

GLD1659

GEOHERMAL RESERVOIR ASSESSMENT

COVE FORT SULPHURDALE UNIT

FINAL REPORT
FOR THE PERIOD
SEPTEMBER 1977 - JULY 1979

D. L. ASH, R. F. DONOVILLE, AND M. S. GULATI

DECEMBER 1979

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UNION OIL COMPANY OF CALIFORNIA
GEOHERMAL DIVISION
UNION OIL CENTER
461 S. BOYLSTON STREET
LOS ANGELES, CALIFORNIA 90017

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ABSTRACT

During 1978 and 1979 Union Oil Company of California drilled three exploratory geothermal wells in the Cove Fort-Sulphurdale geothermal resource area in southwestern Utah to obtain new subsurface data for inclusion in the U.S. Department of Energy's geothermal reservoir assessment program. Existing data from prior investigations which included the drilling of an earlier exploratory well at the Cove Fort-Sulphurdale area was also provided.

Two of the wells were abandoned before reaching target depth because of severe lost circulation and hole sloughing problems. The two completed holes reached depths of 5,221 ft. and 7,735 ft., respectively, and a maximum reservoir temperature of 353°F at 7,320 ft. was measured. The deepest well flow tested at the rate of 47,000 lbs./hr with a wellhead temperature of 200°F and pressure of 3 psig. Based upon current economics, the Cove Fort-Sulphurdale geothermal resource is considered to be sub-commercial for the generation of electrical power.

This report is a synopsis of the exploratory drilling activities and results, and it contains summary drilling, testing, geologic and geochemical information from four exploratory geothermal wells. Detailed information for each of the wells is contained in four separate technical reports available through the University of Utah Research Institute, Earth Science Laboratory (UURI/ESL), Salt Lake City, Utah.

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U. S. DEPARTMENT OF ENERGY
DIVISION OF ENERGY TECHNOLOGY
NEVADA OPERATIONS OFFICE
UNDER CONTRACT DE-AC08-77ET-28405

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INTRODUCTION

The Cove Fort Sulphurdale Unit (CFSU) Final Report has been prepared to compare and summarize results from the four exploratory-geothermal wells drilled on the unit. The general location of CFSU is shown in Figure 1. Specific well locations are shown in Figure 2.

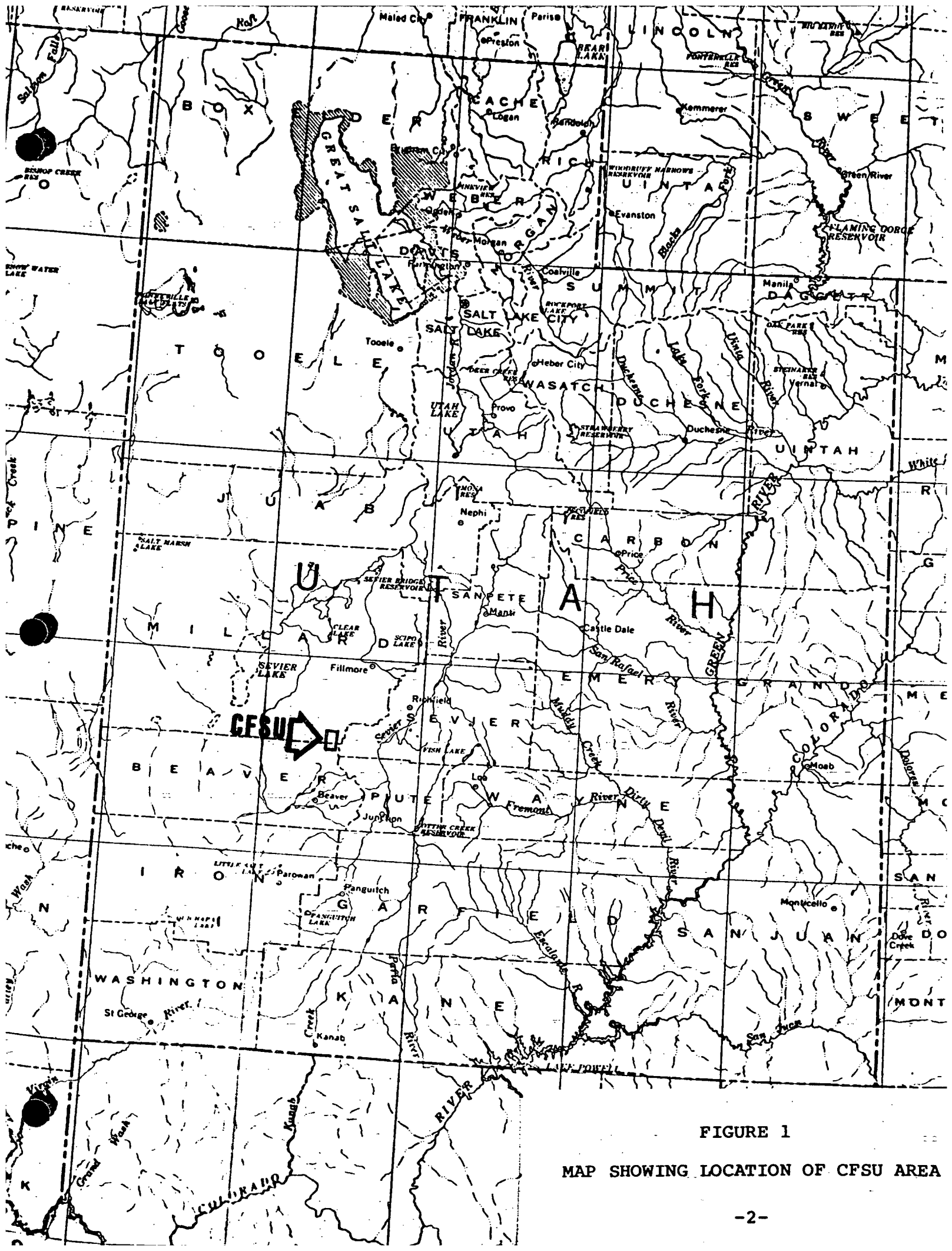


FIGURE 1
 MAP SHOWING LOCATION OF CFSU AREA

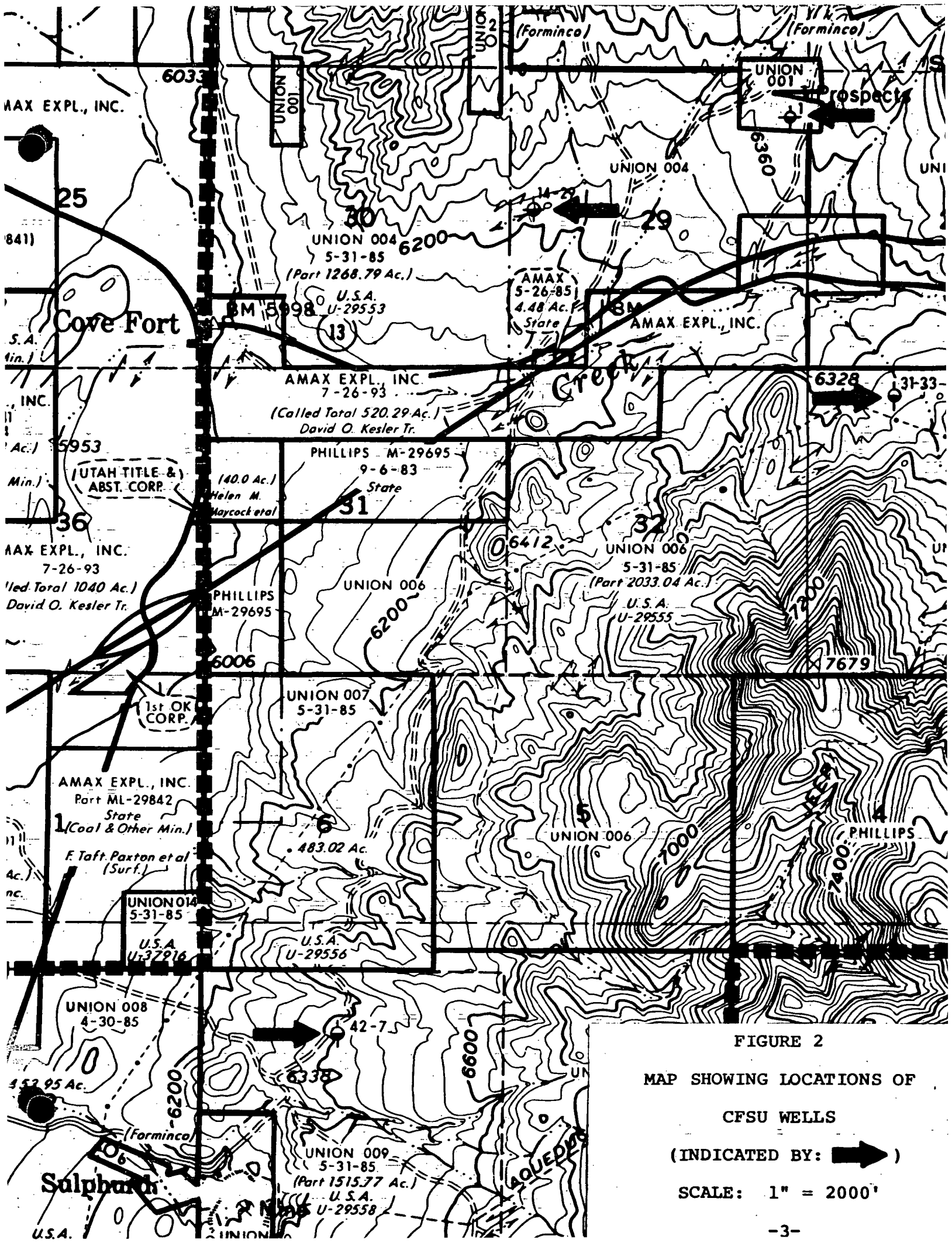



FIGURE 2
 MAP SHOWING LOCATIONS OF
 CFSU WELLS
 (INDICATED BY: )
 SCALE: 1" = 2000'

COVE FORT SULPHURDALE UNIT

DRILLING SUMMARY

The four exploration wells in the Cove Fort Sulphurdale Unit were drilled at the following total depths, days and costs per foot:

1. Forminco #1: 1051'; 34 days; \$594/foot;
2. CFSU #42-7: 7735'; 105 days; \$266/foot;
3. CFSU #31-33: 5221'; 64 days; \$243/foot;
4. CFSU #14-29: 2620'; 45 days; \$407/foot.

The two wells with the highest costs per foot, Forminco #1 and CFSU #14-29 were abandoned before reaching target depth because of severe hole cleaning problems. In the case of Forminco #1 a "sanded dolomite" caused the hole cleaning problems, while in CFSU #14-29 a formation of conventional dolomite/dolomitic limestone caused sloughing problems. CFSU #31-33 was plugged back to 2600' to eliminate cross flow below that point, and a 2-7/8" tubing string was hung to facilitate future temperature surveys. CFSU #42-7 was completed with a 7" liner at total depth and a 7" tie-back to surface.

The major problems contributing to the high costs per foot in the CFSU wells were lost circulation and corrosion. Each of the wells encountered severe lost circulation zones. The major corrosion problems were experienced while drilling with

Cove Fort Sulphurdale Unit/Drilling Summary

aerated water in wells CFSU #42-7 and #31-33. Details of lost circulation and corrosion are discussed in separate sections devoted to these topics.

Fishing jobs were confined to losses of one to two days per well with one exception. While spotting a lost circulation cement plug in Forminco #1, the cement flash set sticking the drill string. A ten day fishing/washing-over operation was required before the well was sidetracked and drilled ahead.

H₂S was encountered in all of the CFSU wells. Only the Forminco #1 well produced high concentrations of H₂S (600 ppm). An extensive H₂S monitoring system was installed on each of the CFSU wells. Personnel were familiarized with H₂S safety equipment and procedures through training and drills. Fortunately no H₂S related injuries were experienced.

The following CFSU Drilling Data Well Comparison Table and the Time vs. Depth Progress Graphs can be used to compare the four wells drilled.

CFSU DRILLING DATA WELL COMPARISON TABLE

| WELL | SPUD DATE | COMPLETION DATE | RIG # | TOTAL DEPTH (FT) | TOTAL DYS | TOTAL COST (\$) | TOTAL COST/FT (\$/FT) |
|--------------------------|-----------|--------------------|---------------------------|------------------|-----------|-----------------|-----------------------|
| Forminco #1 | 7/26/76 | 8/29/76 (Aban.) | Loffland Rig #5 | 1051 | 34 | 624,000 | 594 |
| CFSU #42-7 Permit #0045 | 11/29/77 | 3/14/78 | Loffland Rig #184 | 7735 | 105 | 2,056,000 | 266 |
| CFSU #31-33 Permit #0049 | 5/24/78 | 7/27/78 | Loffland Rig #5 | 5221 | 64 | 1,270,000 | 243 |
| CFSU #14-29 Permit #0072 | 5/25/79 | 7/9/79 (Aban.) | Brinkerhoff Signal Rig #3 | 2620 | 45 | 1,065,000 | 407 |

| WELL | MUD COST | MUD COST/FT (\$/FT) | CMT. PLUGS FOR LOST CIRCULATION | H ₂ S MAX. RECORDED CONCEN. (PPM) | FISHING JOBS | FISHING DAYS | MAX. TEMP. LOGGED |
|--------------------------|----------|---------------------|---------------------------------|--|--------------|--------------|-------------------|
| Forminco #1 | 44,025 | 42 | 9 | 600 | 1 | 10 | -- |
| CFSU #42-7 Permit #0045 | 182,889 | 24 | 37 | <10 | 2 | 1 | 353° F @ 7320' |
| CFSU #31-33 Permit #0049 | 72,437 | 14 | 27 | 10 | 2 | 2 | 294° F @ 4700' |
| CFSU #14-29 Permit #0072 | 35,616 | 14 | 18 | 50 | 2 | 2 | 196° F @ 2180' |

| WELL | CASING PROGRAM (ALL DEPTHS RKB) | | | | | FINAL CONDITION |
|--------------------------|---------------------------------|----------------|----------------------|-------------------------------|----------------------------|--|
| | CONDUCTOR CASING | SURFACE CASING | INTER-MEDIATE CASING | OTHER | OTHER | |
| Forminco #1 | 20" @ 120' | 13-3/8" @ 822' | -- | -- | -- | Abandoned due to inability to clean hole of unconsolidated "sanded dolomite". |
| CFSU #42-7 Permit #0045 | 30" @ 50' | 20" @ 251' | 13-3/8" @ 1552' | Liner 9-5/8": 1345' to 3357' | Liner 7" @ 7615' Tied Back | Suspended with 7" tied back to surface. |
| CFSU #31-33 Permit #0049 | 30" @ 52' | 20" @ 280' | 13-3/8" @ 1733' | Hanging Tubing 2-7/8" @ 2579' | -- | Plugged back to 2600' to eliminate cross flow below that point and hung 2-7/8" tubing at 2579' to facilitate future temperature surveys. |
| CFSU #14-29 Permit #0072 | 30" @ 38' | 20" @ 224' | 13-3/8" @ 1240' | Liner 9-5/8": 998' to 2078' | -- | Abandoned due to inability to clean hole and eliminate fill. |

FORMINCO I

TIME, DAYS

40

36

32

28

24

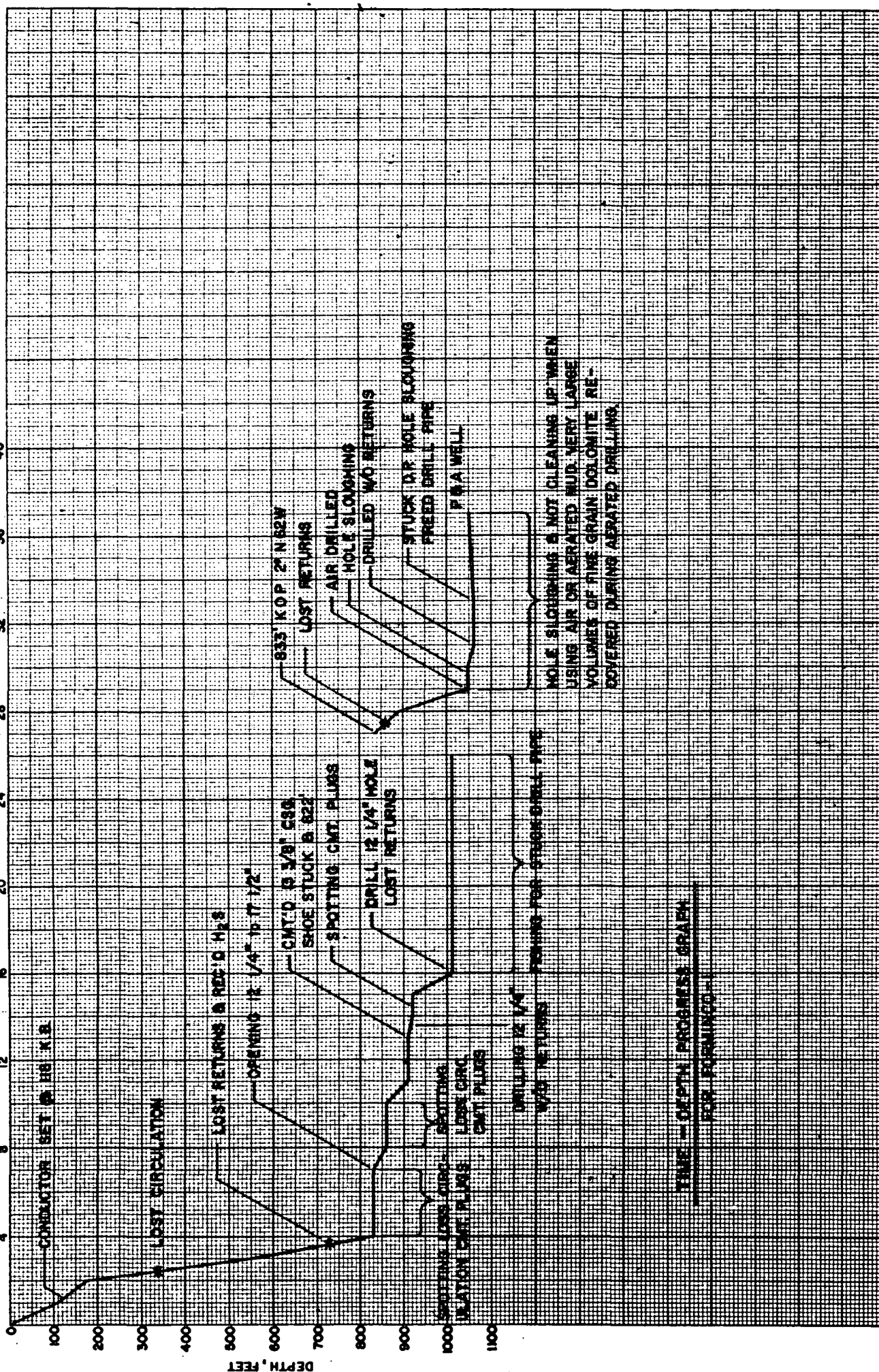
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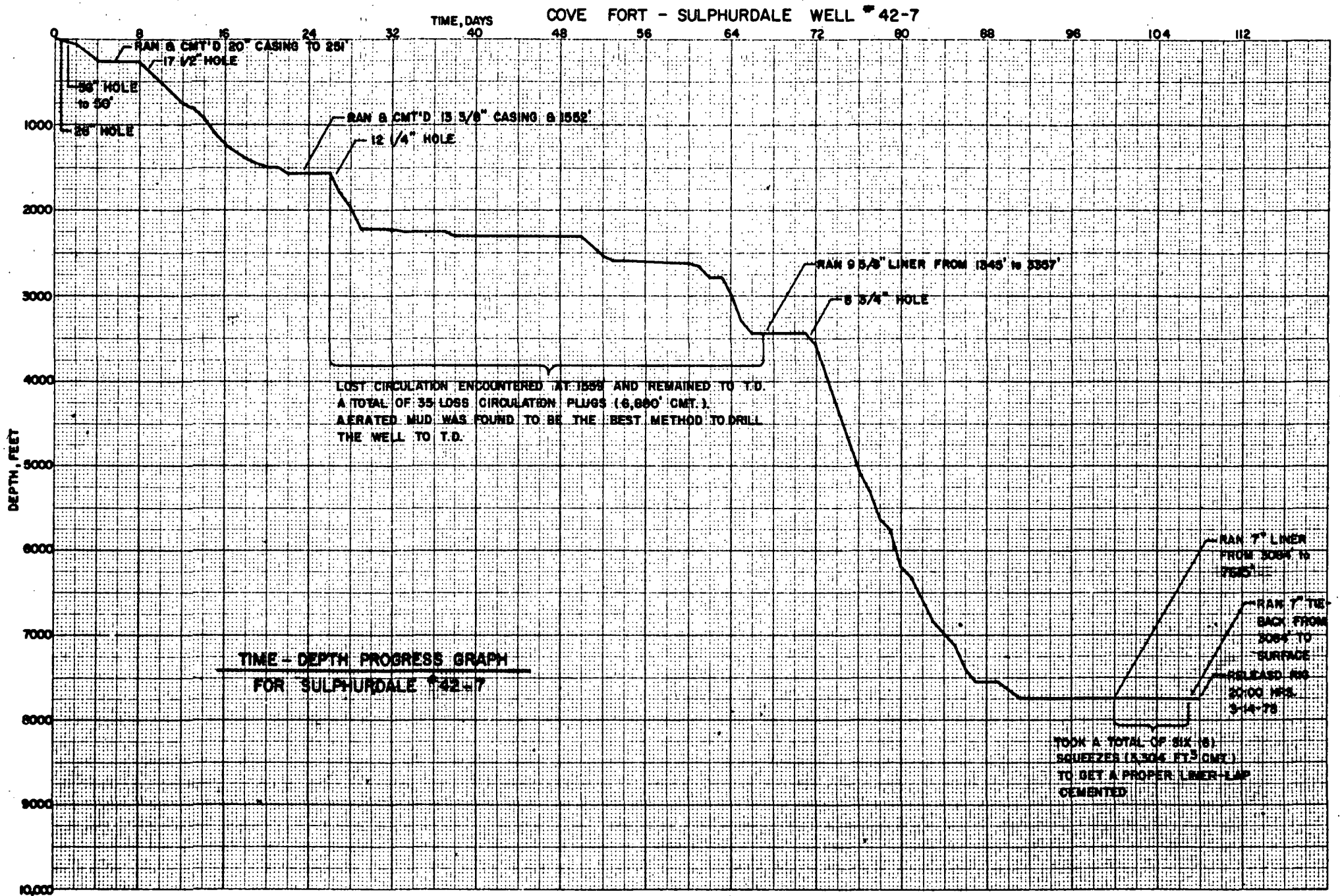
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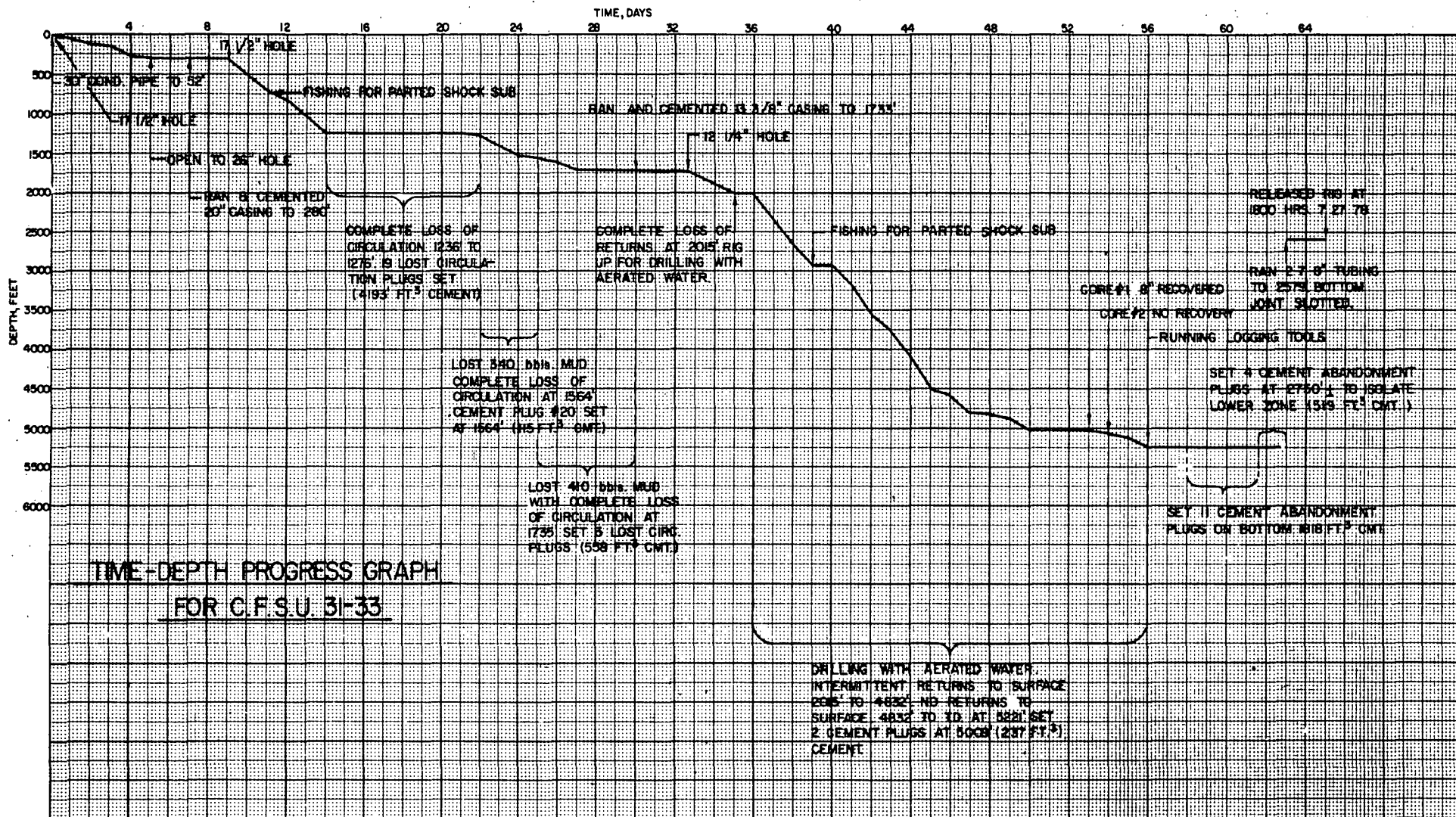
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TIME - DEPTH PROGRESS GRAPH
FOR FORMINCO I





COVE FORT SULPHURDALE UNIT

LOST CIRCULATION SUMMARY

All of the CFSU wells encountered severe lost circulation zones. A wide range of lost circulation materials, including fiber, cellophane, cotton seed hulls, mica, walnut hulls, sodium silicate-calcium chloride, and diatomaceous earth, were attempted with virtually no success. Cement plugs consisting of a variety of slurry types met with very limited, often short term, success in regaining circulation. In some cases it became necessary to drill without returns providing the thief zone accepted drill cuttings and the hole was kept clean. Drilling with aerated water was often effective in competent formations but greatly increased corrosion rates and sometimes resulted in the production of large quantities of formation water causing disposal problems.

Since it is ultimately important to cement casing strings completely from shoe to surface, lost circulation problems were faced as they occurred. When efforts to regain circulation were abandoned and the decision was made to drill ahead, lost circulation problems were only postponed until the next casing point was reached. A total of 91 cement plugs were utilized to combat lost circulation while drilling the four CFSU wells. The following tables compare slurry compositions for each

CFSU/Lost Circulation Summary

of the lost circulation cement plugs. Success of the cement plugs was very limited. There was no single slurry composition that proved conclusively to be the most effective.

Most of the lost circulation problems occurred in carbonate formations. In some cases extensive caverns were encountered as evidenced by the drill string abruptly falling 30'. A satisfactory solution to the more severe lost circulation problems in the CFSU remains to be found.

C.F.S.U. WELL FORMINCO #1 LOST CIRCULATION CEMENT PLUG COMPARISON

| PLUG NO. | TOTAL DEPTH (FT) | OEDP DEPTH (FT) | FORMATION TYPE | S L U R R Y C O M P O S I T I O N | | | | | | | |
|----------|------------------|-----------------|-----------------|-----------------------------------|---------------|------------------|---------|-----------------------|-----------|----------|---------------------|
| | | | | VOLUME (FT ³) | PERLITE RATIO | SILICA FLOUR (%) | GEL (%) | CaCl ₂ (%) | CFR-2 (%) | LCM #/SK | OTHER |
| 1 | 796 | 787 | Sanded Dolomite | 1000 | 2:1 | | 4 | 3 | | ½ | |
| 2 | 796 | 772 | Sanded Dolomite | 435 | 2:1 | | 4 | 3 | | ½ | |
| 3 | 829 | 776 | Sanded Dolomite | 408 | 2:1 | | 4 | | 3/4 | | Caustic Water Flush |
| 4 | 860 | 819 | Sanded Dolomite | 500 | 2:1 | | 4 | 2 | | ½ | Caustic Water Flush |
| 5 | 860 | 713 | Sanded Dolomite | 250 | 1:1 | | 2 | 3 | | ½ | Caustic Water Flush |
| 6 | 860 | 855 | Sanded Dolomite | 250 | | | | 3 | ½ | | |
| 6 | 860 | 855 | Sanded Dolomite | 500 | 1:1 | | 2 | | | ½ | |
| 7 | 910 | 786 | Sanded Dolomite | 500 | 1:1 | | 2 | | ½ | ½ | |
| 8 | 913 | 882 | Sanded Dolomite | 694 | | | | | | | Thix-Set Cement |
| 9 | 1004 | 976 | Sanded Dolomite | 500 | 1:1 | | 2 | 2 | ½ | | |

C.F.S.U. WELL #42-7 LOST CIRCULATION CEMENT PLUG COMPARISON

| PLUG NO. | TOTAL DEPTH (FT) | OEDP DEPTH (FT) | FORMATION TYPE | S L U R R Y C O M P O S I T I O N | | | | | | | | |
|----------|------------------|-----------------|----------------|-----------------------------------|---------------|------------------|---------|-----------------------|-----------|----------|-------|------------------------------|
| | | | | VOLUME (FT ³) | PERLITE RATIO | SILICA FLOUR (%) | GEL (%) | CaCl ₂ (%) | CFR-2 (%) | LCM #/SK | OTHER | |
| 1 | 1494 | 1457 | Andesite | 198 | 1:1 | 40 | 3 | | | | | 0.3% Retarder |
| 2 | 1494 | 1353 | Andesite | 200 | 1:1 | 40 | 3 | | | | | 0.3% Retarder |
| 3 | 2244 | 2202 | Sandstone | 250 | 1:1 | 40 | 3 | | | | | |
| 4 | 2244 | 2046 | Sandstone | 120 | 1:1 | 40 | 3 | | | | | |
| 5 | 2244 | 2046 | Sandstone | 250 | 1:1 | 40 | 3 | | | | | |
| 6 | 2244 | 2060 | Sandstone | 150 | 1:1 | 40 | 3 | | | | | |
| 7 | 2244 | 2172 | Sandstone | 396 | 2:1 | 40 | 3 | | | | | |
| 8 | 2250 | 2205 | Sandstone | 142 | | | | | | | ½ | Thix-Set and Gilsonite |
| 9 | 2250 | 1829 | Sandstone | 142 | | | | | | | ½ | Thix-Set and Gilsonite |
| 10 | 2250 | 1860 | Sandstone | 240 | 1:1 | 40 | 3 | | | | | |
| 11 | 2250 | 2209 | Sandstone | 120 | 1:1 | | 3 | | | | | |
| 12 | 2250 | 2169 | Sandstone | 193 | 2:1 | 40 | 3 | | | | | |
| 13 | 2250 | 2170 | Sandstone | 180 | 1:1 | 40 | 3 | | | | | |
| 14 | 2250 | 1946 | Sandstone | 100 | | | | | | | ½ | Thix-Set and Gilsonite |
| 15 | 2342 | 2108 | Sandstone | 223 | | | | | | | 1½ | Thix-Set and Gilsonite |
| 16 | 2342 | 2232 | Sandstone | 59 | | | | 2 | | | 1½ | Frac Gel Flush |
| 17 | 2342 | 2232 | Sandstone | 118 | | | | 2 | | | 1½ | Frac Gel Flush |
| 18 | 2342 | 2201 | Sandstone | 210 | | | | 2 | | | ½ | Frac Gel Flush |
| 19 | 2342 | 2232 | Sandstone | 136 | | | | 2 | | | ½ | Frac Gel Flush |
| 20 | 2342 | 2239 | Sandstone | 136 | | | | 2 | | | ½ | Frac Gel Flush |
| 21 | 2342 | 2201 | Sandstone | 98 | | | | 2 | | | ½ | 6% Gilsonite |
| 22 | 2342 | 2232 | Sandstone | 88 | | | | 2 | | | ½ | 12% Gilsonite |
| 23 | 2342 | 2233 | Sandstone | 88 | | | | 2 | | | ½ | 8#/sk Gilsonite |
| 24 | 2342 | 2232 | Sandstone | 161 | 2:1 | 40 | 3 | | | | | Frac Gel Flush |
| 24 | 2342 | 2232 | Sandstone | 98 | | | | 2 | | | ½ | 8#/sk Gilsonite |
| 25 | 2342 | 2201 | Sandstone | 161 | 2:1 | 40 | 3 | 3 | | | | NaSi-CaCl ₂ Flush |
| 26 | 2342 | 2201 | Sandstone | 352 | 1:1 | 40 | 3 | 3 | | | | Frac Gel Flush |
| 27 | 2606 | 2575 | Sandstone | 174 | | | | 2 | | | | Thix-Set and Gilsonite |
| 28 | 2606 | 2448 | Sandstone | 175 | | | | 2 | | | | Thix-Set and Gilsonite |
| 29 | 2606 | 2418 | Sandstone | 247 | 2:1 | | 5 | 2 | | | | |
| 30 | 2606 | 2248 | Sandstone | 367 | 2:1 | | 5 | 2 | | | | |
| 31 | 2606 | 2139 | Sandstone | 215 | 1:1 | | 4 | 2 | | | | |
| 32 | 2606 | 2046 | Sandstone | 250 | 1:1 | 40 | 3 | | | | | |
| 33 | 2606 | 1860 | Sandstone | 250 | 1:1 | 40 | 3 | | | | | |
| 34 | 2606 | 1675 | Sandstone | 250 | 1:1 | 40 | 3 | 2 | | | | |
| 35 | 2606 | 1490 | Sandstone | 250 | 1:1 | 40 | 3 | | | | | |
| 36 | 2804 | 2765 | Dolomite | 312 | 1:1 | 40 | 3 | | | ½ | | |
| 37 | 2804 | 2731 | Dolomite | 312 | 1:1 | 40 | 3 | | | | | |

C.F.S.U. WELL #31-33 LOST CIRCULATION CEMENT PLUG COMPARISON

| PLUG NO. | TOTAL DEPTH (FT) | OEDP DEPTH (FT) | FORMATION TYPE | S L U R R Y C O M P O S I T I O N | | | | | | | | |
|----------|------------------|-----------------|------------------------------|-----------------------------------|-----------------------------------|------------------|---------|-----------------------|-----------|---------|------------------------|---------------|
| | | | | VOLUME (FT ³) | PERLITE RATIO | SILICA FLOUR (%) | GEL (%) | CaCl ₂ (%) | CFR-2 (%) | LCM (%) | OTHER | |
| 1 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 375 | 1:1 | 40 | 3 | | ½ | | | |
| 2 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 350 | 1:1 | 40 | 3 | | ½ | | | |
| 3 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 240 | 1:1 | 40 | 3 | | ½ | | Gel Mud-LCM Flush | |
| 4 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 125 | 1:1 | 40 | 3 | | ½ | 15 | | |
| 5 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 225 | 1:1 | 40 | 3 | | ½ | 15 | | |
| 6 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 305 | 2:1 | 40 | 3 | | | | Gel Mud-LCM Flush | |
| 7 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 305 | 2:1 | 40 | 3 | | | | | |
| 8 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 230 | 1:1 | 40 | 3 | | | 15 | | |
| 9 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 230 | 1:1 | 40 | 3 | | | 25 | | |
| 10 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 210 | 1:1 | 40 | 3 | 2 | | 20 | | |
| 11 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 210 | 1:1 | 40 | 3 | 2 | | 20 | | |
| 12 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 210 | 1:1 | 40 | 3 | 2 | | 20 | | |
| 13 | 1241 | 1230 | Dolomitic Limestone/Dolomite | 166 | | | | 2 | | 1#/sk | Thix-Set and Gilsonite | |
| 14 | 1257 | 1230 | Dolomitic Limestone/Dolomite | 166 | | | | 2 | | 1#/sk | 25#/sk Gilsonite | |
| 15 | 1257 | 1230 | Dolomitic Limestone/Dolomite | 210 | 1:1 | 40 | 3 | | ½ | | | |
| 16 | 1257 | 1230 | Dolomitic Limestone/Dolomite | 86 | 1:1 | 40 | 3 | 3 | | | | |
| 17 | 1257 | 1230 | Dolomitic Limestone/Dolomite | 200 | 1:1 | 40 | 3 | 3 | | | | |
| 18 | 1257 | 1230 | Dolomitic Limestone/Dolomite | 235 | 1 Perlite: 1 Sand: 1 Cement | | | | | | Gel-Gilsonite Flush | |
| 19 | 1276 | 1260 | Dolomitic Limestone/Dolomite | 115 | | | | | | | | Pal-Mix Flush |
| 20 | 1564 | 1535 | Dolomitic Limestone/Dolomite | 115 | | | | | | | | Pal-Mix Flush |
| 21 | 1735 | 1649 | Dolomitic Limestone/Dolomite | 104 | | | | 2 | | 1#/sk | 25#/sk Gilsonite | |

C.F.S.U. Well #31-33 Lost Circulation Cement Plug Comparison (Cont'd) -

| PLUG NO. | TOTAL DEPTH (FT) | OEDP DEPTH (FT) | FORMATION TYPE | S L U R R Y C O M P O S I T I O N | | | | | | | |
|----------|------------------|-----------------|----------------------------------|-----------------------------------|---------------|------------------|---------|-----------------------|-----------|---------|------------------------------|
| | | | | VOLUME (FT ³) | PERLITE RATIO | SILICA FLOUR (%) | GEL (%) | CaCl ₂ (%) | CFR-2 (%) | LCM (%) | OTHER |
| 22 | 1735 | 1229 | Dolomitic Limestone/ Dolomite | 104 | | | | 2 | | 1#/sk | 25#/sk Gilsonite |
| 23 | 1735 | 1610 | Dolomitic Limestone/ Dolomite | 104 | 1:1 | 40 | 3 | | ½ | | Pal-Mix Flush |
| 24 | 1735 | 1550 | Dolomitic Limestone/ Dolomite | 101 | 1:1 | 40 | 3 | | ½ | | Pal-Mix Flush |
| 25 | 1735 | 1580 | Dolomitic Limestone/ Dolomite | 145 | 1:1 | 40 | 3 | 2 | | | |
| 26 | 5009 | 4926 | Siltstone/ Sandstone | 112 | 1:1 | 40 | 3 | | ½ | | NaSi-CaCl ₂ Flush |
| 27 | 5009 | 4833 | Siltstone/ Sandstone | 125 | 1:1 | 40 | 3 | | ½ | | |

C.F.S.U. WELL #14-29 LOST CIRCULATION CEMENT PLUG COMPARISON

| PLUG NO. | TOTAL DEPTH (FT) | OEDP DEPTH (FT) | FORMATION TYPE | S L U R R Y C O M P O S I T I O N | | | | | | | |
|----------|------------------|-----------------|------------------------------|-----------------------------------|---------------|------------------|---------|-----------------------|-----------|---------|----------------------|
| | | | | VOLUME (FT ³) | PERLITE RATIO | SILICA FLOUR (%) | GEL (%) | CaCl ₂ (%) | CFR-2 (%) | LCM (%) | OTHER |
| 1 | 833 | 830 | Conglomerate | 265 | 1:1 | 40 | 3 | 2 | ½ | 5 | |
| 2 | 866 | 866 | Conglomerate | 265 | 1:1 | 40 | 3 | 2 | ½ | 5 | |
| 3 | 1249 | 935 | Limestone/Dolomite/Sandstone | 203 | | 20 | | 3 | | | 22% Kolite, 8% D53 |
| 4 | 1249 | 893 | Limestone/Dolomite/Sandstone | 203 | | 20 | | 3 | | | 22% Kolite, 8% D53 |
| 5 | 1249 | 872 | Limestone/Dolomite/Sandstone | 203 | | 20 | | 3 | | | 22% Kolite, 8% D53 |
| 6 | 1249 | 861 | Limestone/Dolomite/Sandstone | 201 | | 20 | | 3 | | | 22% Kolite, 8% D53 |
| 7 | 1330 | 1330 | Limestone/Dolomite/Sandstone | 187 | | | | 2 | | | 12% Kolite, 10% RFC |
| 8 | 1330 | 1295 | Limestone/Dolomite/Sandstone | 181 | | | | 2 | | | 12% Kolite, 10% RFC |
| 9 | 1330 | 1245 | Limestone/Dolomite/Sandstone | 181 | | | | 2 | | | 12% Kolite, 10% RFC |
| 10 | 1345 | 1344 | Limestone/Dolomite/Sandstone | 181 | | | | 2 | | | 12% Kolite, 10% RFC |
| 11 | 1345 | 1343 | Limestone/Dolomite/Sandstone | 248 | | | | 2 | | | 21% Kolite, 8% RFC |
| 12 | 1429 | 1429 | Limestone/Dolomite/Sandstone | 248 | | 20 | | 2 | | | 26% Kolite, 8% RFC |
| 13 | 2080 | 2070 | Limestone/Dolomite/Sandstone | 191 | | 20 | | 2 | | | 25% Kolite, 8.2% RFC |
| 14 | 2080 | 1885 | Limestone/Dolomite/Sandstone | 191 | | 20 | | 2 | | | 25% Kolite, 8.2% RFC |
| 15 | 2080 | 1698 | Limestone/Dolomite/Sandstone | 191 | | 20 | | 2 | | | 25% Kolite, 8.2% RFC |
| 16 | 2080 | 1490 | Limestone/Dolomite/Sandstone | 191 | | 20 | | 2 | | | 25% Kolite, 8.2% RFC |
| 17 | 2080 | 1543 | Limestone/Dolomite/Sandstone | 191 | | 20 | | 2 | | | 25% Kolite, 8.2% RFC |
| 18 | 2080 | 1466 | Limestone/Dolomite/Sandstone | 191 | | 20 | | 2 | | | 25% Kolite, 8.2% RFC |

COVE FORT SULPHURDALE UNIT

CORROSION SUMMARY

Oxygen corrosion at rates in excess of 40#/ft²/yr was experienced while drilling with aerated water in CFSU wells 42-7 and 31-33. During normal drilling with mud oxygen corrosion was effectively controlled by maintaining high pH with caustic and adding an oxygen scavenger, sodium sulfite, with cobalt as a catalyst. When severe lost circulation necessitated drilling with aerated water, oxygen corrosion was greatly accelerated.

After experimenting with a variety of inhibition programs in the field and laboratory, a sodium nitrite-caustic program proved to be the most effective. Laboratory tests with a water designed to duplicate drill water used on well CFSU 42-7 indicated that a sodium nitrite concentration of 2.6 #/bbl and a pH of 11.5 should provide an effective program. Corrosion rates were reduced from over 40#/ft²/yr to 8#/ft²/yr. Although this was a considerable improvement, corrosion rates were still well above the acceptable limit of 2#/ft²/yr.

Lack of success in reducing corrosion rates to acceptable levels using the sodium nitrite program was probably due to the following:

- 1) High concentrations of dissolved salts in the

drill water accelerated corrosion. (These concentrations varied from well to well.)

- 2) Upset conditions allowed concentrations of sodium nitrite and pH to fall below critical levels at times.
- 3) Reaction with drill cuttings, reaction with produced carbon dioxide, and dilution with produced formation water caused a reduction in pH.

Before introducing the sodium nitrite-caustic system, corrosion severely affected both casing and drill pipe. Casing caliper logs indicated casing corrosion. Drill pipe inspection downgraded 54% of the joints inspected in the CFSU well 42-7.

After introducing the sodium nitrite-caustic system on CFSU well 31-33, 14% of the joints inspected were downgraded. Chemical costs of \$68,000 using the sodium nitrite-caustic system on this well were at a breakeven point with the estimated savings in drill pipe damage. Potential casing damage and fishing jobs due to drill pipe failures were avoided making the chemical costs economical.

Although the sodium nitrite-caustic program did not reduce the corrosion rate to an acceptable limit, it appears to be the best practical chemical inhibition

CFSU/Corrosion Summary

system available. A variety of other corrosion control methods were considered and rejected during the drilling of the CFSU wells. Union is currently considering using nitrogen in place of air to eliminate the problem of oxygen corrosion. A new type of nitrogen generator may overcome some of the logistical and economic problems that have precluded the use of this method to date.

GEOLOGIC SUMMARY OF THE
COVE FORT-SULPHURDALE UNIT

The four geothermal exploration wells drilled by the Geothermal Division of Union Oil within the Cove Fort-Sulphurdale Unit area failed to establish the existence of a geothermal resource of sufficient temperature and productivity needed for electrical power utilization. The wells penetrated an underpressured, highly fractured, moderate to low temperature (178°C to 93°C), highly permeable geothermal reservoir consisting of contact metamorphic and sedimentary carbonate rock in a geologically complex area. The lack of production was due to the low temperature and low pressure which together with problems of toxic H₂S gas, lost circulation and fractured and unstable formations, lead to the abandonment of the project.

Figures 3 through 6 summarizes the geology of the four exploratory wells. Lost circulation and blind drilling has prevented the identification of parts of the geologic column.

Summary of the geochemical analyses which best represents the geothermal waters encountered is presented in the following table. Like the geology, the geochemical data is complex. The wide variety of water, ranging from 1320 ppm TDS to

Cove Fort-Sulphurdale Unit Geologic Summary

10,000 ppm TDS was unexpected in the highly permeable reservoir that was thought to be well mixed and geochemically similar throughout the prospect.

The four wells penetrated a variable thickness of surface volcanics of Mid-Tertiary age (200 to over 2000 feet) which lies, with angular unconformity, over highly faulted and folded Lower Mesozoic and Upper Paleozoic sedimentary rocks. Superimposed over a portion of this geologic framework is an aureole of contact metamorphism and mineralization related to a Mid-Tertiary intrusive event.

Static fluid levels in the wells are present between 1200 to 1400 feet below the surface. Very high temperature gradients (13 to 16°F/100 ft.) are present from the surface to the static water level of the reservoir. Below the top of the reservoir, the temperature profiles become nearly isothermal in the highly fractured and permeable geothermal reservoir. These isothermal sections are 300° to 310°F in the #42-7 well, 270° to 275°F in the #31-33 well, and 190° to 195°F (not stable) in the #14-29 well. The maximum temperature measured in the prospect was 353.5°F at 7320 feet in the #42-7 well. The area around the #42-7 well appears to be near the source of the geothermal anomaly, as defined by the deep drilling. The rapid termination of the shallow well temperature anomaly east, south and

Cove Fort-Sulphurdale Unit Geologic Summary

and west of the #42-7 well leave little room for the presence of higher reservoir temperatures, considering the highly convective nature of the reservoir. Therefore, the geothermal anomaly has been evaluated and the reservoir judged to be inadequate for development.

| <u>WELL #</u> | <u>#42-7</u> | <u>#42-7</u> | <u>#31-33</u> | <u>#31-33</u> | <u>#14-29</u> |
|-------------------------------|--------------|--------------|---------------|---------------|---------------|
| pH | 9.98 | 9.54 | 9.79 | 7.44 | 7.41 |
| TDS | 9405 | 4775 | 10,000 | 1320 | 4776 |
| Alkalinity as CO ₃ | 2380 | 470 | 1440 | 200 | 158 |
| Na | 3460 | 1310 | 4000 | 355 | 1220 |
| K | 225 | 585 | 443 | 56.2 | 41.5 |
| Ca | 26.4 | 32.0 | 14.4 | 74.4 | 332 |
| Cl | 2450 | 1820 | 3900 | 502 | 2060 |
| SO ₄ | 1280 | 560 | 760 | 187 | 900 |
| F | 4.7 | 2.3 | 3.6 | 1.03 | 2.5 |
| SiO ₂ | 180 | 170 | 79 | 64.5 | 92 |
| Mg | 12.0 | 4.8 | 3.36 | 19.2 | 115.2 |
| Li | - - | - - | 13.31 | 1.16 | 265 |
| HCO ₃ | 1322 | 265.9 | 658.8 | 244 | 192.8 |
| CO ₃ | - - | 252 | 540 | 0 | 0 |
| B | 0.8 | 0.30 | 0.5 | 0.2 | 6.4 |
| As | 6.08 | 2.88 | 5.71 | 2.99 | 0.75 |
| Cu | 0.324 | 0.271 | 0.166 | 0.914 | 0.010 |
| Pb | - - | 0.022 | 0.420 | 0.006 | 0.005 |
| Ni | 0.493 | 0.007 | 0.975 | - - | 0.085 |
| Ag | 0.015 | 0.011 | 0.037 | - - | - - |
| Zn | 0.075 | 1.811 | 0.041 | 0.104 | 0.350 |

GEOCHEMISTRY OF FORMATION WATERS ENCOUNTERED IN THE COVE FORT-SULPHURDALE
UNIT AREA

**Generalized Lithologic Log
Well Forminco *1**

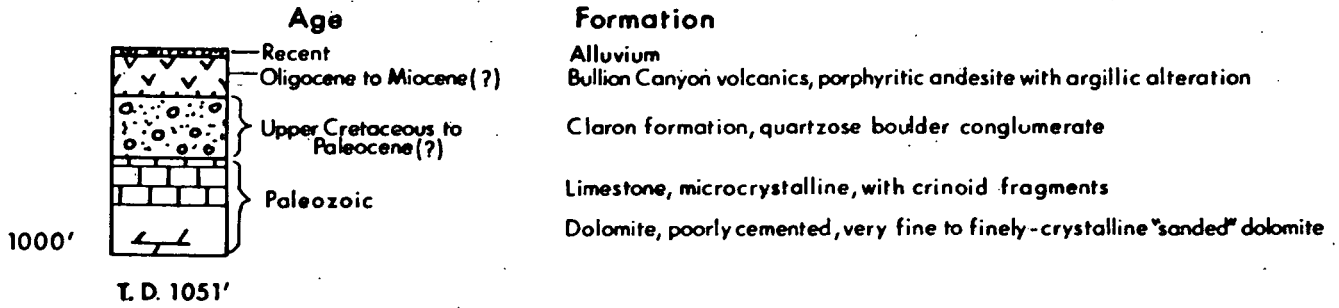


FIGURE 3

**Generalized Lithologic Log
Well *42-7**

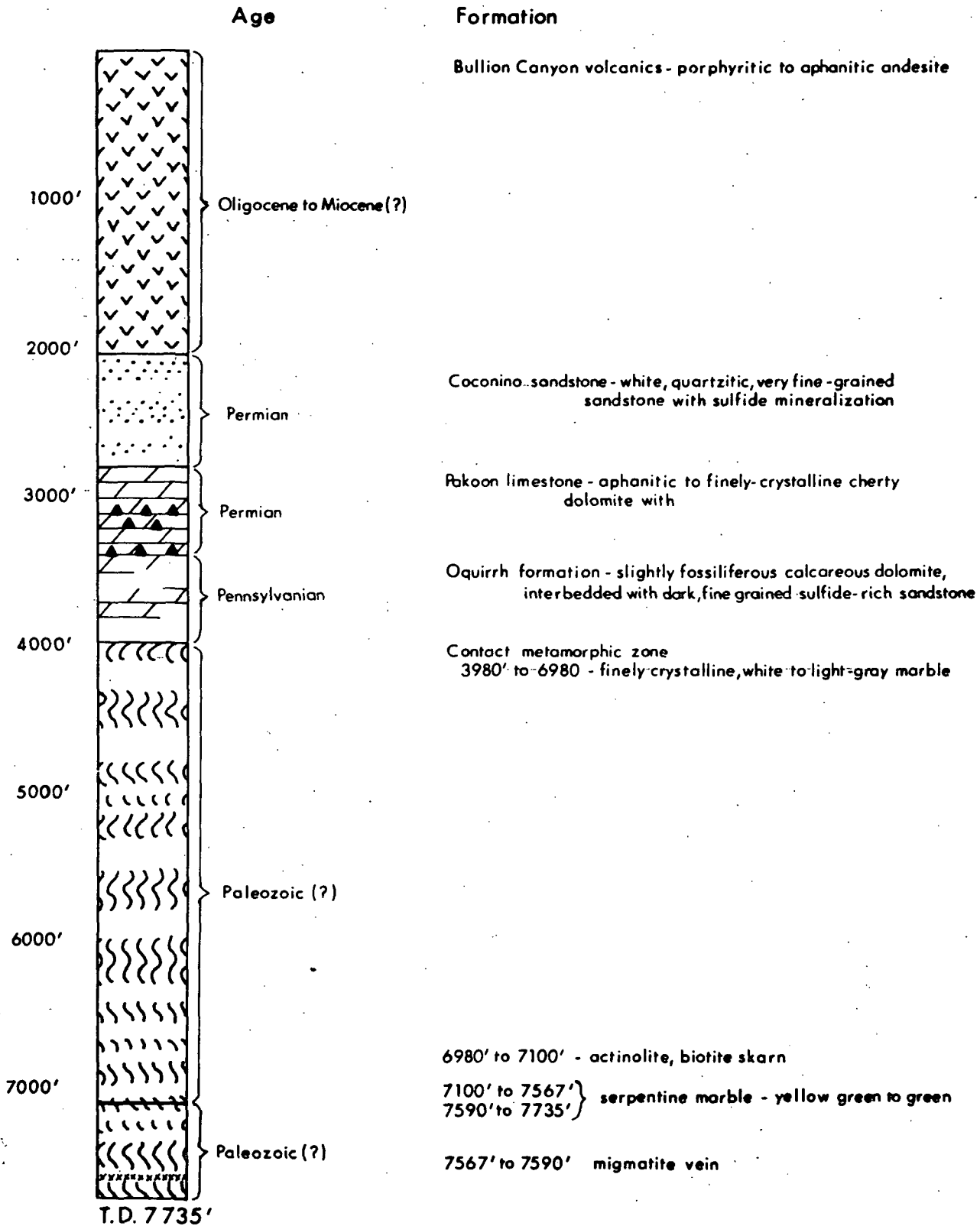


FIGURE 4

**Generalized Lithologic Log
Well #31-33**

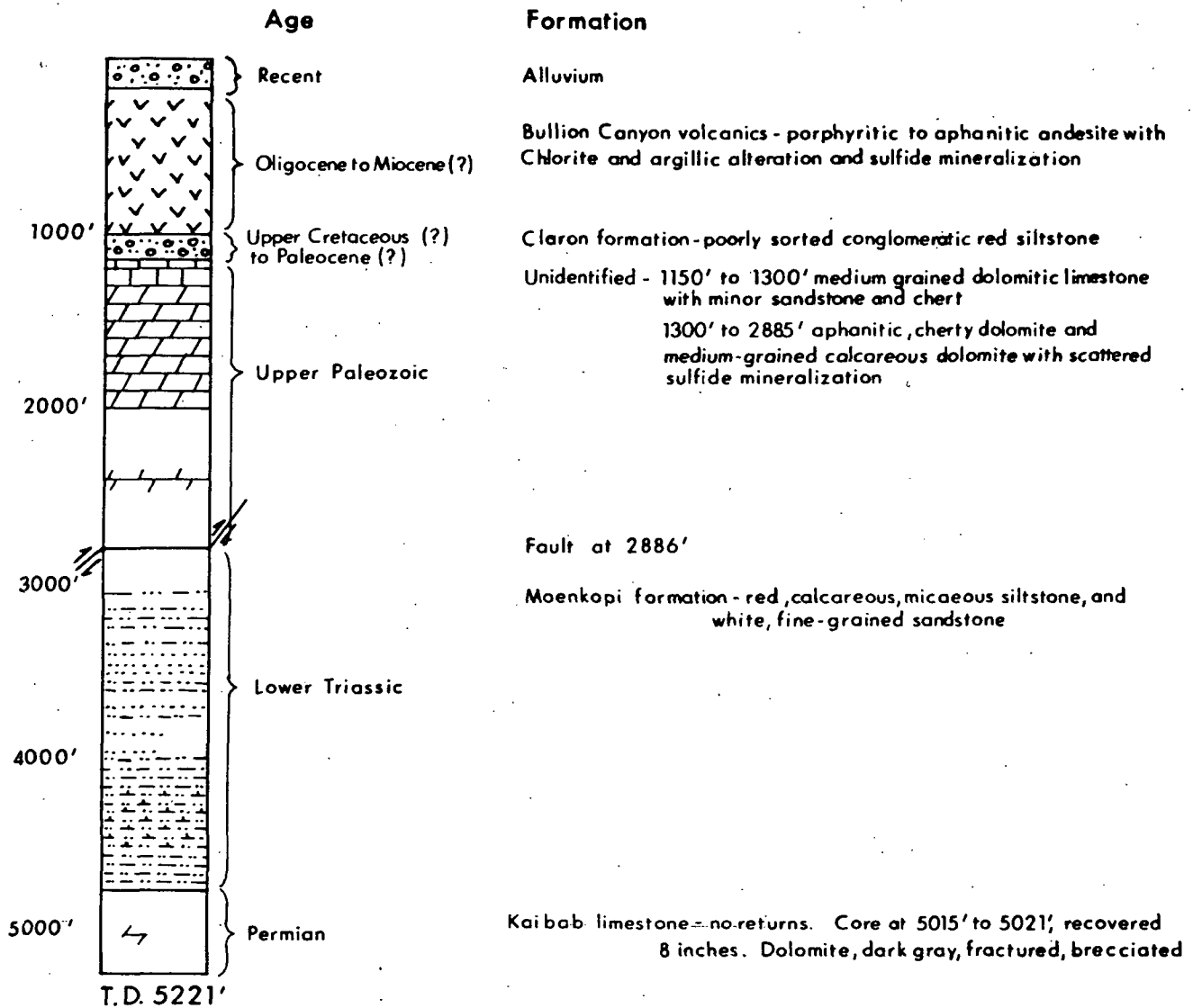


FIGURE 5

DOWNHOLE LOGGING TABLES

The following tables summarize downhole logging runs in the CFSU wells. Logs will be available from:

Rocky Mountain Well Log Service

P.O. Box 3150

Denver, Colorado 80201

(303) 825-2181

COVE FORT-SULPHURDALE #42-7

SCHLUMBERGER
LOGGING DATA

| <u>DATE</u> | <u>TYPE OF LOG RUN</u> | <u>LOGGED INTERVAL</u> | <u>TOTAL DEPTH</u> |
|-------------|--|------------------------|--------------------|
| 1 Feb. 78 | Dual Induction-Laterolog with linear correlating log; SP | 1520' - 3444' | 3447' |
| 1 Feb. 78 | Compensated Neutron Log; GR | 50' - 3428' | 3445' |
| 1 Feb. 78 | Temperature Log | 1320' - 3447' | 3447' |
| 4 Feb. 78 | Cement Bond Log | 162' - 3314' | 3323' |
| 4 Feb. 78 | Temperature Log | 0' - 3058' | 3065' |
| 28 Feb. 78 | Dual Induction-Laterolog with linear correlation log; SP | 3358' - 7692' | 7695' |
| 28 Feb. 78 | Borehole Compensated Sonic Log; GR | 3358' - 7674' | 7681' |
| 28 Feb. 78 | Compensated Neutron-Formation Density with GR, Caliper | 3358' - 7679' | 7680' |
| 28 Feb. 78 | Temperature Log | 300' - 7550' | 7680' |
| 1 Mar. 78 | Four-arm continuous Dipmeter | 3358' - 6003' | 6004' |

"GO-INTERNATIONAL"
LOGGING DATA

| | | | |
|------------|-----------------|---------------|-------|
| 26 Feb. 78 | Temperature Log | 3450' - 7327' | 7332' |
| 26 Feb. 78 | Temperature Log | 300' - 7327' | 7332' |
| 27 Feb. 78 | Temperature Log | 300' - 7327' | 7332' |
| 27 Feb. 78 | Temperature Log | 1200' - 7320' | 7332' |

COVE FORT - SULPHURDALE #31-33

LOGGING DATA

| <u>DATE</u> | <u>TYPE OF LOG RUN</u> | <u>LOGGED INTERVAL</u> | <u>TOTAL DEPTH</u> |
|---------------|--|------------------------|--------------------|
| | <u>Schlumberger</u> | | |
| 7/18/78 | Temperature Log (malfunction suspected) [two maximum reading thermometers run simultaneously] | 0' - 4858' | 4858' |
| | Dipmeter and Four Arm Caliper [three maximum reading thermometers run simultaneously] | 5207' - 1735' | 5207' |
| 7/19/78 | Dual Induction - Laterolog [three maximum reading thermometers run simultaneously] | 5207' - 1735' | 5207' |
| | Compensated Neutron - Formation Density [three maximum reading thermometers run simultaneously] | 5206' - 1735' | 5206' |
| | Temperature Log | 0' - 4858' | 4858' |
| | <u>Geotex</u> | | |
| 7/19/78 | Temperature, Spinner and Water Aquifer Log | 0' - 4858' | 4858' |
| | Radioactive Tracer and Spinner Log | 0' - 4858' | 4858' |
| | <u>R. F. Smith Corporation</u> | | |
| 5/24/78 to | Geothermal Data Log (includes engineering data related to drilling, geological, and other data) | 52' - 5221' | 5221' |
| 7/24/78 | | | |

COVE FORT-SULPHURDALE UNIT #14-29

LOGGING DATA

| <u>DATE</u> | <u>TYPE OF LOG RUN</u> | <u>TOTAL DEPTH</u> | <u>LOGGED INTERVAL</u> | <u>MAXIMUM READING THERMOMETERS</u> | <u>HOURS SINCE FLUID INJECTION</u> |
|-------------|---------------------------------------|--------------------|------------------------|-------------------------------------|------------------------------------|
| | <u>SCHLUMBERGER</u> | | | | |
| 6/27/79 | Dual Induction-Laterolog 8 | 2080' | 2080'-1240' | 121°F | 2-1/2 |
| | Formation Density-Compensated Neutron | 2080' | 2080'-1240' | 127°F | 3-1/2 |
| | Dipmeter and Four Arm Caliper | 2080' | 2080'-1240' | 134°F | 5-1/2 |
| 7/07/79 | Temperature Log | 2620' | 2452'-220' | 186°F | 4-1/2 |
| | Dual Induction-Laterolog 8 | 2620' | 2462'-2078' | 185°F | 6-1/2 |
| | Formation Density-Compensated Neutron | 2620' | 2468'-2078' | 194°F | 7-3/4 |
| | Dipmeter and Four Arm Caliper | 2620' | 2469'-2078' | 198°F | 9-1/4 |
| | Temperature Log | 2620' | 2464'-220' | 198°F | 2 |

RESERVOIR ANALYSIS

The reservoir analysis of Cove Fort-Sulphurdale Unit is based on the following tests:

1. Well #42-7: Flow test, injection test, temperature surveys, pressure surveys, and spinner surveys.
2. Well #31-33: Temperature and pressure surveys.

The important reservoir characteristics of the Cove Fort-Sulphurdale-reservoir are that it is (1) a low temperature, and (2) a low pressure system. Reservoir permeability-thickness product is about 23,000 md-ft.

The wells will make poor producers because of the low pressure. The pressure at 5,000 ft. datum is about 1540 psi which is less than the hydrostatic head of fresh water. The free water surface in the wells is about 1500 ft. below the wellhead.

Well #42-7 produced at a rate of 47,000 lbs/hr at 3 psig wellhead pressure and 200°F± wellhead temperature.

Low temperature resource also reduces the flow rates of the wells. At high temperatures, a larger fraction of the fluid will vaporize in the well-bore thus reducing the bottomhole flowing pressure and increasing the flow from the reservoir.

CFSU/Reservoir Analysis

Permeability of the reservoir is fairly high. We calculated a kH product of around 23,000 md-ft. from the production/injection tests. High permeability and low pressure make these wells good injectors. The wells are capable of taking 1,000,000 lbs/hr at 0 psig wellhead pressure.

Based on the current economics, the resource discovered in the Cove Fort-Sulphurdale Unit is sub-commercial.