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PRELIMINARY GEOLOGY AND GEOTHERMAL RESOURCE POTENTIAL OF THE BELKNAP-FOLEY AREA, OREGON

by

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upon further verification.

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INTRODUCTION

The Belknap-Foley area is located in the central Western Cascade Range of Oregon, approximately 80 km (50 mi) east of Eugene (Figure 1). Limits of the study area were arbitrarily assigned by U.S. Geological Survey (USGS) topographic map limits and natural breaks in the geology and topography (Plate I). This study, performed under U.S. Department of Energy (USDOE) Contract No. DE FC07-79ET27220, was undertaken to estimate the geothermal potential of the area by using various methods including compilation of existing data, reconnaissance geologic mapping, lineament analysis, well and spring geochemistry, and accrual of geothermal-gradient data.

Geographically, the study area is located in the rugged mountains surrounding the valley of the McKenzie River, which bisects the area in an eastwest direction. Total relief is approximately 1,000 m (3,300 ft) in the mountainous areas and approximately 30 m (100 ft) in the river valley.

GEOLOGY

Introduction

The Belknap-Foley area is located at the eastern boundary of the Western Cascades geologic province in the Western Cascades-High Cascades transition zone. Quaternary and late Tertiary lavas and minor tuffs of the High Cascades province are in steep depositional contact with older Western Cascades rocks along this boundary, which appears to be the western margin of a major northsouth-trending High Cascades graben (Allen, 1966; Taylor, 1978, 1980). Because a number of thermal springs and preexisting gradient holes with high values are located along the margin of this graben, much of the mapping effort of this study was directed at carefully defining the nature of the High Cascades-Western Cascades geologic boundary.

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Figure 1: Map showing location of study area.

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The geology and all K/Ar radiometric ages (Table 1) are presented on the accompanying reconnaissance geologic map (Plate I), which was produced during the summer and fall of 1979 and 1980. Areal extent of geologic units was based on mapping and hand-specimen identification of rocks. Data were plotted on USGS topographic maps without the aid of aerial photographs.

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Volcanic stratigraphy

From middle Tértiary to Quaternary time, volcanism in the area changed from silicic pyroclastic activity to eruption of increasingly mafic magmas (Table 2). This change in composition was reflected in higher percentages of lavas relative to tuffs. The oldest mappable unit (unit Tov on the geologic map) is composed of epiclastic volcanic sedimentary rocks, lithic-fragmentrich laharic dacite tuffs, and minor mafic lava flows. These rocks are probably Oligocene to early Miocene in age (Peck and others, 1964). In the Blue River mining district, the Oligocene rocks are locally intruded by Miocene quartzbearing dioritic stocks (unit *Imd*). The Miocene sequence (unit *Imv*) is dominated by highly phyric lavas, autobreccias, and mudflows with two-pyroxene andesite clasts, although lesser volumes of ash-flow, air-fall, and epiclastic tuffs as well as some basaltic flows occur locally. Several Miocene volcanic plugs and plug domes (unit *Imvi*) occur in the western part of the area, and basaltic to andesitic feeder dikes (unit *Imud*) occur in the Blue River valley. The oldest dated rock assigned to the Miocene volcanic sequence in the map area is 19.91+1.94 m.y. old (McBirney and others, 1974). The youngest dated Imv sample is 6.2+0.2 m.y. old (Laursen and Hammond, 1978). The Miocene rocks are overlain by diktytaxitic to compact basaltic to basaltic-andesitic lavas and one small ash flow which cap most of the high ridges in the western part of the area. These Pliocene volcanic rocks (unit Tpv) have a maximum K/Ar age of 8.39+0.36 m.v. (unpublished University of Utah Research Institute (UURI) -K/Ar data, Evans and Foley, analysts) and a minimum age of 3.88+0.06 m.y.

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Table l.

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Radiometric (K/Ar) ages for selected rocks of the Belknap-Foley area

Sample no.*	Location	Rock type	Age**	Stratigraphic unit
MS-254	122 ⁰ 07'30" 44 ⁰ 14'10"	Basalt	^w 19.91 <u>+</u> 1.94 m.y.	Tmv
MS-253	122 ⁰ 12'40" 44 ⁰ 12'45"	Andesite	^w 8.46 <u>+</u> 0.11 m.y.	.Tmv
MS-130	122 ⁰ 06'07" 44 ⁰ 13'10"	Basalt	^w 6.2 <u>+</u> 0.2 m.y.	Tmv
MS-17	122 ⁰ 02'00" 44 ⁰ 12'13"	Andesite	^W 6.2 <u>+</u> 0.2 m.y.	Tmv
A-20	122 ⁰ 02'38" 44 ⁰ 16'39"	Basaltic andesite Ash-flow tuff	^w 5.3+0.2 m.y.	Три
MŞ-205	122 ⁰ 02'55" 44 ⁰ 09'30"	Basaltic andesite	^W 5.06 <u>+</u> 0.06 m.y.	QTv
MS-208	122 ⁰ 06'30" 44 ⁰ 13'00"	Basaltic andesite	^W 3.88+0.06 m.y.	Три
MS-132 MS-110	122 ⁰ 00'50" 44 ⁰ 11'46"	Olivine basalt	^W 2.6+6.2 m.y. ^W 2.1 <u>+</u> 0.1 m.y.	QTv
A-77	122 ⁰ 00'48" 44 ⁰ 17'00"	Basaltic andesite	^w 0.68 <u>+</u> 0.04 m.y.	QTv
U-Cougar	122 ⁰ 14'10" 44 ⁰ 07'46"	Basaltic andesite	^p 16.3 <u>+</u> 1.8 m.y.	Tmvi
U-RI-112	122 ⁰ 16'59" 44 ⁰ 06'30"	Andesite	^p 11.5 <u>+</u> 0.5 m.y.	Tmv
U-RI-85	122 ⁰ 16'10" 44 ⁰ 07'41"	Dacitic ash-flow tuff	^p 13.9 <u>+</u> 0.8 m.y.	Tmv
U-Foley	122 ⁰ 10'29" 44 ⁰ 10'49"	Basalt	^w 2.05 <u>+</u> 0.52 m.y.	QTv
U-Tnw-Top	122 ⁰ 11'49" 44 ⁰ 12'11"	Andesite	^w 8.93 <u>+</u> 0.34 m.y.	Tmν
U-Tpb	122 ⁰ 11'31" 44 ⁰ 12'32"	Basaltic andesite	^W 8.39 <u>+</u> 0.36 m.y.	Трv
U-BF-5	122 ⁰ 12'30" 44 ⁰ 08'45"	Dacite	^w 9.31 <u>+</u> 0.44 m.y.	Tmdc

* References: MS - McBirney and others, 1974; A - Armstrong and others, 1975; U - Unpublished K/Ar data, University of Utah Research Institute, Stanley Evans and Duncan Foley, analysts.

** w = whole rock date; p = plagioclase date.

Table 2. Bulk chemical composition of selected rocks of Belknap-Foley area. (Letters at top of each column indicate sample number and map symbol for stratigraphic unit. All values are in weight percent.)

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Comp nent	o- *T-6 <u>Qbh</u>	J-2 Qtv	J-4 <u>Qtv</u>	J-3 Qtv	S-13 ?	S-16 Tmv	P-7 <u>Tmv</u> ?
SiO,	47.0	47.8	48.38	49.80	53.00	53.0	54.25
Ti0,	··· _	1.63	2.19	1.68	1.10	1.20	1.28
A120	3 -	15.42	15.47	15.42	18.30	18.80	16.46
Fe ₂ 0		1.70	1.83	2.20		0.00	3.08
Fe0	-	9.54	10.36	9.08	_7.80	8.20	5.92
Mno	- -	0.21	0.20	0.21	_	-	0.13
Mg0	- -	4.43	5.80	4.17	5.20	5.90	4.46
Ca0	-	10.20	8.21	9.88	8.80	9.30	8.79
Na ₂ 0	-	3.50	3.60	3.90	3.80	3.10	3.46
K20	-	1.30	0.64	1.25	0.40	0.25	0.80
P_05	-	0.02	0.43	0.15	-	-	0.23
H ₂ 0		1.36	1.39	0.86			1.58
2	Total 47.0	97.11	98.50	98.60	98.40	99.75	100.44
	S-15 	S-14 _Tmv?	S-9 <u>Tmv</u>	S-12 	S-9 . <u>Tmv</u>	S-10 ?	S-17
Si0,	54.30	54.70	55.80	57.20	58.00	60.90	61.20
Ti02	1.10	1.10	1.10	0.95	1.00	1.10	1.55
A120	3 18.80	17.80	18.50	18.20	16.40	17.40	15.20
F ₂ 03 Fe0	-7.80	8.0	7.5	7.00	9.6	6.80	8.1
Mn0	. –		-	-	-		· -
Mg0	5.20	5.90	4.40	4.20	5.90	2.00	2.50
CaO	8.80	8.50	6.60	8.20	4.90	4.80	4.50
Na ₂ 0	3.00	3.90	4.20	3.50	2.80	4.30	4.30
К ₂ 0.	0.15	0.25	1.70	0.40	0.35	1.20	2.00
P2 ⁰ 5	. – .	-	-'	-	· · ·	-	
H ₂ 0			` 			••••••••••••••••••••••••••••••••••••••	<u> </u>
	Total 99.15	100.15	99.80	99.65	98.95	98.50	99.17

*References: P-from Peck, 1964; J-from Jan, 1967; T-from Taylor, 1967; S-from Storch, 1978. - 5 - (Sutter, 1978). The above units occur principally in the Western Cascades province, in the western part of the map (Plate I).

The eastern part of the study area is completely dominated by compact to diktytaxitic basaltic lavas of Quaternary age (units *QTv* and *Qbh* on Plate I). These rocks appear to partially fill in the High Cascade graben described by Allen (1966) and Taylor (1978, 1980). Foley Ridge is a tongue of these Quaternary lavas which filled an east-west-trending canyon cut across the western scarp of the graben about 2.0 m.y. ago (unpublished K/Ar age of 2.05+0.52 m.y. by UURI, Evans and Duncan, analysts).

For this study, the Quaternary lavas were split into two units based on lithology and stratigraphic relationships. Lavas assigned to unit QTv(Pliocene to Pleistocene basalts of the High Cascades) occupy topographic depressions which are clearly related to the present geomorphic setting. Nearly identical rocks located at high elevations of the Western Cascades were assigned to unit T_{Pv} because they occupied topography strongly reversed from the present landscape. K/Ar data, where available, tend to support this division. The Qbh unit (Pleistocene to Holocene basalts of the High Cascades) was identified by extreme freshness of the rock, presence of uneroded tumuli and flow structures on flow tops, obvious control by very youthful drainages, and position above various Quaternary units.

K/Ar dates of samples from units QTv and Qbh are sparse and of relatively low precision and accuracy, but enough are available to provide some age control. Poor precision and accuracy is caused by the relatively low content of K₂O and youthful age of these lavas, which cause very low percentages of radiogenic argon relative to atmospheric argon. The oldest K/Ar date in the area- 2.6 ± 0.2 m.y. -- is for unit QTv (Laurson and Hammond, 1978); the youngest age is 2.05 ± 0.52 m.y. (UURI date previously cited). A single K/Ar date of

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 0.68 ± 0.05 m.y. was obtained from lavas mapped as unit *Qbh* (Laursen and Hammond, 1978).

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Structural geology

Faults are concentrated in two major north-south-trending zones along Cougar Reservoir and along Horse Creek-McKenzie River. Both zones have en echelon north- to northwest-trending normal faults with significant dip-slip offsets down to the east. The lineament map (Figure 2) shows additional northeasterly trends along the northern margin of the area.

The Horse Creek-McKenzie River fault zone appears to define the western margin of a major north-south-trending graben which has been partially filled by a shield-like platform of late Pliocene and Quaternary High Cascades basaltic lavas and lesser andesitic ejecta (Allen, 1966; Taylor, 1978, 1980). The youngest dated unit with significant offset on the High Cascades graben margin is a 3.88-m.y.-old basaltic andesite (unit T_{PV}) on Frissel Point (Sutter, 1978), along the north fork of the McKenzie River. The capping lavas (unit T_{PV}) west of the north fork of the McKenzie River (Plate I) have been dropped down about 900 m (3,000 ft) to the east along a series of north- to northwest-trending en echelon step faults, but the total structural relief on the graben could be much more than this (Taylor, 1980, personal communication). Only minor offsets appear to affect the Quaternary lavas (Plate I).

The Cougar Reservoir fault zone trend is parallel to the High Cascades graben margin and appears to have a similar sense of movement, with Miocene and Oligocene volcanic rocks appearing to be displaced down toward the east across the zone. Miocene volcanic rocks (unit *Imv*) are the youngest units with proven offset in this zone.

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Relation of structures to geothermal systems

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The distribution of hot springs in the area is related to the two major north-south-trending fault zones discussed previously. Terwilliger Hot Springs and Cougar Hot Springs are located along the Cougar Reservoir lineament, while Belknap, Foley, and Bigelow Hot Springs are located along the western margin of the High Cascade graben. Hot-spring orifices do not, in general, issue from fault zones but from joints in lavas near the faults.

Three hypotheses might explain the apparent relation of faults to hot springs:

Faults actively control location of hot springs by serving as conduits for circulation of thermal waters.

Faults serve as passive controls on the location of hot springs by creating major topographic lows which may fortuitously tap sporadic thermal aquifers.

3. Some combination of hypotheses one and two controls the distribution of hot springs.

It is difficult to imagine that fault zones as large as those described here could have no influence on circulation of thermal waters. This is particularly true of the western margin of the High Cascade graben, where the faults are quite young and rocks of different lithology are juxtaposed across the faults. It is also true, however, that hot springs are more likely to issue from topographic lows created by fault-shatter zones, so that hypothesis three above is probably the most logical explanation for control of the hot springs.

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GEOPHYSICS

Two geophysical studies were available for evaluation for this report. The first was a regional aeromagnetic study (Figure 3) performed by the Oregon State University Geophysics Group. This study, which is discussed in detail by Couch (1978) and Connard (1980), seems, in general, to show a close correspondence between magnetic maxima and topographic highs in the Belknap-Foley area. This is due to the fact that the Pliocene and Pleistocene units found capping the ridges tend to have a higher proportion of magnetically susceptible lavas than the older, underlying Miocene and Oligocene rocks.

Site-specific interpretations of the aeromagnetic data for the study area are not obvious. However, regional interpretation by Couch (1978) and Connard (1980) indicates a possible fault with east side down that is located in the approximate location of the Western Cascade-High Cascade transition zone fault mapped for this report (see section on geology) and that strikes in approximately the same trend. They also interpret the depth to the Curie point isotherm (temperature below which a material ceases to be paramagnetic; $\sim 600^{\circ}$ C) to be greater on the west side of the fault than on the east side of the fault. This prediction matches well with Blackwell and others (1978), whose thermal model of the Cascades estimates a similar depth to the 600° C isotherm.

The second geophysical study in this report is a regional gravity survey also performed by the Oregon State University Geophysics Group (Couch, 1978; Pitts, 1979). Their survey consists of a complete Bouguer gravity anomaly map (Figure 4) and a residual anomaly map (Figure 5), both of which are discussed in detail by Couch (1978) and Pitts (1979). The main feature of both these maps is the steep gravity gradient coincident with the High Cascades-Western Cascades transition zone and the location of local thermal

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SALEM, OREGON

1960 REVISED 1977 _____CONTOUR INTERVAL 200 FEET

FIGURE 3. TOTAL FIELD AEROMAGNETIC ANOMALY MAP OF

BELKNAP-FOLEY AREA

(From Connard, 1980) Contour interval 50 gammas

I.G.R.F. 1975 Data reference elevation 9,000 ft Cutoff wavelength 15 km

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springs. Pitts (1979) interprets this anomaly to represent either a large graben-bounding fault zone with east side down, an area of shallow silicic intrusives, or a possible combination of both. Detailed geologic mapping and possibly deep drilling are needed to further refine geologic modeling based on the foregoing geophysical studies.

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WATER CHEMISTRY

During this study, analyses were compiled of four of the five major thermal springs together with analyses of drill-hole waters in the Belknap-Foley area (Table 3). These data indicate that the thermal waters are generally an alkaline, sodium-chloride-rich carbonate water diagnostic of a hotwater-dominated system at depth with elevated reservoir temperatures (Table 4) calculated by methods presented in Appendix A. Preliminary evaluation of the available data indicates the springs may be placed in two groups. The first are the Bigelow, Belknap, and Foley springs, which show similar amounts of silica (60-110 mg/1), Na:K atomic ratios (54.1-78.5), and calculated minimum reservoir temperatures. Other similarities are seen by comparison of relative amounts of ions such as boron, fluoride, and chloride. The second group are those to the west including the Terwilliger spring cluster, Rider Creek and Walker Creek drill-hole waters. (Table 3), and possibly the Cougar Reservoir spring, for which no analyses are available. These springs exhibit lower silica (14-50 mg/l), higher Na:K atomic ratios (80-107), lower amounts of chloride and lithium and higher amounts of sulfate ion, and lower calculated reservoir temperatures (Table 4).

Preliminary data are inconclusive at this point; however, the water group near Cougar Reservoir may represent either a dilute species of the springs to the east or a totally different species. Extensive sampling of thermal spring gases and local cold springs and analyses of all waters for isotopes is needed before a definitive study of the thermal regime can be made.

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Table 3. Spring and well chemistry of the Belknap-Foley area. All measurements are in mg/l, except for pH or as indicated. nt = not tested; tr = trace.

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· · · · · · · · · · · · · · · · · · ·	Belknap Springs	Belknap Springs	Belknap Springs	Belknap Springs (main)	Belknap Springs (east)
Location	16S/6E/11A	16S/6E/11A	16S/6E/11A	16S/6E/11A	165/6E/11A
Date sampled	'03	'72	3/76	3/76	3/76
Temp. (^O C)	86.7	71	nt	89.0	66.0
рӉ	nt	7.62	nt	7.6	· 7.5 [±]
Conductance µmhos/cm	nt	4300	nt	3900	3720
Alkalinity X _h as mg/l HCO ₃ X _c as mg/l CaCO ₃	nt	nt	nt	14 _c	16 _c
Hardness as mg/l CaCO ₃	nt	nt	nt	541	544
Total dissolved solids	2506	nt	2550	2491	2377
sio ₂	81	96	110	79.9	70.6
Na	364	69 0	630	525	490
К	69.0	15.0	17.0	16.8	15.2
Ca	455	210	210	208	198
Mg	13	0.2	0.29	0.3	0.4.
C1	1343	1300	1550	1195	1036
As	nt	0.35	nt	0.24	0.24
В	nt	6.4	3.6	7.6	7.1
Li	nt	0.95	1.3	1.04	0.95
F 84	nt	1.2	0.88	1.11	0.98
Fe (total)	nt	0.02	tr	0.1	0.1
A1	nt	nt	0.1	tr	tr
HCO ₃	nt	17	nt	17	19
PO ₄	nt	0.21	nt	0.27	0.41
SO _A	168	170	150	105	85
NO3	nt	nt	' nt	tr	0.08
NH ₃	nt	nt	nt	0.19	0.15

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Table 3. Spring and well chemistry of the Belknap-Foley area--Continued All measurements are in mg/l, except for pH or as indicated. nt = not tested; tr = trace.

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	Foley Springs	Bigelow Spring	Terwilliger Springs (upper)	Terwilliger Springs <u>(lower)</u>	Terwilliger Springs <u>(upper)</u>
Location	16S/6E/11A	15S/6E/26Ba	17S/5E/20Bb	17S/5E/20Bb	17S/5E/20Bb
Date sampled	3/76	3/76	'73	3/76	3/76
Temp. (^O C)	80.6	61.0	44.0	38.0	42.0
рН	8.0	7.8	7.7	8.4	8.2
Conductance µmhos/cm	4800	3800	2980	2830	2660
Alkalinity X _h as mg/l HCO ₃ X _c as mg/l CaCO ₃	13 _c	18 _c	nt	15 _c	15 _c
Hardness as mg/1 CACO ₃	1284	459	nt	557	484
Total dissolved solids	3333	2566	nt	1892	1763
sio ₂	60	69	50	46	47
Na	475	540	392	335	320
К	11	17	6.3	7.3	6.8
Cà	494	188	225	210	196
Mg	0.8	1	0.1	0.2	0.2
C1	1304	1148	788	769	693
As	0.21	0.11	nt	0.1	0.1
В	10.0	6.5	5.1	6.4	6.2
Li	0.96	1.1	0.52	0.7	0.64
F	0.81	1.4	0.8	0.86	0.87
Fe (total)	tr	0.1	tr	0.1	0.1
A1	tr	tr	nt	tr	tr
HCO3.	nt	nt	19	nt	nt
PO4	0.06	0.32	nt	0.08	0.08
so ₄	550	102	260	192	185
NO ₃	tr	0.02	nt	0.01	tr
NH ₃	0.15	0.39	nt	0.04	0.12
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Table 3.Spring and well chemistry of the Belknap-Foley area--Continued. All measurements are in mg/l, except for pH or as indicated. nt = not tested; tr = trace.

	Contraction of the second		2	i e	i r
•	Well or spring	Rider Creek Drill Hole		Walker Drill	Creek Hole
	location	175/5E/20 Baa	• . •	175/5F	/8Acd
	Date Sampled	7/80		7/80	/ 0/104
en e	Temp ⁰ C	18.5		15	`
	Pemp: 0	7,77		7.37	
•	Conductance, umhos/cm	3400 ga	· • •	810	L
18 - 84 19 - 8 19 - 9	Alkalinity Xh as mg/l HCO ₃	i i nt	e' .	nt	÷
	Xc as mg/l CaCO ₃	nt		nt	
:	Hardness as mg/1 CaCO ₃	427.5		68.4	a ^t h
•	Total dissolved solids mg/l	1962		nt	
	Si0,	14(?)	• •	18(?)	•*.
	Na	449		149	
	K	< 2.50		< 2.50	· .
; , ;	Ca	271		26	• 1
ena e fisi	Mg	0.500		1	
	ĊĨ	925	,	135	
ж _а	As	< 0.625		< 0.625	
fattur i ev	В	7.5		4.2	
	Li	0.49		< 0.050	
	F	0.9	•	0.2	
	FE (total)	0.12		0.29	
	A1	< 0.625		< 0.625	
ut .	HCO3	nt	۰.ť	nt	'
i	PO	nt		nt	
	SO ₄	269		nt	
	NO ₂	nt '		nt	
1997 B	, NH _A ite seint, rit	< 0.1		0.6	
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Table 4. Geothermetric calculations* of minimum reservoir temperatures for selected thermal waters of the Belknap-Foley area

	Belknap Springs	Belknap Springs	Belknap Springs	Belknap Springs (Main)	Belknap Springs (East)	Terwilliger Springs (Lower)	Terwillige Springs (Upper)	er
Flow rate liters/min.	284	300	~250	~250	~250	114	200	· ·
Measured temperature ^O C.	86.7	71	NT	89	66	38	44	
Na:K O _C	226	87	97	107	104	87	74	
Na:K:Ca 1/3 β ^Φ C	202	113	121	125	125	104	95	
Na:K:Ca 4/3 β ^O C	110	82	85	83	83	52	48	
Na:K:Ca Mg corrected ^O C	183	NC	NC	NC	NC	NC	NC	
SiO ₂ conductive	126	135	143	124	119	99	102	
SiO ₂ adiabatic ^O C	123	131	137	122	117	100	103	•
SiO ₂ chalcedony ^O C	98	108	116	97	90	68	72	
SiO ₂ opal ^O C	7	15	23	179	164	-17	-14	
						•	•	

*Methodology for calculations presented in Appendix A. NC = not calculated.

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Table 4. Geothermetric calculations* of minimum reservoir temperatures for selected thermal waters of the Belknap-Foley area -- Continued

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• •	Terwilliger Springs (Upper)	Bigelow Spring	Foley Spring	Ryder Creek Drill Hole	Walker Creek Drill Hole	r
Flow rate liters/min.	200	7.6	227	pumped	pumped	
Measured temperature ^O C	42	61	80.6	18.5	15	
Na:K ^o C	86	. 104	91	34	76	
Na:K:Ca 1/3 β ^O C	103	125	106	61	97	
Na:K:Ca 4/3 β ^O C	51	85	52	23	54	
Na:K:Ca Mg corrected ^O C	NC	120	NC	NC	NC	
SiO ₂ conductive ^O C	99	117	111	NC	NC	
SiO ₂ adiabatic ^O C	100	116	110	NC	NC	
SiO ₂ chalcedony	69	89	82	NC	NC	
SiO ₂ opal ^O C	-16	· -]	-6	NC	NC	

*Methodology for calculations presented in Appendix A. NC = not calculated.

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GEOTHERMAL-GRADIENT AND HEAT-FLOW DATA*

The temperature-gradient and heat-flow results for the Belknap-Foley area are as shown in Table 5. Included in the table are the township/range-section and latitude and longitude location of each hole. In addition, the hole name, date of logging used, and collar elevation are included for each hole. The bottom hole temperature, maximum depth, corrected temperature gradient, and, where available, corrected heat flow are printed in blue on Plate I. These values are also listed in the table, as are the depth interval and average thermal conductivity used for calculation of the gradient and heat flow. The values are given in SI units. To transform units, the following conversion factors were used: $1 \times 10^{-6} \text{ cal/cm}^2 \text{ sec}$ $(HFU) = 41.84 \text{ mWm}^{-2}$, $1 \times 10^{-3} \text{ cal/cm sec}^{\circ}\text{C}$ (TCU) = 0.4184 Wm⁻¹K⁻¹, and 1°C/km = $1 \text{ mKm}^{-1} = 18.2^{\circ}\text{F}/100$ ft. Corrected gradient and corrected heat flow are values for which the topographic effects have been removed. These are significant for many of the sites studied.

The holes are ranked in terms of the quality of the gradient or heat-flow information: high quality (A), good quality (B), marginal quality (C), data with some problems (D), and data for which no useful temperature gradient or heat flow can be estimated (X). All thermal-conductivity measurements were made on cutting samples. Most of the holes shown on the table were drilled specifically for heat-flow studies, and the data quality is relatively high. In general, holes drilled in the Western Cascade rocks give linear gradients below near-surface effects that may vary in depth from 20 to 100 m. Holes 50-150 m deep in High Cascade rocks, such as 15S/6E-11Dc, are often isothermal because of lateral flow of water in the porous young volcanic rocks.

*By D. D. Blackwell, Southern Methodist University, Dallas, Texas.

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Table 5. Geothermal-gradient data, Belknap-Foley area, Oregon

	• .				Bottom	Depth			Uncorr.	Corr.	Corr.			
Two/Rng-	N Lat.	W Long	Hole #	Collar	Temp.	Interval	Avg. TC	#	Gradient	Gradient	HF	Q		ينين حداد معند <i>و</i>
Section	Deg.Min.	Deg.Min.	Date	Elev.	(°C)	(m)	$Wm^{-1}K^{-1}$	TC	°C/km	°C/km -	mWm -2	HF		
145/ 6E- 32DC	44-18.20 1	122- 7.26	WOLF MDW 8/ 1/80	999	18.12	45.0 154.0	1.46	9	90.2 1.8	75.6	110	B		800.000 (100)
155/ 6E- 11DC	44-16.10 1	122- 3.25	CR-TBR 7/26/77	716	75.20	.0 52.0	• • • •	- ' · '		میں . بینی . بینی .		×	۰ روی ۲ ۲ ۲ ۲	
		•												
165/ 6E- 2CA	44-12.13 1	22- 2.97	CR-FP 8/ 5/76	70	14.56	100.0 150.0	1.74 .03	11	84.1 1.4	88 .3	154	C	•	
165/ 4E- 14DBB	44-10.05 1	.22-17.50	BH-3Z 11/26/75	457	10.76	12.5 45.0	1.80	•	37.8 .4	35.0	63	D :	- '''	·
165/ 5e- 30aab	44- 9.31 1	122-14.62	ST DAM 2 8/ 8/79	389	11.74	25.0 61.0	1.32	1	56.3 1.2	53.0	70	C	·• 	
	-			<i>1</i>			•					*	•	
165/ 5E- 30ABB	44- 9.29 1	122-14.88	ST DAM 3 8/ 8/79	- 368	14.16	15.0 85.0	1.33	• 4	54.0	51.0	68	D	-	
165/ 5E- 30ABC	44- 9.13 1	22-14.98	ST DAM 1 8/ 8/79	368	12.91	45.0 79.7	• .	•	50.8 3.6	48.0	· · ·	C		
169/ 6E- 27BB	44 9.06 1	22- 4.69	CR-HC 9/29/76	573	21.56	30.0 150.0	- 1.57 .05	n 12 m	- 96:2 .9	70.9	- 111	B	. ·	
175/ 5e- Bacd	44- 6.39 1	.22-13.99	WLKR CRK 7/24/80	585	15.78	105.0 155.0	(1.59)	-	54.1 .7	52.0	83	B		
175/ 5E- 2017AA	14- 4.90 1	.22-13.84	RIDR CRK 7/31/80	536	24.77	60.0 154.0	1.64 .04	4	128.5 3.6	97.5	159	В	· · ·	
175/ 6E- 25AD	44- 3.94 1	.22- 1.37	MOSQ CRK 8/ 1/80	1005	11.06	115.0 152.0	1.55	÷ 3	62.8 1.4	73.8	114	C	·	
185/ 5E-	44- 1.12 1	.22- 9.81	REBL CRK	780	14.40	55.0 155.0	1.55	3		· · · · · · · · · · · · · · · · · · ·		×	:: 	
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Only one anomalous value is present, and in general the data fall into two groups: those east of the High Cascade-Western Cascade thermal boundary and those west of the boundary. West of the boundary, heat-flow values generally are below 55 mWm^{-2} , while east of the boundary they are generally above 100 mWm⁻² (Blackwell and others, 1978). Typical gradients are $25-35^{\circ}$ C/km and $60-70^{\circ}$ C/km, respectively. The hole with the highest heat-flow value, at Rider Creek, was drilled within half a mile of Terwilliger Hot Springs, indicating that a slightly larger area is associated with the hot springs than is in evidence from the surface manifestations. Obviously, the value itself is biased by its proximity to the hot springs and cannot be considered a regional value.

CONCLUSIONS AND RECOMMENDATIONS

During the course of this investigation, two major north-south lineaments were found to have close correlation with the distribution of thermal springs and areas of increased heat-flow. Geological mapping revealed that both lineaments are the result of major north-south-trending fault zones and that these fault zones must, to a certain extent, control the flow of geothermal waters.

The available analyses indicate that the thermal waters may be separated into two compositional groups based on total ionic content, ionic ratios, and calculated reservoir temperatures. These two groups show a one-to-one correlation with the aforementioned fault zones: the hotter springs (i.e., Bigelow, Belknap, and Foley) being associated with the McKenzie-Horse Creek fault zone which forms the western margin of the High Cascade graben; and the cooler springs (Cougar and Terwilliger) being associated with the Cougar Reservoir fault zone which lies west of the High Cascade graben margin. This correlation is also seen in heat-flow measurements, with the higher values associated with the McKenzie-Horse Creek fault zone and the lower numbers associated with the Cougar Reservoir fault zone.

This preliminary data analysis indicates that the McKenzie-Horse Creek fault zone may control a higher temperature geothermal resource than the Cougar Reservoir fault zone. Both zones, however, contain geothermal resources which warrant further study. To accomplish a detailed assessment of the geothermal resources, the following steps are recommended:

- Detailed mapping (scale of 1:24,000 or greater) of the McKenzie-Horse Creek fault zone making use of existing 1:15,000 U. S. Forest Service color aerial imagery -- to identify and evaluate active thermal structures along this zone.
- 2. Detailed spring and well sampling and analyses of both hot and cool waters, including isotopic and gas analyses -- to help evaluate reservoir conditions.

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- 3. Closely spaced complete Bouguer and residual gravity anomaly studies along the fault zones -- to further refine the gravity anomalies found during previous regional studies and to tie anomalies to mapped structures.
- 4. Resistivity traverses (either dipole-dipole, roving dipole, or telluric) eastwest and north-south along the fault zones -- to further define geothermal aquifers and to locate areas of thermal upwelling and recharge.
- 5. A program of five to ten 500-ft gradient/stratigraphy holes placed at strategic locations -- to refine the evaluation of the Belknap-Foley heat-flow model.
- 6. Five to six 2,000-ft gradient/stratigraphy holes -- to evaluate thermal anomalies and to directly test geothermal aquifers indicated by resistivity traverses and the shallow heat-flow study.
- 7. Feasibility study -- to determine the best method for drilling the very young, loosely consolidated volcanic rocks within the High Cascade graben.

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APPENDIX A

Formulas used in calculations

Na:K (revised):	$t^{O}C = \frac{1217}{\log (Na/K) + 1}$.483 - 273.15 (Fournier	·, 1979)
Na:K:Ca:	$t^{O}C = \frac{1647}{2.24 + F(T)}$	- 273.15 (Fournier an	nd Truesdell, 1973),
where F (T) = β = t ^O C = and conce	log (Na/K) + [β log (1/3 if t> 100 ⁰ C, and 4, calculated reservoir to entrations are express	√Ca/Na)], /3 if t <100 ⁰ C, emperature, ed in molality.	
Magnesium correction	ratio:		
R = (milliequivale) If R <5 or >50, no ca $\Delta t_{Mg} = 10.66-(4.7415)$ $[(1.968 \times 10^7))$ where R = magnesium co $\Delta t_{Mg} = the tem$ the Na: T = Na:K:Ca	(milliequival nts Mg) + (milliequiva lculation was made. Fo (R) + [(325.87) (log K (log R) ² /T ²] + [(1.60) orrection ratio express perature correction the K:Ca 1/3 β calculated 1/3 β calculated temp	ents Mg) lents Ca) + (milliequiv or R between 5-50, R) ²] - [(1.032 X 10 ⁵) (5 X 10 ⁷) (log R) ³ /T ²], sed in equivalents, at is subtracted from temperature, erature in ^O K.	valents K) X 100 (log R) ² /T] -

Or Δt_{Mg} can be obtained by using the graph compiled by Fournier and Potter (1979).

SiO₂ temperature calculations (Fournier and Rowe, 1966):

SiO ₂ (conductive),	$t^{0}C = \frac{1309}{5.19 + \log (Si0_{2})} - 273.15$
SiO ₂ (adiabatic),	$t^{o}C = \frac{1522}{5.75' + \log (SiO_{2})} - 273.15$
SiO ₂ (chalcedony),	$t^{0}C = \frac{1032}{4.69 + \log (SiO_{2})} - 273.15$
SiO ₂ (opal),	$t^{0}C = \frac{731}{4.52 + \log (SiO_{2})} - 273.15,$

where SiO_2 is expressed in mg/l.

References cited:

Fournier, R.O., 1979, A revised equation for the Na/K geothermometer, in Geothermal Resources Council Transactions 3, 1979, p. 221-224.

- Fournier, R.O., and Potter, R.W., II, 1979, Magnesium correction to the Na:K:Ca chemical geothermometer: Geochimica et Cosmochimica Acta, v. 43, p. 1543-1550.
- Fournier, R.O., and Rowe, J.J., 1966, Estimation of underground temperatures from the silica content of water from hot springs and wet-steam wells: American Journal of Science, v. 264, p. 685-697.
- Fournier, R.O., and Truesdell, A.H., 1973, An empirical Na:K:Ca geothermometer for natural waters: Geochimica et Cosmochimica Acta, v. 37, p. 1255-1275.
- Mariner, R.H., Swanson, J.R., Orris, G.J., Presser, T.S., and Evans, W.C., 1980, Chemical and isotopic data for water from thermal springs and wells of Oregon: U.S. Geological Survey Open-File Report 80-737, 50 p.

	•••••	LOCAT	ION SALEM A	15, OREGON				
• .* • -	DEPTH METERS	HOLE Date Depth Feet	NAME: WOLF MEASURED: 9. TEMPER DEG C	MDW 25/80 ATURE DEG F	Geotherm Deg C/KM	AL GRADIENT DEG F/100 FT	ير .	•
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APPENDIX B

	LOCATIC	N: Salem Ai 145/ 6e-3	15, DREGON 32DC	PA	ge 2
DEPTH METERS	Hole NF Date Me Depth Feet	ME: WOLF ASURED: 9 TEMPER DEG C	MDW 125/80 ATURE DEG F	geotherma Deg C/KM	L GRADIENT DEG F/100 FT
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LOCATION: SALEM AMS, OREGON 165/ 6E/ 2CA HOLE NUMBER: CR-FP DATE MEASURED: 9/29/76

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8	9,310	-19,75	76.0	4.2
0	9.470	49.05	64.0	25
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DEPTH METERS	LOCAT HOLE DATE DEPTH FEET	'Ion: Salem A 165/ 5e- Name: St I Measured: E Temper Deg C	ams, oregon -30abb)am 3 3/ 8/79 Rature Deg F	geotherm Deg C/Km	AL GRADIENT DEG F/100 FT	
5.000000000000000000000000000000000000	16.4 32.8 49.2 65.6 98.4 114.8 131.2 147.6 160.4 1896.8 213.2 229.6 246.0 262.8 262.8 262.8 262.8	$10.990 \\ 10.260 \\ 10.330 \\ 10.330 \\ 10.330 \\ 10.410 \\ 10.550 \\ 10.730 \\ 10.910 \\ 11.180 \\ 11.520 \\ 11.780 \\ 12.070 \\ 12.480 \\ 13.000 \\ 13.980 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 14.160 \\ 1$	51.78 50.479 50.559 50.59 50.59 50.74 50.91 50.91 50.91 51.642 50.93 51.642 50.93 51.642 50.93 51.642 50.53 50.746 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.55 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.54 50.55 50.54 50.55 50.54 50.55 50.54 50.55 50.54 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50.55 50 50.55 50 50.55 50 50 50 50 50 50 50 50 50 50 50 50 5	9.9 -144.0 18.9 16.0 16.0 16.0 16.0 16.0 16.0 16.0 10 10 10 10 10 10 10 10 10 10 10 10 10	៰៰៰៰៹៹៰៰៰៰៹៰៷៰៸៹៹៹៰ ៰៰៰៰៰៰៰៹៰៷៰៸៰៷៰៸៹៹៹៰	

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TEMPERATURE, DEG C



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	5.00 115.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.00 150.	16.4 32.8 49.2 65.6 82.0 98.4 114.8 131.2 147.6 164.0 180.4 196.8 213.2 229.6 246.0 261.6	10.440 10.420 10.560 10.600 10.660 10.760 10.890 11.060 11.270 11.530 11.820 12.170 12.410 12.630 12.710 12.910	50.79 50.76 51.01 51.08 51.19 51.37 51.91 51.91 51.91 52.75 53.91 52.75 53.91 54.73 54.73 54.88 55.24	0.0 -4.0 28.0 12.0 20.0 20.0 20.0 20.0 24.0 42.0 58.0 70.0 48.0 44.0 16.0 42.1	0254714979286497 00154714979286497

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TEMPERATURE, DEG C



DATE	NUMBER: CR+HC MEASURED: 9/29/	76			· ·····
DEPTH	DEPTH	TEMPE	RATURE	GEDTHERM	L GRADIENT
METERS	FEEI	DEG C	DEG F	DEG C/KM	DEG F/100 F
	•				
5.0	16.4	<u> </u>	46.62	•0	<u> </u>
10.0	32•8	8•360	47.05	48.0	2+6
12:0	49.2	8 • 930	48•07	114•0	6•3
25.0	82.0	9:851	40:01	102.0	400
. 30.0	98.4	10•360	-50•65	102.0	5.5
35.0	114.8	10:810	51.46	90.0	4.9
40.00	<u>131+2</u>	11.270	52.29	92.0	5.0
45.0	147.6	11+810	53•26	138•0	5+9
50.0	164.0	12.310	54.15	100.0	5+5
· 55+0	180+4	12.910	55•24	120+0	5.5
65 - C	120+0	130350	,⊃6•03 =7,⊃2		4 e 5 7 0
70.00	229.6	14.550	58.19	1080	<u>, • c</u>
75.0	246.0	14,980	58+96	86.0	4.7
60+0	262.4	15.610	50.10	126•0	5.9
: 85+0	278.8	15.830	60.49	4400	2 • 4
90.0	295•2	16•33ጋ	61•39	100=0	5•5
95.0	311.6	16.540	61.95	62•0	3•4
100.0	328.0	17.070	62+73	86•0	4.7
100-0	34404	1/•/00	53.85	126.0	6 • 7
115.0	377.2	18.720	45.70	12000	
120.0	393.6	19.160	56.49	38.0	4.8
125.0	410.0	19•630	67•33	94.0	2.05
130,0	426.4	20.050	68.09	84•0	4.5
135.0	442.8	20.420	68 •76	74.0	401
140.0	459.2	20•830	69.49	82•0	4+5
145+0	475•6	21•240	70.23	82•0	4.00
10000	+ <i>3</i> ⊆ • U	£1.261	V J + D T	6440	500
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DEPTH METERS	Locatic Hole Na Date Me Depth Feet	IN: SALEM A 175/5E- IME: WLKR ASURED: S TEMPER DEG C	MS, DREGON BACD CRK 224/80 ATURE DEG F	geotherma Deg c/km	L GRADIENT DEG F/100 FT	
$ \begin{array}{c} 11.0\\ 13.0\\ 15.0\\ 17.0\\ 19.0\\ 21.0\\ 23.0\\ 25.0\\ 27.0\\ 29.0\\ 31.0\\ 33.0\\ 35.0\\ 37.0\\ 39.0\\ 41.0\\ 43.0\\ 45.0\\ 47.0\\ 49.0\\ 51.0\\ 557.0\\ 559.0\\ 61.0\\ 63.0\\ 65.0\\ 67.0\\ 69.0\\ 71.0\\ 79.0\\ 81.0\\ 85.0\\ 87.0\\ 89.0\\ 91.0\\ \end{array} $	36.1 449.8 56.8 56.9 56.8 56.9 56.8 56.9 56.9 56.9 56.9 56.9 56.9 56.9 56.9	12.410 12.160 12.050 11.940 11.820 11.730 11.510 11.420 11.310 11.340 11.320 11.310 11.320 11.380 11.380 11.380 11.420 11.420 11.580 11.420 11.420 11.420 11.580 11.510 11.580 11.510 11.660 11.980 12.030 12.180 12.980 12.180 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 12.980 1	43899811532236854186987888886512248811854668839981 533333333888888888848888888888888888888	0.000000000000000000000000000000000000	໑ຓຉ຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺	

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DEPTH METERS	LOCAT HOLE DATE DEPTH FEET	TION: SALEM 17S/ SE NAME: WLK MEASURED: T TEMPE DEG C	AMS, OREGON - 8ACD R CRK 9/24/80 RATURE DEG F	PF GEOTHERMF DEG C/KM	AGE 2 AL GRADIENT DEG F/100 FT		
93.0 95.0 97.0 10135.0 1079.0 10135.0 1079.0 101135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 11135.0 111135.0 111111111111111111111111111111111111	905.0 331184.7 3 8 4 0 5 1 6 2 8 3 9 4 0 6 1 7 2 8 4 9 5 0 6 2 7 3 8 33333334517 4 0 5 1 6 2 8 3 9 4 0 6 1 7 2 8 4 9 5 0 6 2 7 3 8 335353577389063966396295285006528851 335529528851 335529528851 35529528851 35529528851 35529528851 35529528851 35529528552851 355295285528552855 355295285528552855 355295285528552855 3552952855528552855 3552952855555555555555555555555555555555	$\begin{array}{c} 12.540\\ 12.640\\ 12.6700\\ 12.6700\\ 12.6700\\ 12.6700\\ 12.6700\\ 12.6700\\ 12.6700\\ 12.6700\\ 12.6700\\ 12.6700\\ 12.6700\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.600\\ 12.6$	57514815333679978257319399400255 5751481555555555555555555555555555555555	ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼	໙ໞຆຉຆຉຆໞ ຎຉຑຉຑຉຑຬຑຆຒຑຆຆຆຑຆຑຌຨຑ ຆຆຆຠຆຠຆຎຆຉຑຠຬຬຑຬຬຬຑຬຬຬຑຬຬຬ	· · · · · ·	

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TEMPERATURE, DEG C



	DEPTH METERS	LOCATI HOLE N DATE M DEPTH FEET	ON: SALEM (175/ SE AME: RIDI EASURED: 9 TEMPEI DEG C	9MS, OREGON -20BAA R CRK 9/23/80 RATURE DEG F	geothermal Deg c/km	_ GRADIENT DEG F/100 FT
	14.0 16.0 18.0 20.0 24.0 20.0 24.0 20.0 24.0 20.0 24.0 20.0 20	45.95 555.06 778.59 905.51 105.1 105.1 118.62 1118.62 1118.1 121.81 131.81 137.41	11.850 11.650 11.540 11.380 11.380 11.360 11.370 11.400 11.450 11.570 11.630 11.630 11.630	37 397 397 397 397 397 397 397 397 397 3	0.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1950.00 -1000.00 -1000.00 -1000.00 -1000.00 -1000.00 -1000.00 -1000.0	059176538449661 0111210001111111
 ··· · ·	44.0 46.0 50.0 52.0 54.0 56.0	144.3 150.9 157.4 164.0 170.6 177.1 183.7	11.810 11.970 12.070 12.160 12.280 12.380 12.380 12.520	53.25 53.73 53.89 54.10 54.28 54.54	40.0 80.0 505.0 40.0 50.0 50.0 70.0	น47537 B
	50 60 60 60 60 60 60 60 60 60 60 60 60 60	190.2 196.4 203.4 209.9 216.5 223.0 229.6	12.660 12.830 12.970 13.290 13.890 14.120 14.330	54.79 55.09 55.392 57.00 57.42 57.79	70.0 85.0 70.0 150.0 300.0 115.0 105.0	3.8 4.7 9.8 9.5 16.3 5.8
 	724.0 74.0 780.0 8824.0 8824.0 882.0 882.0 882.0 882.0 882.0 882.0 882.0 882.0 882.0 882.0 882.0 882.0 892.0 892.0 892.0 892.0	2362.7 2449.3 2552.4 2552.4 269.5 269.5 269.5 269.5 2888.6 2695.6 2888.6 2955.6 2908 295.6 2908 2908.9 308	$14.530 \\ 14.720 \\ 14.940 \\ 15.160 \\ 15.430 \\ 15.620 \\ 15.920 \\ 16.120 \\ 16.370 \\ 16.860 \\ 16.860 \\ 17.110 \\ 16.000 \\ 16.000 \\ 16.000 \\ 17.110 \\ 16.000 \\ 16.000 \\ 17.110 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \\ 1$	58.59 59.27 59.27 60.62 61.47 61.95 61.95 61.47 61.95 62.80	100.0 95.0 110.0 135.0 95.0 150.0 125.0 125.0 125.0 125.0	຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺ ຺

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	LOCA	TION: SALEM AMS	, OREGON	PAC	ie 2
DEPTH METERS	HOLE DATE DEPTH FEET	NAME RIDR C MEASURED 9/2 TEMPERATI DEG C	RK 3/80 URE DEG F	geothermal Deg C/KM	. GRADIENT DEG F/100 FT
96.0 98.0 100.0 102.0 104.0 106.0 108.0 112.0 112.0 112.0 114.0 120.0 124.0 124.0 128.0 130.0 132.0 134.0 138.0 138.0 138.0 140.0 148.0 148.0 148.0 148.0 148.0 148.0 148.0 148.0	94.061728495062738405162839406 3333347407395062738405162839406 333347407395062738405162839406 333347407395062738405162839406	$\begin{array}{c} 17.350\\ 17.660\\ 17.950\\ 18.200\\ 18.500\\ 18.740\\ 19.040\\ 19.040\\ 19.290\\ 19.550\\ 19.550\\ 20.560\\ 20.350\\ 20.560\\ 20.560\\ 20.560\\ 20.560\\ 20.560\\ 21.360\\ 21.360\\ 21.360\\ 21.950\\ 22.230\\ 22.480\\ 22.710\\ 22.940\\ 23.420\\ 23.640\\ 23.850\\ 24.030\\ 24.170\\ 24.480\end{array}$	63.239 64.739 64.739 64.739 66.5779 66.56 66.779 68.699 69.01 71.053 76.68 66.771 68.699 69.711 722 73.74 74.553 77 74.4553 77 77 77 77 77 77 77 77 77 77 77 77 77	$\begin{array}{c} 125.0\\ 125.0\\ 1455.0\\ 12545.0\\ 12545.0\\ 1250.0\\ 1250.0\\ 1250.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\ 1255.0\\$	៰ ຏ໑໑ຉຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨຨ

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DEPTH	LOCATION HOLE NAM DATE MEA DEPTH	· Salem Am 175/6E-2 E· Mosq SURED: 9/ TEMPERA	s, oregon Sad CRK 24/80 Ture	GEOTHERMA	L GRADIENT	. 1
METERS	FEET 49.2	DEG C	DEG F 44,49	DEG C/KM	DEG F/100 : 0.0	FT
179.000000000000000000000000000000000000	55.394 8895.72884 901.2884 901.2885.17 1084.1217.4.0 1084.1217.4.0 1084.1217.4.0 1084.1217.4.0 1084.0 1084.0 1084.0 1084.0 1084.0 1084.0 1084.0 1084.0 1084.0 1087.30.0 108.0 1084.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 100.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 108.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0	66666667777777777777777777777777777777	4444444444444444455555577984555555555555	_ ໑຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺຺	, , , , , , , , , , , , , , , , , , ,	

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1990 - A. C	LOCAT	ION SALEM A	MS, OREGON		
DEPTH METERS	HOLE 1 DATE 1 DEPTH FEET	NAME: REBL 1EASURED: 16 TEMPER DEG C	CRK 2/30/80 ATURE DEG F	geotherma Deg C/Km	L GRADIENT DEG F×100 FT
0 0 0 0 0 0 0 0 0 0 0 0 0 0	32.8 49.60 55.60 914.82 131.60 131.60 1464.4 196.3 9.60 1464.4 199.3 9.60 118.4 199.3 9.60 118.4 199.3 10.60 118.4 199.3 10.60 118.4 199.3 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 119.5 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60	9.350 9.260 9.180 9.080 9.080 9.080 9.080 9.080 9.080 9.080 9.080 9.1200 9.2440 9.290 9.2440 9.290 9.2440 9.290 9.2440 9.290 9.200 10.300 10.300 10.300 11.200 11.200 14.0300 14.0300 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.1500 14.150	44444444444444444444444444444444444444	0.000000000000000000000000000000000000	0001110788866000000784078000479704

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