49.180	112.11.010	4600.00	979907.69	980342.94	-2.57	-159.29	.82	-158.47
PT230	41.49.020	112.12.590	4860.00	979892.33	980342.70	6.76	-158.81	1.99	-156.82
PT231	41.49.700	112. 9.870	4406.00	979912.25	980343.71	-17.03	-167.14	.56	-166.58
PT232	41.49.720	112. 8.680	4378.00	979908.59	980343.74	-23.36	-172.51	.46	-172.05
PT233	41.48.860	112. 7.690	4368.00	979902.44	980342.46	-29.17	-177.98	.45	-177.53
PT234	41.47.560	112. 8.100	4313.00	979903.18	980340.52	-31.66	-178.60	.41	-178.19
PT235	41.50.750	112. 7.550	4408.00	979907.92	980345.29	-22.75	-172.93	.46	-172.47
PT236	41.52.350	112. 8.440	4475.00	979908.92	980347.68	-17.84	-170.30	.94	-169.36
PT237	41.50.580	112. 9.880	4443.00	979913.64	980345.02	-13.47	-164.84	.51	-164.33
PT238	41.50.570	112.11.040	4594.00	979908.15	980345.01	-4.75	-161.26	.66	-160.60
PT239	41.52.300	112.11.130	4408.00	979917.38	980347.60	-15.60	-165.78	.89	-164.89
PT240	41.52.320	112. 9.920	4419.00	979916.56	980347.63	-15.32	-165.87	.76	-165.11
PT241	41.54.900	112.11.180	4382.00	979907.81	980351.49	-31.51	-180.80	1.31	-179.49
PT242	41.47.130	112. 6.110	4382.00	979898.51	980339.89	-29.21	-178.50	.50	-178.00
PT243	41.45.440	112. 5.850	4405.00	979899.18	980337.36	-23.85	-173.92	1.51	-172.41
PT244	41.47.350	112. 4.550	4560.00	979896.16	980340.21	-15.13	-170.49	.64	-169.85
PT247	41.36.580	112. 8.310	4248.00	979888.03	980324.12	-36.53	-181.25	.37	-180.88
PT248	41.36.540	112. 9.570	4249.00	979899.80	980324.06	-24.60	-169.36	.20	-169.16
PT249	41.35.500	112. 7.740	4242.00	979883.14	980322.51	-40.37	-184.89	.40	-184.49
PT253	41.25.000	112.13.990	4208.00	979895.09	980306.84	-15.94	-159.30	-.07	-159.37

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
PT254	41.24.960	112.13.010	4208.00	979888.55	980306.78	-22.43	-165.79	-.04	-165.83
PT255	41.24.960	112.11.400	4208.00	979877.43	980306.78	-33.55	-176.91	.02	-176.89
PT256	41.25.200	112.10.310	4208.00	979872.25	980307.13	-39.08	-182.44	.10	-182.34
PT257	41.25.380	112. 8.550	4208.00	979862.58	980307.41	-49.02	-192.38	.23	-192.15
PT258	41.25.380	112. 7.150	4208.00	979855.90	980307.41	-55.70	-199.06	.45	-198.61
PT259	41.25.380	112. 5.610	4208.00	979854.07	980307.41	-57.53	-200.89	.84	-200.05
PT260	41.26.520	112. 4.210	4208.00	979864.25	980309.11	-49.06	-192.42	1.45	-190.97
PT269	41.33.020	112. 6.610	4230.00	979875.28	980318.80	-45.65	-189.76	.39	-189.37
PT270	41.32.050	112. 5.000	4235.00	979870.97	980317.34	-48.13	-192.41	.62	-191.79
PT271	41.31.790	112. 5.000	4235.00	979874.93	980316.97	-43.70	-187.98	.63	-187.35
PT272	41.36.700	112. 6.190	4252.00	979877.37	980324.30	-46.99	-191.85	.91	-190.94
PT273	41.36.380	112. 3.480	4282.00	979890.48	980323.82	-30.58	-176.46	4.40	-172.06
PT274	41.34.180	112. 1.690	4257.00	979888.79	980320.54	-31.34	-176.37	6.98	-169.39
PT275	41.33.350	112. 1.190	4270.00	979886.32	980319.30	-31.35	-176.82	6.76	-170.06
W0017	40.53.940	111.50.450	5648.00	979743.38	980260.55	14.07	-178.35	5.79	-172.56
W0012	40.54.400	111.54.670	4218.00	979818.66	980261.23	-45.83	-189.53	1.80	-187.73
W0018	40.53.620	111.50.720	5051.00	979779.66	980260.09	-5.33	-177.41	6.23	-171.13
W0019	40.53.060	111.51.440	4751.00	979798.08	980259.24	-14.28	-176.14	4.29	-171.85
W0020	40.53.060	111.52.290	4470.00	979815.80	980259.24	-22.99	-175.28	3.45	-171.83
W0021	40.53.060	111.53.470	4340.00	979821.08	980259.24	-29.94	-177.80	2.33	-175.47
W0022	40.53.050	111.54.660	4244.00	979820.70	980259.23	-39.33	-183.92	1.57	-182.25
W0023	40.53.050	111.55.740	4222.00	979816.30	980259.23	-45.80	-189.64	1.21	-188.43
W0024	40.53.150	111.56.960	4210.00	979816.29	980259.38	-47.10	-190.53	.85	-189.68
W0473	40.52.730	112.10.320	4257.00	979857.88	980258.76	-.47	-145.50	.81	-144.69
W1049	40.53.060	111.54.080	4289.00	979821.48	980259.24	-34.34	-180.46	1.94	-178.52
W1050	40.53.070	111.52.800	4398.00	979819.53	980259.26	-26.06	-175.89	2.92	-172.97
W1051	40.52.710	111.51.140	4932.00	979786.35	980258.73	-8.48	-176.51	4.39	-172.12
W1052	40.52.710	111.50.610	5202.00	979769.82	980258.73	.39	-176.84	4.86	-171.98
W1053	40.53.480	111.51.140	4842.00	979793.30	980259.87	-11.13	-176.09	5.11	-170.98
W1054	40.53.740	111.51.600	4636.00	979806.50	980260.26	-17.70	-175.64	4.91	-170.73
W1055	40.53.620	111.52.300	4416.00	979820.49	980260.09	-24.23	-174.68	3.74	-170.94
W1056	40.53.650	111.53.480	4300.00	979823.76	980260.13	-31.91	-178.41	2.45	-175.96
W1057	40.53.650	111.54.080	4264.00	979822.09	980260.13	-36.97	-182.24	2.02	-180.22

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
W1058	40.53.650	111.54.670	4232.00	979820.11	980260.13	-41.96	-186.14	1.71	-184.43
W1059	40.54.400	111.54.080	4229.00	979821.89	980261.23	-41.56	-185.64	2.20	-183.44
W1060	40.54.400	111.53.460	4256.00	979823.65	980261.23	-37.26	-182.26	2.72	-179.54
W1061	40.54.400	111.52.700	4295.00	979824.58	980261.23	-32.56	-178.89	3.76	-175.13
W1062	40.54.400	111.52.300	4337.00	979823.28	980261.23	-30.01	-177.77	4.61	-173.16
A51	40.54.340	112.10.040	4200.00	979856.58	980261.15	-9.52	-152.61	.54	-152.07
A52	40.54.420	112. 9.460	4200.00	979850.87	980261.27	-15.34	-158.43	.18	-158.25
A59	40.53.480	112. 9.890	4200.00	979859.56	980259.87	-5.15	-148.24	.37	-147.87
A60	40.53.580	112. 9.320	4200.00	979864.41	980260.03	-.57	-143.66	.14	-143.52
A61	40.53.660	112. 8.760	4200.00	979849.58	980260.14	-15.41	-158.50	.07	-158.43
A62	40.53.750	112. 8.210	4200.00	979849.16	980260.27	-16.06	-159.15	.04	-159.11
A63	40.53.840	112. 7.640	4200.00	979851.47	980260.41	-13.88	-156.97	.04	-156.93
A64	40.53.930	112. 7.120	4200.00	979855.39	980260.54	-10.10	-153.19	.04	-153.15
A65	40.54.010	112. 7.560	4200.00	979857.16	980260.66	-8.44	-151.53	.04	-151.49
A66	40.54.220	112. 6.010	4200.00	979859.88	980260.98	-6.04	-149.13	.05	-149.08
A67	40.53.230	112. 9.410	4200.00	979854.36	980259.50	-10.09	-153.18	.14	-153.04
A68	40.52.990	112. 8.930	4200.00	979849.87	980259.14	-14.22	-157.31	.07	-157.24
A69	40.52.750	112. 8.440	4200.00	979846.29	980258.79	-17.45	-160.54	.04	-160.50
A70	40.52.520	112. 7.890	4200.00	979842.78	980258.44	-20.61	-163.70	.03	-163.67
A112	40.54.250	112.10.770	4456.00	979856.43	980261.02	14.54	-137.27	1.29	-135.93
A114	40.53.960	112.11.640	5264.00	979805.72	980260.58	40.27	-139.07	4.47	-134.60
A115	40.53.770	112.12.570	4375.00	979855.68	980260.30	6.89	-142.16	.88	-141.28
A116	40.53.310	112.13.010	4200.00	979853.39	980259.62	3.83	-139.26	.44	-138.82
A164	40.53.420	112.10.530	4326.00	979857.98	980259.78	5.10	-142.28	1.01	-141.27
A165	40.54.250	112.10.770	4456.00	979856.20	980261.02	14.31	-137.50	1.29	-136.21
A167	40.53.960	112.11.640	5264.00	979805.50	980260.58	40.15	-139.19	4.47	-134.72
A168	40.53.770	112.12.570	4375.00	979855.54	980260.30	6.85	-142.20	.88	-141.32
A169	40.53.310	112.13.010	4200.00	979868.38	980259.62	3.82	-139.27	.44	-138.83
A236	40.54.340	112.10.040	4200.00	979857.27	980261.15	-8.83	-151.92	.54	-151.33
A237	40.54.420	112. 9.460	4200.00	979850.87	980261.27	-15.34	-158.43	.18	-158.25
A244	40.53.480	112. 9.890	4200.00	979859.56	980259.87	-5.15	-148.24	.37	-147.87
A245	40.53.580	112. 9.320	4200.00	979864.41	980260.03	-.57	-143.66	.14	-143.52
A246	40.53.660	112. 8.760	4200.00	979849.54	980260.14	-15.45	-158.54	.07	-158.47

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A147	40.53.750	112. 8.210	4200.00	979849.06	980260.27	-16.16	-159.25	.04	-159.21
A248	40.53.840	112. 7.640	4200.00	979851.47	980260.41	-13.88	-156.97	.04	-156.93
A249	40.53.930	112. 7.120	4200.00	979855.29	980260.54	-10.20	-153.29	.04	-153.25
A250	40.54.010	112. 7.560	4200.00	979857.06	980260.66	-8.54	-151.63	.04	-151.59
A251	40.54.220	112. 6.010	4200.00	979859.51	980260.98	-6.31	-149.40	.05	-149.35
A252	40.53.230	112. 9.410	4200.00	979854.36	980259.50	-10.09	-153.18	.14	-153.04
A253	40.52.990	112. 8.930	4200.00	979849.87	980259.14	-14.22	-157.31	.07	-157.24
A254	40.52.750	112. 8.440	4200.00	979846.29	980258.79	-17.45	-160.54	.04	-160.50
A255	40.52.520	112. 7.890	4200.00	979842.78	980258.44	-20.61	-163.70	.03	-163.67
BL33	40.53.720	112. 5.680	4199.00	979857.57	980260.23	-7.70	-150.76	.06	-150.70
BL34	40.53.950	112. 4.580	4199.00	979858.32	980260.57	-7.29	-150.35	.09	-150.25
BL35	40.54.100	112. 4.130	4200.00	979857.83	980260.80	-7.91	-151.00	.11	-150.89
BL36	40.54.250	112. 3.360	4199.00	979856.88	980261.02	-9.17	-152.23	.14	-152.09
BL37	40.54.350	112. 2.920	4199.00	979856.02	980261.16	-10.18	-153.24	.16	-153.08
BL38	40.54.500	112. 2.380	4198.00	979853.58	980261.40	-12.96	-155.98	.19	-155.79
BL40	40.53.900	112. 2.040	4198.00	979849.66	980260.49	-15.97	-158.99	.22	-158.77
W0001	40.57.910	111.53.420	4243.00	979828.60	980266.45	-38.76	-183.31	4.90	-173.41
W0002	40.57.910	111.55.230	4215.00	979820.57	980266.45	-49.42	-193.02	2.05	-190.97
W0003	40.59.490	111.55.190	4241.00	979827.45	980268.81	-42.45	-186.94	2.51	-184.43
W0004	40.59.490	111.54.120	4251.00	979832.19	980268.81	-36.77	-181.60	4.24	-177.36
W0005	40.59.480	111.53.580	4313.00	979828.92	980268.80	-34.20	-181.14	5.58	-175.56
W0006	40.57.900	111.52.950	4332.00	979825.48	980266.44	-33.49	-181.08	6.56	-174.52
W0007	40.58.380	111.52.330	4821.00	979793.66	980267.16	-20.03	-184.29	8.57	-175.71
W0008	40.56.590	111.53.410	4221.00	979823.84	980264.48	-43.61	-187.42	4.16	-183.26
W0009	40.56.530	111.52.770	4309.00	979822.80	980264.40	-36.30	-183.10	6.16	-176.94
W0010	40.54.790	111.52.300	4348.00	979822.30	980261.82	-30.05	-178.18	4.99	-173.19
W0011	40.54.780	111.53.430	4249.00	979823.68	980261.80	-38.46	-183.22	2.91	-180.31
W0013	40.54.670	111.55.410	4207.00	979815.16	980261.65	-50.78	-194.11	1.45	-192.66
W0014	40.54.670	111.56.500	4208.00	979811.98	980261.65	-53.87	-197.23	1.03	-196.20
W0015	40.55.880	111.56.820	4208.00	979810.44	980263.44	-57.20	-200.56	1.01	-199.55
W0016	40.55.280	111.54.800	4207.00	979816.56	980262.55	-50.27	-193.60	1.88	-191.72
W0474	40.54.830	112.10.320	4276.00	979848.89	980261.87	-10.78	-156.46	.64	-155.82
W0475	40.58.550	112.10.970	4246.00	979866.75	980267.40	-1.27	-145.93	.62	-145.31

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE POUGUER
W0476	41.500	112.11.790	4221.00	979880.25	980270.32	6.95	-136.85	.62	-136.23
W0479	41.280	112.14.140	4227.00	979830.43	980269.98	8.04	-135.97	.34	-135.63
W1063	40.54.800	111.51.660	4819.00	979794.89	980261.84	-13.67	-177.85	6.16	-171.69
W1064	40.54.740	111.52.400	4355.00	979821.13	980261.75	-30.99	-179.36	4.55	-174.81
W1065	40.54.740	111.52.680	4287.00	979824.68	980261.75	-33.84	-179.89	4.07	-175.82
W1066	40.55.750	111.53.420	4220.00	979823.77	980263.23	-42.53	-186.30	3.55	-182.75
W1067	40.57.130	111.53.470	4221.00	979824.68	980265.29	-43.59	-187.39	4.37	-183.02
W1068	40.57.140	111.52.950	4285.00	979825.96	980265.30	-36.29	-182.28	6.31	-175.97
W1069	40.57.910	111.54.060	4234.00	979826.68	980266.45	-41.52	-185.77	3.37	-182.40
W1070	40.58.940	111.55.210	4230.00	979825.64	980267.98	-44.47	-188.58	2.32	-186.26
W1071	40.58.940	111.54.630	4233.00	979828.61	980267.98	-41.22	-185.43	2.97	-182.46
W1072	40.58.830	111.53.190	4301.00	979826.16	980267.83	-37.12	-183.65	6.39	-177.26
W1073	40.58.550	111.53.680	4264.00	979827.96	980267.40	-38.37	-183.64	4.41	-179.23
W1074	40.58.330	111.54.050	4237.00	979828.34	980267.08	-40.21	-184.56	3.57	-180.99
W0502	40.59.000	111.50.150	8366.00	979569.70	980268.07	88.53	-196.49	22.26	-174.23
L373	41.820	111.58.030	4214.00	979818.95	980270.80	-55.47	-199.04	1.04	-198.00
L374	41.980	111.57.020	4261.00	979820.38	980271.03	-49.86	-195.03	1.47	-193.56
A37	40.56.810	112.9.290	4203.00	979858.56	980264.82	-10.93	-154.12	.15	-153.97
A38	40.56.860	112.8.740	4200.00	979860.52	980264.90	-9.33	-152.42	.08	-152.34
A39	40.56.980	112.8.170	4200.00	979862.06	980265.07	-7.96	-151.05	.04	-151.01
A40	40.57.070	112.7.610	4200.00	979863.90	980265.20	-6.25	-149.34	.03	-149.31
A41	40.57.140	112.7.020	4200.00	979864.06	980265.30	-6.19	-149.28	.03	-149.25
A42	40.57.000	112.6.730	4200.00	979864.36	980265.10	-5.69	-148.78	.03	-148.75
A43	40.56.850	112.6.450	4200.00	979863.86	980264.88	-5.97	-149.06	.04	-149.02
A44	40.56.700	112.6.180	4200.00	979863.44	980264.65	-6.16	-149.25	.04	-149.21
A45	40.55.930	112.7.270	4200.00	979861.31	980263.51	-7.15	-150.24	.03	-150.21
A46	40.55.840	112.7.820	4200.00	979862.15	980263.37	-6.16	-149.25	.04	-149.21
A47	40.55.770	112.8.380	4200.00	979860.40	980263.27	-7.81	-150.90	.06	-150.84
A48	40.55.680	112.8.920	4200.00	979853.08	980263.15	-15.02	-158.11	.10	-158.01
A49	40.55.600	112.9.460	4200.00	979850.29	980263.03	-17.69	-160.78	.20	-160.58
A50	40.55.520	112.10.000	4234.00	979849.79	980262.91	-14.87	-159.12	.42	-158.70
A53	40.54.510	112.8.890	4200.00	979849.52	980261.41	-16.84	-159.93	.09	-159.84
A54	40.54.600	112.8.350	4200.00	979853.01	980261.55	-13.48	-156.57	.05	-156.52

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A55	40.54.680	112. 7.790	4200.00	979857.87	980261.66	-8.73	-151.82	.04	-151.78
A56	40.54.750	112. 7.260	4200.00	979858.96	980261.77	-7.75	-150.84	.03	-150.81
A57	40.54.850	112. 6.700	4200.00	979859.96	980261.91	-6.89	-149.98	.04	-149.94
A58	40.54.890	112. 6.440	4200.00	979860.29	980261.97	-6.63	-149.72	.04	-149.68
A82	41. 1.210	112.11.120	4200.00	979876.00	980271.37	-.31	-143.40	.11	-143.29
A83	41. 1.380	112.10.670	4202.00	979871.17	980271.62	-5.21	-148.37	.00	-148.37
A100	40.54.870	112.10.310	4281.00	979843.98	980261.94	-15.29	-161.14	.60	-160.54
A101	40.55.500	112.10.300	4307.00	979846.79	980262.88	-10.98	-157.71	.52	-157.19
A102	40.54.980	112.11.000	4613.00	979841.13	980262.11	12.92	-144.24	1.06	-143.18
A103	40.55.530	112.11.000	4544.00	979844.67	980262.93	9.15	-145.66	1.16	-144.50
A104	40.56.320	112.11.180	4654.00	979839.65	980264.09	13.31	-145.25	1.31	-143.94
A105	40.56.930	112.10.820	4410.00	979849.09	980265.00	-1.11	-151.35	.87	-150.48
A106	40.57.390	112.10.930	4439.00	979850.49	980265.68	2.34	-148.89	.88	-148.01
A107	40.57.970	112.11.110	4394.00	979857.16	980266.54	3.92	-145.78	.97	-144.81
A108	40.57.410	112.10.290	4275.00	979857.65	980265.71	-5.95	-151.60	.42	-151.18
A109	40.56.540	112.10.340	4269.00	979853.23	980264.41	-9.64	-155.08	.64	-154.44
A110	40.57.160	112. 9.550	4214.00	979860.12	980265.34	-8.84	-152.41	.18	-152.23
A113	40.54.870	112.11.830	5226.00	979806.74	980261.94	36.36	-141.68	3.35	-138.33
A117	40.55.820	112.13.190	4200.00	979873.82	980263.34	5.54	-137.55	4.53	-133.02
A118	40.55.330	112.13.840	4200.00	979872.79	980262.62	5.22	-137.87	.68	-137.19
A119	40.55.690	112.13.380	4494.00	979855.19	980263.16	14.74	-138.37	.95	-137.42
A120	40.55.520	112.12.450	5030.00	979819.04	980262.91	29.25	-142.12	2.00	-140.12
A121	40.58.990	112.11.370	4213.00	979874.27	980268.05	2.49	-141.04	.94	-140.10
A122	40.59.640	112.11.830	4290.00	979876.18	980269.03	10.67	-135.49	.86	-134.63
A123	41. .340	112.11.800	4235.00	979880.51	980270.07	8.78	-135.50	.57	-134.93
A126	41. .890	112.12.440	4954.00	979834.20	980270.90	29.28	-139.50	2.92	-136.58
A127	41. .290	112.12.450	4805.00	979845.36	980270.00	27.32	-136.38	2.15	-134.23
A128	41. .560	112.13.460	4200.00	979880.97	980270.41	5.62	-137.47	1.66	-135.81
A129	40.59.760	112.14.480	4200.00	979831.08	980269.21	6.92	-136.17	1.18	-134.99
A130	40.59.690	112.13.590	4392.00	979869.47	980269.11	13.47	-136.16	.76	-135.40
A131	40.59.930	112.12.930	4596.00	979858.04	980269.47	20.87	-135.71	.57	-135.14
A132	40.59.040	112.13.360	4845.00	979839.29	980268.15	26.86	-138.20	2.15	-136.05
A133	40.58.210	112.14.860	4200.00	979878.49	980266.91	6.64	-136.45	1.54	-134.91

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A134	40.58.980	112.14.800	4200.00	979880.16	980268.05	7.17	-135.92	1.09	-134.83
A135	40.59.090	112.13.900	4532.00	979859.17	980268.22	17.23	-137.17	1.39	-135.73
A137	41. 1.230	112.14.410	4200.00	979884.76	980271.40	8.41	-134.68	.25	-134.43
A153	40.54.870	112.10.310	4275.00	979844.38	980261.94	-15.46	-161.10	.61	-160.49
A154	40.55.500	112.10.300	4310.00	979846.79	980262.88	-10.69	-157.53	.52	-157.01
A155	40.54.980	112.11.000	4613.00	979841.11	980262.11	12.90	-144.26	1.06	-143.20
A156	40.55.530	112.11.000	4544.00	979844.71	980262.93	9.19	-145.62	1.16	-144.46
A157	40.56.320	112.11.180	4654.00	979839.69	980264.09	13.35	-145.21	1.31	-143.90
A158	40.56.930	112.10.820	4410.00	979849.09	980265.00	-1.11	-151.35	.87	-150.48
A159	40.57.390	112.10.930	4439.00	979850.53	980265.68	2.38	-148.85	.88	-147.97
A160	40.57.970	112.11.110	4394.00	979857.70	980266.54	4.46	-145.24	.97	-144.27
A161	40.57.410	112.10.290	4265.00	979857.65	980265.71	-6.90	-152.20	.43	-151.77
A162	40.56.540	112.10.340	4270.00	979853.23	980264.41	-9.54	-155.02	.64	-154.38
A163	40.57.160	112. 9.550	4210.00	979860.16	980265.34	-9.18	-152.61	.18	-152.43
A166	40.54.870	112.11.830	5226.00	979806.70	980261.94	36.32	-141.72	3.35	-138.37
A170	40.55.820	112.13.190	4200.00	979873.82	980263.34	5.54	-137.55	4.53	-133.02
A171	40.55.330	112.13.840	4200.00	979872.91	980262.52	5.24	-137.85	.68	-137.17
A172	40.55.690	112.13.380	4490.00	979856.36	980263.16	15.53	-137.44	.96	-136.48
A173	40.55.520	112.12.450	5030.00	979833.88	980262.91	44.09	-127.28	2.00	-125.28
A174	40.58.990	112.11.370	4240.00	979874.27	980268.05	5.03	-139.42	.84	-138.58
A175	40.59.640	112.11.830	4270.00	979876.28	980269.03	8.88	-136.59	.94	-135.65
A176	41. .340	112.11.800	4220.00	979881.28	980270.07	8.14	-135.63	.64	-134.99
A179	41. .890	112.12.440	4954.00	979836.55	980270.90	31.63	-137.15	2.92	-134.23
A180	41. .290	112.12.450	4805.00	979845.36	980270.00	27.32	-136.38	2.15	-134.23
A181	41. .560	112.13.460	4200.00	979884.07	980270.41	8.72	-134.37	1.66	-132.71
A182	40.59.760	112.14.480	4200.00	979881.08	980269.21	6.92	-136.17	1.18	-134.99
A183	40.59.690	112.13.590	4392.00	979869.49	980269.11	13.49	-136.14	.76	-135.38
A184	40.59.930	112.12.930	4596.00	979858.10	980269.47	20.93	-135.65	.57	-135.08
A185	40.59.040	112.13.360	4845.00	979839.49	980268.15	27.06	-138.00	2.15	-135.85
A186	40.58.210	112.14.860	4200.00	979878.49	980266.91	6.64	-136.45	1.54	-134.91
A187	40.58.980	112.14.800	4200.00	979880.16	980268.05	7.17	-135.92	1.09	-134.83
A188	40.59.090	112.13.900	4532.00	979859.09	980268.22	17.15	-137.25	1.39	-135.86
A190	41. 1.230	112.14.410	4200.00	979884.56	980271.40	8.21	-134.88	.25	-134.63

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A222	40.56.810	112. 9.290	4203.00	979858.56	980264.82	-10.93	-154.12	.15	-153.97
A223	40.56.860	112. 8.740	4200.00	979860.52	980264.90	-9.33	-152.42	.08	-152.34
A224	40.56.980	112. 8.170	4200.00	979862.06	980265.07	-7.96	-151.05	.04	-151.01
A225	40.57.070	112. 7.610	4200.00	979863.80	980265.20	-6.35	-149.44	.03	-149.41
A226	40.57.140	112. 7.020	4200.00	979864.06	980265.30	-6.19	-149.28	.03	-149.25
A227	40.57.000	112. 6.730	4200.00	979863.86	980265.10	-6.19	-149.28	.03	-149.25
A228	40.56.850	112. 6.450	4200.00	979863.86	980264.88	-5.97	-149.06	.04	-149.02
A229	40.56.700	112. 6.180	4200.00	979863.44	980264.65	-6.16	-149.25	.04	-149.21
A230	40.55.930	112. 7.270	4200.00	979861.31	980263.51	-7.15	-150.24	.03	-150.21
A231	40.55.840	112. 7.820	4200.00	979862.05	980263.37	-6.26	-149.35	.04	-149.31
A232	40.55.770	112. 8.380	4200.00	979860.40	980263.27	-7.81	-150.90	.06	-150.84
A233	40.55.680	112. 8.920	4200.00	979853.08	980263.15	-15.02	-158.11	.10	-158.01
A234	40.55.600	112. 9.460	4200.00	979850.29	980263.03	-17.69	-160.78	.20	-160.58
A235	40.55.520	112.10.000	4234.00	979843.95	980262.91	-15.71	-159.96	.42	-159.54
A238	40.54.510	112. 8.890	4200.00	979849.42	980261.41	-16.94	-160.03	.09	-159.94
A239	40.54.600	112. 8.350	4200.00	979853.01	980261.55	-13.48	-156.57	.05	-156.52
A240	40.54.680	112. 7.790	4200.00	979857.77	980261.66	-8.83	-151.92	.04	-151.88
A241	40.54.750	112. 7.260	4200.00	979858.96	980261.77	-7.75	-150.84	.03	-150.81
A242	40.54.850	112. 6.700	4200.00	979860.06	980261.91	-6.79	-149.88	.04	-149.84
A243	40.54.890	112. 6.440	4200.00	979860.29	980261.97	-6.63	-149.72	.04	-149.68
FL29	40.57.400	111.57.390	4201.00	979812.69	980265.70	-57.86	-200.98	.97	-200.01
BL30	40.56.960	111.59.120	4201.00	979816.96	980265.04	-52.94	-196.06	.58	-195.48
BL31	40.56.450	112. .620	4201.00	979827.95	980264.28	-41.19	-184.31	.35	-183.96
BL32	40.55.980	112. 1.130	4201.00	979835.83	980263.59	-32.61	-175.73	.29	-175.44
BL39	40.54.600	112. 1.890	4199.00	979850.83	980261.55	-15.75	-158.81	.23	-158.58
BL41	40.54.690	112. 1.000	4199.00	979849.15	980261.67	-17.56	-160.62	.30	-160.32
BL42	40.55.190	112. 1.020	4196.00	979843.76	980262.41	-23.98	-166.93	.30	-166.63
BL43	40.55.690	112. .690	4196.00	979837.23	980263.16	-31.26	-174.21	.33	-173.88
BL45	40.56.500	111.59.700	4196.00	979822.49	980264.36	-47.20	-190.15	.46	-189.69
L33	41. 1.160	111.54.490	4481.00	979822.80	980271.30	-27.02	-179.68	4.52	-175.15
W0477	41. 3.540	112.15.000	4237.00	979884.04	980274.85	7.72	-136.63	-.14	-136.77
W0478	41. 2.490	112.13.350	4417.00	979870.67	980273.27	12.86	-137.62	.13	-137.49
TA140	41. 8.360	111.52.930	4684.00	979807.06	980282.03	-34.39	-193.97	20.01	-173.96

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
L357	41. 6.220	111.58.350	4747.00	979800.70	980278.84	-31.64	-193.37	1.08	-192.29
L358	41. 7.400	111.59.830	4769.00	979797.90	980280.59	-34.12	-196.60	.77	-195.83
L359	41. 7.280	111.58.600	4784.00	979799.46	980280.41	-30.97	-193.96	.86	-193.10
L360	41. 7.660	111.57.790	4794.00	979802.84	980280.98	-27.22	-190.55	1.18	-189.37
L361	41. 7.090	112. .940	4595.00	979807.46	980280.14	-40.47	-197.02	.48	-196.54
L362	41. 6.610	111.58.090	4776.00	979800.51	980279.42	-29.58	-192.29	1.02	-191.27
L363	41. 7.280	111.56.580	5015.00	979791.03	980280.41	-17.67	-188.53	2.36	-186.17
L369	41. 7.960	112. 1.510	4571.00	979809.27	980281.44	-42.22	-197.95	.46	-197.49
L370	41. 2.310	111.57.770	4290.00	979820.05	980273.02	-49.44	-195.60	1.25	-194.35
L371	41. 2.310	111.58.700	4259.00	979820.74	980273.02	-51.67	-196.77	.92	-195.85
L372	41. 1.750	111.58.090	4246.00	979820.34	980272.18	-52.46	-197.12	1.09	-196.03
L375	41. 4.120	111.58.430	4382.00	979820.18	980275.71	-43.36	-192.65	1.05	-191.60
L376	41. 2.740	112. .360	4246.00	979822.81	980273.66	-51.46	-196.12	.53	-195.59
A84	41. 1.760	112.10.430	4202.00	979867.91	980272.20	-9.04	-152.20	-.03	-152.23
A85	41. 2.360	112.10.030	4201.00	979864.31	980273.09	-13.63	-156.75	-.05	-156.80
A86	41. 2.990	112. 9.020	4202.00	979863.88	980274.02	-14.89	-158.05	-.05	-158.10
A87	41. 3.300	112. 8.580	4203.00	979863.71	980274.48	-15.44	-158.63	-.04	-158.67
A88	41. 3.930	112. 8.090	4203.00	979863.97	980275.43	-16.13	-159.32	-.03	-159.35
A89	41. 3.740	112.10.070	4203.00	979865.91	980275.14	-13.90	-157.09	-.07	-157.16
A90	41. 4.050	112.10.840	4203.00	979866.14	980275.61	-14.14	-157.33	-.10	-157.43
A91	41. 2.960	112.10.980	4201.00	979873.89	980273.98	-4.94	-148.06	-.08	-148.14
A92	41. 2.390	112.12.000	4200.00	979883.12	980273.13	5.04	-138.05	.20	-137.85
A93	41. 4.160	112.12.080	4202.00	979871.27	980275.77	-9.25	-152.41	-.12	-152.53
A94	41. 5.070	112.12.730	4202.00	979876.56	980277.12	-5.32	-148.48	-.14	-148.62
A95	41. 6.150	112.14.060	4201.00	979878.33	980278.74	-5.27	-148.39	-.17	-148.56
A124	41. 1.550	112.11.920	4257.00	979878.58	980271.87	7.22	-137.81	.47	-137.34
A125	41. 2.140	112.12.950	4641.00	979855.57	980272.75	19.45	-138.66	.88	-137.78
A136	41. 1.710	112.13.540	4464.00	979869.46	980272.12	17.21	-134.87	.18	-134.69
A140	41. 2.180	112.14.520	4389.00	979877.83	980272.82	17.84	-131.69	.00	-131.69
A142	41. 3.330	112.14.390	4348.00	979877.31	980274.53	11.75	-136.38	.11	-136.27
A143	41. 2.470	112.13.340	4422.00	979872.73	980273.25	15.41	-135.24	.13	-135.11
A144	41. 2.390	112.12.000	4200.00	979883.12	980273.13	5.04	-138.05	.20	-137.85
A145	41. 2.390	112.12.000	4200.00	979883.12	980273.13	5.04	-138.05	.20	-137.85

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A146	41. 4.160	112.12.080	4202.00	979871.29	980275.77	-9.23	-152.39	-.12	-152.51
A147	41. 5.070	112.12.730	4202.00	979876.58	980277.12	-5.30	-148.46	-.14	-148.60
A148	41. 6.150	112.14.060	4201.00	979878.43	980278.74	-5.17	-148.29	-.17	-148.46
A177	41. 1.550	112.11.920	4257.00	979878.70	980271.87	7.24	-137.79	.47	-137.32
A178	41. 2.140	112.12.950	4641.00	979855.67	980272.75	19.45	-138.66	.88	-137.73
A189	41. 1.710	112.13.540	4464.00	979869.50	980272.12	17.25	-134.83	.18	-134.65
A193	41. 2.180	112.14.520	4389.00	979877.83	980272.82	17.84	-131.69	.00	-131.69
A195	41. 3.330	112.14.390	4348.00	979877.31	980274.53	11.75	-136.38	.11	-136.27
A196	41. 2.470	112.13.340	4422.00	979872.73	980273.25	15.41	-135.24	.13	-135.11
L1	41. 2.640	111.57.100	4311.00	979823.55	980273.51	-44.47	-191.34	1.66	-189.68
L2	41. 3.610	111.59.240	4327.00	979820.68	980274.95	-47.27	-194.69	.79	-193.90
L3	41. 3.620	112. .360	4300.00	979821.57	980274.97	-48.84	-195.34	.55	-194.79
L5	41. 3.600	112. 3.850	4224.00	979840.00	980274.94	-37.63	-181.54	.17	-181.37
L6	41. 3.780	112. 4.990	4218.00	979849.19	980275.20	-29.27	-172.97	.13	-172.84
L7	41. 4.490	112. 4.970	4231.00	979846.62	980276.27	-31.67	-175.82	.10	-175.72
L8	41. 4.480	112. 6.150	4224.00	979856.07	980276.25	-22.87	-166.78	.08	-166.70
L9	41. 5.360	112. 6.140	4231.00	979853.88	980277.56	-25.71	-169.86	.07	-169.79
L10	41. 5.350	112. 6.710	4227.00	979857.66	980277.55	-22.29	-166.30	.08	-166.22
L11	41. 6.210	112. 6.650	4236.00	979851.18	980278.83	-29.21	-173.53	.07	-173.46
L12	41. 6.210	112. 4.970	4273.00	979840.40	980278.83	-36.51	-182.09	.12	-181.97
L13	41. 6.210	112. 3.830	4311.00	979831.00	980278.83	-42.34	-189.21	.20	-189.01
L14	41. 5.340	112. 3.820	4280.00	979833.49	980277.53	-41.47	-187.28	.18	-187.10
L15	41. 5.350	112. 4.980	4243.00	979844.26	980277.55	-34.20	-178.75	.11	-178.64
L16	41. 5.350	112. 2.660	4323.00	979825.17	980277.55	-45.76	-193.04	.27	-192.77
L17	41. 5.340	112. 1.480	4386.00	979819.03	980277.53	-45.95	-195.38	.39	-194.99
L18	41. 5.340	112. .040	4457.00	979814.93	980277.53	-43.37	-195.22	.59	-194.63
L19	41. 5.360	111.59.220	4492.00	979813.70	980277.56	-41.34	-194.38	.76	-193.62
L20	41. 5.360	111.58.360	4525.00	979813.93	980277.56	-38.01	-192.17	.98	-191.19
L21	41. 5.330	111.56.970	4600.00	979814.32	980277.52	-30.52	-187.24	1.57	-185.67
L22	41. 6.070	111.56.300	4801.00	979805.71	980278.61	-21.32	-184.88	1.96	-182.92
L23	41. 6.480	111.54.530	4887.00	979807.23	980279.22	-12.32	-178.81	6.14	-172.67
L24	41. 5.790	111.54.480	4944.00	979802.67	980278.20	-10.50	-178.94	6.96	-171.93
L25	41. 4.790	111.54.620	4806.00	979808.41	980276.70	-16.24	-179.98	6.05	-173.93

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
L26	41. 4.860	111.55.130	4757.00	979810.63	980276.82	-18.74	-180.81	3.98	-176.83
L27	41. 4.620	111.56.100	4603.00	979815.87	980276.45	-26.62	-183.44	2.35	-181.09
L28	41. 4.480	111.54.610	4787.00	979808.75	980276.25	-17.23	-180.32	5.97	-174.35
L29	41. 3.310	111.55.590	4506.00	979825.33	980274.50	-25.34	-178.85	3.19	-175.66
L30	41. 3.550	111.55.300	4795.00	979809.09	980274.87	-14.76	-178.12	3.78	-174.34
L31	41. 2.520	111.54.330	4662.00	979816.40	980273.32	-18.41	-177.24	7.33	-169.91
L32	41. 1.880	111.54.480	4585.00	979818.54	980272.37	-22.57	-178.78	5.11	-173.67
L34	41. 2.290	111.55.590	4438.00	979826.51	980272.98	-29.03	-180.23	2.97	-177.26
L35	41. 7.100	112. 2.670	4423.00	979819.89	980280.16	-44.24	-194.93	.28	-194.65
L36	41. 7.100	112. 3.840	4359.00	979827.45	980280.16	-42.70	-191.21	.19	-191.02
L37	41. 7.100	112. 5.040	4311.00	979837.47	980280.16	-37.20	-184.07	.15	-183.92
L38	41. 7.100	112. 6.140	4265.00	979848.01	980280.16	-30.98	-176.28	.13	-176.15
L39	41. 7.090	112. 6.700	4234.00	979855.29	980280.14	-26.60	-170.85	.05	-170.80
L40	41. 7.090	112. 7.280	4222.00	979858.69	980280.14	-24.33	-168.17	.03	-168.14
L41	41. 7.950	112. 7.290	4229.00	979857.42	980281.42	-26.22	-170.30	.02	-170.28
L48	41. 7.960	112. 6.140	4262.00	979847.00	980281.44	-33.56	-178.76	.12	-178.64
L50	41. 7.510	111.54.400	4590.00	979825.23	980280.77	-23.80	-180.18	7.26	-172.92
L51	41. 8.370	111.50.010	4797.00	979798.77	980282.05	-32.07	-195.50	9.99	-185.51
L61	41. 8.180	111.53.890	4568.00	979824.69	980281.76	-27.40	-183.03	12.40	-170.63
L63	41. 7.950	111.54.590	4537.00	979829.60	980281.42	-25.07	-179.64	5.76	-173.88
L64	41. 7.950	111.55.210	4517.00	979830.76	980281.42	-25.79	-179.68	3.89	-175.79
L65	41. 8.070	111.56.920	4496.00	979828.58	980281.59	-30.12	-183.29	2.04	-181.25
TA139	41. 8.530	111.55.010	4537.00	979830.13	980282.28	-25.40	-179.97	5.20	-174.77
SR1	41.14.630	112.14.570	4215.00	979898.40	980291.36	3.50	-140.10	-.08	-140.18
SL16	41. 8.620	112.14.270	4197.00	979878.60	980282.41	-9.04	-152.03	-.16	-152.19
L319	41.15.010	112.13.070	4218.00	979894.24	980291.93	-.95	-144.65	-.10	-144.75
L320	41.14.690	112.13.090	4218.00	979892.99	980291.45	-1.72	-145.42	-.11	-145.53
L321	41.15.020	112.10.790	4216.00	979876.37	980291.95	-19.02	-162.65	-.07	-162.72
L322	41.14.690	112.10.490	4218.00	979873.26	980291.45	-21.45	-165.15	-.06	-165.21
L323	41.15.010	112. 9.630	4222.00	979866.16	980291.93	-28.65	-172.49	-.03	-172.52
L324	41.13.350	112. 9.640	4212.00	979864.87	980289.45	-28.40	-171.90	-.05	-171.95
L325	41.14.140	112. 9.630	4219.00	979865.06	980290.63	-28.73	-172.47	-.04	-172.51
L326	41.14.990	112. 8.410	4221.00	979856.70	980291.90	-38.18	-181.98	.01	-181.97

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
L327	41.11.250	112. 9.620	4212.00	979863.52	980286.34	-26.63	-170.13	-.06	-170.19
L328	41.12.110	112. 9.610	4212.00	979863.96	980287.60	-27.46	-170.96	-.06	-171.02
L329	41.13.250	112.10.700	4210.00	979873.48	980289.30	-19.83	-163.26	-.08	-163.34
L330	41.13.310	112.11.900	4208.00	979882.70	980289.39	-10.89	-154.25	-.09	-154.34
L331	41.12.250	112.11.800	4209.00	979876.73	980287.82	-15.19	-158.59	-.07	-158.66
L332	41.11.440	112.11.410	4209.00	979872.71	980286.62	-18.01	-161.41	-.08	-161.49
L333	41.10.440	112.11.110	4209.00	979870.43	980285.12	-18.79	-162.19	-.08	-162.27
L335	41.15.110	112. .530	4255.00	979833.00	980292.08	-58.86	-203.82	.93	-202.89
L336	41.15.010	112. 1.480	4248.00	979831.49	980291.93	-60.87	-205.60	.67	-204.93
L342	41.14.640	112. 2.800	4255.00	979830.64	980291.37	-60.51	-205.47	.43	-205.04
L343	41.14.810	112. 3.750	4241.00	979833.64	980291.64	-59.09	-203.58	.31	-203.27
L344	41.14.940	112. 2.940	4235.00	979837.68	980291.83	-55.81	-200.09	.42	-199.67
L345	41.14.760	112. 6.090	4235.00	979842.34	980291.56	-50.88	-195.16	.15	-195.01
L347	41.12.340	112. 6.100	4226.00	979841.13	980287.95	-49.32	-193.30	.10	-193.20
L348	41.13.210	112. 6.090	4217.00	979842.07	980289.25	-50.53	-194.20	.11	-194.09
L349	41.13.200	112. 2.950	4251.00	979834.20	980289.23	-55.18	-200.01	.38	-199.63
L350	41.13.200	112. 3.800	4258.00	979831.13	980289.23	-57.59	-202.66	.27	-202.39
L351	41.13.200	112. 2.640	4256.00	979828.37	980289.23	-60.54	-205.54	.42	-205.12
L352	41.11.450	112. 2.850	4309.00	979824.67	980286.64	-56.67	-203.47	.41	-203.06
L353	41.11.450	112. 1.500	4473.00	979813.51	980286.64	-52.30	-204.69	.50	-204.19
L354	41.13.200	112. 1.470	4295.00	979825.15	980289.23	-60.09	-206.42	.58	-205.84
L355	41.13.200	112. .240	4326.00	979825.06	980289.23	-57.27	-204.65	.85	-203.80
L356	41.14.670	112. .520	4263.00	979831.40	980291.42	-59.04	-204.28	.90	-203.38
L364	41.14.610	111.58.150	4303.00	979840.60	980291.34	-45.99	-192.59	2.19	-190.40
L365	41.13.380	111.58.140	4304.00	979836.08	980289.50	-48.59	-195.22	2.10	-193.12
L366	41.12.740	111.57.610	4407.00	979832.01	980288.55	-42.02	-192.16	2.34	-189.82
L367	41.12.290	111.59.810	4404.00	979819.83	980287.87	-53.80	-203.84	.89	-202.95
L368	41.11.620	112. .510	4439.00	979816.56	980286.89	-52.80	-204.03	.66	-203.37
L377	41.15.000	112. 8.640	4221.00	979858.04	980291.91	-36.84	-180.65	.00	-180.65
L378	41.15.000	112. 8.870	4221.00	979859.78	980291.91	-35.11	-178.91	-.01	-178.92
L379	41.15.000	112. 9.100	4221.00	979861.39	980291.91	-33.49	-177.30	-.01	-177.31
L380	41.15.000	112. 9.330	4221.00	979863.12	980291.91	-31.77	-175.57	-.02	-175.59
L381	41.15.000	112. 9.860	4220.00	979867.89	980291.91	-27.09	-170.86	-.04	-170.90

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
L382	41.15.000	112.10.090	4219.00	979869.82	980291.91	-25.25	-168.99	-.04	-169.03
L383	41.15.000	112.10.320	4218.00	979871.83	980291.91	-23.34	-167.04	-.05	-167.09
L384	41.15.000	112.10.570	4217.00	979872.80	980291.91	-22.46	-166.13	-.06	-166.19
L385	41.15.000	112.11.020	4216.00	979877.43	980291.91	-17.92	-161.56	-.07	-161.63
L386	41.15.000	112.11.240	4215.00	979878.37	980291.91	-16.58	-160.18	-.08	-160.26
L387	41.15.000	112.11.470	4215.00	979880.37	980291.91	-15.08	-158.68	-.09	-158.77
L388	41.15.000	112.11.700	4215.00	979882.25	980291.91	-13.20	-156.80	-.09	-156.89
L389	41.15.000	112.11.930	4215.00	979883.92	980291.91	-11.53	-155.13	-.10	-155.23
L390	41.15.020	112.12.160	4215.00	979885.57	980291.95	-9.81	-153.41	-.10	-153.51
L391	41.15.020	112.12.390	4215.00	979887.41	980291.95	-8.07	-151.67	-.10	-151.77
L392	41.15.020	112.12.620	4215.00	979839.19	980291.95	-6.29	-149.89	-.11	-150.00
L393	41.15.020	112.12.860	4215.00	979891.54	980291.95	-3.94	-147.54	-.10	-147.64
L394	41.15.020	112.13.310	4219.00	979895.24	980291.95	.14	-143.60	-.09	-143.69
L395	41.15.020	112.13.530	4224.00	979896.73	980291.95	2.10	-141.81	-.05	-141.86
L396	41.14.670	111.59.310	4277.00	979834.92	980291.42	-54.21	-199.92	1.39	-198.53
L397	41.14.670	111.59.490	4273.00	979834.05	980291.42	-55.45	-201.03	1.28	-199.75
L398	41.14.670	111.59.650	4271.00	979833.36	980291.42	-56.33	-201.84	1.20	-200.64
L399	41.14.670	111.59.790	4269.00	979832.63	980291.42	-57.25	-202.69	1.14	-201.55
L400	41.14.780	112. 6.850	4223.00	979845.47	980291.59	-47.91	-191.78	.09	-191.69
L401	41.14.760	112. 6.680	4222.00	979845.36	980291.56	-49.03	-192.92	.10	-192.82
L402	41.14.760	112. 6.410	4232.00	979843.25	980291.56	-50.25	-194.43	.12	-194.31
L404	41.14.760	112. 5.850	4235.00	979840.68	980291.56	-52.54	-196.82	.16	-196.66
L405	41.14.760	112. 5.520	4234.00	979839.09	980291.56	-54.22	-198.47	.18	-198.29
L406	41.14.760	112. 5.500	4234.00	979838.83	980291.56	-54.48	-198.73	.18	-198.55
L407	41.14.950	112. 5.270	4234.00	979838.26	980291.84	-55.33	-199.58	.19	-199.39
L408	41.14.950	112. 5.040	4234.00	979837.00	980291.84	-56.59	-200.84	.21	-200.63
L409	41.14.980	112. 4.640	4235.00	979835.91	980291.88	-57.63	-201.91	.24	-201.67
L410	41.14.990	112. 4.400	4236.00	979834.89	980291.90	-58.57	-202.89	.25	-202.64
L411	41.15.000	112. 3.180	4220.00	979854.77	980291.91	-40.21	-183.93	.02	-183.95
L412	41.15.000	112. 7.930	4220.00	979853.11	980291.91	-41.87	-185.64	.03	-185.61
L413	41.15.000	112. 7.650	4220.00	979851.11	980291.91	-43.87	-187.64	.04	-187.60
L414	41.14.970	112. 7.500	4220.00	979850.48	980291.87	-44.46	-188.23	.05	-188.13
L415	41.14.910	112. 7.320	4220.00	979848.50	980291.78	-46.35	-190.12	.06	-190.06

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
L416	41.14.840	112. 7.110	4215.00	979847.93	980291.68	-47.29	-190.89	.07	-190.82
L417	41.14.980	112. 4.190	4236.00	979834.82	980291.88	-58.62	-202.94	.28	-202.66
L418	41.13.740	112. 1.480	4277.00	979826.25	980290.04	-61.50	-207.21	.60	-206.61
L430	41.14.670	111.59.940	4268.00	979831.76	980291.42	-58.21	-203.62	1.08	-202.54
L431	41.14.660	111.59.020	4278.00	979836.82	980291.41	-52.19	-197.94	1.52	-196.32
L432	41.14.920	111.58.640	4279.00	979839.47	980291.80	-49.85	-195.63	1.98	-193.65
L433	41.14.910	111.58.150	4294.00	979841.36	980291.78	-46.53	-192.82	2.33	-190.49
L434	41.14.950	111.57.380	4317.00	979843.40	980291.84	-42.38	-189.46	3.36	-186.10
L435	41.14.640	111.57.150	4332.00	979843.01	980291.37	-40.89	-188.48	3.47	-185.01
L436	41.14.440	111.56.460	4365.00	979842.07	980291.09	-38.45	-187.16	5.07	-182.09
L437	41.15.000	112. 3.880	4235.00	979834.12	980291.91	-59.45	-203.73	.31	-203.42
L440	41.15.050	112. 2.680	4235.00	979831.57	980291.99	-61.98	-206.26	.47	-205.79
L443	41.15.110	112. 1.000	4252.00	979831.95	980292.08	-60.19	-205.05	.79	-204.26
L462	41.15.110	112. 1.840	4245.00	979831.57	980292.08	-61.13	-205.75	.61	-205.14
L42	41. 8.450	112. 7.320	4236.00	979855.22	980282.16	-28.50	-172.82	.02	-172.80
L43	41. 9.830	112. 6.120	4244.00	979844.21	980284.22	-40.82	-185.41	.08	-185.33
L44	41. 9.830	112. 4.970	4242.00	979837.32	980284.22	-47.90	-192.42	.16	-192.26
L45	41. 9.710	112. 3.820	4305.00	979828.39	980284.05	-50.73	-197.40	.24	-197.16
L46	41. 8.390	112. 3.820	4336.00	979827.72	980282.08	-46.52	-194.24	.21	-194.03
L47	41. 8.390	112. 4.970	4285.00	979836.97	980282.08	-42.06	-188.05	.14	-187.91
L49	41. 8.390	112. 2.670	4423.00	979819.12	980282.08	-46.93	-197.62	.30	-197.32
L62	41. 8.530	111.55.190	4536.00	979830.39	980282.28	-25.23	-179.77	4.72	-175.05
L66	41. 8.380	111.58.120	4459.00	979825.82	980282.06	-36.83	-188.74	1.97	-186.77
L67	41. 8.770	111.58.460	4429.00	979826.61	980282.65	-39.45	-190.34	1.83	-188.51
L68	41. 8.650	111.56.450	4487.00	979833.07	980282.46	-27.34	-180.21	2.74	-177.47
L69	41. 8.620	111.55.080	4495.00	979833.05	980282.41	-26.56	-179.70	3.17	-176.53
L70	41. 9.080	111.56.050	4813.00	979812.10	980283.10	-18.29	-182.26	2.61	-179.65
L71	41. 9.680	111.56.290	4824.00	979812.61	980284.00	-17.64	-181.99	2.73	-179.26
L72	41.10.710	111.56.900	4754.00	979817.35	980285.53	-20.52	-182.48	2.70	-179.78
L73	41.10.740	111.55.930	5062.00	979804.11	980285.58	-5.33	-177.79	5.93	-171.86
L74	41.11.180	111.56.880	4697.00	979820.59	980286.23	-23.85	-183.87	3.12	-180.75
L75	41.10.250	111.58.750	4608.00	979815.07	980284.84	-36.35	-193.34	1.07	-192.27
L76	41. 9.690	111.58.060	4734.00	979810.24	980284.02	-28.50	-189.78	1.41	-188.37

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
L77	41. 9.710	112. 1.510	4539.00	979811.90	980284.05	-45.21	-199.85	.48	-199.37
L78	41. 9.840	112. 8.510	4235.00	979859.76	980284.23	-26.13	-170.41	-.02	-170.43
L79	41. 9.850	112. 9.090	4232.00	979862.86	980284.25	-23.33	-167.51	-.03	-167.54
L80	41. 9.850	112. 8.680	4230.00	979865.58	980284.25	-20.80	-164.91	-.02	-164.93
L81	41. 8.940	112. 8.450	4222.00	979865.53	980282.89	-20.24	-164.08	-.03	-164.11
L82	41. 8.950	112. 7.910	4229.00	979860.81	980282.91	-24.31	-168.39	-.01	-168.40
L83	41. 8.500	112. 7.860	4227.00	979861.35	980282.24	-23.30	-167.31	-.01	-167.32
L84	41.10.750	112. 8.480	4223.00	979857.36	980285.59	-31.02	-174.89	-.01	-174.90
L85	41.11.190	112. 7.310	4227.00	979849.11	980286.25	-39.55	-183.56	.03	-183.53
L86	41.11.460	112. 6.100	4246.00	979840.29	980286.66	-46.98	-191.64	.11	-191.53
L87	41.11.450	112. 2.960	4243.00	979834.78	980286.64	-52.76	-197.32	.56	-196.76
L88	41.11.440	112. 3.800	4261.00	979829.47	980286.62	-56.36	-201.53	.33	-201.20
L89	41.14.050	112. 1.470	4269.00	979827.77	980290.50	-61.19	-206.63	.61	-206.02
L90	41.14.160	111.55.640	4425.00	979838.24	980290.66	-36.20	-186.96	10.99	-175.97
L91	41.14.480	111.54.120	4624.00	979819.86	980291.14	-36.34	-193.88	16.54	-177.34
L92	41.14.600	111.53.750	4651.00	979816.44	980291.32	-37.41	-195.86	16.53	-179.33
SL36	41.21.990	112.13.450	4200.00	979877.51	980302.35	-29.79	-172.88	-.07	-172.95
SL37	41.21.700	112.11.350	4200.00	979872.97	980301.91	-33.89	-176.98	.00	-176.98
SL38	41.21.400	112.10.250	4200.00	979865.84	980301.46	-40.57	-183.66	.04	-183.62
SL39	41.21.180	112. 9.100	4200.00	979858.37	980301.14	-47.72	-190.81	.12	-190.69
L267	41.17.390	112. 1.600	4245.00	979840.00	980295.48	-56.20	-200.82	1.02	-199.80
L141	41.19.460	111.56.180	5213.00	979801.82	980298.58	-6.43	-184.03	8.39	-175.64
L268	41.21.220	112. 2.100	4305.00	979863.55	980301.20	-32.72	-179.39	2.99	-176.40
L269	41.21.650	112. 2.080	4334.00	979862.08	980301.84	-32.11	-179.76	3.16	-176.60
L270	41.21.640	112. 1.190	4624.00	979845.16	980301.83	-21.73	-179.27	4.80	-174.47
L273	41.21.010	112. 3.810	4226.00	979851.98	980300.87	-51.39	-195.37	1.20	-194.17
L274	41.21.110	112. 2.960	4232.00	979860.20	980301.04	-42.78	-186.96	1.82	-185.14
L275	41.20.160	112. 4.920	4221.00	979846.16	980299.61	-56.43	-200.23	.64	-199.59
L276	41.20.160	112. 3.780	4229.00	979848.49	980299.61	-53.34	-197.42	.98	-196.44
L277	41.20.160	112. 2.670	4234.00	979855.92	980299.61	-45.44	-189.69	1.59	-188.10
L278	41.20.140	112. 2.180	4244.00	979860.36	980299.58	-40.03	-184.62	2.06	-182.56
L279	41.20.210	112. 1.730	4282.00	979863.78	980299.69	-33.15	-179.03	2.78	-176.25
L280	41.18.320	112. 4.620	4237.00	979841.89	980296.87	-56.45	-200.80	.45	-200.35

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
L281	41.18.310	112. 3.950	4238.00	979841.26	980296.86	-56.98	-201.36	.56	-200.80
L282	41.18.410	112. 2.660	4242.00	979842.30	980297.00	-55.20	-199.72	.93	-198.79
L283	41.18.400	112. 1.610	4265.00	979845.08	980296.98	-50.74	-196.04	1.27	-194.77
L284	41.18.420	112. .140	4301.00	979854.71	980297.02	-37.75	-184.28	1.91	-182.37
L285	41.19.490	112. 1.110	4294.00	979862.29	980298.62	-32.44	-178.73	2.27	-176.45
L286	41.19.370	112. .280	4409.00	979857.27	980298.43	-26.45	-176.66	2.48	-174.18
L287	41.19.840	111.59.990	4668.00	979841.83	980299.14	-18.24	-177.27	3.10	-174.17
L288	41.20.160	111.59.500	4917.00	979825.22	980299.61	-11.89	-179.41	3.97	-175.44
L289	41.20.650	111.59.980	5156.00	979812.30	980300.35	-3.08	-178.74	4.14	-174.60
L290	41.19.110	111.59.460	4398.00	979857.28	980298.05	-27.10	-176.93	2.94	-173.99
L291	41.18.730	111.58.060	4504.00	979845.77	980297.48	-28.06	-181.51	3.51	-178.00
L292	41.19.670	111.57.940	4976.00	979819.66	980298.88	-11.18	-180.71	4.50	-176.21
L293	41.19.040	111.57.360	4713.00	979831.73	980297.95	-22.92	-183.49	4.48	-179.01
L294	41.19.550	111.56.640	5087.00	979806.91	980298.71	-13.32	-186.63	6.95	-179.63
L295	41.19.010	111.56.790	4661.00	979825.25	980297.91	-34.24	-193.04	6.71	-186.33
L296	41.18.330	111.56.140	4703.00	979825.55	980296.88	-28.97	-189.20	8.29	-180.91
L297	41.17.340	111.57.240	4397.00	979844.46	980295.41	-37.37	-187.17	5.15	-182.02
L298	41.17.340	111.58.090	4345.00	979846.81	980295.41	-39.91	-187.94	2.91	-185.03
L299	41.18.350	111.57.860	4416.00	979849.91	980296.91	-31.63	-182.08	3.55	-178.53
L300	41.16.330	111.58.110	4314.00	979842.84	980293.90	-45.29	-192.26	2.86	-189.40
L301	41.16.010	111.57.120	4429.00	979841.79	980293.41	-35.03	-185.92	5.86	-180.06
L302	41.15.550	111.56.820	4489.00	979837.58	980292.73	-32.91	-185.85	6.43	-179.42
L303	41.15.550	111.58.640	4277.00	979840.69	980292.73	-49.75	-195.46	2.16	-193.30
L304	41.16.290	111.58.620	4282.00	979842.57	980293.84	-48.50	-194.38	2.35	-192.03
L305	41.16.890	111.59.110	4298.00	979843.92	980294.74	-46.55	-192.98	1.88	-191.10
L306	41.17.800	111.59.740	4308.00	979848.50	980296.10	-42.39	-189.16	1.73	-187.43
L307	41.18.240	111.59.470	4318.00	979855.30	980296.76	-35.31	-182.42	2.17	-180.25
L308	41.17.130	111.59.730	4293.00	979843.55	980295.09	-47.74	-194.00	1.55	-192.45
L309	41.17.150	112. .440	4282.00	979840.17	980295.12	-52.19	-198.07	1.25	-196.82
L310	41.18.420	112. 6.100	4214.00	979846.97	980297.02	-53.67	-197.24	.27	-196.97
L311	41.17.780	112. 7.320	4214.00	979851.96	980296.07	-47.74	-191.31	.14	-191.17
L312	41.18.480	112. 8.460	4213.00	979858.82	980297.10	-42.01	-185.54	.08	-185.46
L313	41.18.490	112.10.770	4211.00	979876.88	980297.12	-24.15	-167.62	-.04	-167.66

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
L314	41.17.620	112. 8.600	4211.00	979867.93	980295.82	-31.81	-175.27	.05	-175.22
L315	41.16.300	112. 8.060	4214.00	979858.81	980293.85	-38.67	-182.24	.05	-182.19
L316	41.16.580	112. 7.320	4224.00	979851.01	980294.27	-45.95	-189.86	.11	-189.75
L317	41.15.870	112. 8.480	4215.00	979858.61	980293.21	-38.14	-181.74	.02	-181.72
L318	41.15.290	112.14.290	4673.00	979869.52	980292.35	16.71	-142.49	2.37	-140.12
L334	41.16.040	112. .490	4251.00	979836.78	980293.48	-56.84	-201.67	1.09	-200.58
L337	41.15.830	112. 1.530	4242.00	979834.36	980293.16	-59.79	-204.31	.74	-203.57
L338	41.16.630	112. 1.610	4239.00	979837.08	980294.35	-58.55	-202.97	.97	-202.10
L339	41.16.510	112. 5.490	4228.00	979842.53	980294.17	-53.96	-198.00	.23	-197.77
L340	41.16.750	112. 3.780	4230.00	979837.84	980294.52	-58.81	-202.92	.42	-202.50
L341	41.16.390	112. 2.810	4232.00	979835.94	980293.98	-59.98	-204.16	.55	-203.61
L346	41.15.410	112. 7.320	4216.00	979850.87	980292.53	-45.11	-188.74	.06	-188.68
L442	41.17.330	112. .960	4272.00	979839.66	980295.40	-53.92	-199.46	1.13	-198.33
L446	41.15.570	112. 2.630	4235.00	979833.47	980292.76	-60.95	-205.23	.51	-204.72
L447	41.15.570	112. 2.890	4235.00	979833.58	980292.76	-60.74	-205.02	.47	-204.55
L449	41.16.210	112. 2.190	4237.00	979834.77	980293.73	-60.42	-204.77	.65	-204.12
L450	41.16.130	112. 1.860	4239.00	979834.60	980293.61	-60.29	-204.71	.71	-204.00
L456	41.18.760	111.58.930	4382.00	979855.87	980297.52	-29.48	-178.77	2.97	-175.80
L458	41.18.720	111.57.370	4616.00	979836.39	980297.47	-26.90	-184.16	4.01	-180.15
L460	41.16.460	112. 1.640	4245.00	979836.10	980294.10	-58.72	-203.34	.80	-202.54
L272	41.21.880	112. 2.950	4226.00	979862.51	980302.18	-42.17	-186.15	2.28	-183.87
SL34	41.22.510	112.14.800	4200.00	979884.80	980303.12	-23.27	-166.36	-.09	-166.45
SL35	41.22.250	112.13.630	4200.00	979880.02	980302.73	-27.65	-170.74	-.07	-170.81
L229	41.24.950	112.11.380	4208.00	979877.34	980306.77	-33.62	-176.98	.02	-176.96
L236	41.26.870	112. 9.460	4208.00	979875.52	980309.64	-38.32	-181.68	.12	-181.56
L245	41.28.130	112.10.720	4208.00	979833.39	980311.52	-31.82	-175.18	.03	-175.15
L142	41.28.890	111.55.790	5346.00	979806.54	980312.66	-3.27	-185.40	3.35	-182.05
L143	41.28.890	111.56.940	5513.00	979795.70	980312.66	1.59	-186.23	4.17	-182.06
L228	41.24.950	112.12.440	4208.00	979884.51	980306.77	-26.45	-169.81	-.02	-169.83
L230	41.25.200	112.10.320	4208.00	979872.09	980307.13	-39.24	-182.60	.10	-182.50
L231	41.25.410	112. 9.470	4208.00	979868.15	980307.45	-43.50	-186.86	.13	-186.73
L232	41.25.370	112. 8.550	4208.00	979862.44	980307.39	-49.15	-192.51	.23	-192.23
L233	41.25.370	112. 7.610	4208.00	979857.58	980307.39	-54.01	-197.37	.37	-197.00

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
L256	41.27.640	112. 2.160	4375.00	979868.40	980310.77	-30.86	-179.91	3.55	-176.35
L257	41.27.390	112. 2.630	4325.00	979869.53	980310.41	-34.07	-181.42	2.83	-178.59
L258	41.26.880	112. 4.010	4210.00	979866.96	980309.65	-46.70	-190.13	1.52	-188.61
L259	41.26.930	112. 3.350	4288.00	979871.17	980309.73	-35.23	-181.32	2.04	-179.28
L260	41.26.550	112. 2.170	4322.00	979869.95	980309.16	-32.68	-179.93	5.96	-173.97
L261	41.23.580	112. 2.020	4310.00	979865.22	980304.73	-34.11	-180.95	7.07	-173.88
L263	41.24.740	112. 2.890	4265.00	979868.72	980306.45	-36.56	-181.86	3.43	-178.43
L271	41.22.120	112. 2.480	4255.00	979864.40	980302.54	-37.92	-182.88	3.15	-179.73
L227	41.24.990	112.14.000	4208.00	979895.13	980306.83	-15.90	-159.26	-.07	-159.33
L234	41.25.380	112. 5.610	4208.00	979853.92	980307.41	-57.68	-201.04	.84	-200.20
L235	41.25.380	112. 6.760	4208.00	979854.34	980307.41	-56.76	-200.12	.54	-199.58
L237	41.25.900	112.13.020	4208.00	979887.12	980308.18	-25.26	-168.62	-.04	-168.66
L238	41.26.630	112.13.010	4208.00	979885.30	980309.27	-28.17	-171.53	-.05	-171.58
L242	41.28.770	112.15.000	4209.00	979880.52	980312.47	-36.05	-179.45	-.10	-179.55
L243	41.28.440	112.13.370	4209.00	979878.15	980311.97	-37.92	-181.32	-.07	-181.39
L244	41.28.020	112.11.880	4208.00	979881.22	980311.34	-34.32	-177.68	-.03	-177.71
L246	41.28.750	112. 9.300	4212.00	979884.36	980312.44	-31.90	-175.40	.11	-175.29
L255	41.28.190	112. 2.900	4253.00	979870.56	980311.60	-41.01	-185.90	2.03	-183.87
L262	41.24.220	112. 2.100	4316.00	979865.12	980305.67	-34.59	-181.63	6.70	-174.93
L264	41.24.770	112. 2.120	4353.00	979864.94	980306.49	-32.11	-180.41	6.22	-174.19
L265	41.25.720	112. 2.080	4309.00	979869.42	980307.92	-33.20	-180.00	7.34	-172.66
L266	41.28.290	112. 1.630	4344.00	979872.00	980311.75	-31.15	-179.15	4.29	-174.86
BC 73	41.32.330	112. .870	4271.00	979884.36	980317.77	-31.68	-177.19	5.08	-172.11
FB 1	41.32.400	112. 4.970	4228.00	979869.14	980317.87	-51.05	-195.09	.65	-194.44
BC 74	41.32.500	112. .870	4280.00	979885.17	980318.02	-30.27	-176.08	5.49	-170.59
BC 1	41.32.590	112. 4.970	4228.00	979868.97	980318.16	-51.51	-195.55	.56	-194.89
BC 75	41.32.680	112. .870	4290.00	979885.42	980318.30	-29.36	-175.52	6.47	-169.05
BC 2	41.32.770	112. 4.980	4228.00	979869.24	980318.43	-51.51	-195.55	.67	-194.88
BC 76	41.32.880	112. .970	4285.00	979884.56	980318.59	-30.87	-176.86	6.28	-170.53
BC 3	41.32.950	112. 4.980	4229.00	979869.28	980318.70	-51.64	-195.72	.68	-195.04
BC 77	41.33.040	112. 1.090	4292.00	979885.24	980318.84	-29.89	-176.11	5.94	-170.17
BC 4	41.33.120	112. 4.980	4231.00	979869.31	980318.95	-51.67	-195.82	.70	-195.12
BC 5	41.33.300	112. 4.980	4232.00	979869.43	980319.21	-51.72	-195.90	.72	-195.18

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
BC 78	41.33.360	112. 1.170	4270.00	979886.08	980319.31	-31.60	-177.07	7.01	-170.06
BC 6	41.33.480	112. 4.980	4233.00	979869.62	980319.49	-51.72	-195.93	.75	-195.13
BC 7	41.33.490	112. 4.980	4233.00	979869.67	980319.51	-51.69	-195.90	.75	-195.15
BC 79	41.33.530	112. 1.300	4294.00	979885.45	980319.56	-30.22	-176.51	6.64	-169.87
BC 8	41.33.640	112. 4.980	4234.00	979869.98	980319.73	-51.59	-195.84	.77	-195.07
BC 80	41.33.750	112. 1.380	4298.00	979885.64	980319.90	-29.99	-176.42	6.87	-169.55
BC 9	41.33.790	112. 4.980	4235.00	979870.06	980319.95	-51.55	-195.83	.80	-195.03
BC 81	41.33.930	112. 1.470	4270.00	979887.41	980320.16	-31.12	-176.59	7.19	-169.40
BC 10	41.34.070	112. 4.990	4235.00	979870.37	980320.37	-51.66	-195.94	.85	-195.09
BC 82	41.34.130	112. 1.630	4268.00	979888.19	980320.45	-30.81	-176.22	7.09	-169.13
BC 83	41.34.250	112. 1.710	4265.00	979887.79	980320.64	-31.69	-176.99	7.03	-169.96
BC 11	41.34.240	112. 4.990	4235.00	979870.57	980320.62	-51.71	-195.99	.88	-195.11
BC 12	41.34.410	112. 4.990	4235.00	979870.85	980320.87	-51.68	-195.96	.91	-195.05
BC 84	41.34.490	112. 1.870	4265.00	979889.08	980320.99	-30.75	-176.05	6.62	-169.43
BC 13	41.34.590	112. 4.990	4236.00	979871.29	980321.15	-51.42	-195.74	.96	-194.79
BC 85	41.34.720	112. 1.980	4265.00	979889.32	980321.34	-30.86	-176.16	7.12	-169.04
BC 14	41.34.760	112. 4.990	4237.00	979871.50	980321.40	-51.27	-195.62	1.01	-194.61
BC 86	41.34.880	112. 2.140	4253.00	979890.09	980321.57	-31.44	-176.34	6.43	-169.91
BC 15	41.34.940	112. 5.000	4238.00	979872.08	980321.68	-50.98	-195.36	1.05	-194.31
BC 87	41.35.050	112. 2.260	4251.00	979890.93	980321.84	-31.05	-175.88	6.76	-169.12
BC 16	41.35.150	112. 5.000	4236.00	979872.84	980321.98	-50.70	-195.02	1.12	-193.90
BC 88	41.35.200	112. 2.410	4260.00	979890.93	980322.05	-30.43	-175.56	6.04	-169.52
BC 89	41.35.330	112. 2.550	4270.00	979890.37	980322.24	-30.23	-175.71	5.49	-170.22
BC 17	41.35.330	112. 5.000	4235.00	979873.55	980322.24	-50.35	-194.63	1.18	-193.45
BC 18	41.35.600	112. 5.000	4235.00	979874.26	980322.66	-50.05	-194.33	1.27	-193.05
BC 90	41.35.630	112. 2.680	4267.00	979890.28	980322.70	-31.06	-176.43	6.08	-170.35
BC 91	41.35.790	112. 2.690	4263.00	979889.72	980322.95	-32.24	-177.48	6.86	-170.62
BC 19	41.35.800	112. 5.000	4239.00	979874.83	980322.96	-49.41	-193.83	1.34	-192.49
P10	41.29.750	111.58.000	5054.00	979827.01	980313.92	-11.53	-183.72	11.10	-172.62
L248	41.30.590	112. 6.120	4214.00	979875.12	980315.18	-43.69	-187.26	.41	-186.85
L253	41.30.170	112. 1.960	4292.00	979869.09	980314.55	-41.76	-187.98	1.76	-186.22
L158	41.34.780	112.14.600	4265.00	979912.92	980321.43	-7.35	-152.65	.76	-151.89
L214	41.33.010	112.11.810	4233.00	979901.57	980318.79	-19.07	-163.28	.01	-163.27

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
L131	41.32.290	111.57.440	5675.00	979801.76	980317.71	17.84	-175.50	1.87	-173.63
L133	41.30.480	112. .880	4452.00	979868.09	980315.00	-28.15	-179.83	2.22	-177.61
L134	41.30.330	111.56.690	5200.00	979819.04	980314.78	-6.63	-183.79	2.02	-181.77
L140	41.29.610	111.56.610	5206.00	979816.27	980313.70	-7.76	-185.12	2.56	-182.56
L144	41.29.980	111.59.200	4613.00	979862.16	980314.26	-18.20	-175.36	9.13	-166.23
L159	41.34.620	112.13.970	4261.00	979912.26	980321.20	-8.14	-153.31	.46	-152.85
L160	41.34.420	112.13.120	4239.00	979910.86	980320.89	-11.31	-155.73	.34	-155.39
L161	41.34.090	112.11.320	4246.00	979906.51	980320.39	-14.50	-159.16	.04	-159.12
L162	41.35.460	112.12.380	4257.00	979914.17	980322.45	-7.86	-152.89	.35	-152.54
L163	41.35.360	112.13.500	4425.00	979903.53	980322.30	-2.56	-153.31	.73	-152.58
L164	41.35.850	112.12.320	4322.00	979910.76	980323.03	-5.74	-152.99	.27	-152.72
L170	41.35.570	112.10.650	4248.00	979905.58	980322.61	-17.46	-162.19	.11	-162.08
L171	41.31.920	112. 2.810	4223.00	979868.77	980317.16	-51.17	-195.04	1.45	-193.59
L172	41.32.540	112. 3.790	4224.00	979868.65	980318.09	-52.13	-196.04	1.00	-195.04
L173	41.32.400	112. 4.960	4228.00	979869.36	980317.87	-50.83	-194.87	.65	-194.22
L174	41.32.820	112. 6.560	4228.00	979874.64	980318.50	-46.18	-190.22	.39	-189.83
L175	41.33.870	112. 7.150	4235.00	979878.30	980320.07	-43.43	-187.71	.38	-187.33
L176	41.34.070	112. 7.720	4237.00	979882.02	980320.37	-39.82	-184.17	.31	-183.86
L177	41.34.770	112. 8.900	4238.00	979890.35	980321.41	-32.44	-176.82	.21	-176.61
L178	41.34.080	112. 9.470	4238.00	979894.30	980320.37	-27.45	-171.83	.13	-171.70
L179	41.33.940	112.10.630	4237.00	979901.26	980320.17	-20.38	-164.73	.06	-164.67
L180	41.35.610	112. 7.690	4230.00	979883.19	980322.66	-41.60	-185.71	.41	-185.30
L188	41.35.590	112. 5.000	4235.00	979874.33	980322.64	-49.97	-194.25	1.27	-192.98
L189	41.34.930	112. 4.990	4238.00	979871.99	980321.65	-51.04	-195.42	1.05	-194.37
L190	41.34.070	112. 4.990	4235.00	979870.35	980320.37	-51.68	-195.96	.85	-195.11
L191	41.33.420	112. 4.980	4233.00	979869.56	980319.41	-51.69	-195.90	.74	-195.16
L198	41.34.250	112. 1.720	4265.00	979887.95	980320.64	-31.53	-176.83	6.93	-169.90
L199	41.33.360	112. 1.180	4270.00	979886.16	980319.31	-31.52	-176.99	6.91	-170.08
L200	41.32.310	112. .870	4259.00	979834.38	980317.74	-32.76	-177.86	5.16	-172.70
L201	41.32.160	112. 1.900	4230.00	979873.18	980317.52	-46.47	-190.58	2.31	-188.27
L202	41.31.780	112. 1.740	4262.00	979871.33	980316.95	-44.74	-189.94	2.18	-187.76
L203	41.31.500	112. .880	4326.00	979874.74	980316.53	-34.89	-182.27	2.96	-179.31
L204	41.31.020	112. .330	4413.00	979873.24	980315.82	-27.49	-177.84	3.38	-174.46

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
L205	41.33.300	112. 7.720	4233.00	979881.54	980319.21	-39.42	-183.63	.28	-183.35
L206	41.32.560	112. 8.300	4232.00	979885.00	980318.12	-35.06	-179.24	.20	-179.04
L207	41.32.110	112. 9.460	4231.00	979890.50	980317.44	-28.87	-173.02	.09	-172.93
L208	41.32.120	112.10.630	4226.00	979895.32	980317.45	-24.63	-168.61	.03	-168.58
L209	41.31.250	112.10.610	4221.00	979891.53	980316.16	-27.49	-171.30	.03	-171.27
L210	41.31.240	112.11.220	4223.00	979890.95	980316.14	-27.98	-171.85	.20	-171.85
L211	41.30.590	112.10.600	4225.00	979890.32	980315.18	-27.46	-171.40	.02	-171.38
L212	41.29.510	112.10.580	4215.00	979889.88	980313.55	-27.21	-170.81	.02	-170.79
L213	41.33.000	112.10.640	4239.00	979898.83	980318.77	-21.22	-165.64	.04	-165.60
L215	41.32.990	112. 9.470	4239.00	979894.12	980318.76	-25.92	-170.34	.10	-170.24
L216	41.32.980	112. 8.310	4234.00	979885.57	980318.75	-34.93	-179.18	.21	-178.97
L251	41.30.650	112. 2.610	4336.00	979868.86	980315.27	-38.56	-186.28	1.21	-185.07
L254	41.29.200	112. .930	4336.00	979876.90	980313.09	-28.35	-176.07	4.23	-171.84
MB95	41.31.740	112. 1.300	4305.00	979876.83	980316.90	-35.14	-181.81	2.52	-179.29
MB96	41.33.120	112. 7.700	4230.00	979874.81	980318.95	-46.27	-190.38	.27	-190.11
MB97	41.34.140	112.12.300	4245.00	979906.48	980320.48	-14.72	-159.34	.08	-159.26
L247	41.29.310	112. 7.720	4212.00	979879.20	980313.27	-37.88	-181.38	.24	-181.14
L249	41.30.580	112. 5.280	4218.00	979873.00	980315.16	-45.42	-189.12	.55	-188.57
L250	41.30.590	112. 2.840	4220.00	979868.23	980315.18	-50.02	-193.79	1.42	-192.37
L252	41.30.660	112. 1.590	4429.00	979869.36	980315.28	-29.33	-180.22	1.70	-178.52
BW1	41.31.230	112. 2.090	4281.00	979870.38	980316.12	-43.07	-188.92	1.60	-187.32
BW2	41.32.610	112. 4.150	4223.00	979869.70	980318.20	-51.28	-195.15	.88	-194.27
BW3	41.32.230	112. 2.160	4231.00	979876.07	980317.62	-43.58	-187.73	2.06	-185.67
BC 92	41.35.950	112. 2.860	4275.00	979889.54	980323.18	-31.54	-177.18	6.16	-171.02
BC 24	41.35.960	112. 6.150	4255.00	979874.92	980323.20	-48.05	-193.01	.80	-192.21
BC 20	41.35.980	112. 5.000	4241.00	979875.39	980323.22	-48.92	-193.41	1.41	-192.00
BC 93	41.36.090	112. 3.050	4285.00	979889.91	980323.38	-30.42	-176.41	5.53	-170.88
BC 21	41.36.150	112. 5.000	4241.00	979876.20	980323.48	-48.37	-192.86	1.51	-191.35
BC 94	41.36.220	112. 3.280	4285.00	979890.37	980323.59	-30.16	-176.15	4.88	-171.27
BC 25	41.36.230	112. 6.160	4257.00	979875.32	980323.60	-47.87	-192.90	.84	-192.05
BC 22	41.36.300	112. 5.000	4242.00	979876.78	980323.70	-47.92	-192.44	1.59	-190.85
BC 23	41.36.300	112. 5.580	4247.00	979875.48	980323.70	-48.75	-193.44	1.13	-192.31
BC 22	41.36.300	112. 5.050	4242.00	979876.84	980323.70	-47.86	-192.38	1.53	-190.85

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
BC111	41.36.350	112. 4.870	4242.00	979877.07	980323.77	-47.70	-192.22	1.72	-190.50
BC 95	41.36.390	112. 3.480	4282.00	979890.21	980323.84	-30.86	-176.74	4.43	-172.31
BC110	41.36.440	112. 4.660	4242.00	979879.34	980323.91	-45.56	-190.08	2.02	-188.06
BC 26	41.36.450	112. 6.170	4256.00	979875.73	980323.92	-47.87	-192.87	.87	-192.00
BC109	41.36.500	112. 4.450	4242.00	979881.35	980323.99	-43.14	-187.66	2.35	-185.31
BC 96	41.36.600	112. 3.650	4276.00	979890.21	980324.16	-31.74	-177.42	4.43	-172.99
BC108	41.36.650	112. 4.180	4251.00	979885.40	980324.23	-38.97	-183.80	3.02	-180.78
BC 27	41.36.670	112. 6.170	4255.00	979876.54	980324.26	-47.40	-192.36	.91	-191.45
BC107	41.36.740	112. 4.020	4261.00	979887.64	980324.36	-35.93	-181.10	3.51	-177.59
BC 97	41.36.820	112. 3.830	4274.00	979889.82	980324.48	-32.65	-178.26	4.22	-174.04
BC 28	41.36.850	112. 6.180	4257.00	979877.12	980324.52	-46.98	-192.01	.95	-191.06
BC 98	41.36.980	112. 3.960	4278.00	979890.48	980324.72	-31.85	-177.60	3.98	-173.62
BC 29	41.37.080	112. 6.180	4260.00	979877.51	980324.87	-46.67	-191.80	.99	-190.81
BC 99	41.37.130	112. 4.080	4285.00	979890.93	980324.94	-30.96	-176.95	3.81	-173.14
BC100	41.37.270	112. 4.200	4284.00	979891.39	980325.15	-30.81	-176.76	3.66	-173.10
BC 30	41.37.380	112. 6.180	4262.00	979878.73	980325.32	-45.71	-190.91	1.04	-189.87
BC101	41.37.410	112. 4.310	4283.00	979892.08	980325.36	-30.42	-176.34	3.50	-172.84
BC 31	41.37.580	112. 5.190	4265.00	979879.38	980325.61	-45.07	-190.37	1.07	-189.30
BC102	41.37.600	112. 4.450	4286.00	979892.10	980325.64	-30.40	-176.42	3.28	-173.14
BC103	41.37.760	112. 4.550	4280.00	979892.42	980325.89	-30.89	-176.71	3.26	-173.45
BC 32	41.37.760	112. 6.190	4267.00	979890.06	980325.89	-44.48	-189.85	1.10	-188.75
BC104	41.37.920	112. 4.650	4273.00	979892.70	980326.12	-31.50	-177.08	3.12	-173.96
BC 33	41.37.930	112. 6.190	4268.00	979891.34	980326.13	-43.34	-188.75	1.13	-187.62
BC105	41.38.080	112. 4.710	4278.00	979892.06	980326.35	-31.90	-177.65	3.10	-174.55
BC 69	41.38.090	112. 4.960	4265.00	979889.70	980326.37	-35.51	-180.81	2.56	-178.25
BC 70	41.38.090	112. 5.280	4260.00	979886.78	980326.37	-38.90	-184.03	2.12	-181.91
BC 71	41.38.100	112. 5.570	4265.00	979885.39	980326.38	-39.83	-185.13	1.69	-183.44
BC 72	41.38.110	112. 5.880	4271.00	979884.30	980326.40	-40.37	-185.88	1.39	-184.49
BC 34	41.38.110	112. 6.200	4270.00	979892.96	980326.40	-41.80	-187.28	1.16	-186.12
BC 68	41.38.240	112. 4.960	4269.00	979890.44	980326.60	-34.62	-180.06	2.68	-177.38
BC 35	41.38.310	112. 6.200	4270.00	979885.11	980326.70	-39.95	-185.43	1.19	-184.24
BC 67	41.38.430	112. 4.980	4271.00	979892.35	980326.87	-32.79	-178.30	2.63	-175.67
BC106	41.38.430	112. 4.730	4305.00	979892.30	980326.87	-29.64	-176.31	3.07	-173.24

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER	
BC 36	41.38.430	112.	6.200	4270.00	979886.17	980326.87	-39.07	-184.54	1.22	-183.32
BC 37	41.38.600	112.	6.200	4270.00	979888.59	980327.14	-36.91	-182.39	1.26	-181.13
BC 66	41.38.620	112.	5.030	4291.00	979893.19	980327.17	-30.37	-176.56	2.53	-174.03
BC 38	41.38.780	112.	6.200	4270.00	979890.43	980327.41	-35.34	-180.81	1.30	-179.51
BC 65	41.38.790	112.	5.040	4284.00	979895.51	980327.42	-28.86	-174.81	2.65	-172.16
BC 64	41.38.940	112.	5.050	4283.00	979896.97	980327.65	-27.82	-173.74	2.65	-171.09
BC 39	41.38.940	112.	6.200	4270.00	979892.05	980327.65	-33.97	-179.44	1.32	-178.12
BC 63	41.39.120	112.	5.050	4282.00	979898.31	980327.91	-26.84	-172.72	2.78	-169.94
BC 40	41.39.130	112.	6.200	4274.00	979892.99	980327.93	-32.93	-178.54	1.36	-177.18
BC 41	41.39.300	112.	6.200	4278.00	979893.42	980328.18	-32.37	-178.12	1.37	-176.75
BC 62	41.39.380	112.	5.050	4285.00	979898.82	980328.30	-26.43	-172.42	2.90	-169.52
BC 42	41.39.470	112.	6.200	4282.00	979894.08	980328.44	-31.60	-177.48	1.39	-176.09
BC 61	41.39.580	112.	5.150	4291.00	979899.45	980328.60	-25.54	-171.73	2.80	-168.93
BC 43	41.39.640	112.	6.200	4286.00	979894.46	980328.69	-31.09	-177.11	1.42	-175.69
BC 44	41.39.830	112.	6.210	4290.00	979894.41	980328.98	-31.05	-177.21	1.43	-175.78
BC 60	41.39.840	112.	5.280	4303.00	979897.75	980328.99	-26.50	-173.10	2.63	-170.47
BC 48	41.40.000	112.	5.990	4290.00	979895.00	980329.23	-30.71	-176.87	1.56	-175.21
BC 49	41.40.000	112.	5.750	4290.00	979895.30	980329.23	-30.41	-176.57	1.95	-174.62
BC 50	41.40.010	112.	5.440	4297.00	979896.41	980329.24	-28.66	-175.05	2.39	-172.65
BC 51	41.40.010	112.	5.280	4305.00	979897.13	980329.24	-27.18	-173.85	2.68	-171.17
BC 50	41.40.010	112.	5.440	4297.00	979896.30	980329.24	-28.77	-175.16	2.39	-172.77
BC 45	41.40.000	112.	6.210	4293.00	979894.49	980329.23	-30.94	-177.20	1.45	-175.75
BC 46	41.40.140	112.	6.210	4295.00	979894.08	980329.45	-31.37	-177.70	1.48	-176.22
BC 52	41.40.180	112.	5.320	4305.00	979896.38	980329.50	-28.19	-174.86	2.71	-172.15
BC 47	41.40.300	112.	6.210	4296.00	979893.27	980329.68	-32.33	-178.69	1.51	-177.18
BC 53	41.40.330	112.	5.330	4299.00	979895.46	980329.72	-29.90	-176.36	2.81	-173.55
BC 55	41.40.680	112.	5.330	4299.00	979894.19	980330.24	-31.69	-178.15	3.08	-175.07
BC 56	41.40.850	112.	5.340	4299.00	979894.47	980330.49	-31.66	-178.12	3.19	-174.93
BC 57	41.41.030	112.	5.340	4303.00	979894.98	980330.77	-31.05	-177.65	3.32	-174.33
BC 58	41.41.200	112.	5.340	4305.00	979895.41	980331.02	-30.67	-177.34	3.48	-173.86
BC 59	41.41.420	112.	5.350	4312.00	979896.01	980331.35	-29.75	-176.66	3.59	-173.07
BC 54	41.40.500	112.	5.330	4301.00	979894.76	980329.98	-30.67	-177.20	2.89	-174.31
P169	41.39.990	112.10.700	4277.00	979901.71	980329.21	-25.21	-170.92	.17	-170.75	

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
SI11	41.42.570	112.10.450	4320.00	979909.71	980333.07	-17.02	-164.20	.27	-163.93
SI12	41.42.620	112. 9.850	4290.00	979911.57	980333.15	-18.06	-164.22	.31	-163.91
SI95	41.41.600	112.12.050	4352.00	979910.79	980331.62	-11.48	-159.75	.12	-159.63
SI96	41.41.600	112.13.250	4309.00	979909.53	980331.62	-16.69	-163.49	.31	-163.19
SI97	41.41.600	112.14.450	4304.00	979903.82	980331.62	-22.97	-169.60	.27	-169.33
SI111	41.37.500	112.13.800	4262.00	979916.41	980325.49	-8.20	-153.40	.87	-152.53
SI112	41.38.950	112.10.700	4271.00	979910.78	980327.66	-15.15	-160.66	.15	-160.51
SI113	41.38.050	112. 9.750	4262.00	979915.96	980326.31	-9.47	-154.67	.23	-154.44
L157	41.36.150	112.14.060	4828.00	979880.13	980323.48	10.76	-153.72	.82	-152.90
L165	41.36.220	112.12.300	4285.00	979913.80	980323.59	-6.73	-152.72	.48	-152.24
L166	41.36.790	112.12.310	4256.00	979916.17	980324.43	-7.94	-152.94	.48	-152.46
L167	41.37.390	112.11.800	4258.00	979910.82	980325.34	-14.00	-159.07	.19	-158.89
L168	41.37.410	112.10.670	4259.00	979908.39	980325.36	-16.37	-161.47	.14	-161.33
L169	41.37.420	112. 9.990	4232.00	979904.49	980325.37	-22.82	-167.00	.19	-166.81
L181	41.36.540	112. 9.560	4249.00	979899.55	980324.06	-24.85	-169.61	.20	-169.41
L182	41.37.470	112. 8.920	4254.00	979893.00	980325.45	-32.32	-177.25	.30	-176.95
L183	41.37.380	112. 7.560	4262.00	979892.21	980325.32	-42.23	-187.43	.54	-186.89
L184	41.36.580	112. 8.330	4248.00	979887.61	980324.12	-36.95	-181.67	.36	-181.31
L185	41.37.380	112. 6.190	4262.00	979878.86	980325.32	-45.58	-190.78	1.03	-189.75
L186	41.36.680	112. 6.180	4255.00	979876.69	980324.27	-47.36	-192.32	.91	-191.41
L187	41.35.960	112. 6.160	4255.00	979874.84	980323.20	-48.13	-193.09	.79	-192.30
L192	41.36.300	112. 5.060	4242.00	979876.81	980323.70	-47.89	-192.41	1.52	-190.89
L193	41.36.500	112. 4.430	4242.00	979831.37	980323.99	-43.12	-187.64	2.38	-185.26
L194	41.36.640	112. 4.190	4251.00	979885.66	980324.21	-38.70	-183.53	2.99	-180.54
L195	41.37.120	112. 4.060	4285.00	979890.78	980324.93	-31.10	-177.09	3.86	-173.23
L196	41.36.820	112. 3.840	4274.00	979889.98	980324.48	-32.49	-178.10	4.17	-173.93
L197	41.36.390	112. 3.490	4282.00	979890.26	980323.84	-30.81	-176.69	4.39	-172.30
BW4	41.38.050	112. 5.400	4265.00	979889.95	980326.31	-35.20	-180.50	1.88	-178.62
BW5	41.39.930	112. 5.800	4297.00	979896.53	980329.12	-28.32	-174.71	1.96	-172.85
BW6	41.42.770	112. 6.100	4326.00	979901.42	980333.37	-25.05	-172.43	1.93	-170.50
BW7	41.42.620	112. 8.200	4322.00	979898.16	980333.15	-28.46	-175.71	.59	-175.12
SI113	41.43.010	112.13.550	4336.00	979912.76	980333.73	-13.13	-160.85	.50	-160.35
SI114	41.42.950	112.13.700	4344.00	979913.73	980333.64	-11.31	-159.31	.45	-158.86

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
SI55	41.44.380	112. 9.850	4342.00	979908.77	980335.77	-18.58	-166.51	.41	-166.10
SI56	41.46.120	112. 9.920	4370.00	979911.44	980338.37	-15.89	-164.77	.66	-164.11
SI57	41.48.780	112. 9.990	4412.00	979911.75	980342.34	-15.60	-165.91	.66	-165.25
SI93	41.46.050	112.13.150	4507.00	979903.37	980338.27	-10.97	-164.52	19.37	-145.15
SI94	41.45.200	112.14.400	4471.00	979903.09	980337.01	-13.38	-165.70	9.74	-155.96
PW8	41.44.510	112. 6.950	4376.00	979898.34	980335.98	-26.03	-175.12	.79	-174.33
BW9	41.45.730	112. 6.270	4397.00	979898.79	980337.80	-25.43	-175.23	.84	-174.39
BW10	41.46.650	112. 5.960	4439.00	979897.70	980339.16	-23.93	-175.16	.62	-174.54
BW11	41.48.230	112. 4.520	4467.00	979906.18	980341.51	-15.16	-167.35	.47	-166.88
BW30	41.47.390	112. 9.200	4361.00	979904.39	980340.27	-25.68	-174.26	.50	-173.76
612	41.50.070	112. 5.500	4514.00	979903.24	980344.27	-16.44	-170.23	.43	-169.80
613	41.50.070	112. 6.600	4445.00	979907.70	980344.27	-18.47	-169.91	.37	-169.54
614	41.50.150	112. 7.750	4408.00	979905.81	980344.38	-23.95	-174.13	.41	-173.72
615	41.50.530	112.10.100	4494.00	979913.57	980344.95	-8.67	-161.78	.52	-161.26
616	41.56.500	112.10.450	4456.00	979905.51	980353.88	-29.24	-181.05	2.55	-178.50
617	41.56.500	112.10.900	4426.00	979908.06	980353.88	-29.51	-180.30	1.88	-178.42
618	41.56.500	112.11.800	4468.00	979914.17	980353.88	-19.45	-171.67	1.39	-170.23
619	41.56.500	112.12.800	4385.00	979920.23	980353.88	-21.20	-170.59	1.11	-169.48
SI33	41.53.550	112.12.500	4474.00	979914.01	980349.47	-14.63	-167.06	1.15	-165.91
SI34	41.54.850	112.14.000	4578.00	979914.92	980351.42	-5.89	-161.86	1.48	-160.38
SI58	41.50.510	112.11.130	4596.00	979908.09	980344.92	-4.53	-161.11	.69	-160.42
BW22	41.53.050	112. 8.200	4834.00	979884.90	980348.73	-9.14	-173.83	1.36	-172.47
BW23	41.53.050	112.10.650	4486.00	979907.50	980348.73	-19.28	-172.11	.83	-171.28
BW31	41.50.190	112. 9.000	4324.00	979913.23	980344.44	-24.50	-171.81	.56	-171.25
6110	41.57.800	112.10.750	4412.00	979913.70	980355.84	-27.15	-177.46	4.08	-173.38
6111	41.58.400	112.11.450	4419.00	979911.81	980356.73	-29.27	-179.82	2.52	-177.30
6112	41.58.450	112.12.600	4400.00	979912.76	980356.80	-30.18	-180.08	1.36	-178.72
6113	41.58.500	112.13.900	4471.00	979917.36	980356.87	-18.98	-171.30	1.11	-170.19
6114	42. .000	112.11.850	4467.00	979920.02	980359.12	-18.93	-171.12	3.17	-167.95
SI35	41.56.550	112.13.950	4499.00	979920.55	980353.96	-10.23	-163.51	1.15	-162.36
SI52	41.58.260	112.14.250	4509.00	979921.63	980356.52	-10.77	-164.39	1.18	-163.21
A2	41. 6.470	111.54.180	5201.00	979787.71	980279.21	-2.30	-179.49	6.94	-172.55
A1	41. 6.480	111.54.300	5178.00	979790.50	980279.22	-1.68	-178.09	6.17	-171.92

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A3	41. 6.480	111.54.450	5032.00	979798.98	980279.22	-6.93	-178.36	5.88	-172.48
A100	41. 6.490	111.54.650	4885.00	979807.11	980279.23	-12.64	-179.07	5.20	-173.87
A105	41. 6.500	111.54.720	4880.00	979806.39	980279.25	-13.84	-180.10	4.78	-175.32
A110	41. 6.490	111.54.840	4874.00	979806.15	980279.23	-14.64	-180.69	4.27	-176.42
A115	41. 6.480	111.54.940	4884.00	979804.85	980279.22	-14.98	-181.37	3.87	-177.50
A120	41. 6.440	111.55.040	4902.00	979803.22	980279.16	-14.86	-181.87	3.54	-178.33
A125	41. 6.400	111.55.140	4918.00	979801.73	980279.10	-14.79	-182.34	3.35	-178.99
A130	41. 6.370	111.55.230	4922.00	979801.25	980279.06	-14.85	-182.54	3.23	-179.31
A135	41. 6.330	111.55.340	4917.00	979801.26	980279.00	-15.24	-182.76	3.02	-179.74
A140	41. 6.290	111.55.430	4904.00	979801.79	980278.95	-15.89	-182.96	2.87	-180.09
A145	41. 6.250	111.55.530	4883.00	979802.85	980278.88	-16.74	-183.10	2.71	-180.39
A150	41. 6.210	111.55.640	4858.00	979804.28	980278.83	-17.60	-183.11	2.54	-180.57
A155	41. 6.180	111.55.730	4842.00	979805.15	980278.78	-18.19	-183.15	2.44	-180.71
A160	41. 6.150	111.55.820	4833.00	979805.47	980278.74	-18.68	-183.34	2.34	-181.00
A165	41. 6.110	111.55.930	4825.00	979805.55	980278.66	-19.18	-183.56	2.24	-181.32
A170	41. 6.090	111.56.020	4816.00	979805.82	980278.64	-19.82	-183.90	2.17	-181.73
A175	41. 6.080	111.56.140	4807.00	979806.03	980278.62	-20.45	-184.22	2.07	-182.15
A180	41. 6.080	111.56.240	4799.00	979806.10	980278.62	-21.13	-184.63	1.99	-182.64
A185	41. 6.080	111.56.350	4795.00	979805.96	980278.62	-21.65	-185.01	1.90	-183.11
A190	41. 6.090	111.56.450	4793.00	979805.64	980278.64	-22.17	-185.46	1.82	-183.64
A195	41. 6.110	111.56.560	4792.00	979805.33	980278.66	-22.60	-185.86	1.73	-184.13
A200	41. 6.120	111.56.660	4791.00	979805.08	980278.70	-22.97	-186.20	1.68	-184.52
A205	41. 6.140	111.56.770	4789.00	979804.75	980278.73	-23.52	-186.68	1.61	-185.07
A210	41. 6.150	111.56.880	4785.00	979804.61	980278.74	-24.06	-187.08	1.54	-185.54
A215	41. 6.160	111.56.990	4779.00	979804.61	980278.76	-24.63	-187.45	1.48	-185.97
A220	41. 6.180	111.57.100	4778.00	979804.27	980278.78	-25.09	-187.87	1.42	-186.45
A225	41. 6.200	111.57.200	4779.00	979803.77	980278.81	-25.53	-188.35	1.40	-186.95
A230	41. 6.210	111.57.310	4779.00	979803.32	980278.83	-25.99	-188.81	1.36	-187.45
A235	41. 6.210	111.57.430	4775.00	979803.14	980278.83	-26.55	-189.23	1.30	-187.93
A240	41. 6.220	111.57.530	4772.00	979802.87	980278.84	-27.12	-189.70	1.28	-188.42
A245	41. 6.220	111.57.640	4769.00	979802.59	980278.84	-27.68	-190.16	1.25	-188.91
A250	41. 6.220	111.57.740	4768.00	979802.18	980278.84	-28.19	-190.63	1.25	-189.38
A255	41. 6.220	111.57.860	4767.00	979801.77	980278.84	-28.69	-191.10	1.20	-189.90

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A260	41. 6.220	111.57.950	4766.00	979801.33	980278.84	-29.23	-191.60	1.20	-190.40
A265	41. 6.220	111.58.070	4765.00	979800.92	980278.84	-29.73	-192.07	1.18	-190.89
A270	41. 6.220	111.58.180	4759.00	979800.88	980278.84	-30.34	-192.47	1.17	-191.30
A275	41. 6.210	111.58.290	4750.00	979801.04	980278.83	-31.00	-192.83	1.12	-191.71
A280	41. 6.210	111.58.400	4746.00	979800.95	980278.83	-31.47	-193.16	1.07	-192.09
A285	41. 6.230	111.58.500	4743.00	979800.74	980278.86	-31.99	-193.58	1.11	-192.47
A290	41. 6.220	111.58.620	4741.00	979800.58	980278.84	-32.33	-193.85	1.03	-192.82
A295	41. 6.220	111.58.720	4730.00	979800.94	980278.84	-33.00	-194.15	1.01	-193.14
A300	41. 6.220	111.58.830	4713.00	979801.89	980278.84	-33.65	-194.22	.92	-193.30
A305	41. 6.220	111.58.940	4697.00	979802.74	980278.84	-34.31	-194.33	.87	-193.46
A310	41. 6.220	111.59.060	4686.00	979803.28	980278.84	-34.80	-194.45	.83	-193.62
A315	41. 6.220	111.59.160	4672.00	979804.03	980278.84	-35.37	-194.54	.79	-193.75
A320	41. 6.220	111.59.270	4654.00	979805.02	980278.84	-36.07	-194.63	.73	-193.90
A325	41. 6.220	111.59.380	4635.00	979805.99	980278.84	-36.89	-194.80	.69	-194.11
A330	41. 6.220	111.59.490	4617.00	979807.01	980278.84	-37.56	-194.86	.67	-194.19
A335	41. 6.220	111.59.590	4606.00	979807.56	980278.84	-38.05	-194.97	.65	-194.32
A340	41. 6.220	111.59.700	4600.00	979807.85	980278.84	-38.32	-195.04	.63	-194.41
A345	41. 6.220	111.59.800	4592.00	979808.22	980278.84	-38.70	-195.15	.61	-194.54
A350	41. 6.220	111.59.920	4575.00	979809.19	980278.84	-39.32	-195.19	.59	-194.60
A355	41. 6.220	112. .010	4555.00	979810.38	980278.84	-40.02	-195.20	.59	-194.61
A360	41. 6.220	112. .130	4535.00	979811.59	980278.84	-40.69	-195.19	.58	-194.61
A365	41. 6.220	112. .250	4532.00	979811.67	980278.84	-40.89	-195.29	.57	-194.72
A370N	41. 6.220	112. .360	4528.00	979811.71	980278.84	-41.23	-195.49	.54	-194.95
AD3	41. 5.360	111.54.610	4878.00	979806.27	980277.56	-12.47	-178.66	5.78	-172.89
AD4	41. 5.350	111.54.730	4842.00	979808.18	980277.55	-13.93	-178.89	5.21	-173.68
AD5	41. 5.350	111.54.900	4753.00	979813.53	980277.55	-16.95	-178.88	4.83	-174.05
AD6	41. 5.370	111.55.080	4709.00	979815.31	980277.58	-19.34	-179.77	4.29	-175.48
AD2	41. 5.320	111.55.240	4755.00	979810.74	980277.50	-19.50	-181.50	3.64	-177.86
AD1	41. 5.330	111.55.460	4746.00	979810.56	980277.52	-20.55	-182.24	3.21	-179.03
AB37	41. 5.330	111.56.110	4626.00	979816.54	980277.52	-25.86	-183.46	2.32	-181.14
AB36	41. 5.330	111.56.220	4592.00	979818.43	980277.52	-27.16	-183.61	2.25	-181.36
AB35	41. 5.330	111.56.330	4563.00	979819.99	980277.52	-28.33	-183.79	2.21	-181.53
AB34	41. 5.330	111.56.450	4563.00	979819.37	980277.52	-28.95	-184.41	2.08	-182.33

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
AB33	41. 5.330	111.56.540	4591.00	979816.98	980277.52	-28.71	-185.12	1.92	-183.20
AB32	41. 5.330	111.56.650	4616.00	979814.70	980277.52	-28.64	-185.90	1.80	-184.10
AB31	41. 5.330	111.56.740	4605.00	979814.86	980277.52	-29.51	-186.40	1.73	-184.67
AB30	41. 5.330	111.56.860	4601.00	979814.61	980277.52	-30.14	-186.89	1.64	-185.25
AB29	41. 5.330	111.56.980	4599.00	979814.37	980277.52	-30.57	-187.25	1.57	-185.68
AB28	41. 5.330	111.57.080	4589.00	979814.46	980277.52	-31.42	-187.76	1.51	-186.25
AB27	41. 5.350	111.57.190	4583.00	979814.32	980277.55	-32.15	-188.29	1.46	-186.83
AB26	41. 5.340	111.57.300	4573.00	979814.48	980277.53	-32.91	-188.71	1.41	-187.30
AE25	41. 5.340	111.57.410	4565.00	979814.60	980277.53	-33.55	-189.07	1.36	-187.71
AB24	41. 5.340	111.57.520	4561.00	979814.45	980277.53	-34.07	-189.46	1.31	-188.15
AB23	41. 5.350	111.57.640	4556.00	979814.37	980277.55	-34.64	-189.86	1.26	-188.60
AB22	41. 5.350	111.57.740	4548.00	979814.56	980277.55	-35.20	-190.15	1.22	-188.93
AB21	41. 5.350	111.57.860	4540.00	979814.75	980277.55	-35.77	-190.44	1.18	-189.26
AB20	41. 5.350	111.57.970	4535.00	979814.72	980277.55	-36.27	-190.77	1.14	-189.63
AB19	41. 5.350	111.58.070	4531.00	979814.53	980277.55	-36.83	-191.20	1.10	-190.10
AB18	41. 5.350	111.58.190	4525.00	979814.49	980277.55	-37.44	-191.60	1.05	-190.55
AB17	41. 5.350	111.58.300	4525.00	979814.08	980277.55	-37.85	-192.01	1.01	-191.00
AB16	41. 5.350	111.58.400	4522.00	979813.92	980277.55	-38.29	-192.35	.97	-191.38
AB15	41. 5.350	111.58.510	4516.00	979814.00	980277.55	-38.77	-192.63	.94	-191.69
AB14	41. 5.350	111.58.620	4514.00	979813.82	980277.55	-39.14	-192.93	.91	-192.02
AB13	41. 5.350	111.58.720	4512.00	979813.59	980277.55	-39.56	-193.28	.88	-192.40
AB12	41. 5.350	111.58.840	4508.00	979813.59	980277.55	-39.94	-193.52	.85	-192.67
AB11	41. 5.350	111.58.950	4502.00	979813.74	980277.55	-40.35	-193.73	.83	-192.90
AB10	41. 5.350	111.59.060	4497.00	979813.82	980277.55	-40.74	-193.95	.81	-193.14
AB9	41. 5.360	111.59.160	4494.00	979813.80	980277.56	-41.05	-194.16	.77	-193.39
AB8A	41. 5.350	111.59.270	4491.00	979813.77	980277.55	-41.36	-194.36	.75	-193.61
AB8	41. 5.350	111.59.580	4477.00	979814.14	980277.55	-42.30	-194.83	.67	-194.16
AB7	41. 5.350	111.59.710	4474.00	979814.15	980277.55	-42.57	-195.00	.65	-194.35
AB6	41. 5.350	111.59.820	4471.00	979814.24	980277.55	-42.77	-195.09	.63	-194.46
AP4	41. 5.350	111.59.970	4458.00	979815.03	980277.55	-43.20	-195.08	.60	-194.48
AB3	41. 5.350	112. .150	4451.00	979815.40	980277.55	-43.49	-195.13	.57	-194.56
AB2	41. 5.350	112. .260	4444.00	979815.77	980277.55	-43.78	-195.18	.56	-194.62
A370	41. 5.360	112. .360	4442.00	979815.75	980277.56	-44.00	-195.33	.54	-194.79

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER		
A375	41.	5.360	112.	.470	4449.00	979815.13	980277.56	-43.96	-195.53	.52	-195.01
A380	41.	5.360	112.	.590	4452.00	979814.81	980277.56	-43.99	-195.67	.50	-195.17
A385	41.	5.360	112.	.700	4447.00	979815.08	980277.56	-44.20	-195.70	.50	-195.20
A390	41.	5.360	112.	.780	4436.00	979815.73	980277.56	-44.58	-195.71	.48	-195.23
A395	41.	5.360	112.	.890	4420.00	979816.79	980277.56	-45.03	-195.61	.47	-195.14
A400	41.	5.360	112.	1.000	4407.00	979817.63	980277.56	-45.41	-195.55	.46	-195.09
A405	41.	5.360	112.	1.110	4404.00	979817.80	980277.56	-45.52	-195.56	.44	-195.12
A410	41.	5.360	112.	1.220	4396.00	979818.32	980277.56	-45.75	-195.52	.43	-195.09
A415	41.	5.360	112.	1.320	4391.00	979818.69	980277.56	-45.85	-195.45	.41	-195.04
A420	41.	5.360	112.	1.440	4388.00	979818.97	980277.56	-45.86	-195.35	.40	-194.95
A425	41.	5.360	112.	1.540	4382.00	979819.40	980277.56	-45.99	-195.28	.39	-194.89
A430	41.	5.360	112.	1.650	4377.00	979819.84	980277.56	-46.02	-195.14	.37	-194.77
A435	41.	5.360	112.	1.760	4372.00	979820.23	980277.56	-46.10	-195.05	.36	-194.69
A440	41.	5.360	112.	1.860	4366.00	979820.74	980277.56	-46.16	-194.90	.35	-194.55
A445	41.	5.360	112.	1.980	4357.00	979821.53	980277.56	-46.21	-194.65	.34	-194.31
A450	41.	5.360	112.	2.090	4352.00	979822.00	980277.56	-46.21	-194.48	.33	-194.15
A455	41.	5.360	112.	2.200	4346.00	979822.50	980277.56	-46.18	-194.24	.31	-193.93
A460	41.	5.360	112.	2.300	4337.00	979823.42	980277.56	-46.20	-193.96	.31	-193.65
A465	41.	5.360	112.	2.410	4333.00	979823.92	980277.56	-46.08	-193.70	.30	-193.40
A470	41.	5.360	112.	2.520	4330.00	979824.41	980277.56	-45.87	-193.39	.29	-193.10
A475	41.	5.360	112.	2.630	4326.00	979824.99	980277.56	-45.67	-193.05	.27	-192.78
A480	41.	5.360	112.	2.740	4321.00	979825.68	980277.56	-45.45	-192.66	.27	-192.39
A485	41.	5.360	112.	2.850	4314.00	979826.53	980277.56	-45.26	-192.23	.26	-191.97
A490	41.	5.360	112.	2.960	4312.00	979827.05	980277.56	-44.92	-191.83	.24	-191.59
A495	41.	5.360	112.	3.070	4311.00	979827.57	980277.56	-44.50	-191.37	.24	-191.13
A500	41.	5.360	112.	3.180	4304.00	979828.50	980277.56	-44.23	-190.86	.23	-190.63
A505	41.	5.360	112.	3.290	4302.00	979829.10	980277.56	-43.82	-190.38	.22	-190.16
A510	41.	5.360	112.	3.390	4297.00	979829.95	980277.56	-43.44	-189.83	.21	-189.62
A515	41.	5.360	112.	3.500	4293.00	979830.76	980277.56	-43.00	-189.26	.20	-189.06
A520	41.	5.360	112.	3.610	4288.00	979831.63	980277.56	-42.60	-188.69	.19	-188.50
A525	41.	5.360	112.	3.730	4282.00	979832.66	980277.56	-42.14	-188.02	.19	-187.83
A530	41.	5.360	112.	3.840	4280.00	979833.38	980277.56	-41.61	-187.42	.18	-187.24
A535	41.	5.360	112.	3.950	4278.00	979834.19	980277.56	-40.98	-186.73	.17	-186.56

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER		
A540	41.	5.360	112.	4.060	4276.00	979835.04	980277.56	-40.32	-186.00	.17	-185.83
A545	41.	5.360	112.	4.170	4272.00	979835.96	980277.56	-39.78	-185.32	.16	-185.16
A550	41.	5.360	112.	4.280	4271.00	979836.79	980277.56	-39.04	-184.55	.15	-184.40
A555	41.	5.360	112.	4.380	4270.00	979837.54	980277.56	-38.39	-183.86	.14	-183.72
A560	41.	5.360	112.	4.490	4266.00	979839.59	980277.56	-37.71	-183.05	.14	-182.91
A565	41.	5.360	112.	4.600	4262.00	979839.56	980277.56	-37.12	-182.32	.13	-182.19
A570	41.	5.360	112.	4.720	4256.00	979840.92	980277.56	-36.32	-181.32	.12	-181.20
A575	41.	5.360	112.	4.820	4246.00	979842.42	980277.56	-35.76	-180.42	.12	-180.30
A580	41.	5.360	112.	4.930	4244.00	979843.33	980277.56	-35.04	-179.63	.11	-179.52
A585	41.	5.360	112.	5.040	4242.00	979844.33	980277.56	-34.23	-178.75	.10	-178.65
A590	41.	5.360	112.	5.150	4240.00	979845.30	980277.56	-33.45	-177.90	.10	-177.80
A595	41.	5.360	112.	5.260	4239.00	979846.22	980277.56	-32.62	-177.04	.09	-176.95
A600	41.	5.360	112.	5.360	4239.00	979847.04	980277.56	-31.80	-176.22	.09	-176.13
A605	41.	5.360	112.	5.470	4238.00	979847.96	980277.56	-30.98	-175.36	.08	-175.23
A610	41.	5.360	112.	5.580	4237.00	979848.84	980277.56	-30.19	-174.54	.08	-174.46
A615	41.	5.360	112.	5.690	4235.00	979849.83	980277.56	-29.39	-173.67	.08	-173.59
A620	41.	5.360	112.	5.800	4234.00	979850.72	980277.56	-28.59	-172.84	.07	-172.77
A625	41.	5.360	112.	5.910	4233.00	979851.57	980277.56	-27.84	-172.05	.07	-171.98
A630	41.	5.360	112.	6.020	4233.00	979852.35	980277.56	-27.06	-171.27	.07	-171.20
A635	41.	5.360	112.	6.130	4234.00	979853.24	980277.56	-26.07	-170.32	.08	-170.24
A640	41.	5.360	112.	6.240	4230.00	979854.01	980277.56	-25.68	-169.79	.08	-169.71
A645	41.	5.360	112.	6.350	4229.00	979854.77	980277.56	-25.01	-169.09	.07	-169.02
A650	41.	5.360	112.	6.460	4228.00	979855.53	980277.56	-24.35	-168.39	.06	-168.33
A655	41.	5.360	112.	6.570	4227.00	979856.26	980277.56	-23.71	-167.72	.06	-167.66
A660	41.	5.360	112.	6.680	4227.00	979856.89	980277.56	-23.08	-167.09	.08	-167.01
A665	41.	5.360	112.	6.790	4225.00	979857.65	980277.56	-22.51	-166.45	.07	-166.38
A670	41.	5.360	112.	6.900	4221.00	979858.47	980277.56	-22.07	-165.87	.05	-165.82
A675	41.	5.360	112.	7.000	4217.00	979859.31	980277.56	-21.60	-165.27	.05	-165.22
A680	41.	5.360	112.	7.120	4215.00	979859.80	980277.56	-21.30	-164.90	.04	-164.86
A685	41.	5.360	112.	7.230	4208.00	979860.87	980277.56	-20.89	-164.25	.04	-164.21
A690	41.	5.360	112.	7.330	4208.00	979861.39	980277.56	-20.37	-163.73	.03	-163.70
A695	41.	5.360	112.	7.450	4208.00	979861.78	980277.56	-19.98	-163.34	.02	-163.32
A700	41.	5.360	112.	7.560	4209.00	979862.09	980277.56	-19.57	-162.97	.01	-162.96

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A705	41. 5.360	112. 7.660	4209.00	979862.44	980277.56	-19.22	-162.62	.02	-162.60
A710	41. 5.360	112. 7.770	4210.00	979862.62	980277.56	-18.95	-162.38	.02	-162.36
A715	41. 5.360	112. 7.890	4210.00	979862.83	980277.56	-18.74	-162.17	.00	-162.17
A720	41. 5.360	112. 8.000	4209.00	979863.09	980277.56	-18.57	-161.97	.00	-161.97
A725	41. 5.360	112. 8.100	4210.00	979863.21	980277.56	-18.36	-161.79	-.01	-161.80
A730	41. 5.360	112. 8.210	4210.00	979863.35	980277.56	-18.22	-161.65	-.01	-161.66
A735	41. 5.360	112. 8.320	4210.00	979863.47	980277.56	-18.10	-161.53	-.01	-161.54
A740	41. 5.360	112. 8.430	4210.00	979863.59	980277.56	-17.98	-161.41	-.02	-161.43
A745	41. 5.360	112. 8.550	4210.00	979863.73	980277.56	-17.84	-161.27	-.03	-161.30
A750	41. 5.360	112. 8.650	4210.00	979863.89	980277.56	-17.68	-161.11	-.03	-161.14
A755	41. 5.360	112. 8.760	4209.00	979864.06	980277.56	-17.60	-161.00	-.03	-161.03
A760	41. 5.360	112. 8.870	4211.00	979864.23	980277.56	-17.24	-160.71	-.03	-160.74
A765	41. 5.360	112. 8.980	4211.00	979864.43	980277.56	-17.05	-160.51	-.04	-160.55
A770	41. 5.360	112. 9.090	4211.00	979864.70	980277.56	-16.78	-160.24	-.04	-160.28
A775	41. 5.360	112. 9.200	4211.00	979864.96	980277.56	-16.52	-159.98	-.03	-160.01
A780	41. 5.360	112. 9.310	4211.00	979865.24	980277.56	-16.23	-159.70	-.03	-159.73
A785	41. 5.360	112. 9.410	4211.00	979865.51	980277.56	-15.97	-159.43	-.05	-159.48
A790	41. 5.360	112. 9.520	4210.00	979865.87	980277.56	-15.70	-159.13	-.05	-159.18
A795	41. 5.360	112. 9.630	4210.00	979866.15	980277.56	-15.42	-158.85	-.05	-158.90
A800	41. 5.360	112. 9.740	4210.00	979866.46	980277.56	-15.11	-158.54	-.04	-158.53
A805	41. 5.360	112. 9.850	4209.00	979866.73	980277.56	-14.93	-158.33	-.06	-158.39
A810	41. 5.360	112. 9.960	4209.00	979866.92	980277.56	-14.74	-158.14	-.07	-158.21
A815	41. 5.360	112.10.070	4208.00	979867.13	980277.56	-14.63	-157.99	-.08	-158.07
A820	41. 5.360	112.10.170	4207.00	979867.32	980277.56	-14.53	-157.86	-.08	-157.94
A825	41. 5.360	112.10.280	4207.00	979867.51	980277.56	-14.34	-157.67	-.09	-157.76
A830	41. 5.360	112.10.400	4207.00	979867.64	980277.56	-14.21	-157.54	-.10	-157.64
A835	41. 5.360	112.10.500	4207.00	979867.67	980277.56	-14.18	-157.51	-.10	-157.61
A840	41. 5.360	112.10.620	4207.00	979867.69	980277.56	-14.16	-157.49	-.11	-157.60
A845	41. 5.360	112.10.730	4207.00	979867.75	980277.56	-14.10	-157.43	-.10	-157.53
A850	41. 5.360	112.10.830	4208.00	979867.76	980277.56	-14.00	-157.36	-.10	-157.46
A855	41. 5.360	112.10.940	4208.00	979867.78	980277.56	-13.98	-157.34	-.11	-157.45
A860	41. 5.360	112.11.050	4209.00	979867.70	980277.56	-13.96	-157.36	-.11	-157.47
A865	41. 5.350	112.11.160	4209.00	979867.67	980277.55	-13.97	-157.37	-.11	-157.48

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A870	41. 5.340	112.11.270	4208.00	979867.68	980277.53	-14.05	-157.41	-.11	-157.52
A875	41. 5.320	112.11.370	4209.00	979867.69	980277.50	-14.01	-157.37	-.12	-157.49
A880	41. 5.290	112.11.470	4209.00	979867.64	980277.46	-13.92	-157.32	-.12	-157.44
A885	41. 5.250	112.11.570	4208.00	979867.70	980277.40	-13.90	-157.26	-.12	-157.39
A890	41. 5.220	112.11.680	4208.00	979867.66	980277.34	-13.88	-157.24	-.12	-157.36
A895	41. 5.180	112.11.770	4209.00	979867.69	980277.28	-13.79	-157.15	-.12	-157.27
A900	41. 5.150	112.11.870	4208.00	979867.75	980277.24	-13.69	-157.05	-.12	-157.17
A905	41. 5.110	112.11.970	4208.00	979867.83	980277.18	-13.55	-156.91	-.13	-157.04
A910	41. 5.070	112.12.070	4208.00	979867.99	980277.12	-13.33	-156.69	-.13	-156.82
A915	41. 5.040	112.12.160	4209.00	979868.10	980277.08	-13.08	-156.48	-.13	-156.61
A920	41. 5.010	112.12.260	4209.00	979868.34	980277.04	-12.80	-156.20	-.13	-156.33
A925	41. 4.970	112.12.360	4209.00	979868.60	980276.98	-12.47	-155.87	-.13	-156.00
A930	41. 4.930	112.12.470	4209.00	979868.94	980276.92	-12.08	-155.48	-.13	-155.61
A935	41. 4.900	112.12.560	4208.00	979869.33	980276.87	-11.74	-155.10	-.14	-155.24
A940	41. 4.870	112.12.670	4208.00	979869.73	980276.83	-11.30	-154.66	-.14	-154.80
A945	41. 4.830	112.12.760	4208.00	979870.21	980276.77	-10.76	-154.12	-.14	-154.26
A950	41. 4.790	112.12.850	4209.00	979870.64	980276.70	-10.16	-153.56	-.13	-153.69
A955	41. 4.740	112.12.930	4209.00	979871.09	980276.62	-9.63	-153.03	-.14	-153.17
A960	41. 4.680	112.13.020	4209.00	979871.63	980276.54	-9.01	-152.41	-.14	-152.55
A965	41. 4.620	112.13.090	4209.00	979872.10	980276.45	-8.45	-151.85	-.14	-151.99
A970	41. 4.580	112.13.160	4209.00	979872.61	980276.39	-7.88	-151.28	-.14	-151.42
A975	41. 4.530	112.13.230	4209.00	979873.11	980276.32	-7.31	-150.71	-.14	-150.85
A980	41. 4.460	112.13.300	4209.00	979873.60	980276.22	-6.72	-150.12	-.14	-150.26
A985	41. 4.400	112.13.360	4208.00	979874.10	980276.13	-6.23	-149.59	-.14	-149.73
A990	41. 4.340	112.13.430	4209.00	979874.50	980276.03	-5.63	-149.03	-.14	-149.17
A995	41. 4.270	112.13.500	4209.00	979875.03	980275.93	-5.00	-148.40	-.14	-148.54
A1000	41. 4.200	112.13.560	4209.00	979875.58	980275.83	-4.35	-147.75	-.14	-147.89
A1005	41. 4.140	112.13.630	4209.00	979876.13	980275.74	-3.71	-147.11	-.14	-147.25
A1010	41. 4.070	112.13.700	4209.00	979876.68	980275.63	-3.05	-146.45	-.14	-146.59
A1015	41. 4.020	112.13.760	4210.00	979877.28	980275.56	-2.29	-145.72	-.14	-145.86
A1020	41. 3.950	112.13.830	4210.00	979878.12	980275.46	-1.35	-144.78	-.14	-144.92
A1025	41. 3.880	112.13.900	4210.00	979878.87	980275.34	-.48	-143.91	-.14	-144.05
A1030	41. 3.820	112.13.970	4209.00	979879.70	980275.26	.34	-143.06	-.14	-143.20

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
A1035	41. 3.750	112.14.030	4209.00	979880.41	980275.16	1.16	-142.24	-.13	-142.37
A1040	41. 3.680	112.14.100	4208.00	979881.17	980275.05	1.92	-141.44	-.13	-141.57
A1045	41. 3.620	112.14.170	4211.00	979881.80	980274.97	2.91	-140.55	-.13	-140.68
A1050	41. 3.560	112.14.230	4207.00	979883.25	980274.87	4.09	-139.24	-.12	-139.36
1350	40.52.700	111.50.600	5202.00	979770.68	980258.72	1.26	-175.97	4.89	-171.03
1351	40.52.700	111.51.140	4932.00	979787.17	980258.72	-7.64	-175.67	4.39	-171.28
1352	40.53.050	111.54.650	4244.00	979821.55	980259.23	-38.48	-183.07	1.57	-181.40
1353	40.53.050	111.55.730	4222.00	979817.17	980259.23	-44.93	-188.77	1.22	-187.55
1354	40.53.060	111.51.440	4751.00	979798.95	980259.24	-13.41	-175.27	4.29	-170.98
1355	40.53.060	111.52.280	4470.00	979816.51	980259.24	-22.18	-174.47	3.47	-171.00
1356	40.53.060	111.53.470	4340.00	979821.91	980259.24	-29.11	-176.97	2.33	-174.64
1357	40.53.060	111.54.080	4289.00	979822.27	980259.24	-33.55	-179.67	1.94	-177.73
1358	40.53.060	111.52.790	4398.00	979820.33	980259.24	-25.23	-175.07	2.93	-172.14
1359	40.53.150	111.56.960	4210.00	979817.05	980259.38	-46.34	-189.77	.85	-188.92
1360	40.53.480	111.51.140	4842.00	979794.12	980259.87	-10.31	-175.27	5.11	-170.16
1361	40.53.620	111.50.720	5051.00	979780.50	980260.09	-4.49	-176.57	6.23	-170.34
1362	40.53.620	111.52.300	4416.00	979821.30	980260.09	-23.42	-173.87	3.74	-170.13
1363	40.53.650	111.53.480	4300.00	979824.50	980260.13	-31.07	-177.57	2.45	-175.12
1364	40.53.650	111.54.080	4264.00	979822.86	980260.13	-36.20	-181.47	2.02	-179.45
1365	40.53.650	111.54.670	4232.00	979820.38	980260.13	-41.19	-185.37	1.71	-183.66
1366	40.53.740	111.51.590	4636.00	979807.37	980260.26	-16.83	-174.77	4.96	-169.81
1367	40.53.930	111.50.450	5648.00	979744.24	980260.54	14.95	-177.47	5.82	-171.65
1370	40.54.400	111.52.300	4337.00	979824.08	980261.23	-29.21	-176.97	4.61	-172.36
1371	40.54.400	111.52.700	4295.00	979825.50	980261.23	-31.74	-178.07	3.76	-174.31
1372	40.54.400	111.53.450	4256.00	979824.44	980261.23	-36.47	-181.47	2.73	-178.74
1373	40.54.400	111.54.070	4229.00	979822.96	980261.23	-40.49	-184.57	2.20	-182.37
1374	40.54.400	111.54.670	4218.00	979819.52	980261.23	-44.97	-188.67	1.80	-186.87
1375	40.54.670	111.55.400	4207.00	979816.00	980261.65	-49.94	-193.27	1.46	-191.81
1376	40.54.670	111.56.500	4208.00	979812.34	980261.65	-53.01	-196.37	1.03	-195.34
1378	40.54.770	111.53.420	4249.00	979824.52	980261.79	-37.61	-182.37	2.92	-179.45
1379	40.54.790	111.52.300	4348.00	979823.51	980261.82	-29.24	-177.37	4.99	-172.38
1380	40.54.800	111.51.650	4819.00	979795.67	980261.84	-12.89	-177.07	6.18	-170.89
1385	40.55.280	111.54.800	4207.00	979817.39	980262.55	-49.44	-192.77	1.88	-190.89

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
1386	40.55.730	111.52.400	4355.00	979821.79	980263.22	-31.80	-180.17	6.24	-173.93
1387	40.55.730	111.52.670	4287.00	979825.37	980263.22	-34.62	-180.67	5.31	-175.36
1389	40.55.750	111.53.420	4220.00	979824.50	980263.23	-41.80	-185.57	3.55	-182.02
1390	40.55.880	111.56.810	4208.00	979811.13	980263.44	-56.51	-199.87	1.01	-198.86
1395	40.56.530	111.52.760	4309.00	979823.53	980264.40	-35.57	-182.37	6.22	-176.15
1396	40.56.590	111.53.410	4221.00	979824.59	980264.48	-42.86	-186.67	4.16	-182.51
1397	40.57.130	111.53.470	4221.00	979825.40	980265.29	-42.86	-186.67	4.37	-182.30
1398	40.57.140	111.52.940	4285.00	979826.67	980265.30	-35.58	-181.57	6.38	-175.19
1402	40.57.890	111.52.940	4332.00	979826.17	980266.42	-32.78	-180.37	6.63	-173.74
1403	40.57.910	111.53.420	4243.00	979829.34	980266.45	-38.01	-182.57	4.90	-177.67
1404	40.57.910	111.54.050	4234.00	979827.38	980266.45	-40.82	-185.07	3.39	-181.68
1405	40.57.910	111.55.220	4215.00	979821.22	980266.45	-48.77	-192.37	2.06	-190.31
1408	40.58.330	111.54.050	4237.00	979829.03	980267.08	-39.52	-183.87	3.57	-180.30
1410	40.58.370	111.52.330	4821.00	979794.35	980267.14	-19.32	-183.57	8.55	-175.02
1414	40.58.550	111.53.680	4264.00	979828.53	980267.40	-37.70	-182.97	4.41	-178.56
1416	40.58.820	111.53.180	4301.00	979826.82	980267.81	-36.44	-182.97	6.44	-176.53
1417	40.58.940	111.54.620	4233.00	979829.27	980267.98	-40.56	-184.77	2.99	-181.73
1418	40.58.940	111.55.210	4230.00	979826.35	980267.98	-43.76	-187.87	2.32	-185.55
1420	40.59.000	111.50.150	8366.00	979570.62	980268.07	89.45	-195.57	22.26	-173.31
1425	40.59.480	111.53.570	4313.00	979829.59	980268.80	-33.53	-180.47	5.62	-174.85
1426	40.59.480	111.54.110	4251.00	979832.91	980268.80	-36.04	-180.87	4.25	-176.62
1427	40.59.480	111.55.190	4241.00	979828.21	980268.80	-41.68	-186.17	2.51	-183.66
1431	41. .100	111.52.340	5010.00	979783.29	980269.72	-15.18	-185.87	15.09	-170.79
1437	41. 2.300	111.56.920	4304.00	979826.13	980273.00	-42.04	-188.67	1.72	-186.95
1443	41. 4.720	111.55.130	4757.00	979811.75	980276.60	-17.40	-179.47	3.98	-175.49
1446	41. 7.190	111.59.000	4788.00	979797.08	980280.29	-32.85	-195.97	.82	-195.15
1447	41. 7.480	111.58.180	4788.00	979800.52	980280.73	-29.85	-192.97	.98	-191.99
1448	41. 7.790	111.58.300	4790.00	979808.04	980281.17	-22.58	-185.77	.99	-184.78
1449	41. 8.510	111.55.190	4536.00	979830.66	980282.25	-24.93	-179.47	4.64	-174.83
1459	41.13.100	111.58.000	4304.00	979831.31	980289.09	-52.94	-199.57	2.24	-197.33
1462	41.14.150	111.55.640	4425.00	979838.82	980290.65	-35.61	-186.37	10.98	-175.39
1499	41.29.980	111.59.200	4633.00	979860.45	980314.26	-18.03	-175.87	8.77	-167.10
1501	41.30.080	111.56.570	5145.00	979820.68	980314.41	-9.78	-185.07	2.23	-182.84

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
1503	41.30.290	111.56.690	5200.00	979819.70	980314.73	-5.91	-183.07	2.03	-181.04
2206	40.52.730	112.10.310	4257.00	979858.71	980258.76	.36	-144.67	.78	-143.89
2213	40.54.830	112.10.310	4276.00	979849.68	980261.87	-9.99	-155.67	.62	-155.05
2222	40.58.550	112.10.970	4246.00	979867.51	980267.40	-.51	-145.17	.62	-144.55
2225	41. .280	112.14.140	4227.00	979881.13	980269.98	8.74	-135.27	.34	-134.93
2226	41. .500	112.11.780	4221.00	979880.93	980270.32	7.63	-136.17	.60	-135.57
2230	41. 2.480	112.13.340	4417.00	979871.41	980273.26	13.61	-136.87	.13	-136.74
2231	41. 2.750	112. .350	4246.00	979823.38	980273.67	-50.91	-195.57	.53	-195.04
2234	41. 3.530	112.14.990	4237.00	979884.68	980274.84	8.38	-135.97	-.14	-136.11
2242	41. 6.200	112. 6.650	4231.00	979854.42	980278.81	-26.42	-170.57	.06	-170.51
2243	41. 6.620	112. 6.650	4231.00	979854.45	980279.44	-27.02	-171.17	.05	-171.12
2245	41. 7.100	112. .920	4595.00	979808.03	980280.16	-39.92	-196.47	.48	-195.99
2258	41. 9.260	112. 1.520	4541.00	979812.19	980283.37	-44.06	-198.77	.47	-198.30
2259	41.10.580	112. 1.180	4493.00	979815.03	980285.34	-47.70	-200.77	.50	-200.27
2261	41.11.240	112. 9.650	4212.00	979863.47	980286.32	-26.67	-170.17	-.06	-170.23
2279	41.16.880	112.10.780	4217.00	979876.97	980294.73	-21.10	-164.77	-.05	-164.82
2281	41.17.360	112. 1.600	4245.00	979839.91	980295.45	-56.25	-200.87	1.02	-199.85
2288	41.23.930	112.11.480	4208.00	979878.02	980305.23	-31.41	-174.77	.01	-174.76
2289	41.24.290	112. 2.000	4266.00	979864.98	980305.77	-39.53	-184.87	8.57	-176.30
2291	41.24.670	112. 2.090	4353.00	979864.73	980306.34	-32.17	-180.47	6.41	-174.06
2292	41.24.730	112. 2.890	4266.00	979868.54	980306.43	-36.63	-181.97	3.43	-178.54
2296	41.24.950	112.11.390	4208.00	979877.25	980306.77	-33.71	-177.07	.02	-177.05
2297	41.24.950	112.13.010	4208.00	979883.35	980306.77	-22.61	-165.97	-.04	-166.01
2298	41.25.000	112.13.990	4208.00	979894.92	980306.84	-16.11	-159.47	-.07	-159.54
2301	41.25.190	112.10.310	4208.00	979872.01	980307.12	-39.31	-182.67	.10	-182.57
2304	41.25.370	112. 5.600	4208.00	979853.88	980307.39	-57.71	-201.07	.84	-200.23
2305	41.25.370	112. 7.150	4208.00	979855.68	980307.39	-55.91	-199.27	.45	-198.82
2306	41.25.370	112. 8.540	4208.00	979862.38	980307.39	-49.21	-192.57	.23	-192.34
2313	41.26.510	112. 4.210	4208.00	979864.09	980309.10	-49.21	-192.57	1.45	-191.12
2318	41.27.980	112.13.090	4208.00	979879.47	980311.28	-36.01	-179.37	-.06	-179.43
2319	41.28.010	112.11.900	4207.00	979880.28	980311.33	-35.34	-178.67	-.03	-178.70
2321	41.28.130	112.10.720	4207.00	979883.06	980311.52	-32.74	-176.07	.03	-176.04
2329	41.28.760	112. 9.290	4212.00	979883.90	980312.45	-32.37	-175.87	.11	-175.76

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
2330	41.28.760	112.14.960	4209.00	979879.68	980312.45	-36.87	-180.27	-.10	-180.37
2333	41.29.000	112. 7.700	4209.00	979878.82	980312.80	-38.07	-181.47	.24	-181.23
2335	41.29.500	112.10.580	4215.00	979889.11	980313.55	-27.97	-171.57	.02	-171.55
2338	41.30.380	112. .530	4498.00	979867.44	980314.85	-24.33	-177.57	2.56	-175.01
2340	41.30.500	112. 1.000	4448.00	979868.42	980315.03	-28.23	-179.77	2.10	-177.67
2341	41.30.580	112. 6.490	4214.00	979874.89	980315.16	-43.90	-187.47	.36	-187.11
2342	41.30.590	112. 4.580	4218.00	979870.17	980315.18	-48.27	-191.97	.70	-191.27
2343	41.30.590	112.10.600	4225.00	979890.15	980315.18	-27.63	-171.57	.02	-171.55
2345	41.30.650	112. 2.630	4236.00	979868.27	980315.27	-48.55	-192.87	1.45	-191.42
2347	41.30.700	112. .700	4448.00	979864.93	980315.34	-32.03	-183.57	2.42	-181.15
2348	41.30.800	112. .890	4403.00	979871.97	980315.48	-29.36	-179.37	2.27	-177.10
2349	41.30.850	112. 6.290	4214.00	979874.68	980315.55	-44.50	-188.07	.39	-187.68
2353	41.31.220	112. 9.440	4223.00	979888.50	980316.11	-30.40	-174.27	.09	-174.18
2354	41.31.220	112.11.210	4223.00	979890.10	980316.11	-28.80	-172.67	.00	-172.67
2355	41.31.480	112. 8.000	4212.00	979883.25	980316.50	-37.07	-180.57	.19	-180.38
2356	41.31.490	112. .890	4326.00	979874.82	980316.52	-34.79	-182.17	2.94	-179.23
2357	41.31.790	112. 2.060	4238.00	979870.86	980316.97	-47.49	-191.87	1.95	-189.92
2358	41.31.790	112. 5.000	4235.00	979874.74	980316.97	-43.89	-188.17	.63	-187.54
2359	41.32.030	112. 3.500	4224.00	979867.65	980317.32	-52.36	-196.27	1.04	-195.23
2360	41.32.050	112. 5.000	4235.00	979870.71	980317.34	-48.29	-192.57	.62	-191.95
2362	41.32.390	112. 4.970	4228.00	979869.35	980317.86	-50.83	-194.87	.65	-194.22
2366	41.32.980	112. 7.700	4233.00	979880.44	980318.75	-40.16	-184.37	.27	-184.10
2367	41.32.990	112. 9.460	4239.00	979893.19	980318.76	-26.85	-171.27	.10	-171.17
2368	41.32.990	112.10.640	4239.00	979897.99	980318.76	-22.05	-166.47	.04	-166.43
2369	41.33.010	112.11.810	4233.00	979900.68	980318.79	-19.96	-164.17	.01	-164.16
2370	41.33.020	112. 6.610	4230.00	979875.07	980318.80	-45.86	-189.97	.39	-189.58
2371	41.33.350	112. 1.190	4270.00	979886.17	980319.30	-31.49	-176.97	6.76	-170.21
2375	41.33.890	112.11.810	4243.00	979905.39	980320.10	-15.62	-160.17	.03	-160.14
2378	41.34.180	112. 1.690	4257.00	979888.59	980320.54	-31.54	-176.57	6.98	-169.59
2381	41.34.610	112.13.970	4261.00	979911.79	980321.18	-8.60	-153.77	.44	-153.33
2382	41.34.760	112.14.600	4265.00	979912.47	980321.40	-7.77	-153.07	.73	-152.34
2387	41.35.240	112.12.260	4240.00	979912.18	980322.11	-11.12	-155.57	.30	-155.27
2391	41.35.500	112. 7.730	4242.00	979882.96	980322.51	-40.55	-185.07	.40	-184.67

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
2394	41.35.570	112.10.670	4248.00	979904.90	980322.61	-18.14	-162.87	.11	-162.76
2402	41.36.530	112. 9.560	4249.00	979899.57	980324.04	-24.81	-169.57	.20	-169.37
2403	41.36.580	112. 8.300	4248.00	979887.81	980324.12	-36.74	-181.47	.37	-181.10
2404	41.36.700	112. 6.190	4252.00	979877.15	980324.30	-47.21	-192.07	.91	-191.16
2412	41.37.810	112.14.180	4258.00	979917.35	980325.96	-8.10	-153.17	.69	-152.48
2413	41.37.820	112.12.350	4264.00	979912.10	980325.98	-12.80	-158.07	.26	-157.81
2414	41.37.820	112.13.580	4262.00	979915.92	980325.98	-9.17	-154.37	.51	-153.86
2415	41.37.840	112.11.270	4262.00	979906.26	980326.01	-18.87	-164.07	.12	-163.95
2416	41.37.850	112. 3.280	4866.00	979862.43	980326.02	-5.89	-171.67	8.03	-163.64
2417	41.37.940	112. 8.320	4257.00	979887.70	980326.15	-38.04	-183.07	.42	-182.65
2424	41.38.110	112. 6.200	4270.00	979883.37	980326.40	-41.39	-186.87	1.16	-185.71
2432	41.38.420	112. 4.970	4271.00	979892.58	980326.87	-32.56	-178.07	2.65	-175.42
2433	41.38.500	112. 3.590	4796.00	979865.70	980326.98	-10.17	-173.57	6.64	-166.93
2438	41.39.350	112. 8.360	4272.00	979883.31	980328.27	-38.13	-183.67	.47	-183.20
2441	41.39.970	112. 4.280	4651.00	979878.19	980329.18	-13.51	-171.97	4.40	-167.57
2442	41.39.980	112.14.200	4259.00	979905.22	980329.20	-23.37	-168.47	.48	-167.99
2443	41.40.000	112. 6.220	4293.00	979894.82	980329.23	-30.61	-176.87	1.44	-175.43
2444	41.40.010	112. 5.450	4297.00	979896.49	980329.24	-28.58	-174.97	2.37	-172.60
2445	41.40.010	112.12.470	4268.00	979906.93	980329.24	-20.86	-166.27	.26	-166.01
2446	41.40.030	112.11.900	4270.00	979905.13	980329.27	-22.49	-167.97	.20	-167.77
2447	41.40.040	112.10.730	4276.00	979901.89	980329.28	-25.19	-170.87	.17	-170.70
2448	41.40.100	112. 9.580	4278.00	979895.67	980329.38	-31.32	-177.07	.29	-176.78
2450	41.40.180	112. 8.390	4281.00	979891.11	980329.50	-35.72	-181.57	.49	-181.08
2454	41.41.420	112. 5.350	4312.00	979896.20	980331.35	-29.56	-176.47	3.59	-172.88
2460	41.41.720	112.14.270	4291.00	979905.71	980331.80	-22.48	-168.67	.43	-168.24
2461	41.41.770	112.13.100	4294.00	979910.20	980331.87	-17.78	-164.07	.36	-163.71
2462	41.41.780	112.11.950	4298.00	979910.38	980331.89	-17.24	-163.67	.24	-163.43
2464	41.41.810	112.10.790	4301.00	979906.85	980331.94	-20.54	-167.07	.20	-166.87
2465	41.41.830	112.10.190	4306.00	979905.18	980331.97	-21.77	-168.47	.25	-168.22
2466	41.41.860	112. 9.040	4300.00	979904.18	980332.01	-23.37	-169.87	.42	-169.45
2468	41.41.870	112. 7.880	4302.00	979896.77	980332.02	-30.61	-177.17	.65	-176.52
2480	41.42.770	112. 7.060	4237.00	979900.22	980333.37	-34.62	-178.97	1.23	-177.74
2482	41.42.910	112. 5.510	4339.00	979903.31	980333.59	-22.14	-169.97	3.62	-166.35

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
2485	41.43.180	112.13.550	4409.00	979909.71	980333.98	-9.56	-159.77	.42	-159.35
2491	41.43.580	112.14.420	4464.00	979907.50	980334.57	-7.19	-159.27	.76	-158.51
2502	41.44.690	112. 5.920	4453.00	979895.42	980336.23	-21.96	-173.67	1.70	-171.97
2508	41.45.170	112.12.730	5127.00	979870.21	980336.95	15.50	-159.17	1.41	-157.76
2513	41.45.320	112.10.880	4479.00	979903.21	980337.13	-7.68	-160.27	.90	-159.37
2514	41.45.340	112. 7.640	4346.00	979898.32	980337.21	-30.11	-178.17	.53	-177.64
2515	41.45.350	112. 8.840	4344.00	979905.86	980337.23	-22.77	-170.77	.48	-170.29
2516	41.45.350	112. 9.730	4350.00	979911.50	980337.23	-16.57	-164.77	.49	-164.23
2517	41.45.350	112.11.810	4963.00	979880.92	980337.23	10.51	-158.57	1.50	-157.07
2520	41.45.440	112. 5.840	4405.00	979899.03	980337.36	-24.00	-174.07	1.54	-172.53
2534	41.46.780	112.10.670	4839.00	979883.50	980339.37	4.39	-160.47	1.64	-158.83
2537	41.47.080	112. 9.770	4383.00	979914.59	980339.80	-12.95	-162.27	.69	-161.58
2538	41.47.120	112. 6.110	4382.00	979898.33	980339.88	-29.38	-178.67	.50	-178.17
2540	41.47.350	112. 4.550	4560.00	979895.88	980340.21	-15.41	-170.77	.64	-170.13
2541	41.47.560	112. 8.090	4313.00	979903.01	980340.52	-31.83	-178.77	.41	-178.36
2561	41.48.380	112. 9.820	4423.00	979910.13	980341.74	-15.58	-166.27	.60	-165.67
2567	41.48.820	112. 9.830	4408.00	979912.09	980342.40	-15.69	-165.87	.57	-165.30
2568	41.48.860	112. 7.690	4368.00	979902.15	980342.46	-29.46	-178.27	.45	-177.82
2569	41.48.880	112. 5.180	4469.00	979904.71	980342.48	-17.42	-169.67	.44	-169.23
2570	41.48.880	112. 6.350	4391.00	979907.19	980342.43	-22.27	-171.87	.33	-171.54
2573	41.49.010	112.12.590	4860.00	979892.05	980342.68	6.50	-159.07	2.02	-157.05
2575	41.49.180	112.11.000	4600.00	979907.41	980342.94	-2.85	-159.57	.82	-158.75
2578	41.49.700	112. 9.860	4406.00	979912.02	980343.71	-17.26	-167.37	.55	-166.82
2579	41.49.720	112. 8.680	4378.00	979908.33	980343.74	-23.62	-172.77	.46	-172.31
2591	41.50.200	112. 6.380	4413.00	979907.36	980344.47	-22.02	-172.37	.43	-171.94
2599	41.50.570	112.11.030	4594.00	979907.94	980345.01	-4.96	-161.47	.66	-160.81
2600	41.50.570	112. 9.880	4443.00	979913.40	980345.01	-13.70	-165.07	.51	-164.56
2602	41.50.750	112. 7.550	4408.00	979907.58	980345.29	-22.99	-173.17	.46	-172.71
2607	41.51.500	112. 6.400	4499.00	979903.84	980346.41	-19.39	-172.67	.73	-171.94
2618	41.52.300	112.11.120	4408.00	979917.09	980347.60	-15.89	-166.07	.89	-165.13
2619	41.52.310	112. 9.920	4419.00	979916.35	980347.62	-15.62	-166.17	.76	-165.41
2620	41.52.340	112. 7.600	4521.00	979903.77	980347.66	-13.64	-167.67	1.03	-166.64
2621	41.52.340	112. 8.440	4475.00	979908.63	980347.66	-18.11	-170.57	.93	-169.64

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
2622	41.52.370	112. 6.440	4641.00	979897.61	980347.70	-13.56	-171.67	1.07	-170.60
2629	41.52.760	112. 6.730	4790.00	979839.26	980348.29	-8.48	-171.67	1.29	-170.38
2637	41.53.180	112. 9.970	4502.00	979907.66	980348.91	-17.79	-171.17	.97	-170.20
2638	41.53.180	112.11.120	4396.00	979912.12	980348.91	-23.30	-173.07	.94	-172.13
2639	41.53.200	112. 8.780	4738.00	979889.04	980348.95	-14.25	-175.67	1.23	-174.44
2640	41.53.210	112. 7.610	4891.00	979885.57	980348.96	-3.24	-169.87	1.67	-168.20
2648	41.53.360	112.14.090	4856.00	979898.01	980349.20	5.57	-159.87	2.43	-157.44
2651	41.53.570	112.12.910	4556.00	979914.31	980349.50	-6.15	-161.37	1.21	-160.16
2666	41.54.820	112.14.680	4798.00	979900.67	980351.37	.59	-162.87	1.71	-161.16
2667	41.54.880	112.13.190	4480.00	979917.74	980351.47	-12.34	-164.97	1.09	-163.88
2668	41.54.890	112.11.180	4382.00	979907.53	980351.48	-31.78	-181.07	1.31	-179.76
2681	41.56.290	112. 8.900	5223.00	979872.18	980353.58	9.87	-168.07	6.21	-161.86
2682	41.56.590	112.14.410	4601.00	979917.13	980354.02	-4.12	-160.87	1.22	-159.65
2683	41.56.600	112.13.820	4474.00	979921.06	980354.03	-12.14	-164.57	1.14	-163.43
2684	41.56.600	112.12.800	4372.00	979919.78	980354.03	-23.02	-171.97	1.14	-170.83
2685	41.56.650	112.11.210	4374.00	979909.03	980354.10	-33.65	-182.67	1.76	-180.91
2686	41.56.660	112.10.490	4443.00	979905.21	980354.12	-31.00	-182.37	2.68	-179.69
2694	41.57.520	112.11.210	4378.00	979908.60	980355.41	-35.02	-184.17	2.27	-181.90
2698	41.57.740	112.10.870	4436.00	979911.14	980355.73	-27.34	-178.47	3.19	-175.28
2714	41.58.490	112.11.690	4403.00	979911.65	980356.86	-31.06	-181.07	2.20	-178.87
2715	41.58.540	112.14.200	4441.00	979920.04	980356.93	-19.17	-170.47	1.11	-169.36
2716	41.58.550	112.13.250	4369.00	979914.59	980356.96	-31.42	-180.27	1.22	-179.05
2717	41.58.580	112.12.340	4364.00	979909.33	980357.00	-37.19	-185.87	1.57	-184.30
2718	41.58.600	112.11.600	4411.00	979911.54	980357.03	-30.59	-180.87	2.48	-178.39
LV	41.15.530	112.29.900	4205.00	979906.54	980292.70	9.36	-133.90	.00	-133.90
SS2	40.44.110	112.12.810	4197.00	979825.41	980245.92	-25.74	-158.73	.00	-168.73
N0101	41.21.675	112. 3.809	4220.97	979853.21	980301.87	-51.63	-195.44	1.40	-194.04
N0102	41.21.673	112. 3.192	4224.63	979859.21	980301.87	-45.29	-189.22	1.88	-187.34
N0103	41.21.668	112. 2.960	4226.40	979861.57	980301.87	-42.66	-186.65	2.13	-184.52
N0104	41.21.661	112. 2.735	4234.05	979863.26	980301.85	-40.34	-184.59	2.42	-182.17
N0105	41.21.660	112. 2.503	4263.27	979863.30	980301.85	-37.55	-182.79	2.71	-180.03
N0106	41.21.654	112. 2.300	4289.66	979862.98	980301.84	-35.38	-181.52	2.97	-178.55
N0107	41.21.645	112. 2.075	4334.83	979861.18	980301.83	-32.91	-180.60	3.29	-177.31

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER	
N0108	41.21.650	112.	1.852	4379.08	979859.08	980301.84	-30.87	-180.06	3.71	-176.35
N0109	41.21.651	112.	1.638	4438.50	979855.70	980301.84	-28.66	-179.87	4.07	-175.80
N0110	41.21.627	112.	1.423	4527.99	979850.36	980301.81	-25.55	-179.81	4.41	-175.40
N0111	41.21.635	112.	1.183	4632.67	979844.02	980301.81	-22.04	-179.87	4.78	-175.09
N0112	41.21.630	112.	.998	4725.90	979839.49	980301.81	-18.80	-179.81	5.19	-174.62
N0113	41.21.735	112.	.677	4873.10	979829.07	980301.97	-14.53	-180.56	6.24	-174.32
N0114	41.21.763	112.	.421	5022.83	979819.64	980302.00	-9.91	-181.03	7.32	-173.72
N0201	41.20.998	112.	2.976	4253.45	979858.53	980300.87	-42.26	-187.17	1.70	-185.47
N0202	41.21.100	112.	2.867	4256.23	979860.26	980301.02	-40.43	-185.43	1.85	-183.58
N0203	41.21.099	112.	2.543	4266.64	979862.73	980301.01	-36.96	-182.32	2.20	-180.12
N0204	41.21.090	112.	2.328	4298.62	979863.49	980301.01	-33.19	-179.64	2.41	-177.23
N0205	41.21.096	112.	2.105	4301.67	979863.51	980301.01	-32.88	-179.44	2.84	-176.60
N0206	41.21.094	112.	1.989	4288.82	979863.46	980301.01	-34.14	-180.26	3.17	-177.09
N0207	41.21.095	112.	1.778	4466.31	979853.80	980301.01	-27.11	-179.27	2.92	-176.35
N0208	41.21.095	112.	1.564	4573.48	979812.05	980301.01	-58.78	-214.59	3.16	-211.43
N0209	41.21.093	112.	1.347	4790.94	979812.05	980301.01	-38.32	-201.55	3.44	-198.10
N0301	41.20.558	112.	1.461	4693.86	979839.31	980300.21	-19.40	-179.31	2.77	-176.54
N0302	41.20.599	112.	1.721	4438.53	979854.88	980300.27	-27.90	-179.11	2.58	-176.53
N0304	41.20.615	112.	2.120	4250.24	979861.34	980300.30	-39.18	-183.98	2.65	-181.33
N0305	41.20.580	112.	2.307	4237.16	979862.71	980300.23	-38.98	-183.33	2.37	-180.96
N0306	41.20.547	112.	2.418	4236.24	979864.03	980300.20	-37.70	-182.03	2.12	-179.91
N0307	41.20.541	112.	2.674	4247.88	979857.11	980300.18	-43.51	-188.24	1.75	-186.49
N0308	41.20.611	112.	2.855	4248.02	979855.77	980300.30	-44.96	-189.68	1.54	-183.04
N0309	41.20.739	112.	3.176	4249.56	979853.57	980300.48	-47.20	-191.98	1.43	-190.55
N0310	41.21.013	112.	3.806	4232.82	979850.26	980300.89	-52.49	-196.70	1.20	-195.50
N0401	41.20.161	112.	3.793	4229.66	979847.76	980299.61	-54.01	-198.11	.98	-197.13
N0402	41.20.157	112.	3.268	4232.35	979850.61	980299.61	-50.91	-195.10	1.19	-193.91
N0403	41.20.154	112.	2.716	4235.03	979854.43	980299.61	-46.83	-191.12	1.54	-189.58
N0404	41.20.155	112.	2.523	4237.01	979856.31	980299.61	-44.77	-189.12	1.71	-187.41
N0405	41.20.154	112.	2.290	4242.13	979858.47	980299.61	-42.12	-186.65	1.96	-184.69
N0406	41.20.155	112.	2.093	4244.36	979861.01	980299.61	-39.37	-183.98	2.18	-181.80
N0407	41.20.146	112.	1.892	4251.67	979862.78	980299.59	-36.90	-181.75	2.50	-179.25
N0408	41.20.146	112.	1.761	4263.17	979863.44	980299.59	-35.16	-180.40	2.79	-177.61

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER	
N0409	41.20.147	112.	1.639	4291.90	979862.19	980299.59	-33.71	-179.93	2.75	-177.18
N0410	41.20.150	112.	1.475	4360.48	979858.69	980299.59	-30.76	-179.31	2.71	-176.60
N0411	41.20.153	112.	1.315	4455.05	979853.21	980299.61	-27.36	-179.14	2.61	-176.53
N0412	41.20.156	112.	1.094	4602.89	979844.86	980299.61	-21.80	-178.62	2.55	-176.07
N0413	41.20.162	112.	.791	4780.73	979834.30	980299.62	-15.65	-178.52	2.87	-175.65
N0414	41.20.161	112.	.407	4828.89	979831.70	980299.61	-13.70	-178.22	3.05	-175.17
N0415	41.20.162	112.	.003	4877.03	979828.36	980299.62	-12.53	-178.69	3.36	-175.33
N0501	41.19.799	112.	2.892	4234.90	979850.80	980299.07	-49.94	-194.21	1.26	-192.95
N0502	41.19.754	112.	2.434	4237.03	979854.46	980299.02	-46.02	-190.37	1.56	-188.81
N0503	41.19.711	112.	2.216	4238.12	979856.70	980298.94	-43.60	-187.99	1.72	-186.27
N0504	41.19.588	112.	1.933	4251.41	979858.09	980298.77	-40.79	-185.63	1.78	-183.85
N0505	41.19.658	112.	1.799	4261.26	979859.47	980298.87	-38.58	-183.76	1.98	-181.78
N0506	41.19.697	112.	1.620	4265.08	979862.55	980298.93	-35.21	-180.51	2.15	-178.36
N0507	41.19.705	112.	1.463	4278.09	979862.40	980298.94	-34.14	-179.89	2.30	-177.59
N0601	41.19.137	112.	2.797	4239.56	979846.89	980298.09	-52.43	-196.87	1.08	-195.79
N0602	41.19.249	112.	2.379	4242.58	979850.64	980298.26	-48.56	-193.10	1.33	-191.77
N0603	41.19.258	112.	1.943	4251.45	979854.11	980298.27	-44.27	-189.11	1.60	-187.51
N0604	41.19.320	112.	1.735	4260.03	979857.76	980298.36	-39.90	-185.04	1.77	-183.27
N0605	41.19.338	112.	1.617	4261.35	979859.05	980298.38	-38.51	-183.69	1.83	-181.86
N0606	41.19.355	112.	1.518	4267.39	979859.75	980298.41	-37.27	-182.66	1.89	-180.77
N0607	41.19.395	112.	1.365	4275.68	979859.78	980298.48	-36.53	-182.19	2.03	-180.16
N0608	41.19.439	112.	1.221	4286.65	979861.65	980298.55	-33.70	-179.74	2.18	-177.56
N0609	41.19.486	112.	1.147	4293.12	979861.69	980298.60	-33.10	-179.36	2.25	-177.11
N0610	41.19.573	112.	1.077	4300.19	979862.13	980298.73	-32.13	-178.63	2.42	-176.21
N0611	41.19.610	112.	1.013	4313.27	979861.74	980298.80	-31.35	-178.30	2.53	-175.77
N0612	41.19.664	112.	.939	4338.50	979860.78	980298.88	-30.02	-177.83	2.58	-175.25
N0613	41.19.781	112.	.780	4454.10	979854.30	980299.05	-25.80	-177.55	2.52	-175.03
N0614	41.19.868	112.	.563	4559.56	979848.40	980299.17	-21.90	-177.24	2.73	-174.51
N0615	41.19.953	112.	.377	4664.85	979841.95	980299.30	-18.58	-177.51	2.98	-174.53
N0701	41.18.594	112.	2.505	4236.89	979844.36	980297.28	-54.40	-198.75	1.07	-197.68
N0702	41.18.677	112.	2.049	4249.17	979846.19	980297.40	-51.53	-196.30	1.28	-195.02
N0703	41.18.684	112.	1.625	4261.12	979848.47	980297.41	-48.14	-193.31	1.42	-191.89
N0704	41.18.812	112.	1.361	4261.50	979852.62	980297.60	-44.14	-189.33	1.65	-187.68

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
N0705	41.18.958	112. 1.075	4268.98	979856.95	980297.82	-39.33	-184.77	1.84	-182.93
N0706	41.19.030	112. .922	4279.30	979858.44	980297.94	-36.99	-182.78	1.98	-180.80
N0707	41.19.114	112. .712	4300.28	979859.58	980298.05	-33.99	-180.50	2.17	-178.33
N0708	41.19.211	112. .505	4327.72	979859.90	980298.20	-31.23	-178.67	2.33	-176.34
N0709	41.19.294	112. .349	4368.59	979858.62	980298.33	-28.80	-177.63	2.41	-175.22
N0710	41.19.321	112. .122	4418.08	979856.21	980298.36	-26.59	-177.10	2.52	-174.58
N0711	41.19.381	111.59.916	4471.55	979853.35	980298.46	-24.52	-176.86	2.69	-174.17
N0712	41.19.527	111.59.800	4535.20	979849.57	980298.68	-22.53	-177.04	3.08	-173.96
N0713	41.19.680	111.59.703	4608.44	979845.20	980298.90	-20.23	-177.23	3.20	-174.03
N0714	41.19.819	111.59.599	4704.88	979838.99	980299.10	-17.57	-177.86	3.40	-174.46
N0715	41.19.990	111.59.543	4830.71	979830.47	980299.36	-14.51	-179.09	3.71	-175.33
N0716	41.20.164	111.59.517	4918.47	979824.97	980299.62	-12.02	-179.59	3.93	-175.66
N0717	41.20.332	111.59.454	4992.85	979820.04	980299.87	-10.21	-180.31	4.37	-175.94
N0718	41.20.481	111.59.426	5073.65	979814.77	980300.09	-8.10	-180.95	4.84	-176.11
N0801	41.19.739	112. 1.809	4259.79	979862.34	980298.98	-35.97	-181.09	2.05	-179.05
N0802	41.19.829	112. 1.841	4257.39	979862.89	980299.12	-35.78	-180.82	2.10	-178.72
N0803	41.19.906	112. 1.879	4255.69	979863.07	980299.23	-35.87	-180.86	2.13	-178.73
N0804	41.19.985	112. 1.914	4252.86	979863.55	980299.35	-35.78	-180.67	2.17	-178.50
N0805	41.20.059	112. 1.943	4250.61	979863.85	980299.47	-35.81	-180.62	2.25	-178.37
N0806	41.20.204	112. 2.002	4251.29	979863.98	980299.69	-35.83	-180.67	2.47	-178.20
N0807	41.20.286	112. 2.029	4254.79	979864.13	980299.80	-35.46	-180.42	2.43	-177.99
N0808	41.20.362	112. 2.069	4260.29	979864.15	980299.91	-35.04	-180.18	2.33	-177.85
N0809	41.20.438	112. 2.119	4268.31	979863.82	980300.03	-34.73	-180.15	2.28	-177.87
N0810	41.20.526	112. 2.119	4274.72	979864.28	980300.16	-33.80	-179.44	2.37	-177.07
N0811	41.20.635	112. 2.032	4271.99	979866.17	980300.33	-32.34	-177.88	2.76	-175.12
N0901	41.19.767	112. 1.601	4267.23	979862.15	980299.03	-35.51	-180.89	2.26	-178.63
N0902	41.19.849	112. 1.610	4267.83	979862.71	980299.14	-35.00	-180.40	2.32	-178.08
N0903	41.19.913	112. 1.674	4268.64	979862.89	980299.25	-34.85	-180.28	2.34	-177.94
N0904	41.19.990	112. 1.697	4266.19	979862.96	980299.36	-35.12	-180.47	2.45	-178.02
N0905	41.20.042	112. 1.725	4266.09	979863.01	980299.44	-35.16	-180.50	2.61	-177.89
N0906	41.20.216	112. 1.790	4263.00	979863.15	980299.70	-35.57	-180.80	2.82	-177.98
N0907	41.20.317	112. 1.838	4267.28	979862.73	980299.84	-35.73	-181.11	2.77	-178.34
N0908	41.20.391	112. 1.874	4273.93	979862.98	980299.96	-34.97	-180.58	2.73	-177.85

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE ROUGUER
N0909	41.20.470	112. 1.922	4273.13	979863.33	980300.08	-34.82	-180.40	2.71	-177.69
N0910	41.20.552	112. 1.983	4271.50	979853.65	980300.20	-34.77	-180.29	2.70	-177.59
N1001	41.19.784	112. 1.361	4287.49	979862.64	980299.05	-33.13	-179.20	2.51	-176.69
N1002	41.19.844	112. 1.399	4288.27	979862.82	980299.14	-32.97	-179.06	2.52	-176.54
N1003	41.19.926	112. 1.463	4287.97	979862.72	980299.26	-33.21	-179.30	2.56	-176.74
N1004	41.19.997	112. 1.499	4288.43	979862.64	980299.37	-33.36	-179.47	2.65	-176.82
N1005	41.20.088	112. 1.565	4288.68	979862.73	980299.51	-33.39	-179.50	2.79	-176.71
N1006	41.20.228	112. 1.693	4307.24	979851.71	980299.71	-32.86	-179.60	2.69	-176.92
N1007	41.20.305	112. 1.751	4305.39	979861.84	980299.83	-33.02	-179.70	2.70	-177.00
N1008	41.20.387	112. 1.787	4292.47	979862.50	980299.96	-33.71	-179.95	2.82	-177.13
N1009	41.20.473	112. 1.832	4284.52	979863.30	980300.08	-33.78	-179.75	2.90	-176.84
N1010	41.20.545	112. 1.852	4283.97	979863.73	980300.20	-33.51	-179.47	3.13	-176.34
N1011	41.20.621	112. 1.887	4290.26	979863.68	980300.31	-33.09	-179.26	3.03	-176.23
N1101	41.19.819	112. 1.230	4318.32	979861.76	980299.10	-31.16	-178.28	2.59	-175.69
N1102	41.19.878	112. 1.313	4316.63	979861.77	980299.19	-31.39	-178.46	2.59	-175.87
N1103	41.19.945	112. 1.399	4311.42	979861.95	980299.29	-31.81	-178.69	2.59	-176.10
N1104	41.19.988	112. 1.089	4514.90	979850.40	980299.36	-24.29	-178.11	2.44	-175.67
T0101	41.40.529	112. 6.216	4298.14	979893.20	980330.02	-32.54	-178.97	1.54	-177.43
T0102	41.40.570	112. 5.977	4298.84	979892.86	980330.09	-32.88	-179.33	1.80	-177.53
T0103	41.40.620	112. 5.776	4291.17	979893.20	980330.16	-33.33	-179.52	2.15	-177.37
T0104	41.40.605	112. 5.546	4297.58	979892.86	980330.12	-33.03	-179.45	2.50	-176.95
T0105	41.40.585	112. 5.346	4302.51	979895.19	980330.10	-30.22	-176.80	2.92	-173.88
T0106	41.40.620	112. 5.131	4310.02	979897.05	980330.16	-27.71	-174.54	3.52	-171.02
T0107	41.40.620	112. 4.892	4318.73	979898.81	980330.16	-25.13	-172.26	4.43	-167.83
T0108	41.40.618	112. 4.676	4333.58	979900.59	980330.16	-21.85	-169.49	5.58	-163.91
T0109	41.40.623	112. 4.437	4400.47	979901.51	980330.16	-14.74	-164.66	7.25	-157.41
T0110	41.40.624	112. 4.224	4553.00	979902.18	980330.16	.28	-154.84	8.47	-146.37
T0111	41.40.631	112. 4.018	4768.51	979902.45	980330.17	20.80	-141.65	10.09	-131.56
T0112	41.40.624	112. 3.908	5031.97	979901.15	980330.16	44.30	-127.13	9.08	-118.05
T0201	41.40.176	112. 8.070	4277.34	979889.88	980329.48	-37.28	-183.00	.56	-182.44
T0202	41.40.168	112. 7.102	4279.04	979892.06	980329.48	-34.93	-180.71	.91	-179.80
T0203	41.40.186	112. 6.614	4251.57	979894.09	980329.50	-35.51	-180.35	1.30	-179.05
T0204	41.40.155	112. 6.216	4290.51	979894.25	980329.46	-31.65	-177.82	1.49	-176.33

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER	
T0205	41.40.167	112.	5.988	4292.05	979894.42	980329.48	-31.35	-177.57	1.71	-175.86
T0206	41.40.170	112.	5.553	4296.68	979895.41	980329.48	-29.93	-176.31	2.29	-174.02
T0207	41.40.173	112.	5.324	4301.60	979897.22	980329.48	-27.66	-174.21	2.72	-171.49
T0208	41.40.175	112.	5.108	4336.66	979898.08	980329.48	-23.50	-171.24	3.00	-168.24
T0209	41.40.175	112.	4.885	4338.36	979899.08	980329.48	-22.34	-170.14	3.67	-166.47
T0210	41.40.180	112.	4.669	4368.76	979899.76	980329.50	-18.81	-167.65	4.31	-163.34
T0211	41.40.178	112.	4.444	4466.65	979900.09	980329.50	-9.28	-161.45	4.85	-156.60
T0212	41.40.182	112.	4.248	4574.65	979900.19	980329.50	.98	-154.87	5.29	-149.58
T0213	41.40.188	112.	4.008	4728.04	979900.38	980329.52	15.58	-145.50	6.41	-139.09
T0214	41.40.187	112.	3.798	4857.76	979900.77	980329.50	28.19	-137.31	7.01	-130.30
T0215	41.40.193	112.	3.585	5003.23	979901.48	980329.52	42.57	-127.89	8.17	-119.72
T0216	41.40.193	112.	3.428	5171.74	979902.71	980329.52	59.65	-116.55	8.73	-107.82
T0301	41.40.005	112.	5.782	4290.39	979895.10	980329.24	-30.59	-176.76	1.93	-174.83
T0302	41.40.008	112.	5.556	4294.48	979895.99	980329.24	-29.31	-175.62	2.20	-173.42
T0303	41.40.011	112.	5.340	4298.87	979897.48	980329.24	-27.41	-173.87	2.60	-171.27
T0304	41.40.014	112.	5.101	4342.48	979898.20	980329.26	-22.60	-170.55	2.86	-167.69
T0305	41.40.024	112.	4.869	4437.88	979898.50	980329.27	-13.34	-164.53	3.09	-161.44
T0306	41.40.019	112.	4.649	4444.94	979899.10	980329.26	-12.07	-163.50	3.71	-159.79
T0401	41.39.856	112.	5.762	4285.69	979895.75	980329.01	-30.15	-176.16	1.94	-174.22
T0402	41.39.859	112.	5.541	4289.86	979896.54	980329.02	-28.98	-175.13	2.22	-172.91
T0403	41.39.859	112.	5.327	4297.47	979897.94	980329.02	-26.86	-173.27	2.57	-170.70
T0404	41.39.861	112.	5.102	4356.61	979898.53	980329.02	-20.71	-169.14	2.71	-166.43
T0405	41.39.869	112.	4.875	4441.43	979898.52	980329.04	-12.76	-164.07	2.96	-161.11
T0406	41.39.867	112.	4.650	4515.24	979898.11	980329.04	-6.23	-160.06	3.38	-156.67
T0501	41.39.727	112.	6.220	4289.31	979894.68	980328.82	-30.69	-176.82	1.41	-175.41
T0502	41.39.725	112.	6.012	4287.64	979895.47	980328.82	-30.06	-176.13	1.61	-174.52
T0503	41.39.727	112.	5.782	4285.45	979896.14	980328.82	-29.59	-175.59	1.89	-173.70
T0504	41.39.727	112.	5.548	4286.60	979897.00	980328.82	-28.62	-174.66	2.19	-172.47
T0505	41.39.727	112.	5.346	4290.91	979898.38	980328.82	-26.84	-173.02	2.50	-170.52
T0506	41.39.729	112.	5.085	4388.96	979898.38	980328.82	-17.62	-167.14	2.58	-164.56
T0507	41.39.733	112.	4.865	4478.31	979898.57	980328.83	-9.03	-161.60	2.82	-158.78
T0508	41.39.743	112.	4.680	4562.15	979898.16	980328.84	-1.57	-157.00	3.26	-153.74
T0509	41.39.741	112.	4.439	4604.06	979898.42	980328.84	2.63	-154.22	3.73	-150.49

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
T0510	41.39.738	112. 4.248	4659.95	979898.67	980328.83	8.16	-150.60	4.16	-146.44
T0511	41.39.759	112. 3.788	4788.58	979899.50	980328.87	21.14	-142.00	5.68	-136.32
T0512	41.39.753	112. 3.370	5012.85	979900.65	980328.86	43.30	-127.48	7.62	-119.86
T0513	41.39.757	112. 2.971	5457.46	979900.25	980328.86	84.72	-101.21	9.41	-91.80
T0601	41.39.588	112. 5.759	4284.07	979896.46	980328.61	-29.19	-175.14	1.87	-173.27
T0602	41.39.585	112. 5.544	4283.38	979897.67	980328.61	-28.05	-173.98	2.13	-171.84
T0603	41.39.583	112. 5.316	4288.39	979898.74	980328.61	-26.50	-172.60	2.51	-170.09
T0604	41.39.593	112. 5.148	4302.34	979899.26	980328.62	-24.69	-171.26	2.74	-168.52
T0605	41.39.603	112. 4.901	4484.26	979899.15	980328.64	-7.70	-160.48	2.68	-157.80
T0606	41.39.612	112. 4.683	4545.77	979898.28	980328.64	-2.79	-157.66	3.15	-154.50
T0701	41.39.439	112. 5.775	4282.38	979896.78	980328.40	-28.82	-174.71	1.81	-172.90
T0702	41.39.444	112. 5.548	4281.87	979898.17	980328.40	-27.48	-173.35	2.05	-171.31
T0703	41.39.441	112. 5.346	4281.54	979899.00	980328.40	-26.68	-172.55	2.39	-170.16
T0704	41.39.449	112. 5.115	4304.27	979899.84	980328.41	-23.71	-170.35	2.68	-167.67
T0705	41.39.462	112. 4.908	4454.50	979899.53	980328.42	-9.90	-161.66	2.62	-159.04
T0706	41.39.454	112. 4.660	4489.39	979898.40	980328.41	-7.73	-160.68	3.10	-157.58
T0801	41.39.287	112. 6.208	4282.00	979893.22	980328.16	-32.18	-178.06	1.35	-176.71
T0802	41.39.298	112. 5.917	4281.60	979895.16	980328.18	-30.29	-176.16	1.50	-174.56
T0803	41.39.298	112. 5.766	4281.27	979897.01	980328.18	-28.47	-174.33	1.78	-172.55
T0804	41.39.298	112. 5.557	4280.78	979898.22	980328.18	-27.31	-173.15	2.02	-171.13
T0805	41.39.300	112. 5.356	4284.25	979899.29	980328.18	-25.91	-171.87	2.30	-169.57
T0806	41.39.305	112. 5.125	4282.39	979900.08	980328.19	-25.31	-171.20	2.74	-168.46
T0807	41.39.311	112. 4.901	4344.74	979899.81	980328.20	-19.73	-167.75	2.88	-164.87
T0808	41.39.311	112. 4.690	4427.15	979898.67	980328.20	-13.12	-163.94	3.06	-160.88
T0809	41.39.311	112. 4.462	4481.11	979897.51	980328.20	-9.20	-161.87	3.54	-158.33
T0810	41.39.309	112. 4.248	4546.72	979897.40	980328.19	-3.12	-158.02	4.00	-154.02
T0811	41.39.309	112. 4.030	4686.32	979897.92	980328.19	10.53	-149.13	4.54	-144.59
T0812	41.39.316	112. 3.799	4739.55	979898.23	980328.20	15.83	-145.64	5.27	-140.37
T0813	41.39.316	112. 3.586	4869.79	979898.38	980328.20	28.23	-137.68	6.09	-131.59
T0814	41.39.325	112. 3.138	5136.24	979897.99	980328.22	52.89	-122.10	8.21	-113.89
T0815	41.39.325	112. 2.739	5592.66	979897.76	980328.22	95.59	-94.95	9.30	-85.65
T0901	41.39.151	112. 5.772	4277.19	979896.29	980327.96	-29.36	-175.08	1.76	-173.32
T0902	41.39.156	112. 5.524	4277.09	979897.78	980327.97	-27.89	-173.60	2.05	-171.55

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
T0903	41.39.158	112. 5.323	4284.68	979898.71	980327.97	-26.24	-172.22	2.32	-169.90
T0904	41.39.173	112. 5.102	4293.39	979899.20	980327.98	-24.95	-171.22	2.65	-169.57
T0905	41.39.176	112. 4.889	4307.87	979898.97	980328.00	-23.83	-170.60	3.05	-167.55
T0906	41.39.186	112. 4.664	4358.83	979898.06	980328.02	-19.96	-168.47	3.38	-165.08
T1001	41.38.752	112. 7.446	4276.57	979833.79	980327.36	-41.32	-187.01	.67	-186.34
T1002	41.38.791	112. 7.071	4239.63	979884.82	980327.42	-43.82	-188.26	.84	-187.42
T1003	41.38.812	112. 6.635	4274.01	979886.63	980327.45	-38.80	-184.41	1.00	-183.41
T1004	41.38.842	112. 6.220	4269.63	979889.94	980327.51	-35.97	-181.43	1.29	-180.14
T1005	41.38.839	112. 5.979	4268.32	979891.77	980327.49	-34.24	-179.66	1.48	-178.18
T1006	41.38.844	112. 5.778	4270.96	979893.70	980327.51	-32.08	-177.59	1.68	-175.91
T1007	41.38.855	112. 5.557	4277.01	979895.00	980327.52	-30.23	-175.94	1.88	-174.06
T1008	41.38.863	112. 5.339	4281.99	979895.92	980327.53	-28.85	-174.73	2.16	-172.57
T1009	41.38.881	112. 5.115	4291.24	979896.83	980327.56	-27.10	-173.30	2.47	-170.83
T1010	41.38.897	112. 4.898	4301.80	979897.08	980327.58	-25.87	-172.43	2.87	-169.56
T1011	41.38.906	112. 4.677	4319.93	979896.92	980327.59	-24.34	-171.52	3.35	-168.17
T1012	41.38.929	112. 4.448	4345.53	979896.58	980327.62	-22.30	-170.35	3.96	-166.39
T1013	41.38.952	112. 4.231	4457.56	979896.48	980327.66	-11.91	-163.77	4.24	-159.53
T1014	41.38.978	112. 4.009	4553.40	979896.50	980327.70	-2.80	-157.93	4.89	-153.04
T1015	41.39.006	112. 3.801	4686.30	979897.04	980327.74	10.09	-149.57	5.45	-144.12
T1016	41.39.043	112. 3.588	4834.83	979897.45	980327.80	24.42	-140.30	6.24	-134.06
T1017	41.39.076	112. 3.374	4990.21	979897.14	980327.85	38.67	-131.34	7.19	-124.15
T1018	41.39.098	112. 3.157	5142.31	979896.60	980327.88	52.40	-122.79	8.09	-114.70
T1019	41.39.115	112. 2.937	5412.38	979896.42	980327.91	77.59	-106.80	9.00	-97.80
T1101	41.38.418	112. 5.631	4264.09	979887.94	980326.87	-37.85	-183.12	1.73	-181.39
T1102	41.38.419	112. 5.327	4267.28	979889.66	980326.87	-35.83	-181.21	2.11	-179.10
T1103	41.38.422	112. 5.106	4275.41	979891.00	980326.87	-33.72	-179.38	2.39	-176.99
T1104	41.38.424	112. 4.902	4298.06	979892.49	980326.87	-30.11	-176.54	2.68	-173.86
T1105	41.38.425	112. 4.654	4338.79	979893.95	980326.87	-24.82	-172.64	3.06	-169.58
T1106	41.38.436	112. 4.386	4380.05	979894.92	980326.89	-19.98	-169.21	3.70	-165.51
T1107	41.38.439	112. 4.164	4413.88	979895.30	980326.89	-16.42	-166.80	4.53	-162.27
T1108	41.38.434	112. 4.002	4427.31	979895.51	980326.89	-14.95	-165.78	5.53	-160.25
T1109	41.38.438	112. 3.785	4575.71	979895.07	980326.89	-1.43	-157.32	6.25	-151.07
T1110	41.38.438	112. 3.608	4845.49	979895.61	980326.89	24.49	-140.59	6.38	-134.22

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
Q0101	41.53.106	112.12.668	4766.00	979902.16	980348.81	1.64	-160.74	1.35	-159.39
Q0102	41.53.150	112.12.290	4477.66	979917.47	980348.87	-10.24	-162.79	1.18	-161.61
Q0103	41.53.156	112.11.820	4404.09	979915.06	980348.88	-19.57	-159.62	1.10	-168.52
Q0104	41.53.154	112.11.378	4385.13	979913.58	980348.88	-22.74	-172.13	.99	-171.14
Q0105	41.53.160	112.10.945	4403.63	979911.06	980348.89	-23.62	-173.65	.93	-172.72
Q0106	41.53.171	112.10.504	4477.21	979907.21	980348.90	-20.56	-173.10	.86	-172.24
Q0107	41.53.190	112.10.070	4487.93	979908.14	980348.93	-18.65	-171.55	.96	-170.59
Q0108	41.53.187	112. 9.072	4558.81	979894.45	980348.93	-25.68	-180.99	1.51	-179.43
Q0109	41.53.187	112. 8.628	4762.74	979887.31	980348.93	-13.64	-175.90	1.28	-174.62
Q0110	41.53.192	112. 8.181	4856.05	979882.45	980348.95	-9.74	-175.18	1.44	-173.74
Q0111	41.53.205	112. 7.709	4876.43	979835.44	980348.96	-4.84	-170.98	1.62	-169.36
Q0112	41.53.242	112. 6.733	4991.62	979875.10	980349.02	-4.40	-174.46	1.93	-172.53
Q0201	41.52.283	112.12.586	4699.86	979906.42	980347.57	.92	-159.20	1.32	-157.88
Q0202	41.52.288	112.12.158	4550.39	979914.82	980347.59	-4.76	-159.78	1.21	-158.57
Q0203	41.52.284	112.11.847	4491.44	979915.43	980347.57	-9.67	-162.69	1.08	-161.61
Q0204	41.52.287	112.11.461	4441.42	979915.25	980347.59	-14.58	-165.89	.96	-164.93
Q0205	41.52.305	112.11.090	4411.07	979916.88	980347.62	-15.83	-166.11	.87	-165.24
Q0206	41.52.303	112.10.850	4362.27	979918.32	980347.60	-18.97	-167.58	.94	-166.65
Q0207	41.52.309	112.10.632	4365.93	979919.20	980347.62	-17.76	-166.50	.88	-165.62
Q0208	41.52.315	112.10.387	4411.26	979915.82	980347.63	-16.89	-167.18	.77	-166.41
Q0209	41.52.313	112.10.138	4421.13	979915.36	980347.62	-16.41	-167.03	.77	-166.26
Q0210	41.52.314	112. 9.926	4424.12	979916.22	980347.62	-15.26	-165.99	.76	-165.23
Q0211	41.52.311	112. 9.703	4426.96	979917.73	980347.62	-13.50	-164.32	.76	-163.55
Q0212	41.52.313	112. 9.490	4432.17	979917.53	980347.62	-13.20	-164.20	.78	-163.42
Q0213	41.52.315	112. 9.264	4438.35	979916.42	980347.63	-13.74	-164.95	.81	-164.14
Q0214	41.52.317	112. 9.048	4448.40	979914.66	980347.63	-14.56	-166.11	.83	-165.23
Q0215	41.52.326	112. 8.758	4450.87	979911.70	980347.65	-17.30	-168.94	.92	-168.02
Q0216	41.52.332	112. 8.538	4474.80	979909.44	980347.65	-17.31	-169.76	.90	-168.86
Q0217	41.52.336	112. 8.315	4482.64	979907.64	980347.66	-18.39	-171.11	.96	-170.15
Q0218	41.52.340	112. 8.096	4486.22	979908.02	980347.66	-17.67	-170.51	1.00	-169.51
Q0219	41.52.333	112. 7.850	4488.24	979909.94	980347.65	-15.54	-168.45	1.07	-167.38
Q0220	41.52.345	112. 7.603	4517.71	979908.23	980347.68	-14.51	-168.43	1.04	-167.39
Q0221	41.52.359	112. 7.111	4579.63	979903.89	980347.69	-13.04	-169.06	1.02	-168.04

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
Q0222	41.52.368	112. 6.722	4613.38	979900.41	980347.70	-13.36	-170.53	1.06	-169.47
Q0223	41.52.370	112. 6.439	4642.09	979897.47	980347.70	-13.60	-171.75	1.06	-170.69
Q0224	41.52.380	112. 5.972	4702.65	979891.85	980347.72	-13.54	-173.75	1.11	-172.64
Q0225	41.52.361	112. 5.569	4762.51	979887.11	980347.69	-12.62	-174.87	1.19	-173.68
Q0226	41.52.765	112. 4.168	5517.14	979851.32	980348.30	21.96	-166.01	1.67	-164.34
Q0301	41.51.869	112.11.076	4452.23	979917.57	980346.96	-10.61	-162.30	.83	-161.47
Q0302	41.51.880	112.10.852	4431.47	979919.28	980346.98	-10.87	-161.85	.79	-161.06
Q0303	41.51.892	112.10.643	4416.34	979919.66	980346.99	-11.93	-162.39	.75	-161.64
Q0304	41.51.886	112.10.367	4341.68	979923.53	980346.99	-15.08	-163.00	.86	-162.14
Q0305	41.51.890	112.10.145	4326.21	979923.49	980346.99	-16.58	-163.97	.88	-163.09
Q0306	41.51.891	112. 9.926	4338.56	979921.77	980346.99	-17.14	-164.95	.81	-164.14
Q0307	41.51.890	112. 9.700	4404.86	979916.94	980346.99	-15.73	-165.80	.71	-165.09
Q0308	41.51.892	112. 9.472	4418.18	979918.96	980346.99	-12.46	-162.98	.69	-162.29
Q0309	41.51.894	112. 9.240	4412.11	979916.78	980346.99	-15.21	-165.52	.70	-164.83
Q0310	41.51.910	112. 8.981	4418.54	979915.36	980347.02	-16.06	-166.59	.70	-165.89
Q0311	41.51.909	112. 8.519	4430.27	979911.50	980347.02	-18.81	-169.75	.73	-169.02
Q0312	41.51.912	112. 8.296	4433.13	979910.14	980347.02	-19.90	-170.94	.76	-170.18
Q0313	41.51.908	112. 8.069	4437.28	979909.86	980347.02	-19.79	-170.97	.79	-170.18
Q0314	41.51.912	112. 7.809	4440.93	979911.05	980347.02	-18.26	-169.56	.84	-168.72
Q0315	41.51.913	112. 7.572	4451.32	979912.00	980347.02	-16.33	-167.98	.85	-167.13
Q0401	41.51.720	112.10.142	4410.52	979918.92	980346.73	-12.95	-163.22	.70	-162.51
Q0402	41.51.695	112. 9.893	4401.22	979918.30	980346.70	-14.42	-164.37	.68	-163.69
Q0403	41.51.707	112. 9.658	4320.87	979923.00	980346.71	-17.29	-164.50	.82	-163.68
Q0404	41.51.719	112. 9.430	4374.11	979918.80	980346.73	-16.50	-165.52	.68	-164.84
Q0405	41.51.686	112. 9.195	4398.10	979916.81	980346.69	-16.19	-166.03	.65	-165.38
Q0406	41.51.754	112. 8.974	4411.52	979915.41	980346.79	-16.43	-166.73	.66	-166.07
Q0407	41.51.775	112. 8.554	4424.04	979912.11	980346.81	-18.58	-169.30	.68	-168.62
Q0501	41.51.580	112.10.130	4428.51	979918.70	980346.52	-11.28	-162.15	.68	-161.47
Q0502	41.51.574	112. 9.898	4417.19	979918.38	980346.51	-12.65	-163.14	.65	-162.49
Q0503	41.51.571	112. 9.666	4358.62	979920.99	980346.51	-15.55	-164.04	.68	-163.36
Q0504	41.51.560	112. 9.441	4355.79	979920.13	980346.49	-16.66	-165.05	.68	-164.37
Q0505	41.51.542	112. 9.206	4403.74	979915.98	980346.47	-16.27	-166.30	.62	-165.68
Q0506	41.51.605	112. 8.973	4408.11	979915.02	980346.57	-16.92	-167.10	.62	-166.48

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
Q0507	41.51.609	112. 8.546	4419.41	979912.74	980346.57	-18.14	-168.70	.62	-168.08
Q0602	41.51.238	112.12.759	5003.21	979834.13	980346.02	8.72	-161.74	1.40	-160.34
Q0603	41.51.236	112.12.555	4869.20	979892.05	980346.02	4.03	-161.86	1.39	-160.47
Q0604	41.51.489	112.12.247	4739.99	979899.94	980346.39	-.61	-162.09	1.12	-160.97
Q0605	41.51.485	112.11.844	4667.10	979904.04	980346.38	-3.35	-162.36	.92	-161.44
Q0606	41.51.477	112.11.452	4554.77	979910.50	980346.38	-7.46	-162.64	.84	-161.80
Q0607	41.51.467	112.11.057	4497.08	979915.53	980346.37	-7.84	-161.05	.77	-160.28
Q0608	41.51.462	112.10.813	4463.68	979918.67	980346.35	-7.83	-159.90	.73	-159.17
Q0609	41.51.454	112.10.567	4436.42	979919.79	980346.34	-9.26	-160.40	.70	-159.70
Q0610	41.51.448	112.10.368	4438.61	979919.42	980346.34	-9.42	-160.64	.66	-159.98
Q0611	41.51.440	112.10.128	4445.65	979917.65	980346.32	-10.51	-161.97	.63	-161.34
Q0612	41.51.432	112. 9.903	4422.01	979918.98	980346.30	-11.39	-162.04	.61	-161.43
Q0613	41.51.442	112. 9.651	4395.96	979919.41	980346.32	-13.43	-163.19	.61	-162.58
Q0614	41.51.446	112. 9.446	4321.73	979923.11	980346.32	-16.71	-163.94	.74	-163.20
Q0615	41.51.448	112. 9.148	4392.33	979916.76	980346.34	-16.43	-166.08	.62	-165.46
Q0616	41.51.451	112. 8.966	4406.13	979914.64	980346.34	-17.26	-167.37	.59	-166.78
Q0617	41.51.465	112. 8.526	4412.99	979912.57	980346.35	-18.60	-168.94	.59	-168.35
Q0618	41.51.473	112. 8.290	4418.63	979911.74	980346.37	-19.01	-169.55	.59	-168.96
Q0619	41.51.481	112. 8.051	4422.64	979910.66	980346.38	-19.73	-170.40	.61	-169.79
Q0620	41.51.477	112. 7.825	4422.95	979910.33	980346.38	-20.03	-170.72	.64	-170.08
Q0621	41.51.476	112. 7.562	4426.79	979909.87	980346.37	-20.11	-170.93	.67	-170.26
Q0622	41.51.497	112. 6.947	4463.11	979906.63	980346.41	-19.98	-172.03	.70	-171.33
Q0623	41.51.503	112. 6.442	4500.92	979903.50	980346.41	-19.45	-172.79	.71	-172.03
Q0624	41.51.489	112. 5.875	4552.67	979900.79	980346.39	-17.38	-172.48	.81	-171.67
Q0625	41.51.519	112. 5.261	4698.53	979891.51	980346.44	-12.98	-173.06	1.10	-171.96
Q0626	41.51.523	112. 4.826	5001.30	979869.91	980346.44	-6.11	-176.50	1.49	-175.00
Q0627	41.51.524	112. 4.423	5493.66	979844.13	980346.44	14.43	-172.74	3.45	-169.29
Q0701	41.51.283	112.10.067	4474.08	979915.69	980346.09	-9.56	-161.99	.64	-161.35
Q0702	41.51.269	112. 9.904	4432.23	979918.58	980346.05	-10.58	-161.58	.59	-160.99
Q0703	41.51.268	112. 9.653	4403.73	979919.54	980346.05	-12.30	-162.33	.59	-161.74
Q0704	41.51.265	112. 9.427	4325.50	979923.18	980346.05	-16.02	-163.38	.71	-162.67
Q0705	41.51.262	112. 9.185	4318.19	979921.94	980346.05	-17.94	-165.05	.70	-164.35
Q0706	41.51.305	112. 8.958	4401.54	979914.53	980346.12	-17.58	-167.53	.58	-166.95

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
Q0707	41.51.321	112. 8.535	4410.21	979911.83	980346.15	-19.49	-169.75	.56	-169.19
Q0801	41.51.145	112.10.074	4470.76	979915.11	980345.87	-10.24	-162.55	.60	-161.95
Q0802	41.51.127	112. 9.892	4433.40	979917.71	980345.85	-11.14	-162.18	.58	-161.60
Q0803	41.51.122	112. 9.614	4406.36	979919.47	980345.84	-11.90	-162.02	.57	-161.45
Q0804	41.51.148	112. 9.426	4397.24	979918.02	980345.88	-14.26	-164.07	.57	-163.50
Q0805	41.51.138	112. 9.170	4317.86	979921.47	980345.87	-18.26	-165.36	.68	-164.68
Q0806	41.51.174	112. 8.971	4374.09	979915.93	980345.91	-18.56	-167.58	.57	-167.01
Q0807	41.51.182	112. 8.532	4406.80	979911.07	980345.93	-20.36	-170.49	.53	-169.96
Q0901	41.50.973	112.11.036	4547.17	979911.80	980345.62	-6.12	-161.04	.70	-160.34
Q0902	41.50.985	112.10.798	4567.83	979910.58	980345.63	-5.30	-160.92	.67	-160.25
Q0903	41.50.990	112.10.573	4574.53	979908.98	980345.65	-6.39	-162.24	.66	-161.53
Q0904	41.50.995	112.10.354	4536.83	979910.95	980345.65	-7.96	-162.53	.64	-161.89
Q0905	41.51.002	112.10.079	4467.91	979914.44	980345.66	-10.97	-163.19	.56	-162.63
Q0906	41.50.996	112. 9.891	4429.89	979916.61	980345.65	-12.36	-163.29	.55	-162.74
Q0907	41.51.000	112. 9.618	4405.53	979918.54	980345.66	-12.74	-162.83	.55	-162.28
Q0908	41.50.997	112. 9.414	4398.22	979916.86	980345.65	-15.09	-164.93	.54	-164.40
Q0909	41.51.006	112. 9.172	4340.05	979919.62	980345.66	-17.82	-165.68	.60	-165.08
Q0910	41.51.025	112. 8.951	4339.22	979917.37	980345.70	-20.18	-168.01	.60	-167.41
Q0911	41.51.026	112. 8.531	4402.48	979910.62	980345.70	-20.98	-170.97	.50	-170.47
Q0912	41.51.026	112. 8.282	4398.94	979909.94	980345.70	-21.99	-171.86	.51	-171.35
Q0913	41.51.030	112. 7.994	4397.31	979910.02	980345.71	-22.08	-171.89	.52	-171.37
Q0914	41.51.031	112. 7.774	4417.26	979908.92	980345.71	-21.30	-171.80	.51	-171.28
Q0915	41.51.039	112. 7.548	4419.26	979907.33	980345.73	-22.72	-173.28	.52	-172.76
Q1001	41.50.855	112.10.086	4467.38	979913.87	980345.45	-11.37	-163.57	.54	-163.03
Q1002	41.50.853	112. 9.887	4431.56	979915.48	980345.45	-13.13	-164.11	.54	-163.57
Q1003	41.50.853	112. 9.631	4404.91	979916.59	980345.45	-14.53	-164.60	.53	-164.07
Q1004	41.50.850	112. 9.391	4398.62	979915.59	980345.43	-16.11	-165.96	.52	-165.44
Q1005	41.50.855	112. 9.169	4390.10	979914.59	980345.45	-17.92	-167.49	.51	-166.98
Q1006	41.50.882	112. 8.946	4338.16	979916.62	980345.48	-20.81	-168.61	.56	-168.05
Q1007	41.50.900	112. 8.519	4396.39	979910.40	980345.51	-21.58	-171.36	.48	-170.88
Q1101	41.50.693	112.10.093	4464.08	979913.71	980345.20	-11.59	-163.68	.53	-163.15
Q1102	41.50.685	112. 9.887	4438.56	979914.10	980345.19	-13.60	-164.81	.52	-164.29
Q1103	41.50.705	112. 9.631	4408.99	979915.12	980345.21	-15.38	-165.59	.52	-165.07

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
Q1104	41.50.705	112. 9.418	4406.07	979913.44	980345.21	-17.34	-167.45	.51	-166.94
Q1105	41.50.700	112. 9.162	4395.75	979912.63	980345.21	-19.12	-168.87	.50	-169.37
Q1106	41.50.731	112. 8.937	4311.14	979916.93	980345.26	-22.82	-169.70	.62	-169.08
Q1107	41.50.737	112. 8.513	4391.65	979909.88	980345.27	-22.32	-171.93	.48	-171.45
Q1201	41.50.491	112.12.964	5422.09	979860.02	980344.89	25.13	-159.59	2.44	-157.15
Q1202	41.50.511	112.12.650	4988.69	979887.33	980344.92	11.64	-158.32	1.44	-156.87
Q1203	41.50.521	112.12.257	4862.49	979895.38	980344.94	7.81	-157.85	1.13	-156.72
Q1204	41.50.538	112.11.823	4766.77	979899.89	980344.97	3.28	-159.11	.95	-159.17
Q1205	41.50.548	112.11.423	4650.76	979905.14	980344.98	-2.39	-160.83	.78	-160.05
Q1206	41.50.560	112.10.997	4591.23	979907.89	980344.99	-5.25	-161.67	.65	-161.02
Q1207	41.50.570	112.10.751	4561.72	979908.33	980345.01	-7.10	-162.52	.61	-161.91
Q1208	41.50.570	112.10.533	4539.08	979910.56	980345.01	-7.50	-162.14	.57	-161.57
Q1209	41.50.577	112.10.321	4503.57	979913.02	980345.02	-8.40	-161.83	.55	-161.28
Q1210	41.50.572	112.10.093	4465.35	979913.64	980345.02	-11.37	-163.50	.53	-162.97
Q1211	41.50.560	112. 9.880	4444.17	979913.28	980344.99	-13.69	-165.10	.51	-164.59
Q1212	41.50.557	112. 9.641	4421.35	979912.94	980344.99	-16.18	-166.81	.50	-166.31
Q1213	41.50.555	112. 9.421	4410.73	979911.33	980344.99	-18.29	-168.56	.49	-169.07
Q1214	41.50.575	112. 9.159	4397.75	979911.41	980345.02	-19.96	-169.79	.48	-169.31
Q1215	41.50.583	112. 8.948	4388.48	979910.59	980345.04	-21.67	-171.18	.47	-170.71
Q1216	41.50.567	112. 8.508	4390.22	979908.65	980345.01	-23.41	-172.98	.45	-172.53
Q1217	41.50.512	112. 8.242	4392.66	979907.33	980344.94	-24.43	-174.09	.44	-173.65
Q1218	41.50.513	112. 8.033	4391.23	979907.05	980344.94	-24.85	-174.45	.43	-174.02
Q1219	41.50.525	112. 7.754	4392.74	979907.02	980344.95	-24.75	-174.41	.44	-173.97
Q1220	41.50.529	112. 7.529	4394.80	979906.67	980344.95	-24.91	-174.64	.44	-174.19
Q1221	41.50.493	112. 6.794	4415.57	979909.09	980344.91	-20.49	-170.92	.46	-170.45
Q1222	41.50.630	112. 6.377	4427.25	979907.74	980345.11	-20.94	-171.77	.55	-171.22
Q1223	41.50.188	112. 6.372	4414.82	979907.13	980344.44	-22.05	-172.46	.42	-172.04
Q1224	41.50.186	112. 5.797	4446.07	979905.51	980344.44	-20.73	-172.20	.45	-171.75
Q1225	41.50.190	112. 5.191	4495.41	979903.15	980344.44	-18.45	-171.60	.49	-171.11
Q1226	41.50.197	112. 4.614	4547.84	979901.43	980344.45	-15.25	-170.19	.56	-169.63
Q1227	41.50.427	112. 4.207	4660.47	979897.97	980344.80	-8.47	-167.25	.80	-166.45
Q1228	41.50.657	112. 4.052	4779.31	979893.58	980345.14	-1.92	-164.75	.91	-163.83
Q1229	41.50.676	112. 3.597	5021.83	979882.81	980345.17	9.99	-161.10	1.22	-159.88

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER
Q1301	41.50.437	112.10.099	4460.95	979913.73	980344.82	-11.49	-163.47	.53	-162.94
Q1302	41.50.432	112. 9.874	4439.58	979913.05	980344.80	-14.17	-165.42	.51	-164.91
Q1303	41.50.435	112. 9.641	4418.80	979912.33	980344.82	-16.86	-167.40	.49	-166.91
Q1304	41.50.427	112. 9.425	4401.29	979911.78	980344.80	-19.04	-168.99	.49	-168.50
Q1305	41.50.422	112. 9.206	4392.73	979911.09	980344.79	-20.51	-170.17	.47	-169.70
Q1306	41.50.449	112. 8.969	4381.83	979910.39	980344.84	-22.29	-171.58	.47	-171.11
Q1307	41.50.428	112. 8.503	4376.80	979908.77	980344.80	-24.35	-173.47	.45	-173.02
Q1401	41.49.667	112.12.654	5101.23	979879.80	980343.67	15.95	-157.84	1.19	-156.65
Q1402	41.49.669	112.12.163	4925.43	979890.44	980343.67	10.05	-157.75	.96	-156.79
Q1403	41.49.689	112.11.568	4701.84	979903.06	980343.70	1.62	-158.57	.87	-157.70
Q1404	41.49.685	112.11.010	4572.85	979910.66	980343.70	-2.91	-158.70	.76	-157.94
Q1405	41.49.696	112.10.434	4476.66	979912.67	980343.71	-9.97	-162.48	.64	-161.84
Q1406	41.49.602	112. 9.852	4404.58	979911.84	980343.56	-17.43	-167.49	.55	-166.94
Q1407	41.49.715	112. 9.244	4404.41	979910.66	980343.74	-18.80	-168.86	.47	-168.39
Q1408	41.49.727	112. 8.033	4366.83	979905.93	980343.76	-27.08	-175.85	.42	-175.44
Q1409	41.49.733	112. 7.510	4377.52	979903.90	980343.77	-28.12	-177.26	.38	-176.88
Q1410	41.49.730	112. 6.942	4383.88	979904.04	980343.76	-27.37	-176.72	.37	-176.35
Q1411	41.49.736	112. 6.378	4405.40	979905.64	980343.77	-23.76	-173.85	.36	-173.49
Q1501	41.49.015	112.12.640	4901.81	979890.70	980342.70	9.07	-157.93	1.85	-156.08
Q1502	41.49.134	112.12.050	4830.00	979894.70	980342.87	6.14	-158.41	1.11	-157.30
Q1503	41.49.183	112.11.532	4781.90	979896.36	980342.94	3.21	-159.71	.91	-158.80
Q1504	41.49.166	112.10.987	4594.53	979907.31	980342.91	-3.44	-159.97	.81	-159.16
Q1505	41.49.175	112.10.430	4471.46	979913.46	980342.92	-8.88	-161.22	.70	-160.51
Q1506	41.49.119	112. 9.824	4399.74	979912.09	980342.85	-16.92	-166.82	.56	-166.26
Q1507	41.48.851	112. 8.070	4313.61	979906.98	980342.45	-29.73	-176.69	.40	-176.29
Q1508	41.48.857	112. 7.511	4368.54	979901.79	980342.46	-29.77	-178.60	.39	-178.21
Q1509	41.48.866	112. 6.919	4367.25	979904.17	980342.48	-27.52	-176.31	.35	-175.96
Q1510	41.48.865	112. 6.345	4390.45	979907.13	980342.48	-22.38	-171.96	.33	-171.63
Q1614	41.50.259	112. 9.863	4432.77	979912.78	980344.55	-14.83	-165.85	.52	-165.33
Q1615	41.50.093	112. 9.853	4416.04	979913.00	980344.31	-15.94	-166.39	.53	-165.86
Q1616	41.49.932	112. 9.881	4409.51	979912.45	980344.06	-16.85	-167.08	.55	-166.53
Q1617	41.49.771	112. 9.858	4408.54	979911.50	980343.81	-17.64	-167.84	.55	-167.29
Q1701	41.54.333	112. 9.105	4959.91	979877.84	980350.65	-6.28	-175.26	2.93	-172.33

STAT.	LATITUDE	LONGITUDE	ELEV.	OBSERVED GRAVITY	THEOR. GRAVITY	FREE AIR	SIMPLE BOUGUER	T.C.	COMPLETE BOUGUER	
Q1702	41.54.083	112.	9.359	4810.13	979883.96	980350.27	-13.87	-177.75	2.08	-175.67
Q1703	41.53.618	112.	9.646	4660.76	979893.01	980349.57	-18.17	-176.96	1.24	-175.72
Q1704	41.53.384	112.	9.693	4578.81	979900.42	980349.22	-18.12	-174.11	1.10	-173.01
Q1705	41.53.192	112.	9.558	4561.19	979902.23	980348.95	-17.69	-173.08	1.05	-172.03
Q1706	41.52.974	112.	9.410	4524.15	979906.30	980348.61	-16.77	-170.90	1.02	-169.88
Q1707	41.52.838	112.	9.264	4511.31	979907.77	980348.41	-16.30	-170.00	.99	-169.01
Q1708	41.52.614	112.	9.088	4481.18	979911.02	980348.07	-15.55	-168.22	.96	-167.26
Q1709	41.52.488	112.	8.967	4459.66	979912.37	980347.88	-16.04	-167.97	.95	-167.02
Q1710	41.52.172	112.	8.795	4440.55	979912.75	980347.41	-16.99	-168.27	.84	-167.43
Q1711	41.51.906	112.	8.758	4427.11	979913.18	980347.02	-17.43	-168.26	.70	-167.56
Q1712	41.51.755	112.	8.754	4422.72	979913.47	980346.79	-17.32	-168.00	.65	-167.35
Q1713	41.51.598	112.	8.750	4414.98	979913.96	980346.55	-17.32	-167.74	.61	-167.13
Q1714	41.51.454	112.	8.753	4412.44	979913.24	980346.34	-18.06	-168.39	.60	-167.79
Q1715	41.51.296	112.	8.742	4407.63	979912.63	980346.10	-18.99	-169.05	.57	-168.48
Q1716	41.51.159	112.	8.748	4403.70	979912.17	980345.90	-19.52	-169.55	.54	-169.01
Q1717	41.51.020	112.	8.745	4400.62	979911.73	980345.70	-20.04	-169.97	.52	-169.45
Q1718	41.50.873	112.	8.750	4396.62	979911.20	980345.48	-20.73	-170.52	.53	-169.99
Q1719	41.50.716	112.	8.708	4389.45	979910.63	980345.23	-21.72	-171.27	.50	-170.77
Q1720	41.50.557	112.	8.756	4392.22	979909.23	980344.99	-22.63	-172.27	.49	-171.79
Q1721	41.50.424	112.	8.751	4387.50	979907.99	980344.79	-24.21	-173.69	.49	-173.20
Q1722	41.50.239	112.	8.762	4319.29	979912.85	980344.53	-25.41	-172.56	.52	-172.04
Q1723	41.49.917	112.	8.687	4353.09	979909.89	980344.03	-24.69	-173.00	.45	-172.55
Q1724	41.49.594	112.	8.644	4376.66	979908.26	980343.55	-23.63	-172.73	.45	-172.28
Q1725	41.49.271	112.	8.666	4371.65	979907.22	980343.07	-24.65	-173.59	.45	-173.14
Q1726	41.48.953	112.	8.654	4370.99	979906.38	980342.60	-25.09	-174.00	.42	-173.58

Listing of repeat stations for the Northern Wasatch

The following listing identifies any two stations which are located within 0.02 minutes of Latitude and Longitude of each other and the difference (STATION2-STATION1) between the Simple Bouguer gravity values of the two stations.

STATION1	STATION2	DIFF
A165	A112	.23000
A167	A114	.12000
A168	A115	.04000
A169	A116	.01000
A236	A51	-.69000
A237	A52	.00000
A244	A59	.00000
A245	A60	.00000
A246	A61	.04000
A147	A62	.10000
A248	A63	.00000
A249	A64	.10000
A250	A65	.10000
A251	A66	.27000
A252	A67	.00000
A253	A68	.00000
A254	A69	.00000
A255	A70	.00000
A153	A100	-.04000
A154	A101	-.18000
A155	A102	.02000
A156	A103	-.04000
A157	A104	-.04000
A158	A105	.00000
A159	A106	-.04000
A160	A107	-.54000
A161	A108	.60000
A162	A109	-.06000
A163	A110	.20000
A166	A113	.04000
A170	A117	.00000
A171	A118	-.02000
A172	A119	-.93000
A173	A120	-14.84000
A174	A121	-1.62000

STATION1	STATION2	DIFF
A175	A122	1.10000
A176	A123	.13000
A179	A126	-2.35000
A180	A127	.00000
A181	A128	-3.10000
A182	A129	.00000
A183	A130	-.02000
A184	A131	-.06000
A185	A132	-.20000
A186	A133	.00000
A187	A134	.00000
A188	A135	.08000
A190	A137	.20000
A222	A37	.00000
A223	A38	.00000
A224	A39	.00000
A225	A40	.10000
A226	A41	.00000
A227	A42	.50000
A228	A43	.00000
A229	A44	.00000
A230	A45	.00000
A231	A46	.10000
A232	A47	.00000
A233	A48	.00000
A234	A49	.00000
A235	A50	.84000
A238	A53	.10000
A239	A54	.00000
A240	A55	.10000
A241	A56	.00000
A242	A57	-.10000
A243	A58	.00000
A144	A92	.00000
A145	A92	.00000

STATION1	STATION2	DIFF
A145	A144	.00000
A146	A93	-.02000
A147	A94	-.02000
A148	A95	-.10000
A177	A124	-.02000
A178	A125	.00000
A189	A136	-.04000
A193	A140	.00000
A195	A142	.00000
A196	A143	.00000
L406	L405	.26000
L229	PT255	.07000
L245	PT181	-.71000
L230	PT256	.16000
L232	PT257	.13000
L259	PTF21	-3.88000
L227	PT253	-.04000
L234	PT259	.15000
L244	PT182	-.76000
L246	PT180	-.52000
L265	PTF22	-.44000
FB 1	PT169	.35000
BC 78	PT275	.25000
BC 7	BC 6	-.03000
L214	PT161	-.67000
L144	PT173	-.36000
L159	PT157	-.24000
L170	PT159	-.48000
L173	PT169	.13000
L173	FB 1	-.22000
L188	BC 18	-.08000
L189	BC 15	.06000
L190	BC 10	.02000
L198	BC 83	-.16000
L199	PT275	.17000

STATION1	STATION2	DIFF
L199	BC 78	-.08000
L200	BC 73	.67000
L203	PT172	.28000
L210	PT163	-.65000
L211	PT164	.00000
L212	PT165	-.58000
L213	PT166	-.69000
L215	PT167	-.73000
L251	PT176	-6.44000
BC 95	PT273	.28000
BC 34	PT125	.56000
BC 67	PT120	.36000
BC 50	PT118	.30000
BC 50	PT118	.41000
BC 45	PT119	.51000
BC 59	PT117	.37000
L181	PT248	.25000
L185	BC 30	-.13000
L186	PT272	.47000
L186	BC 27	-.04000
L187	BC 24	.08000
L192	BC 22	.03000
L193	BC109	-.02000
L194	BC108	-.27000
L195	BC 99	.14000
L196	BC 97	-.16000
L197	PT273	.23000
L197	BC 95	-.05000
AB29	L21	.01000
A635	L9	.46000
1350	W1052	-.87000
1351	W1051	-.84000
1352	W0022	-.85000
1353	W0023	-.87000
1354	W0019	-.87000

STATION1	STATION2	DIFF
1355	W0020	-.81000
1356	W0021	-.83000
1357	W1049	-.79000
1358	W1050	-.82000
1359	W0024	-.76000
1360	W1053	-.82000
1361	W0018	-.84000
1362	W1055	-.81000
1363	W1056	-.84000
1364	W1057	-.77000
1365	W1058	-.77000
1366	W1054	-.87000
1367	W0017	-.88000
1370	W1062	-.80000
1371	W1061	-.82000
1372	W1060	-.79000
1373	W1059	-1.07000
1374	W0012	-.86000
1375	W0013	-.84000
1376	W0014	-.86000
1378	W0011	-.85000
1379	W0010	-.81000
1380	W1063	-.78000
1385	W0016	-.83000
1389	W1066	-.73000
1390	W0015	-.69000
1395	W0009	-.73000
1396	W0008	-.75000
1397	W1067	-.72000
1398	W1068	-.71000
1402	W0006	-.71000
1403	W0001	-.74000
1404	W1069	-.70000
1405	W0002	-.65000
1408	W1074	-.69000

STATION1	STATION2	DIFF
1410	W0007	-.71000
1414	W1073	-.67000
1416	W1072	-.68000
1417	W1071	-.66000
1418	W1070	-.71000
1420	W0502	-.92000
1425	W0005	-.67000
1426	W0004	-.73000
1427	W0003	-.77000
1449	L62	-.30000
1462	L90	-.59000
1499	PT173	.15000
1499	L144	.51000
1501	PT174	.06000
2206	W0473	-.83000
2213	W0474	-.79000
2222	W0475	-.76000
2225	W0479	-.70000
2226	W0476	-.68000
2230	W0478	-.75000
2230	A143	1.63000
2230	A196	1.63000
2231	L376	-.55000
2234	W0477	-.66000
2242	L11	-2.96000
2245	L361	-.55000
2292	L263	.11000
2296	PT255	.16000
2296	L229	.09000
2297	PT254	.18000
2298	PT253	.17000
2298	L227	.21000
2301	PT256	.23000
2301	L230	.07000
2304	PT259	.18000

STATION1	STATION2	DIFF
2304	L234	.03000
2305	PT258	.21000
2306	PT257	.19000
2306	L232	.06000
2313	PT260	.15000
2318	PT183	.19000
2319	PT182	.23000
2319	L244	.99000
2321	PT181	.18000
2321	L245	.89000
2329	PT180	-.05000
2329	L246	.47000
2330	PT184	.21000
2333	PT179	.15000
2335	PT165	.18000
2335	L212	.76000
2338	PT175	.16000
2341	PT178	.17000
2342	PT177	.23000
2343	PT164	.17000
2343	L211	.17000
2345	PT176	.15000
2345	L251	6.59000
2353	PT162	.22000
2354	PT163	.17000
2354	L210	.82000
2356	PT172	.18000
2356	L203	-.10000
2357	PT171	.13000
2358	PT271	.19000
2359	PT170	.17000
2360	PT270	.16000
2362	PT169	.13000
2362	FB 1	-.22000
2362	L173	.00000

STATION1	STATION2	DIFF
2366	PT168	.23000
2367	PT167	.20000
2367	L215	.93000
2368	PT166	.14000
2368	L213	.83000
2369	PT161	.22000
2369	L214	.89000
2370	PT269	.21000
2371	PT275	.15000
2371	BC 78	-.10000
2371	L199	-.02000
2375	PT160	.17000
2378	PT274	.20000
2381	PT157	.22000
2381	L159	.46000
2382	L158	.42000
2387	PT158	.15000
2391	PT249	.18000
2394	PT159	.20000
2394	L170	.68000
2402	PT248	.21000
2402	L181	-.04000
2403	PT247	.22000
2404	PT272	.22000
2404	L186	-.25000
2412	PT130	.20000
2413	PT128	.19000
2414	PT129	.21000
2415	PT127	.16000
2416	PT124	.14000
2417	PT126	.15000
2424	PT125	.15000
2424	BC 34	-.41000
2432	PT120	.13000
2432	BC 67	-.23000

STATION1	STATION2	DIFF
2433	PT123	.10000
2441	PT122	.20000
2442	PT145	.19000
2443	PT119	.18000
2443	BC 45	-.33000
2444	PT118	.22000
2444	BC 50	-.08000
2444	BC 50	-.19000
2445	PT144	.20000
2446	PT143	.15000
2447	PT146	.15000
2448	PT147	.19000
2450	PT148	.14000
2454	PT117	.18000
2454	BC 59	-.19000
2460	PT133	.13000
2461	PT132	.22000
2462	PT131	.13000
2464	PT111	.18000
2465	PT112	.23000
2466	PT113	.21000
2468	PT114	.21000
2480	PT115	.20000
2482	PT116	.18000
2485	PT142	.21000
2491	PT141	.12000
2508	PT188	.21000
2513	PT186	.21000
2514	PT189	.20000
2516	PT185	.13000
2517	PT187	.15000
2520	PT243	.15000
2534	PT226	.14000
2537	PT227	.25000
2538	PT242	.17000

STATION1	STATION2	DIFF
2540	PT244	.28000
2541	PT234	.17000
2561	PT228	.22000
2568	PT233	.29000
2569	PT191	.28000
2570	PT190	.28000
2573	PT230	.26000
2575	PT229	.28000
2578	PT231	.23000
2579	PT232	.26000
2591	PT195	.24000
2599	PT238	.21000
2600	PT237	.23000
2602	PT235	.24000
2607	PT196	.21000
2618	PT239	.29000
2619	PT240	.30000
2621	PT236	.27000
2622	PT197	.27000
2637	PT203	.27000
2638	PT204	.26000
2639	PT202	.24000
2640	PT201	.26000
2648	PT206	.22000
2651	PT205	.28000
2666	PT209	.26000
2667	PT208	.32000
2668	PT241	.27000
2681	PT216	.22000
2682	PT212	.20000
2684	PT213	.28000
2685	PT214	.27000
2686	PT215	.28000
2694	PT217	.31000
2698	PT220	.30000

STATION1	STATION2	DIFF
2715	PT223	.25000
2716	PT222	.24000
2717	PT221	.30000
2718	PT218	.26000
N0107	L269	.83700
N0111	L270	.60400
N0310	L273	1.33000
N0401	L276	.68800
N0716	L288	.18100
T0204	BC 46	.11900
T0207	BC 52	-.65300
T0604	BC 61	-.46700
T0801	BC 41	-.05700
Q0210	PT240	.12000
Q0210	2619	-.18000
Q0220	2620	.75800
Q0223	PT197	.35000
Q0223	2622	.08000
Q1211	PT237	.26200
Q1211	2600	.03200
Q1223	PT195	.32800
Q1223	2591	.08800
Q1504	2575	.40400
Q1510	PT190	.36900
Q1510	2570	.08900

BASED ON 375 SAMPLES, THE VARIANCE IS 1.12795
 THE STANDARD DEVIATION IS 1.06205 AVERAGE ERROR IS .05447

Memo

March 7, 1980

①

To: Howard Ross

Re: Open filing of principal facts of gravity data -- DOE funds.

Cooperative project: ESL, UGMS, & U. of Utah - G.G. Duff

I. Phase I -- Jordan Valley -- March 1980 -- (UGMS interested)

A. Field work -- optional but desirable

Tie several base stations together -- 1-2 days work only

B. Office work -- Sierpa & Cook

Prelim. { 1:250,000 station
1:125,000

Computer

NO terrain corrections

Final. { 1:162,500
sta Locat
S. Bouguer Gravity
Contoured

C. Mid-April, 15th

II Phase II -- Wasatch Front -- April + 1st part of May 1980

A. Areas:

1) Utah Valley -- UGMS interested

2) Jack Valley -- Cook "

3) From Salt Lake Salient to Idaho state line -- UGMS interested

B. Field work

Tie several base stations together -- 1-2 days work only.

C. Office work -- Sierpa & Cook

Computer

NO terrain corrections.

III Phase III -- E $\frac{1}{4}$ of 1° x 2° sheets -- Delta, Tooele, Utah -- May + early June

A. Office work -- Sierpa & Cook

B. NO terrain corrections

IV Phase IV -- June 1980 -- Sierpa & Cook

A. Terrain corrections of all of above data.

B. Complete (terrain-corrected) Bouguer gravity anomaly map - to be published by UGMS

Funding

Scholarship - Surfa - Mon. March 10, '80
Student

Computer

Travel -

Administration

Technical supervision by Cook

Cook to report progress weekly to Howard Ross.

Surfa to work directly under supervision of Cook

Scheduling of Laura Surfa (2.0 hrs/week) \$8.00/hr ±

1980 Month	GG Dept \$6.00/hr ±	DOE (2.0 hrs/week)	DMAAC # \$8.00/hr ±
March 10-31*	yes*	full time yes*	-
April	yes*	1/2	1/2 ##
May	yes*	1/2	1/2 ##
June	yes*	1/2	1/2 ##

* = funds available.

still pending for W. 3/4 of 1° x 2° sheet } Della Toole. K.L. Cook

Note: Cook may get some USGS funding for entire Brighton City 1° x 2° sheet. (still pending).

Acknowled

- 1) _____
- 2) _____
- 3) _____
- 4) _____

Contingent on funding by DMAAC.

112°30'

Max Christensen USGS	DOE Bringham City
DM A 625	DOE Tooe
	Delta
	Richfield

Howard Rose

KLC

30
June 13, 1980

MEMORANDUM

To: Wil Forsberg

From: Kenneth L. Cook

Subject: Transmittal of gravity data to you for the project:
"Gravity data in the Wasatch Front, Utah, area" K. L. Cook
Co-Principal Investigator.

A. Attached herewith, for your transmittal to the Utah Geological and Mineral Survey (UGMS) (after prior approval by Duncan Foley, Co-Principal Investigator) is one copy of the following for the UGMS and one copy for your files.

1. Phase I: Jordan Valley area

Notes: a. The required material for this project to date was already submitted by you to the UGMS prior to the deadline of mid-April, 1980 (for 1) the listing of the principal facts of the gravity stations -- which also included the terrain corrections -- for the Jordan Valley area and 2) the work-sheet complete Bouguer gravity anomaly map, with a contour interval of 2 milligals).

b. Therefore, no more data are now required to be submitted to the UGMS on Jordan Valley, *except as noted below.* **

c. However, it should be emphasized that the UGMS is expected to submit any new gravity data for the Jordan Valley area to me by August 1, 1980. Also I have informally requested to Wally Gwynn and Pete Murphy that these new gravity data be tied to the University of Utah gravity base station; *and they have assured me that this will be done.

2. Phase II: Utah Valley area

1. List of principal facts of gravity stations, including terrain corrections out to 100 miles (167.7 km). ✓

2. The following maps, plotted by the computer, with an "x" showing gravity station locations, at a scale of 1:62,500: ✓

a. 2 maps with designation of station numbers only.

* and should be submitted on IBM computer cards.

- b. 2 maps with complete Bouguer gravity anomaly values only. ✓

Note: Two maps of contiguous areas were required for the Utah Valley area at the required scale of 1:62,500. ✓

Ken to keep maps on 6/30/80 to correct data values. ESL to keep principal facts.

Phase III: Northern Wasatch Front area

1. List of principal facts of the gravity stations, including terrain corrections out to 100 miles (167.7 km).
2. The following maps showing gravity station locations, at a scale of 1:62,500 (plotted by the computer):
 - a. Map with the designation of station numbers only.
 - b. Map with the complete Bouguer gravity anomaly values only.

B. Attached herewith, for your transmittal to the Earth Science Laboratory Division (to the attention of Howard Ross) is one copy of the following:

- ✓ 1. East one-quarter of the Tooele Utah 1°x2° quadrangle. #
 - a. List of principal facts of the gravity stations, including terrain corrections out to 100 miles (166.7 km).
 - b. The following maps, plotted by the computer, with an "x" showing gravity station locations, at a scale of 1:62,500:
 - (1) Map with designation of station numbers only.
 - (2) Map with the complete Bouguer gravity anomaly values only.
- ✓ 2. East one-quarter of the Delta, Utah 1°x2° quadrangle. #
 - a. List of principal facts of the gravity stations, including terrain corrections out to 100 miles (166.7 km).
 - b. The following maps, plotted by the computer, with an "x" showing gravity station locations, at a scale of 1:62,500:
 - (1) Map with designation of station numbers only.
 - (2) Map with complete Bouguer gravity anomaly values only.

Kenneth L. Cook

Kenneth L. Cook

cc: Laura Serpa
Gary Reynolds

These are combined into one map.
* * Two overlap maps (corrected) with 1) station designations on one } A) 1 set for U9ms
2) Complete Bouguer gravity values on the other } B) 1 set for ESL.

Edward Ross

June 13, 1980

MEMORANDUM

To: Wil Forsberg

From: Kenneth L. Cook

Subject: Transmittal of gravity data to you for the project:
"Gravity data in the Wasatch Front, Utah, area" K. L. Cook
Co-Principal Investigator.

A. Attached herewith, for your transmittal to the Utah Geological and Mineral Survey (UGMS) (after prior approval by Duncan Foley, Co-Principal Investigator) is one copy of the following for the UGMS and one copy for your files.

1. Phase I: Jordan Valley area

Notes: a. The required material for this project to date was already submitted by you to the UGMS prior to the deadline of mid-April, 1980 (for 1) the listing of the principal facts of the gravity stations -- which also included the terrain corrections -- for the Jordan Valley area and 2) the work-sheet complete Bouguer gravity anomaly map, with a contour interval of 2 milligals).

b. Therefore, no more data are now required to be submitted to the UGMS on Jordan Valley.

c. However, it should be emphasized that the UGMS is expected to submit any new gravity data for the Jordan Valley area to me by August 1, 1980. Also I have informally requested to Wally Gwynn and Pete Murphy that these new gravity data be tied to the University of Utah gravity base station; *and they have assured me that this will be done.

2. Phase II: Utah Valley area

1. List of principal facts of gravity stations, including terrain corrections out to 100 miles (167.7 km).

2. The following maps, plotted by the computer, with an "x" showing gravity station locations, at a scale of 1:62,500:

a. 2 maps with designation of station numbers only.

* and should be submitted on IBM computer cards.

Callcom P
plotter errors

- b. 2 maps with complete Bouguer gravity anomaly values only. *ok*

Note: Two maps of contiguous areas were required for the Utah Valley area at the required scale of 1:62,500.

3. Phase III: Northern Wasatch Front area

1. List of principal facts of the gravity stations, including terrain corrections out to 100 miles (167.7 km).
2. The following maps showing gravity station locations, at a scale of 1:62,500 (plotted by the computer):
 - a. Map with the designation of station numbers only.
 - b. Map with the complete Bouguer gravity anomaly values only.

B. Attached herewith, for your transmittal to the Earth Science Laboratory Division (to the attention of Howard Ross) is one copy of the following:

1. East one-quarter of the Tooele Utah 1°x2° quadrangle.
 - a. List of principal facts of the gravity stations, including terrain corrections out to 100 miles (166.7 km).
 - b. The following maps, plotted by the computer, with an "x" showing gravity station locations, at a scale of 1:62,500:
 - (1) Map with designation of station numbers only.
 - (2) Map with the complete Bouguer gravity anomaly values only.
2. East one-quarter of the Delta, Utah 1°x2° quadrangle.
 - a. List of principal facts of the gravity stations, including terrain corrections out to 100 miles (166.7 km).
 - b. The following maps, plotted by the computer, with an "x" showing gravity station locations, at a scale of 1:62,500:
 - (1) Map with designation of station numbers only.
 - (2) Map with complete Bouguer gravity anomaly values only.

Combined into 1 map

Kenneth L. Cook

Kenneth L. Cook

cc: Laura Serpa
Gary Reynolds

MEMORANDUM

To: Wil Forsberg

April 21, 1980

From: Kenneth L. Cook

Subject: Submittal to UGMS of information concerning terrain corrections

In the research proposal dated March 21, 1980 to the Utah Geological and Mineral Survey entitled "Gravity data in the Wasatch Front area, Utah," (K.L. Cook and D. Foley, as P.I.'s) it was agreed to submit to them by May 1, 1980 the following information:

The radial distances to which the terrain corrections (if any) have been made for the stations in each of the surveys," (see footnotes to Tables 2 and 3 on the original proposal pages 9 and 12, respectively).

Attached herewith is the desired information, which is in the form of updated and amended copies of Tables 1, 2, and 3, which appeared on the original proposal on pages 6, 9, and 12, respectively.

Please transmit the information to the UGMS.

Kenneth L. Cook
Kenneth L. Cook

cc: Laura Serpa

Table 1 --- Approximate number of stations in Jordan Valley area.

<u>Name</u>	<u>Area Designation</u>	<u>Approximate No. of Stations</u>
U. of Utah Special studies, 1978	Profiles	801 ^{1/}
Cook and Berg, 1961,1972	7	583 ^{2/}
Fox, R. C., 1979	1	183 ^{3/}
Gay, 1980	2	564 ^{4/}
Mabey et al., 1962	27	43 ^{5/}
	Total	1,453

^{1/} Terrain corrections were not made.

^{2/} Terrain corrections out to a radial distance of 6.1 miles from each station, using Hammer zone chart.

^{3/} Terrain corrections out to a radial distance of 22,000 feet from each station.

^{4/} Terrain corrections out to a radial distance of 100 miles (167km) from each station, using a computer.

^{5/} Terrain corrections out to a radial distance of 100 miles from each station.

Note: For all terrain corrections made, a density of 2.67 gm/cc was used.

Table 2 --- Approximate number of stations in Utah Valley area.

Name	Area Designation	Approximate No. of Stations
Cook and Berg, 1961, 1972	7	332 ^{1/}

1/ Terrain corrections out to a radial distance of 6.1 miles, using Hammer zone chart.

Note: For all terrain corrections made, a density of 2.67 gm/cc was used.

Table 3 --- Approximate number of stations in the Northern Wasatch area.

Name	Area Designation	Approximate No. of Stations
U. of Utah Special studies (Cook & Groenewold, 1978, 1979)	2	40 <u>1/</u>
Cook et al., 1967	4	800 <u>2/</u>
Lum, 1970	5	
Novotny, 1970	6	
Cook and Berg, 1961; 1972	7	
Peterson, 1974	36	200 <u>3/</u>
Peterson and Oriel, 1970	39	
Total		1,040

1/ Terrain corrections out to a radial distance of 100 miles (167 km) from each station, using a computer.

2/ Terrain corrections out to a radial distance of generally 6.1 miles.

3/ Terrain corrections out to a radial distance of 100 miles (167 km) from each station, using a computer.

Note: For all terrain corrections made, a density of 2.67 gm/cc was used.