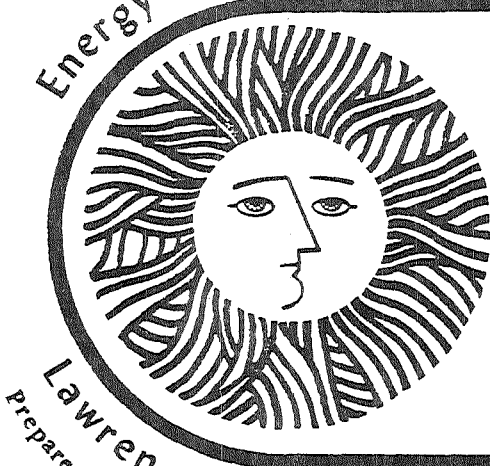


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Reservoir Evaluation Tests On RRGE 1
And RRGE 2, Raft River Geothermal
Project, Idaho

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RESERVOIR EVALUATION TESTS ON RRGE 1 AND RRGE 2,
RAFT RIVER GEOTHERMAL PROJECT, IDAHO

by

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ABSTRACT

This report presents results of the production and interference tests conducted on the geothermal wells RRGE 1 and RRGE 2 in Raft River Valley, Idaho during September - November, 1975. In all, three tests were conducted, two of them being short-duration production tests and one, a long duration interference test. In addition to providing estimates on the permeability and storage parameters of the geothermal reservoir, the tests also indicated the possible existence of barrier boundaries. The data collected during the tests also indicated that the reservoir pressure varies systematically in response to the changes in the Earth's gravitational field caused by the passage of the sun and the moon. Overall, the results of the tests indicate that the geothermal reservoir in southern Raft River valley is fairly extensive and significantly permeable and merits further exploration.

INTRODUCTION

Between January and July, 1975, the Idaho National Engineering Laboratory (INEL) drilled two deep wells in the Known Geothermal Resource Area (KGRA) in southern Raft River Valley and successfully produced hot water at about 147°C (about 297°F) with free artesian flow of over 1500 liters (400 gallons) per minute. Upon completion of the wells, Dr. Jay Kunze, Director, Raft River Geothermal Project, requested the help of the Geothermal Group of Lawrence Berkeley Laboratory (LBL) to conduct appropriate reservoir tests on the two successful wells with a view to gaining as much knowledge as possible about the reservoir to guide further exploration and development. Accordingly, the LBL Geothermal Group carried out production as well as interference tests on the two geothermal wells during the last 3 weeks of September and the first week of November, 1975. The tests yielded useful data on the physical parameters of the geothermal reservoir in Raft River Valley as well as providing clues about the possible reservoir geometry. Based on these tests the drilling of a third well was commenced during April 1976.

The purpose of this progress report is to present the findings of the first reservoir evaluation tests.

GEOMORPHOLOGY, GEOLOGY AND STRUCTURE

The Raft River KGRA is located on a north trending intermontane valley which is bounded on the west (Fig. 1) by the Jim Sage and Cotterell mountains, on the south by the Raft River mountain range, and on the east by Black Pine and Sublett mountain ranges. The valley is about 38 miles long and about 12 to 15 miles wide and is drained

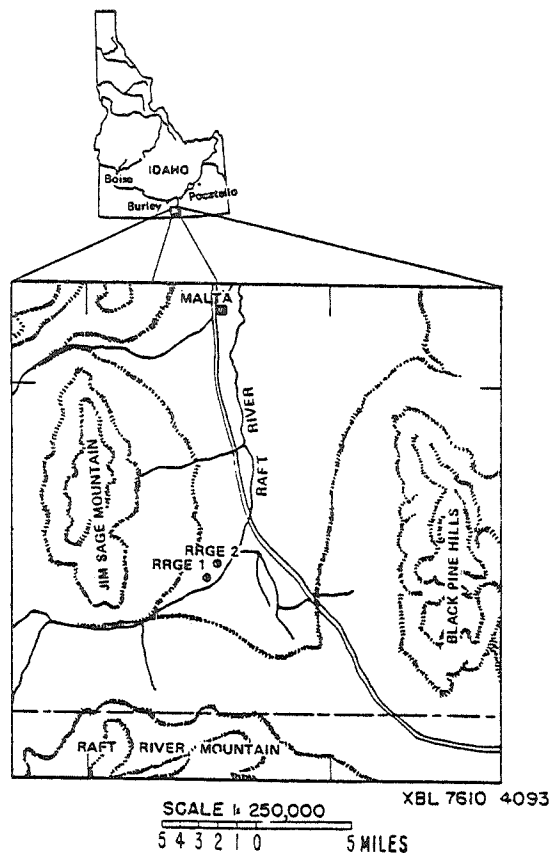


Fig. 1: Location map of the Raft River valley geothermal field, Idaho.

by the perennial Raft River, which flows into the Snake River to the north. The floor of the valley is at an average elevation of about 4600 feet while the surrounding hill ranges attain elevations of up to 9800 feet. The valley is relatively flat and slopes gently towards the north. At the southwestern extremity of the valley the Raft River flows through a gap (known as the "Narrows") between the north-south Jim Sage mountains and the east-west trending Raft River mountains. The latter reportedly forms one of the few east-west trending mountain ranges in the North American Cordillera (Williams et al., 1975).

The Raft River valley lies in a graben formed by down faulting in late Tertiary times (Williams et al., 1975). The basin lies in the northern part of the Basin and Range province near its structural junction with Snake River volcanic plains. The basin is filled with Tertiary and Pleistocene sediments to depths of about 5900 feet. The Jim Sage and Cotterell mountains on the west are made up of Tertiary volcanic rocks and sediments while the Black Pine and Sublett ranges on the east are mainly made up of Paleozoic sediments. To the south, the Raft River mountains ex-

pose Precambrian adamellite (quartz monzonite) capped by Paleozoic metasediments (Williams et al., 1975). The two geothermal wells, RRGE 1 and RRGE 2, terminate in the adamellites indicating that the Precambrian rocks of the Raft River mountains form the floor of the Raft River basin.

A bulk of the sediments filling the basin belong to the Salt Lake formation of Miocene age, attaining thicknesses of up to 5900 ft (Williams et al., 1975). The Salt Lake formation comprises tufaceous sandstone, siltstone and conglomerate. At the bottom, the Salt Lake formation is separated from the Adamellite basement by Paleozoic metamorphic rocks comprising quartzites and schists.

The Salt Lake formation is overlain by Pleistocene sand, gravel, silt and clay (the Raft River formation) which does not outcrop in the valley. The Raft River formation is in turn overlain by alluvial and pluvial sediments.

Structurally (Fig. 2), the Raft River basin is considerably faulted; by north-south faults at the base of the Jim Sage-Cotterell hills on the west and at the base of the Black Pine-Sublett ranges on the east and by east-west faults at the foot of the

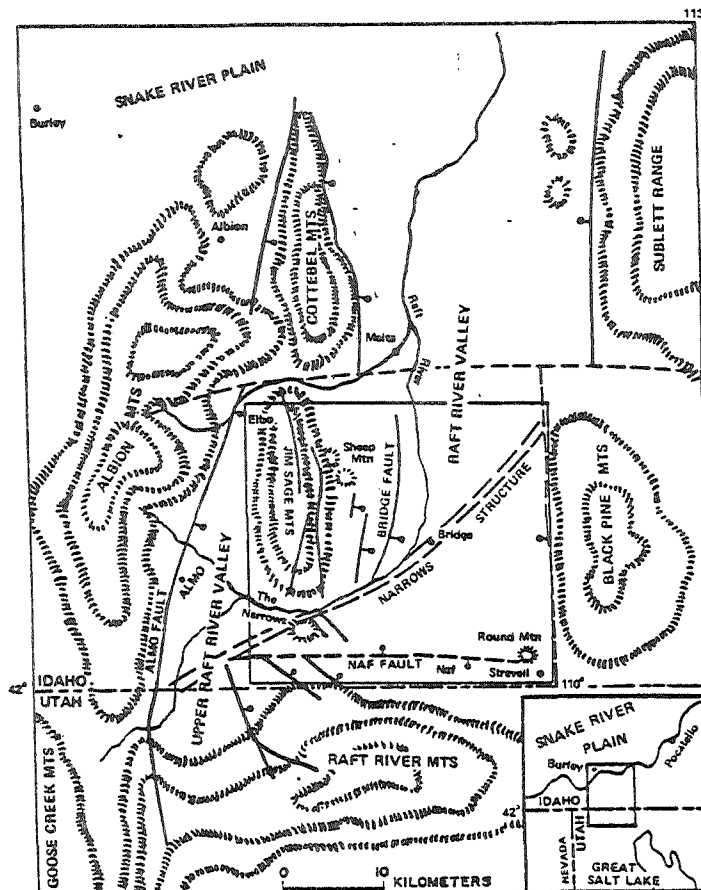
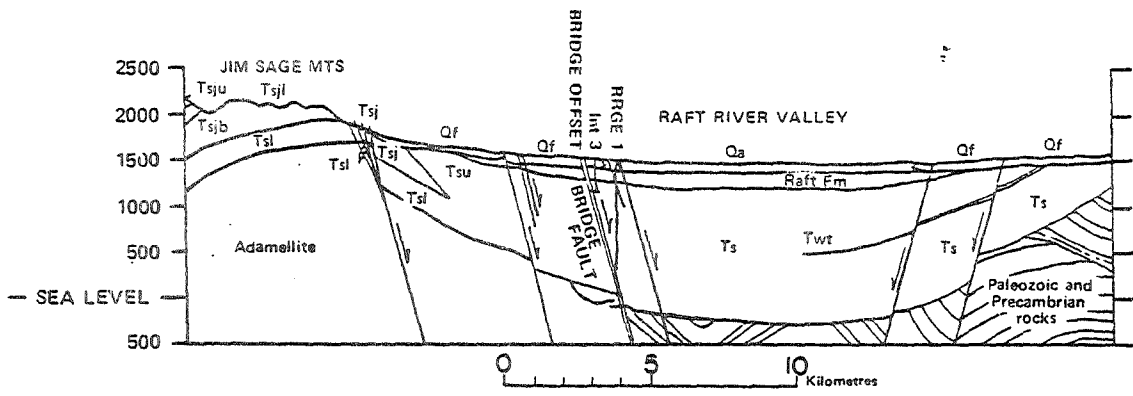
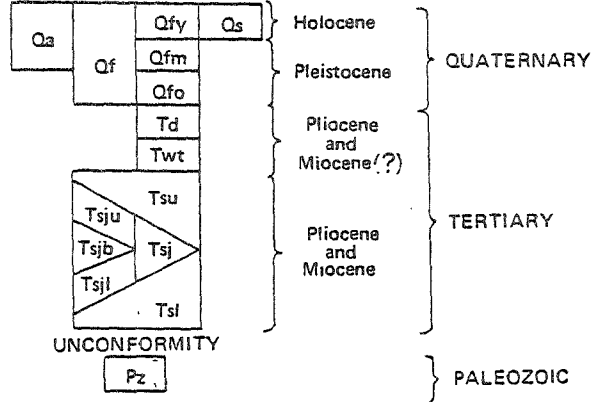


Fig. 2: Structural geology in and around the Raft River valley geothermal field (after Williams et al., 1975).



CORRELATION OF MAP UNITS



LIST OF MAP UNITS

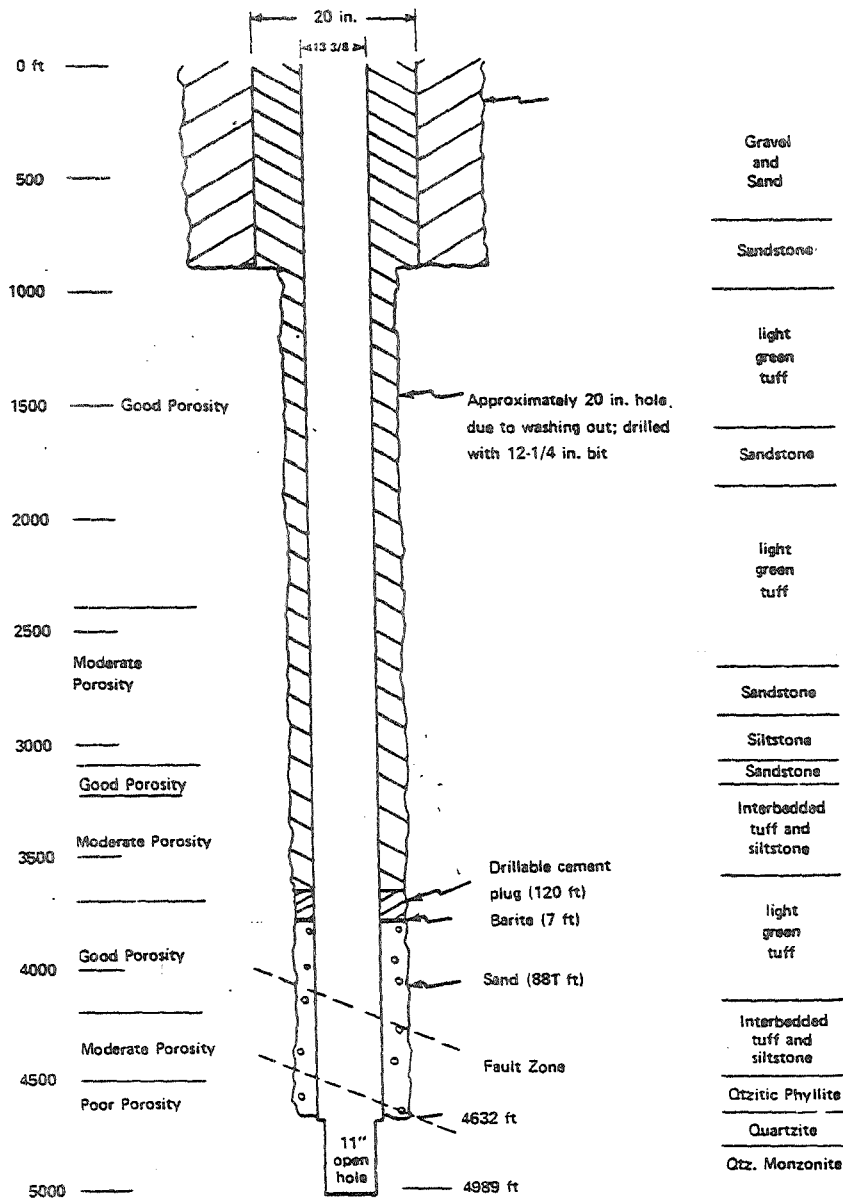
SURFICIAL	
Qa	Alluvium
Qf	Fan gravels
Qfy	Young
Qfm	Middle
Qfo	Old
Qs	Silt
Td	VOLCANIC DOME
Twt	WELDED TUFF
Ts	SALT LAKE FORMATION
Tsu	Upper member
Tsj	Volcanic member at Jim Sage Mountain
Tsju	Upper Flow unit Upper flow unit
Tsjb	Vitrophyre breccia unit
Tsjl	Lower flow unit
Tsl	Lower member
Pz	PALEOZOIC ROCKS

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Fig. 3: Geologic cross section across part of the Raft River valley (after Williams et al., 1975).

Raft River mountains on the south. All the fault planes apparently dip towards the basin, rendering the basin a complex graben. The "Narrows" structure, which has been picked up by geophysical measurements (Williams et al., 1975), is an incompletely understood structural lineament trending ENE at the SW corner of the basin and NE (Fig. 2) at the NE corner of the basin.

The most important structural element in the vicinity of RRGE 1 and RRGE 2 is the Bridge Fault, which seemingly outcrops 2250 feet west of RRGE 1 and trends north-south and dips east at approximately 60 degrees near the surface. The Bridge Fault was apparently intercepted at RRGE 1 at about 4200 feet. In Fig. 3 is reproduced a geological section prepared by Williams et al. (1975) along a WNW-ESE line passing just south of RRGE 1.



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Fig. 4: Profile showing completion details of geothermal well RRGE 1 (prepared by Aerojet Nuclear Company).

SUBSURFACE CORRELATION

The geothermal wells RRGE 1 and RRGE 2 are located in Section 23, Township 15S, Range 26E. The distance between the wells is approximately 4000 feet with RRGE 2 located towards NE from RRGE 1. The completion data for the two wells are summarized in Table I, and the well profiles are sketched in Figs. 4 and 5.

Tentative correlation of the borehole logs of the two wells (Fig. 6) by the geologists of Aerojet Nuclear Company indicate that the sediments apparently dip towards RRGE 2. In particular, the correlation shows that the base of the Raft River formation is offset downward by about 200 feet toward RRGE 2, suggesting an apparent dip of about

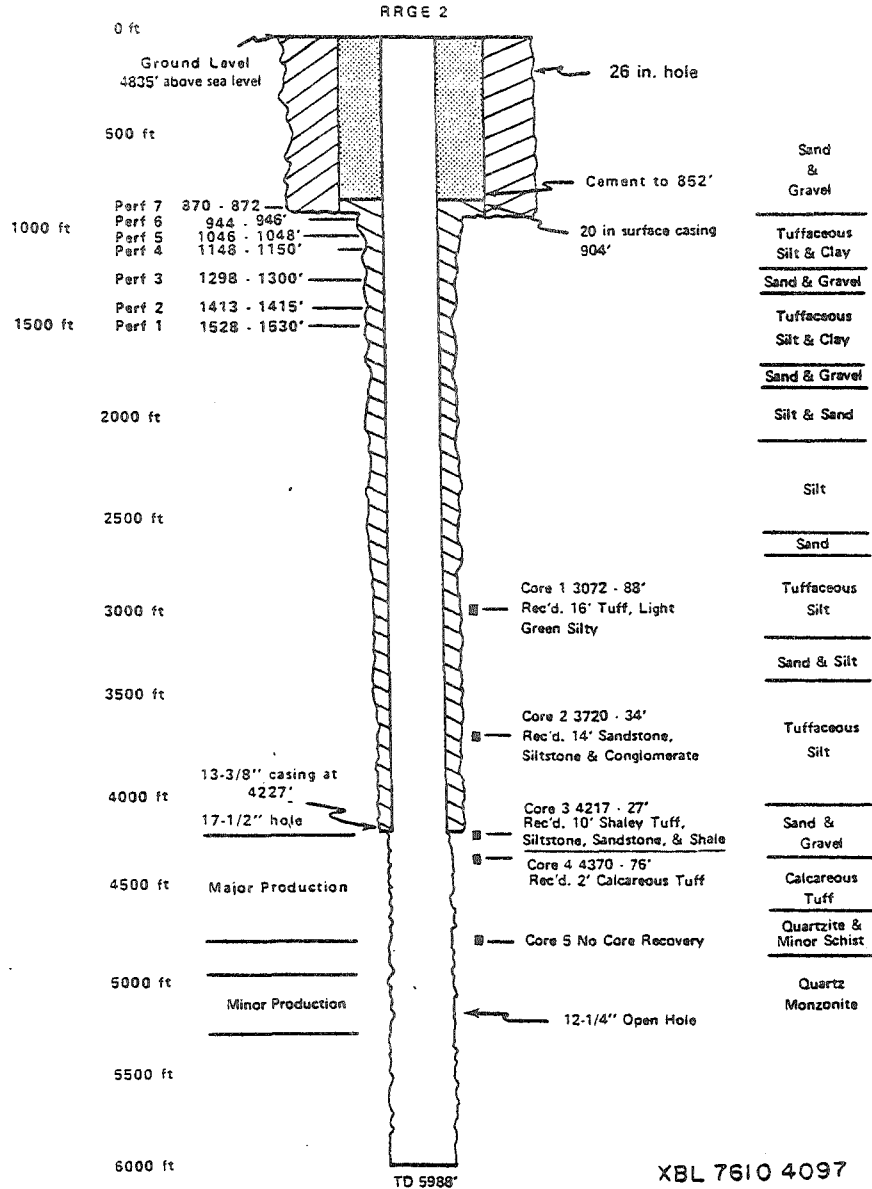


Fig. 5: Profile showing completion details of geothermal well RRGE 2 (prepared by Aerojet Nuclear Company).

three degrees toward NE. With depth, the dips increase gradually and at about 4500 feet in RRGE 2, the deposits are about 500 feet deeper than the comparable sediments in RRGE 1, indicating an apparent dip of about seven degrees. The upper part of the Elba quartzite of Precambrian age, which underlies the Salt Lake formation in RRGE 1 and in

RRGE 2, is apparently almost horizontal between the two wells. While a prominent fault zone (Bridge fault?) was pierced in RRGE 1 between 3800 and 4500 feet, ~~the available data from RRGE 2 failed to indicate the presence of any such pronounced fault zone.~~

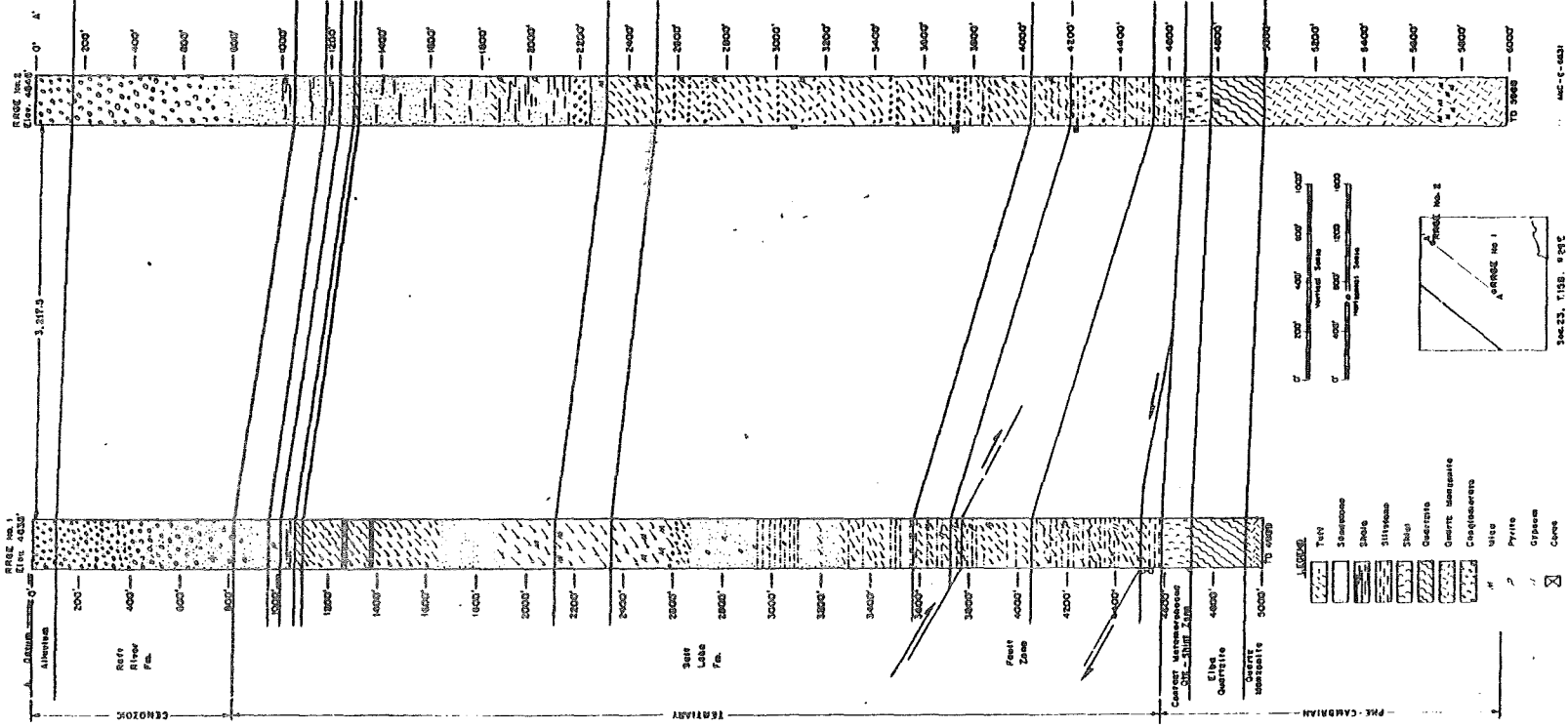


Fig. 6:
Stratigraphic correlation of
geothermal wells RAGE 1 and
RAGE 2 (prepared by Aerojet
Nuclear Company).

TABLE 1

	RRGE 1	RRGE 2
Total depth, ft	4,989	5,988
Casing:		
Diameter, in	13-3/8	13-3/8
Depth, ft	3,624	4,227
Uncased hole:		
Diameter, in	20	12-1/4
Depth range, ft	3,624-4,989	4,227-5,988
Major production, depth range	3,624-4,200(?)	4,227-5,000(?)
Reservoir temperature, °F (°C)	= 294 (146)	= 294 (146)
Well head pressure, psi	= 150	= 150

RESERVOIR TESTS AND INSTRUMENTATION

The basic aims of the reservoir tests were to evaluate the permeability and storage parameters of the reservoir and to decipher reservoir geometry. The tests essentially consisted in producing fluid from one of the wells at controlled rates and over prolonged periods of time and observing the water pressure changes in the producing well itself or in the other well. Since the wells have positive well head pressures (artesian), controlled flow can be achieved by carefully opening the well head valve. Also, since the theory of the tests is based on a single homogeneous fluid, the flow had to be so controlled that there can be no flashing or formation of a vapor phase within the well.

Since the wells are over 4000 feet apart, the pulse introduced at one well can create only very small pressure changes in the observation well. A key piece of equipment in the tests was therefore a very sensitive quartz crystal pressure gage which can be conveniently lowered into the well to any desired depth and which communicates with surface recording equipment through a conductor cable. The pressure gage has a resolution of 0.01 psi (over the range 0 - 10,000 psi) and can withstand temperatures of up to 300°F. Since the maximum reservoir temperatures recorded at RRGE 1 and RRGE 2 were only about 294°F, the aforesaid pressure gage was very well suited for monitoring pressure changes in an active producing well or in a quiet well.

During the tests, use was also made of a similar, but less expensive quartz pressure gage, which could measure pressure changes only at the well head. Since both RRGE 1 and RRGE 2 have positive well head pressures, this "surface pressure gage" was especially well suited for monitoring pressure changes in the observation well during the interference test.

In regard to instrumentation, one of the objectives of the tests was to evaluate the performance of the less expensive surface pressure gage in comparison to the more expensive downhole gage. Towards this end, both the instruments were installed in the same well (RRGE 1) during a long duration interference test and simultaneous pressure measurements were made, with the downhole gage set at approximately 1000 feet. The data so collected are presented in Plate 2. A comparison of the data from the instruments for the period from September 30 to October 6, 1975 shows that the pressure changes sensed by the two instruments agree reasonably well in general except for the fact that the surface gage data tend to show somewhat enhanced peaks during the early afternoon periods (between 1200 and 1800 hours). It is worthwhile pointing out here that in setting up the surface gage, an air column was used as a buffer to protect the pressure sensing crystal from the water in the well. It seems reasonable to infer that the accentuated pressure readings indicated by the surface gage during the early afternoons are to be attributed to the expansion of the air column buffer due to the increased temperatures.

The experience gained in regard to the surface pressure gage has showed that the surface pressure gage is indeed a valuable, economical alternative to the considerably more expensive downhole gage whenever one is interested only in measuring transient well head pressure changes in observation wells. It is felt that the anomalous readings induced by the air column buffer due to its susceptibility to temperature changes can be minimized or even eliminated by replacing the air column by a buffer of an inert oil, such as silicone oil.

DESCRIPTION OF RESERVOIR TESTS

In all, three tests were conducted between September 12 and November 7, 1975. Two of these were production well tests in which the pressure gage was positioned in the production well within the producing interval. This was necessary in order to assure a fairly stable temperature environment for the pressure gage, which is temperature sensitive. The production well tests were both of short duration and lasted less than 30 hours. After shutting down production, pressure buildup within the well was monitored for less than 24 hours.

The third test was an interference test in which fluid was produced from RRGE 2 and the pressure changes were monitored in RRGE 1. Since the latter was quiet and fluid filled, it was not essential to position the instrument close to the bottom of the well. The interference test, which provides data on a large portion of the reservoir between the two wells, was of a long duration. During this test, RRGE 2 was flowed for approximately 26 days.

The specifications of the tests conducted are given in Table 2.

TABLE 2

Test No.	Description	Duration Hours	Production Well No.	Flow Rate gpm	Pressure Gage in Well No.	Depth, ft	Maximum Pressure Drop Well No.	Δp , psi
1	Short term test on RRGE #2	15	RRGE #2	225	RRGE #2	5200	RRGE #2	39
2	Long term test on RRGE #2	615 1/2	RRGE #2	400	RRGE #1	1000	RRGE #1	3.6
3	Short term test on RRGE #1	30	RRGE #1	26	RRGE #1	4700	RRGE #1	1.1

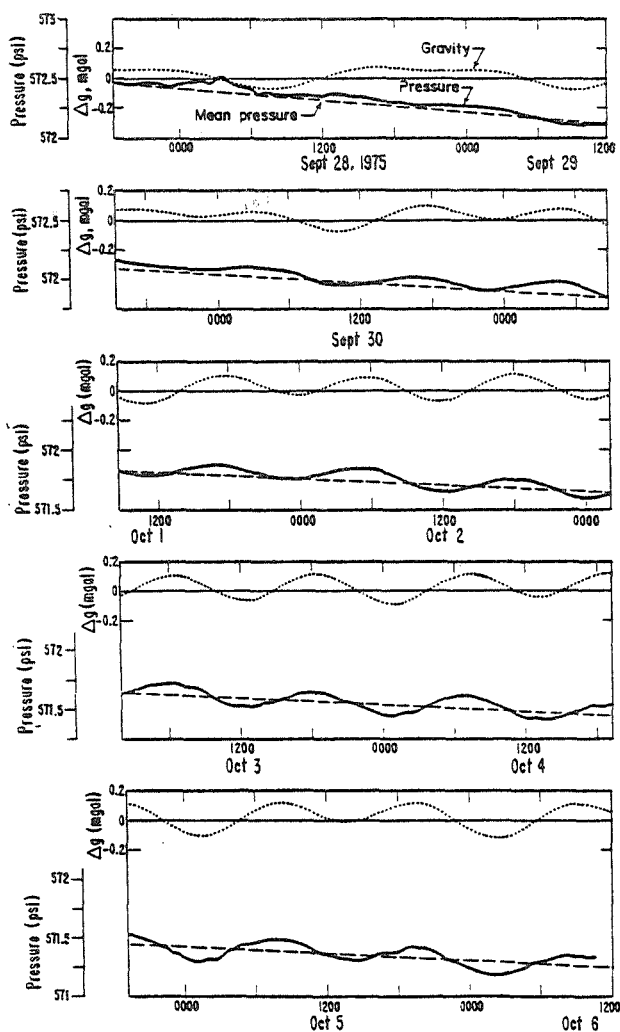
INFLUENCE OF EARTH TIDES ON OBSERVED WATER PRESSURES

A significant phenomenon that came to light from the water pressure data collected during the long duration interference tests (Plate 2) and the short duration production test on RRGE 1 (Plate 3) was that the water pressure in the reservoir responds systematically to the changes in the earth's gravitational field induced by the paths of the moon and the sun. The field data indicated regular fluctuations in water pressures with wave lengths varying from 10 to 12 hours and with amplitudes of up to 0.1 psi about the mean.

For a proper evaluation of the pressure data, the gravitational changes at the location of RRGE 1 over the period of the tests was calculated by Dr. Howard Oliver of the U. S. Geological Survey, Menlo Park, California. Figure 7 shows a comparison between the calculated gravity variation and water pressure variation in RRGE 1 between September 28 and October 6, 1975. It can be seen from the figure that there is good correlation between gravity change and pressure change. A cross spectral analysis of the data showed that the troughs and crests of the water pressure wave tend to lead the corresponding features of the gravity wave by about 37 minutes. Due consideration had to be given to the tidal influence before the interference data could be analyzed.

THEORY OF PUMPING TESTS

Before we present and discuss the results, it is pertinent to briefly describe the theoretical basis of interpretation. The analytical model used for interpretation is that of transient potential distribution around a continuous line source (axisymmetric system) in an infinite, homogeneous horizontal slab of finite thickness. By the principle of superposition and using image concepts, the model can be extended to non-infinite or bounded systems. Details of this interpretive technique can be found in Witherspoon et al., 1967, or Ferris et al., 1962. The aim of interpretation is to determine the reservoir kH , the reservoir storativity, ϕcH (where K is the permeability coefficient, H is reservoir thickness, ϕ is porosity and c reservoir compressibility) and decipher the existence of barriers or other boundaries. The



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Fig. 7: Correlation between variation in the earth's gravitational field and water pressure in RRGE 1 during the long-term interference test.

transient pressure change around a line source in an initially static system is given by the relation (often known as the Theis equation)

$$\Delta P = \frac{q\mu P_D}{(v)kH} \quad (1)$$

where ΔP is pressure change, q is constant flow rate, μ is fluid viscosity (assumed to 0.18 cp at 294°F and 2000 psi), P_D is dimensionless pressure and v is a constant depending on units used. Moreover, P_D is expressed as an integral of the dimensionless time t_D

$$P_D = 1/2 \int_u^\infty \frac{e^{-u}}{u} du \quad (2)$$

where $u = 1/4 t_D$. The dimensionless time t_D is given by

$$t_D = \frac{kt}{\phi\mu cr^2} \quad (3)$$

in which t is time and r is the radius to the point of observation. ~~In order to evaluate kH and ϕcH using (1), (2) and (3) a technique of curve matching is conventionally used, by plotting the pressure drawdown data on a log-log graph paper. Or, for $t_D \gg 1$, an asymptotic approximation may be used in which drawdown is plotted as a function of the log of time. In addition to kH and ϕcH , the departure of the plotted data from the type curve in the log-log plot or the occurrence of breaks in the slopes of the straightline segments of the semi-log plot would indicate the presence of barrier or leaky boundaries in the system.~~

RESULTS OF TESTS AND INTERPRETATION

(1) Short term production test, RRGE 2: The short term production test on RRGE 2 was conducted between September 12 and 13, 1975. The data collected during this test is presented in Appendix 1 and the time history of pressure change is shown in Plate 1. During this test, the well was flowed at a near-constant rate of 225 gpm for 15 hours. After shutting down the flow, pressure buildup was observed for an additional 2.25 hours. The maximum pressure drawdown observed during the production period was approximately 37.5 psi. The total pressure recovery during the 2.25 hours of buildup observation was about 24.25 psi. During this test, the quartz pressure gage was installed at a depth of 5200 feet where the absolute static pressure was about 2261 psi.

A log-log plot of the pressure drawdown data collected from this short term test is presented in Fig. 8. It can be seen from the figure that between 15 and 600 seconds of the start of production, the drawdown data closely matches the Theis' type-curve. Computations based on this early drawdown data indicate the following parameters for the reservoir in the vicinity of RRGE 2: $kH = 47,600$ millidarcy-feet; $\phi cH = 2.91 \times 10^{-2}$ ft/psi, assuming an effective well radius of one foot. Since the exact production thickness of the reservoir is not known, the fundamental parameters, permeability and compressibility have not been computed.

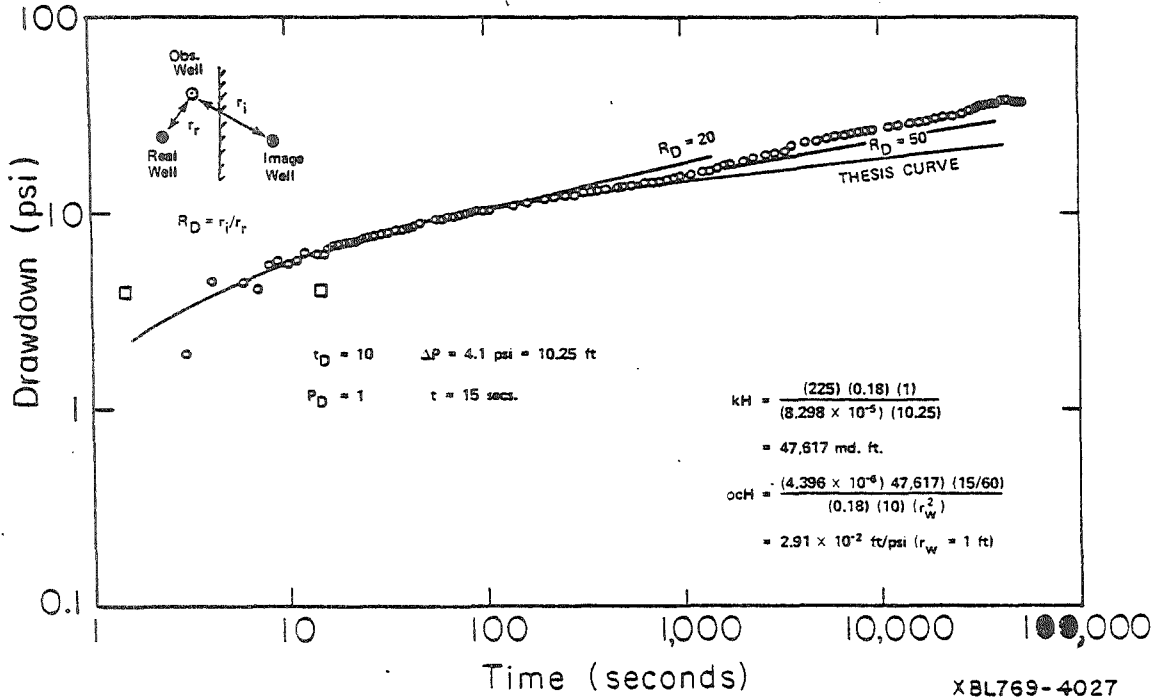


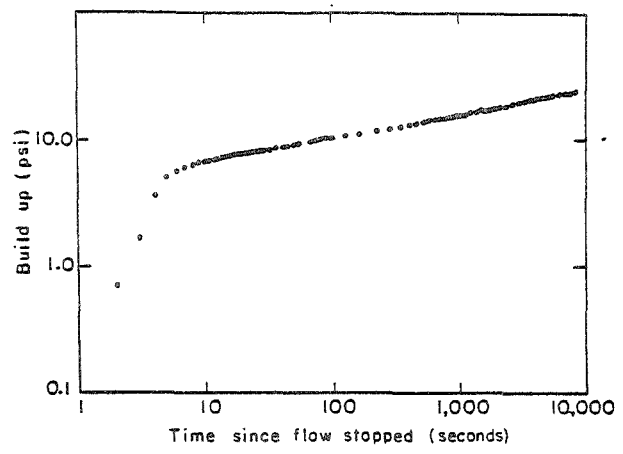
Fig. 8: Short-term production test, RRGE 2: Log-log plot of drawdown versus time.

barrier B RR2

The data presented in Fig. 8 also show that after about 600 seconds, the drawdown data gradually departs from the Theis type-curve, showing larger drawdowns than those suggested by the type-curve. This kind of departure could normally be indicative of the presence of one or more barrier boundaries in the vicinity of RRGE 2. Figure 8 suggests that if indeed a barrier boundary exists near RRGE 2, it is equivalent to an "image" well located at a distance of between twenty and fifty times the effective radius of the well. However, it is possible that (H.J. Ramey, personal communication) the observed departure from the type-curve could have been caused by other factors such as gradual changes in production rates or commingling of different producing horizons.

A semi-log plot of the drawdown data is presented in Fig. 9. It is seen from this figure that the data within the first 800 seconds of production fall on a fairly well-defined straightline indicating a kH value of about 47,300 millidarcy-feet and a ϕcH value of 3.0×10^{-2} ft/psi assuming an effective well radius of one foot. It is interesting to note from this figure the drawdown data plot on three distinct line segments; the second and the third line segments may indicate the probable presence of a barrier boundary near RRGE 2.

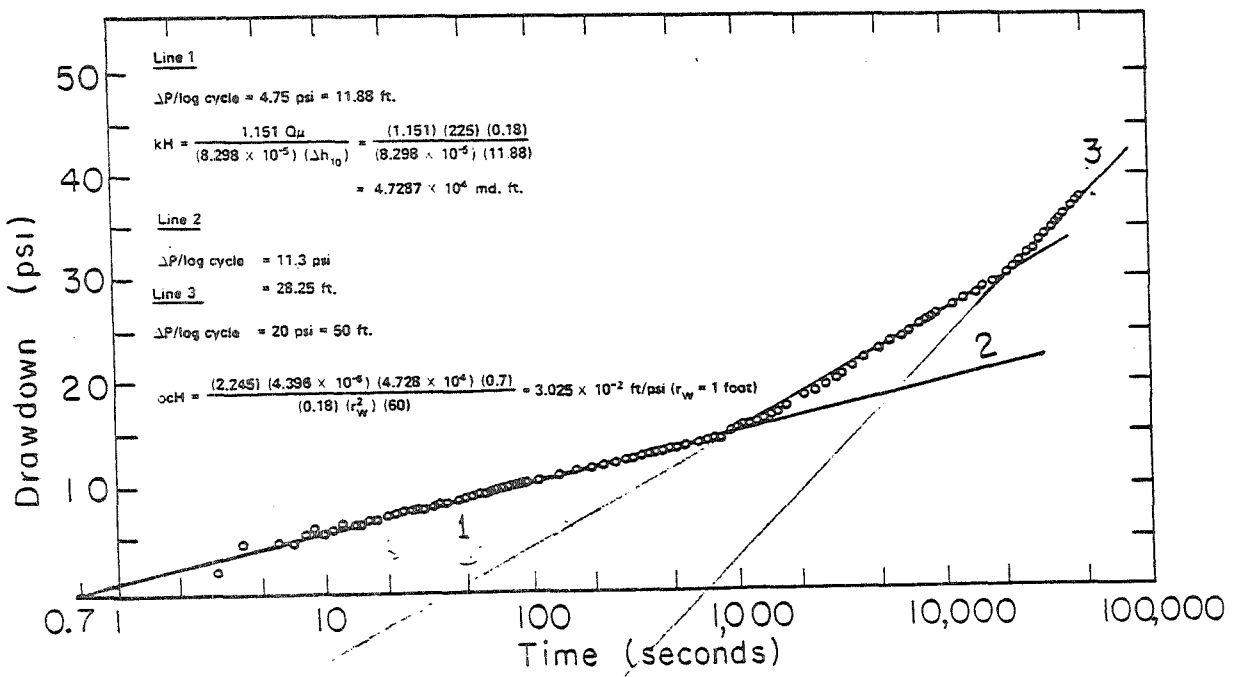
A log-log plot of the pressure buildup data is presented in Fig. 10. The buildup plot is of considerable interest in gaining an insight as to whether the reservoir may or may not be fractured in the vicinity of RRGE 2. It is known from petroleum engineering literature that when pressure



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Fig. 10: Short-term production test, RRGE 2: Log-log plot of build up versus time.

buildup is plotted on a log-log graph paper the presence of a unit slope in the early drawdown data is indicative of well bore storage effects while the existence of a half-slope is indicative of the presence of large, highly permeable fractures close to the well bore. It is very well seen from Fig. 10 that even within the first ten seconds of shutting down the flow, one fails to discern the presence of a unit slope or a half-slope, leading to the inference that for purposes of overall interpretation, one could effectively treat the reservoir as a porous medium.



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Fig. 9: Short-term production test, RRGE 2: Semi-log plot of drawdown versus time.

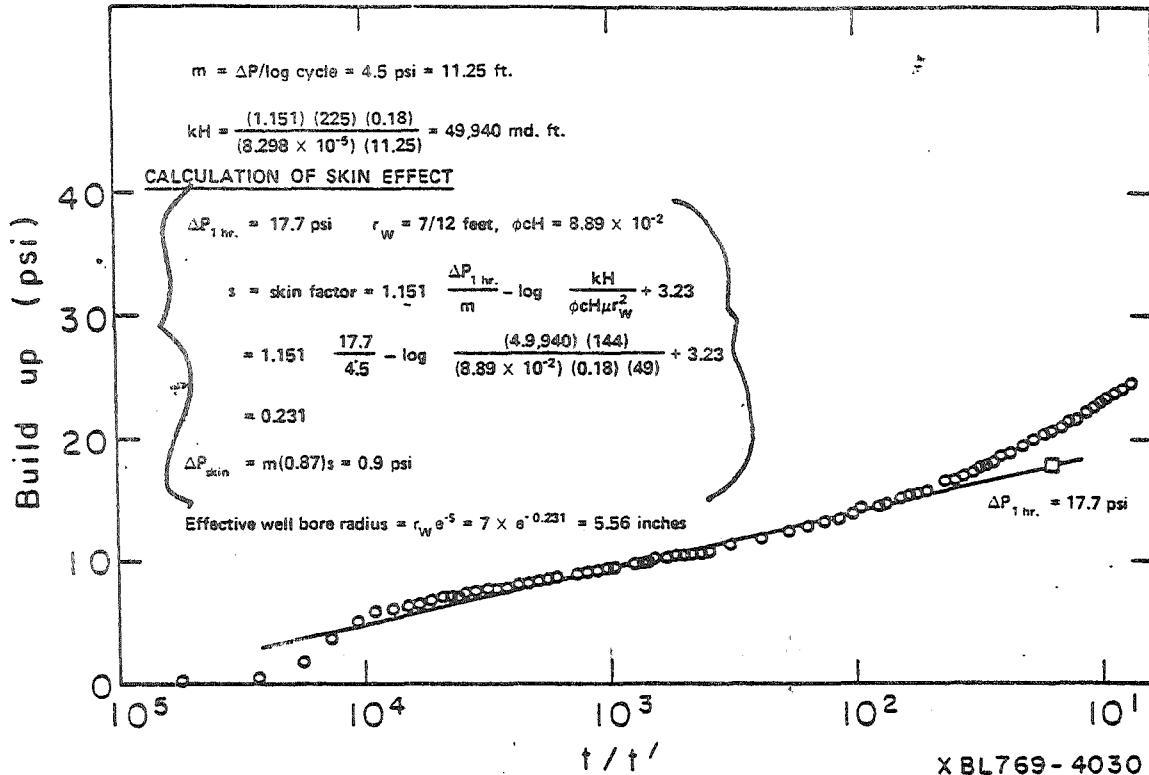


Fig. 11: Short-term production test, RRGE 2: Build up as a function of $\log t/t'$.

A plot of pressure buildup as a function of t/t' , where t is the time since flow started and t' is the time since flow stopped is given in Fig. 11. Since we are aware of the possible presence of barrier boundaries from the drawdown history, the interpretation of the buildup data is rendered somewhat difficult. The drawdown data indicated that the first barrier boundary became noticeable after about 800 seconds of production. Figure 11 indicates a pronounced break in slope at $t/t' \approx 6 \times 10^1$, which corresponds to about 900 seconds. Thus for buildup analysis we fit a straight-line for $t/t' > 6 \times 10^1$ or $t' < 900$ seconds and obtain a kH of about 49,900 millidarcy-feet, which is in reasonable agreement with the kH values indicated by the drawdown data.

Computations in regard to skin effect according to the method of Matthews and Russell (1976) indicate that excess pressure drop due to skin effect is about 0.9 psi, or about 5 per cent of the total drawdown of 37.5 psi and that the effective well bore radius is about 5.6 inches as compared with the actual radius of about 7 inches. This probably suggests that the borehole is not significantly damaged.

(2) Long term interference test: The long term interference test was conducted between September 20 and October 30, 1975, when RRGE 2 was flowed at a near constant discharge of 400 gpm and the water pressure changes were monitored in RRGE 1, 4000 feet away, which acted as the observation well. The production on RRGE 2 lasted for 615.5

hours, extending from 2230 hours on September 20 to 1400 hours on October 16, 1975.

During the course of the test water pressures were monitored in RRGE 1, both at the surface and downhole. The downhole measurements were made with the downhole gage located at approximately 575 psi. The static well head pressure was about 150 psi. The maximum pressure drawdown in RRGE 1 due to production from RRGE 2 was 3.6 psi. The data gathered from the two gages are presented in Appendix 2 and are graphically shown in Plate 2.

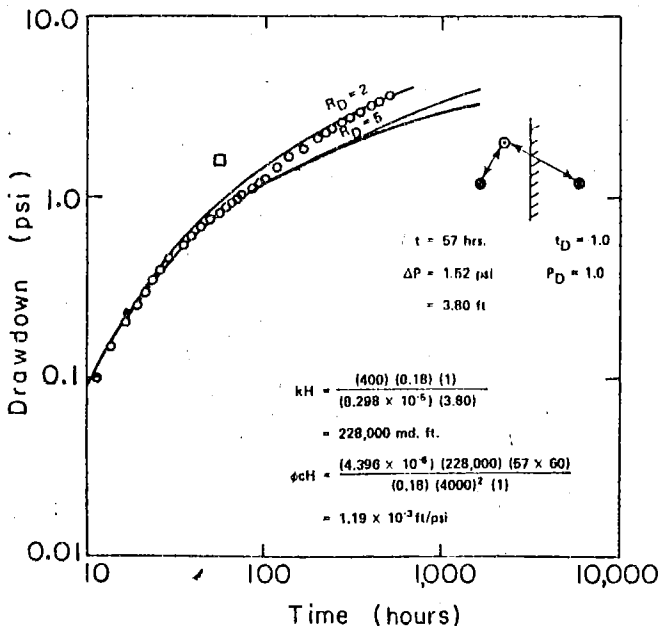
The downhole gage was available for use only for a limited period of time, from September 20 until October 6, 1975. Within this period, the performance of the downhole instrument was frequently interrupted by leakage of water through the cable head and consequent instrument malfunction. Such malfunctions occurred five times between September 20 and October 11, 1975 and on each of these occasions the instrument had to be removed from the well, repaired and relowered into the well. Each time the instrument was removed from its setting and repositioned, there was a change in the absolute pressures recorded, the magnitude of the shift being approximately about 1 psi. These shifts are to be attributed to the sensitivity of the instrument to perturbations in temperature and total pressure. However, these slight changes in absolute pressures had no effect on the recorded changes in pressure. It may be noted here that for reservoir interpretation, it is the pressure differentials that are critical and not the absolute pressures.

In preparing the graph of pressure history presented in Plate 2, appropriate adjustments were made in the aforesaid shifts in order to establish overall continuity.

The surface pressure gage was used throughout the period of test from September 20 to October 30, 1975. However, continuous recording equipment was not installed until September 30 and hence only sparse data could be collected during the first ten days of the test. The pressure transient data at RRGE 1, relating to the last ten days of the production period and the entire buildup to data, were collected exclusively from the surface instrument.

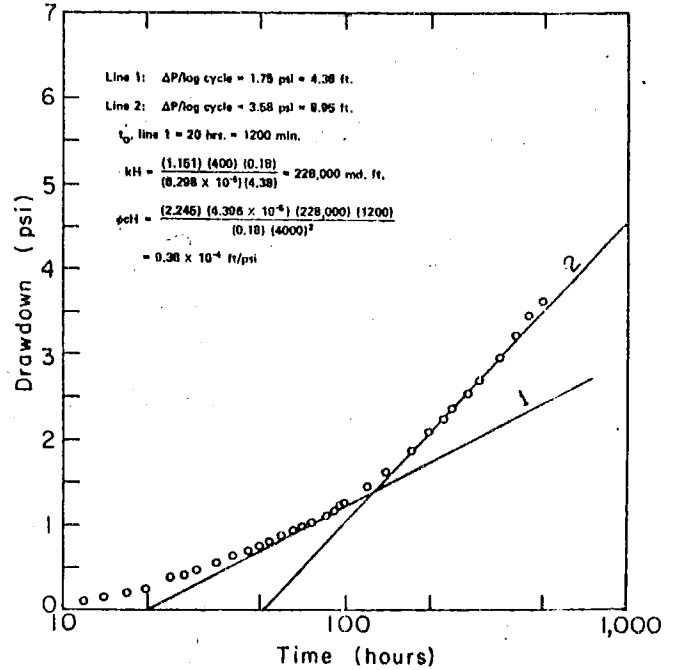
As seen from Plate 2, both the downhole and the surface data show the effect of earth tides superposed on the pressure transient caused by the producing well. For a proper interpretation of the interference effects, it was necessary to filter out the effects of the earth tides. In as much as the correlation between the water pressure data and the computed variation in gravity is extremely good (Plate 2), it was possible to eliminate earth tide effects from the fluid pressure data by simply considering (for purposes of interpretation) only the pressure data relating to those instants of time when the computed gravity variation was zero. This procedure was followed in carrying out the interpretation of the drawdown and the buildup data described below.

The interpretation of the drawdown data collected from the downhole instrument at a depth of 1000 feet is presented in Figs. 12 and 13. The log-log plot shown in Fig. 12 shows that the data collected closely match the Theis' type curve during the first 70 hours of drawdown history, suggesting the following parameters for the large portion of the reservoir between the wells: $kH =$



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Fig. 12: Long-term interference test: Log-log plot of drawdown versus time for RRGE 1.



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Fig. 13: Long-term interference test: Semi-log plot of drawdown versus time for RRGE 1.

228,000 millidarcy feet and $\phi cH = 1.19 \times 10^{-3}$ ft/psi. After about 70 hours, the observed drawdowns gradually depart from the type curve of Theis, indicating the presence of a barrier boundary. It is further seen from Fig. 12 that the data points roughly fall between the lines labeled $2R_D$ and $5R_D$ suggesting that the barrier boundary could be treated effectively equivalent to an "image well" located at a distance of approximately $3R_D$ from RRGE 1, where $R_D = 4000$ ft is the distance between the producing well RRGE 2 and the observation well RRGE 1. Theoretically, the barrier boundary should coincide with the perpendicular bisector between the producing well RRGE 2 and the image well. However, since we only have a two-well system, it is impossible to determine the orientation of the image well with reference to RRGE 1 and hence it is not possible to locate the barrier boundary accurately.

A semi-log plot of the drawdown data is presented in Fig. 13. The prominent break in the slope of the straight line at about 130 hours is also indicative of the effects of a barrier boundary. The early drawdown data in Fig. 9 suggest the following parameters for the reservoir: $kH = 228,000$ millidarcy feet, $\phi cH = 9.38 \times 10^{-4}$ ft/psi. Calculations based on the slope change after 130 hours suggest that the barrier boundary is equivalent to an image well located about 11,000 feet from RRGE 1 in an unknown direction.

As mentioned earlier, the pressure buildup data was collected exclusively from the surface instrument. The buildup data is interpreted graphically in Figs. 14 and 15. The pressure buildup values used in the interpretation are corrected buildup values, arrived at after removing the ef-

facts of the production well and its image from the actually observed drawdown. The components of drawdown due to the production well and its image were in turn evaluated by extrapolating the drawdown curve into the buildup period.

A comparison of Figs. 14 and 12 and Figs. 15 and 13 indicate reasonable agreement in the reservoir behavior observed during production and buildup. In addition to confirming the presence of a barrier boundary, the early drawdown data from Fig. 14 suggest the following reservoir parameters: $kH = 192,800$ millidarcy feet; $\phi cH = 1.06 \times 10^{-3}$ ft/psi. Similarly, the semi-log plot in Fig. 15 indicates, for the reservoir, a kH value of 210,000 millidarcy feet and a ϕcH value of 8.20×10^{-4} ft/psi. Calculations based on the slope change seen in Fig. 11 indicate that the barrier boundary is effectively equivalent to an image well located about 8,500 feet away from RRGE 1.

(3) Short term production test, RRGE 1: The short term test on RRGE 1 was conducted between November 4 and November 7, 1975. After making observations on background reservoir pressure for about 18 hours, the well was flowed at an average discharge of 26.5 gpm for a period of 30 hours from 0845 hours on November 5 to 1445 hours on November 6, 1975. After shutting down flow, pressure buildup was monitored for approximately 19 hours. During the test, the downhole pressure instrument was positioned at a depth of 4700 feet within the well.

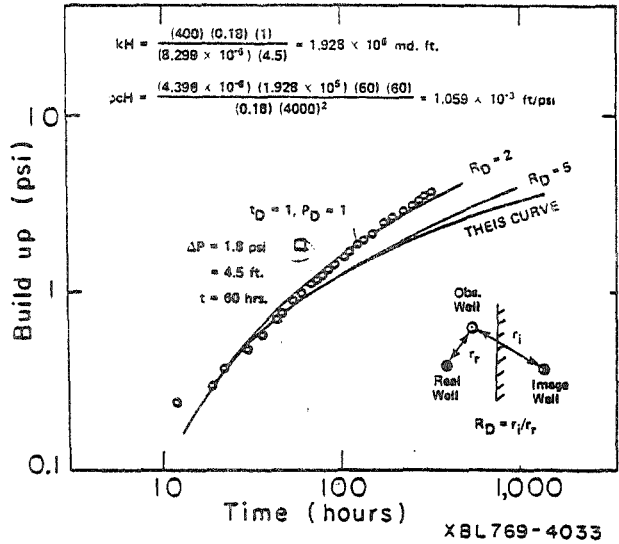


Fig. 14: Long-term interference test: Log-log plot of build up versus time for RRGE 1.

The pressure data collected during the test are summarized in Appendix 3 and the time history of pressure change is graphically presented in Plate 3. The maximum pressure drawdown at the end of 30 hours of production was approximately 1.1 psi.

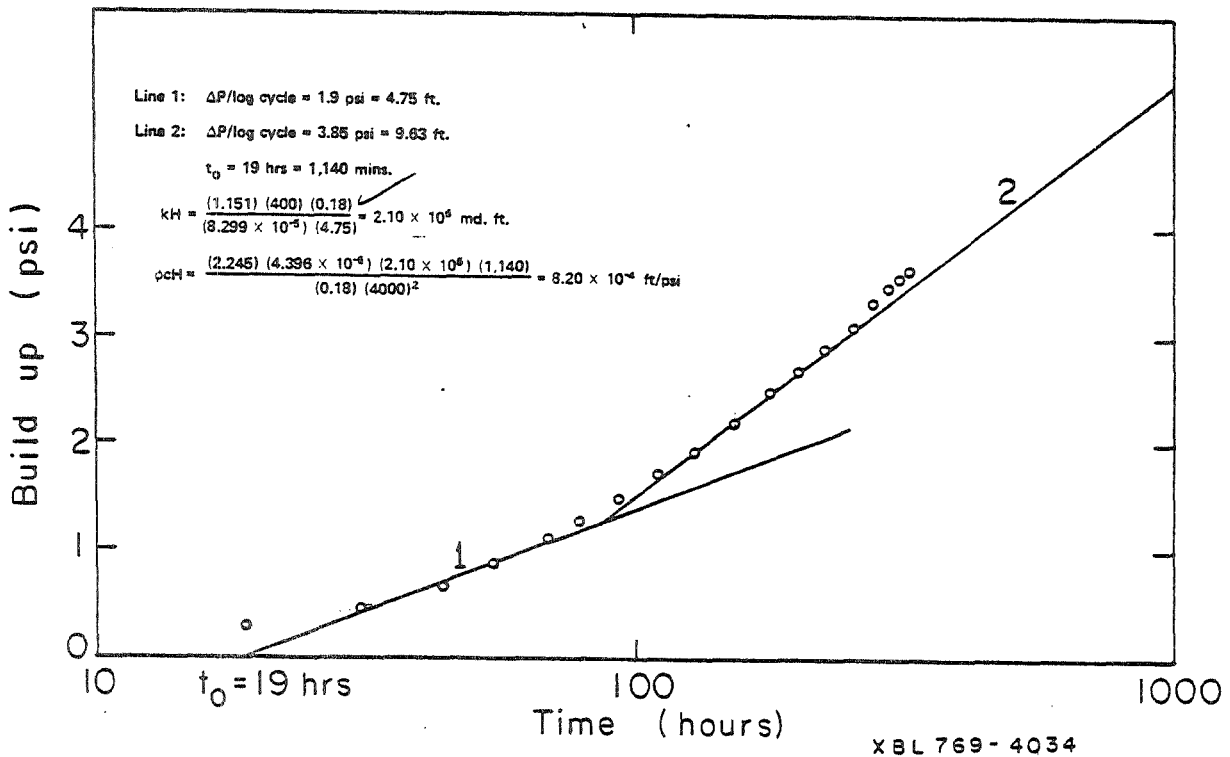
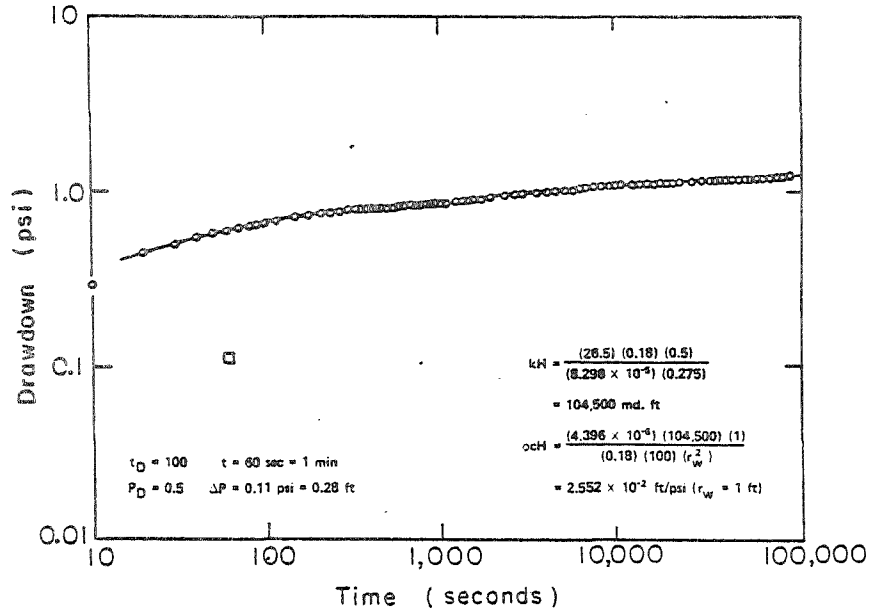
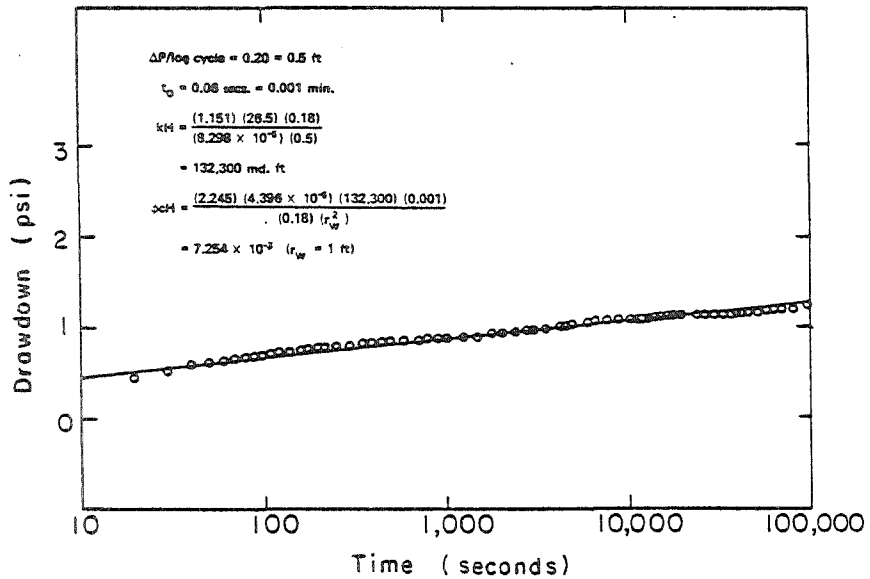


Fig. 15: Long-term interference test: Semi-log plot of build up versus time for RRGE 1.



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Fig. 16: Short-term production test, RRGE 1: Log-log plot of drawdown versus time.



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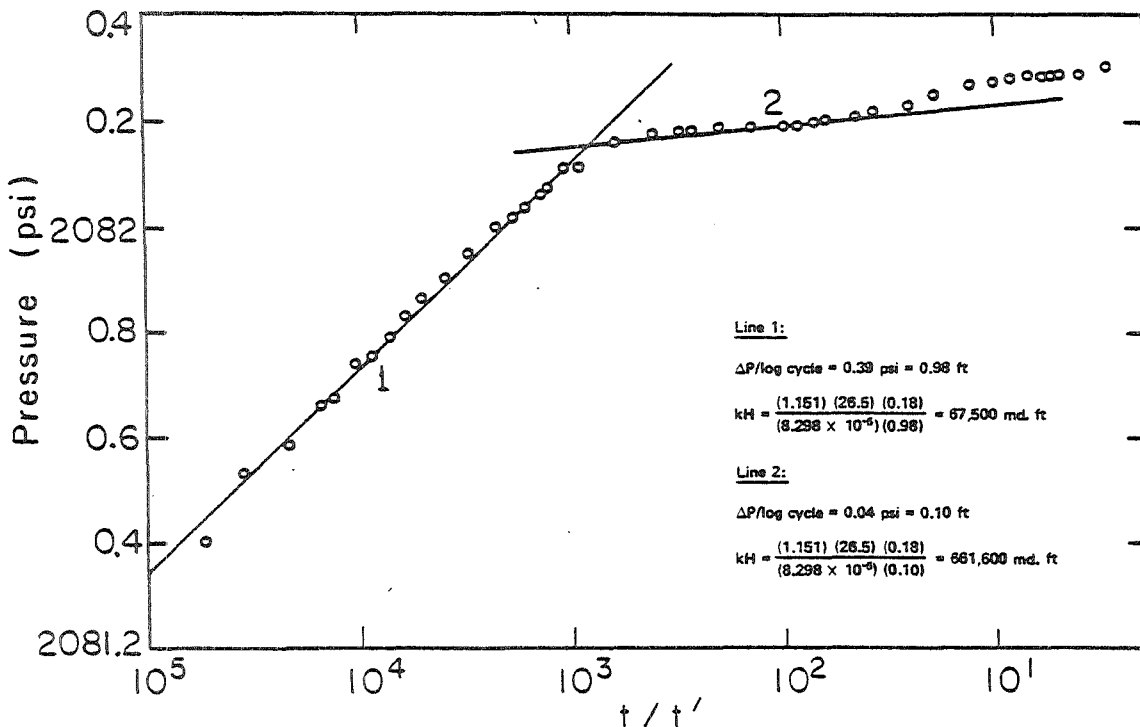
Fig. 17: Short-term production test, RRGE 1: Semi-log plot of drawdown versus time.

It can be seen from Plate 3 that throughout the period of observation the observed pressure data indicate significant influence of earth tides. This is to be expected, since the maximum pressure due to well production is small, being only about 1.1 psi.

The interpretation of the pressure drawdown data is presented in Figs. 16 and 17. It should be pointed out here that the significant presence of earth tide effects has rendered the interpretation considerably difficult. Since the flow duration extended only for 30 hours and since during this 30-hour period zero-gravitational change occurred only twice (at 2200 hours on November 5 and 0625 hours on November 6) it was not possible to eliminate the earth tide effects by the same procedure that was employed in the interpretation of the interference test. ~~Nor has it been possible to establish precise correlation coefficients between the tidal function and the pressure variation.~~ Under these conditions, the best that could be done was to interpret, in an average sense, the actual observed drawdown data. Thus, it is seen from Fig. 16 that matching against Theis' type curve yields a kH value of 105,000 millidarcy feet and a ϕcH value of 2.56×10^{-2} ft/psi, assuming an effective well radius of 1 foot. Again, as seen from Fig. 17, the semi-log plot of the time-drawdown relation suggests a kH value of 132,000 millidarcy feet and a ϕcH value of 7.2×10^{-3} ft/psi, assuming an effective well radius of one foot.

Figure 18 is a plot of the buildup pressures as a function of t/t' where t is the time since flow started and t' is the time since flow shut down. It is readily seen from the figure that there is more than one straight line segment discernible in the plot and it is difficult to conclude the correct one. Computations show that the first line segment indicates a kH of about 67,500 millidarcy feet, which appears somewhat low when compared with the drawdown interpretation. Similar calculations based on the slope of the second line segment indicate a kH value of 661,600 millidarcy feet which seems unreasonably high. The difficulty associated with the interpretation of the buildup data is to be attributed to the masking effects of earth tides.

(4) Summary of test results: The reservoir parameters, as computed from the different tests, are summarized in Table 3. As can be seen from the table, the long duration interference test has indicated a kH of approximately 225,000 millidarcy feet and a ϕcH of about 1×10^{-3} for the large portion of the reservoir included between the two wells RRGE 1 and RRGE 2. If we assume a compressibility value of 1×10^{-5} psi⁻¹ for the rock matrix and an overall porosity of 0.1, then the thickness of the producing horizon works out to about 1000 feet, which seems reasonable from available geological data. This would, in turn, imply an overall average permeability of about 225 millidarcy for the reservoir material which is a satisfactory value.



XBL769 - 4036

Fig. 18: Short-term production test, RRGE 1: Build up as a function of $\log t/t'$.

Both the short-term tests have indicated somewhat lower values of kH than the interference test. The computation of the storage parameter, ϕcH , from the short term tests has been rendered difficult due to lack of information on the effective well radius.

The short term test on RRGE 2 has indicated a fairly low value of kH ($\approx 50,000$ millidarcy feet), probably indicating a region of low permeability close to that well. The short term test on RRGE 1 has indicated a kH value ($\approx 130,000$ millidarcy feet) which is much closer to the interference test results, indicating that the reservoir material near that well is much closer to the overall reservoir in respect of permeability.

The interference test has definitely indicated that the reservoir has a barrier boundary that is effectively equivalent to an image well located 12,000 feet from RRGE 1. The precise determination of the location of a hydrological boundary is a problem of triangulation and hence, with only two wells available for testing, it is at present not possible to locate the position of the boundary.

The short term test on RRGE 2 has also indicated the presence of a barrier boundary (or boundaries?) very close to that well, possibly within a few hundred feet. Whether this boundary is indicative of the Bridge Fault which supposedly lies close to RRGE 2 at depth, is uncertain. Alternatively, the possibility exists that the departures observed from the ideal behavior in the short term test data may not be indicative of barrier boundary effects but may be due to other causes such as variation of discharge or commingling of different producing zones.

SUMMARY, CONCLUSIONS AND RECOMMENDATIONS

The Raft River Valley geothermal field is located on a faulted graben filled with sediments ranging in age from Mio-Pliocene (the Salt Lake formation) to Pleistocene (the Raft River formation) with a total thickness of about 5000 feet. The sediments rest on a basement of Adamellite, with an intervening zone of metamorphic rocks, about 200 feet thick.

The successful geothermal wells, RRGE 1 and RRGE 2, have indicated that the geothermal reservoir occurs at the base of the Salt Lake formation and that the producing horizon is probably about 1000 feet thick, extending from about 3600 feet to about 4800 feet. The reservoir temperature is approximately 294°F (146°C).

Three hydraulic tests were conducted to estimate the production parameters of the reservoir. The primary task of these tests was the careful and accurate measurement of water pressure changes in the wells. Towards this end, successful use was made of a sensitive quartz pressure gage, capable of an accuracy of 0.01 psi over an absolute pressure range of 0 - 10,000 psi and with a temperature tolerance of up to 300°F. The tests also showed that a less expensive quartz pressure gage, capable of measuring only wellhead pressures, provides a useful alternative to the more expensive down-hole gage when one is interested only in accurately monitoring wellhead pressure changes in a shut-in observation well.

The data collected during the tests have revealed the interesting fact that the reservoir responds systematically to the small changes in the earth's gravitational field induced by the paths

TABLE 3

TEST	DRAWDOWN		BUILDUP	
	Log-log plot	Semi-log plot		
Short term * production test, RRGE 2	kH md-feet	47,600	47,300	49,900
	ϕcH ft/psi	2.91×10^{-2} ($r_w = 1$ ft)	3.03×10^{-2} ($r_w = 1$ ft)	
Long term ** interference test	kH md-feet	228,000	228,000	193,000 (210,000 by semi-log plot)
	ϕcH ft/psi	1.19×10^{-3}	9.38×10^{-4}	1.06×10^{-3} (8.20×10^{-4} by semi-log plot)
Short term production test, RRGE 1	kH md-feet	105,000	132,000	67,500 (?)
	ϕcH ft/psi	2.56×10^{-2} ($r_w = 1$ ft)	7.2×10^{-3} ($r_w = 1$ ft)	

* This test indicated the possible presence of a barrier boundary in the vicinity of RRGE 2.

** This test indicated the possible presence of a barrier boundary, equivalent to an image well located about 12,000 feet from RRGE 1.

of the sun and the moon. Appropriate corrections had to be made for these earth tide effects before one could interpret the pressure transient data for the reservoir production parameters.

The long duration interference test has shown that the geothermal reservoir at the Raft River site is in general highly transmissible, with a kH of about 225,000 millidarcy feet. Assuming a total thickness of 1000 feet for the reservoir, this suggests an average reservoir permeability of 225 millidarcy. The interference test has also shown that the geothermal reservoir is bounded in some direction. With only two wells available for testing, it is not at present possible to precisely locate this boundary.

The short duration production tests indicated that the reservoir is probably less permeable in the vicinity of RRGE 2 and that a barrier boundary (Bridge fault?) may be present within a few hundred feet of RRGE 2.

The reservoir tests so far conducted have definitely established that the geothermal reservoir in the Raft River valley is fairly extensive and significantly permeable. The reservoir, therefore, merits further exploration. From the point of view of reservoir assessment, an important question is that of reservoir geometry. In order to accurately determine the location of the barrier boundaries that have been indicated by the tests so far conducted, it is necessary to have additional wells. From available geological information, a favorable location for a third geothermal well would be a site one to two miles southeast of the existing wells, towards the center of the valley.

ACKNOWLEDGMENTS

Dr. Jay Kunz and Messrs. Lowell Miller, Roger Stoker, Gregg Mines, Don Suckling and Gary Cooper of the Idaho National Engineering Laboratory provided the necessary field assistance and facilities in the successful completion of the tests. During the early stages of the tests, Dr. George Miller, Oil Instruments Ltd., helped initiate the use of the downhole quartz pressure gauge. Ms. Jeanette Mullaney of Lawrence Berkeley Laboratory assisted with the processing of field data.

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APPENDIX 1

RRGE 2 SHORT-TERM TEST DATA.

RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

RISE 2 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE	TIME	FLOW RATE / (GPM) / (PSIA) / (PSIA)	WELL HEAD / PRESSURE / (PSIA) / (PSIA)	REMARKS
09/12/75	211406	2287.97		
09/12/75	211416	2288.00		
09/12/75	211420	2288.01		
09/12/75	211430	2288.03		
09/12/75	211440	2288.05		
09/12/75	211450	2288.02		
09/12/75	211500	2288.02		
09/12/75	211500	2288.00		
09/12/75	211700	2288.08		
09/12/75	211800	2288.06		
09/12/75	211900	2288.11		
09/12/75	212000	2288.12		
09/12/75	212000	2288.16		
09/12/75	212300	2288.16		
09/12/75	212342	2288.13		
09/12/75	212346	2288.13		
09/12/75	212348	2288.15		
09/12/75	212349	2288.13		
09/12/75	212340	2288.13		
09/12/75	212350	2288.16		
09/12/75	212351	2288.15		
09/12/75	212352	2288.13		
09/12/75	212353	2288.15		
09/12/75	212354	2288.13		
09/12/75	212355	2288.16		
09/12/75	212356	2288.15		
09/12/75	212358	2288.12		
09/12/75	212359	2288.16		
09/12/75	212400	2288.13		
09/12/75	212401	2288.13		
09/12/75	212402	2288.15		
09/12/75	212403	2288.15		
09/12/75	212406	2288.15		
09/12/75	212406	2288.16		
09/12/75	212407	2288.16		
09/12/75	212408	2288.16		
09/12/75	212410	2288.15		
09/12/75	212411	2288.12		
09/12/75	212412	2288.15		
09/12/75	212413	2288.12		
09/12/75	212417	2288.14		
09/12/75	212419	2288.14		
09/12/75	212419	2288.13		
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09/12/75	212428	2288.13		
09/12/75	212430	2288.16		
09/12/75	212431	2288.14		
09/12/75	212432	2288.16		
09/12/75	212433	2288.13		
09/12/75	212436	2288.15		
09/12/75	212438	2288.16		
09/12/75	212438	2288.15		
09/12/75	212439	2288.15		
09/12/75	212440	2288.13		
09/12/75	212441	2288.16		
09/12/75	212442	2288.16		
09/12/75	212443	2288.13		
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09/12/75	212457	2288.16		
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09/12/75	212459	2288.16		
09/12/75	212500	2288.15		
09/12/75	212501	2288.16		
09/12/75	212502	2288.15		
09/12/75	212503	2288.16		
09/12/75	212504	2288.15		
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09/12/75	212506	2288.15		
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09/12/75	212508	2288.15		
09/12/75	212509	2288.15		
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09/12/75	212595	2288.12		
09/12/75	212596	2288.12		
09/12/75	212597	2288.12		
09/12/75	212598	2288.12		
09/12/75	212599	2288.12		
09/12/75	212600	2288.12		
09/12/75	212601	2288.12		
09/12/75	212602	2288.12		
09/12/75	212603	2288.12		

VALUE OPENED FOR PRODUCTION, PLONMATEC10 GPM.

ASSUMED ZERO TIME FOR PRESSURE DRAWDOWN.

RAGE 2 SHORT-TERM TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE	TIME	FLOW RATE / (GPM)	DOWNHOLE PRESSURE / (PSIA)	WELL HEAD PRESSURE / (PSIA)	REMARKS
19/12/75	21560.4	2269.07			
19/12/75	21560.0	2269.01			
19/12/75	21560.7	2268.96			
19/12/75	21560.9	2268.97			
19/12/75	21561.0	2268.95			
19/12/75	21561.1	2268.92			
19/12/75	21561.2	2268.90			
19/12/75	21561.3	2268.87			
19/12/75	21561.4	2268.83			
19/12/75	21561.5	2268.87			
19/12/75	21561.6	2268.86			
19/12/75	21561.7	2268.82			
19/12/75	21561.8	2268.82			
19/12/75	21561.9	2268.81			
19/12/75	21562.0	2268.80			
19/12/75	21562.1	2268.79			
19/12/75	21562.2	2268.77			
19/12/75	21562.3	2268.74			
19/12/75	21562.4	2268.71			
19/12/75	21562.5	2268.67			
19/12/75	21562.6	2268.62			
19/12/75	21562.7	2268.57			
19/12/75	21562.8	2268.52			
19/12/75	21562.9	2268.47			
19/12/75	21563.0	2268.41			
19/12/75	21563.1	2268.36			
19/12/75	21563.2	2268.31			
19/12/75	21563.3	2268.26			
19/12/75	21563.4	2268.21			
19/12/75	21563.5	2268.16			
19/12/75	21563.6	2268.11			
19/12/75	21563.7	2268.06			
19/12/75	21563.8	2268.01			
19/12/75	21563.9	2267.96			
19/12/75	21564.0	2267.91			
19/12/75	21564.1	2267.86			
19/12/75	21564.2	2267.81			
19/12/75	21564.3	2267.76			
19/12/75	21564.4	2267.71			
19/12/75	21564.5	2267.66			
19/12/75	21564.6	2267.61			
19/12/75	21564.7	2267.56			
19/12/75	21564.8	2267.51			
19/12/75	21564.9	2267.46			
19/12/75	21565.0	2267.41			
19/12/75	21565.1	2267.36			
19/12/75	21565.2	2267.31			
19/12/75	21565.3	2267.26			
19/12/75	21565.4	2267.21			
19/12/75	21565.5	2267.16			
19/12/75	21565.6	2267.11			
19/12/75	21565.7	2267.06			
19/12/75	21565.8	2267.01			
19/12/75	21565.9	2266.96			
19/12/75	21566.0	2266.91			
19/12/75	21566.1	2266.86			
19/12/75	21566.2	2266.81			
19/12/75	21566.3	2266.76			
19/12/75	21566.4	2266.71			
19/12/75	21566.5	2266.66			
19/12/75	21566.6	2266.61			
19/12/75	21566.7	2266.56			
19/12/75	21566.8	2266.51			
19/12/75	21566.9	2266.46			
19/12/75	21567.0	2266.41			
19/12/75	21567.1	2266.36			
19/12/75	21567.2	2266.31			
19/12/75	21567.3	2266.26			
19/12/75	21567.4	2266.21			
19/12/75	21567.5	2266.16			
19/12/75	21567.6	2266.11			
19/12/75	21567.7	2266.06			
19/12/75	21567.8	2266.01			
19/12/75	21567.9	2265.96			
19/12/75	21568.0	2265.91			
19/12/75	21568.1	2265.86			
19/12/75	21568.2	2265.81			
19/12/75	21568.3	2265.76			
19/12/75	21568.4	2265.71			
19/12/75	21568.5	2265.66			
19/12/75	21568.6	2265.61			
19/12/75	21568.7	2265.56			
19/12/75	21568.8	2265.51			
19/12/75	21568.9	2265.46			
19/12/75	21569.0	2265.41			
19/12/75	21569.1	2265.36			
19/12/75	21569.2	2265.31			
19/12/75	21569.3	2265.26			
19/12/75	21569.4	2265.21			
19/12/75	21569.5	2265.16			
19/12/75	21569.6	2265.11			
19/12/75	21569.7	2265.06			
19/12/75	21569.8	2265.01			
19/12/75	21569.9	2264.96			
19/12/75	21570.0	2264.91			
19/12/75	21570.1	2264.86			
19/12/75	21570.2	2264.81			
19/12/75	21570.3	2264.76			
19/12/75	21570.4	2264.71			
19/12/75	21570.5	2264.66			
19/12/75	21570.6	2264.61			
19/12/75	21570.7	2264.56			
19/12/75	21570.8	2264.51			
19/12/75	21570.9	2264.46			
19/12/75	21571.0	2264.41			
19/12/75	21571.1	2264.36			
19/12/75	21571.2	2264.31			
19/12/75	21571.3	2264.26			
19/12/75	21571.4	2264.21			
19/12/75	21571.5	2264.16			
19/12/75	21571.6	2264.11			
19/12/75	21571.7	2264.06			
19/12/75	21571.8	2264.01			
19/12/75	21571.9	2263.96			
19/12/75	21572.0	2263.91			
19/12/75	21572.1	2263.86			
19/12/75	21572.2	2263.81			
19/12/75	21572.3	2263.76			
19/12/75	21572.4	2263.71			
19/12/75	21572.5	2263.66			
19/12/75	21572.6	2263.61			
19/12/75	21572.7	2263.56			
19/12/75	21572.8	2263.51			
19/12/75	21572.9	2263.46			
19/12/75	21573.0	2263.41			
19/12/75	21573.1	2263.36			
19/12/75	21573.2	2263.31			
19/12/75	21573.3	2263.26			
19/12/75	21573.4	2263.21			
19/12/75	21573.5	2263.16			
19/12/75	21573.6	2263.11			
19/12/75	21573.7	2263.06			
19/12/75	21573.8	2263.01			
19/12/75	21573.9	2262.96			
19/12/75	21574.0	2262.91			
19/12/75	21574.1	2262.86			
19/12/75	21574.2	2262.81			
19/12/75	21574.3	2262.76			
19/12/75	21574.4	2262.71			
19/12/75	21574.5	2262.66			
19/12/75	21574.6	2262.61			
19/12/75	21574.7	2262.56			
19/12/75	21574.8	2262.51			
19/12/75	21574.9	2262.46			
19/12/75	21575.0	2262.41			
19/12/75	21575.1	2262.36			
19/12/75	21575.2	2262.31			
19/12/75	21575.3	2262.26			
19/12/75	21575.4	2262.21			
19/12/75	21575.5	2262.16			
19/12/75	21575.6	2262.11			
19/12/75	21575.7	2262.06			
19/12/75	21575.8	2262.01			
19/12/75	21575.9	2261.96			
19/12/75	21576.0	2261.91			
19/12/75	21576.1	2261.86			
19/12/75	21576.2	2261.81			
19/12/75	21576.3	2261.76			
19/12/75	21576.4	2261.71			
19/12/75	21576.5	2261.66			
19/12/75	21576.6	2261.61			
19/12/75	21576.7	2261.56			
19/12/75	21576.8	2261.51			
19/12/75	21576.9	2261.46			
19/12/75	21577.0	2261.41			
19/12/75	21577.1	2261.36			
19/12/75	21577.2	2261.31			
19/12/75	21577.3	2261.26			
19/12/75	21577.4	2261.21			
19/12/75	21577.5	2261.16			
19/12/75	21577.6	2261.11			
19/12/75	21577.7	2261.06			
19/12/75	21577.8	2261.01			
19/12/75	21577.9	2260.96			
19/12/75	21578.0	2260.91			
19/12/75	21578.1	2260.86			
19/12/75	21578.2	2260.81			
19/12/75	21578.3	2260.76			
19/12/75	21578.4	2260.71			
19/12/75	21578.5	2260.66			
19/12/75	21578.6	2260.61			
19/12/75	21578.7	2260.56			
19/12/75	21578.8	2260.51			
19/12/75	21578.9	2260.46			
19/12/75	21579.0	2260.41			
19/12/75	21579.1	2260.36			
19/12/75	21579.2	2260.31			
19/12/75	21579.3	2260.26			
19/12/75	21579.4	2260.21			
19/12/75	21579.5	2260.16			
19/12/75	21579.6	2260.11			
19/12/75	21579.7	2260.06			
19/12/75	21579.8	2260.01			
19/12/75	21579.9	2259.96			
19/12/75	21580.0	2259.91			
19/12/75	21580.1	2259.86			
19/12/75	21580.2	2259.81			
19/12/75	21580.3	2259.76			
19/12/75	21580.4	2259.71			
19/12/75	21580.5	2259.66			
19/12/75	21580.6	2259.61			
19/12/75	21580.7	2259.56			
19/12/75	21580.8	2259.51			
19/12/75	21580.9	2259.46			
19/12/75	21581.0	2259.41			
19/12/75	21581.1	2259.36			
19/12/75	21581.2	2259.31			
19/12/75	21581.3	2259.26			
19/12/75	21581.4	2259.21			
19/12/75	21581.5	2259.16			
19/12/75	21581.6	2259.11			
19/12/75	21581.7	2259.06			
19/12/75	21581.8	2259.01			
19/12/75	21581.9	2258.96			
19/12/75	21582.0	2258.91			
19/12/75	21582.1	2258.86			
19/12/75	21582.2	2258.81			
19/12/75	21582.3	2258.76			
19/12/75	21582.4	2258.71			
19/12/75	21582.5	2258.66			
19/12/75	21582.6	2258.61			
19/12/75	21582.7	2258.56			
19/12/75	21582.8	2258.51			
19/12/75	21582.9	2258.46			
19/12/75	21583.0	2258.41			
19/12/75	21583.1				

RAGE 2 SHORT-TERM TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE /	TIME /	FLOW RATE /	DOWNHOLE /	WELL HEAD /	REMARKS	DATE /	TIME /	FLOW RATE /	DOWNHOLE /	WELL HEAD /	REMARKS
/	/	(GPM) /	PRESSURE /	PRESSURE /		/	/	(GPM) /	PRESSURE /	PRESSURE /	
/	/	(PSIA) /	(PSIA) /	(PSIA) /		/	/	(PSIA) /	(PSIA) /	(PSIA) /	
09/12/75	213910	2282.20				09/12/75	221900				2277.90
09/12/75	213920	2282.19				09/12/75	221950				2277.79
09/12/75	213930	2282.16				09/12/75	222000				2277.69
09/12/75	213940	2282.15				09/12/75	222050				2277.58
09/12/75	213950	2282.06				09/12/75	222100				2277.46
09/12/75	214000	2282.02				09/12/75	222150				2277.32
09/12/75	214010	2282.07				09/12/75	222200				2277.20
09/12/75	214020	2282.03				09/12/75	222250				2277.10
09/12/75	214030	2282.01				09/12/75	222300				2276.99
09/12/75	214040	2282.00				09/12/75	222350				2276.89
09/12/75	214050	2282.00				09/12/75	222400				2276.76
09/12/75	214100	2282.00				09/12/75	222450				2276.64
09/12/75	214110	2282.07				09/12/75	222500				2276.53
09/12/75	214120	2282.07				09/12/75	222550				2276.46
09/12/75	214130	2282.07				09/12/75	222600				2276.35
09/12/75	214140	2282.07				09/12/75	222650				2276.24
09/12/75	214150	2282.07				09/12/75	222700				2276.17
09/12/75	214200	2282.07				09/12/75	222750				2276.09
09/12/75	214210	2282.07				09/12/75	222800				2276.02
09/12/75	214220	2282.07				09/12/75	222850				2275.92
09/12/75	214230	2282.07				09/12/75	222900				2275.83
09/12/75	214240	2282.07				09/12/75	222950				2275.74
09/12/75	214250	2282.07				09/12/75	223000				2275.64
09/12/75	214300	2282.07				09/12/75	223050				2275.53
09/12/75	214310	2282.07				09/12/75	223100				2275.41
09/12/75	214320	2282.07				09/12/75	223150				2275.30
09/12/75	214330	2282.07				09/12/75	223200				2275.17
09/12/75	214340	2282.07				09/12/75	223250				2275.06
09/12/75	214350	2282.07				09/12/75	223300				2274.92
09/12/75	214360	2282.07				09/12/75	223350				2274.81
09/12/75	214370	2282.07				09/12/75	223400				2274.71
09/12/75	214380	2282.07				09/12/75	223450				2274.61
09/12/75	214390	2282.07				09/12/75	223500				2274.50
09/12/75	214400	2282.07				09/12/75	223550				2274.41
09/12/75	214410	2282.07				09/12/75	223600				2274.31
09/12/75	214420	2282.07				09/12/75	223650				2274.22
09/12/75	214430	2282.07				09/12/75	223700				2274.13
09/12/75	214440	2282.07				09/12/75	223750				2274.03
09/12/75	214450	2282.07				09/12/75	223800				2273.95
09/12/75	214460	2282.07				09/12/75	223850				2273.83
09/12/75	214470	2282.07				09/12/75	223900				2273.71
09/12/75	214480	2282.07				09/12/75	223950				2273.63
09/12/75	214490	2282.07				09/12/75	224000				2273.55
09/12/75	214500	2282.07				09/12/75	224050				2273.46
09/12/75	214510	2282.07				09/12/75	224100				2273.36
09/12/75	214520	2282.07				09/12/75	224150				2273.27
09/12/75	214530	2282.07				09/12/75	224200				2273.15
09/12/75	214540	2282.07				09/12/75	224250				2273.06
09/12/75	214550	2282.07				09/12/75	224300				2272.92
09/12/75	214560	2282.07				09/12/75	224350				2272.81
09/12/75	214570	2282.07				09/12/75	224400				2272.71
09/12/75	214580	2282.07				09/12/75	224450				2272.62
09/12/75	214590	2282.07				09/12/75	224500				2272.53
09/12/75	214600	2282.07				09/12/75	224550				2272.44
09/12/75	214610	2282.07				09/12/75	224600				2272.35
09/12/75	214620	2282.07				09/12/75	224650				2272.26
09/12/75	214630	2282.07				09/12/75	224700				2272.17
09/12/75	214640	2282.07				09/12/75	224750				2272.08
09/12/75	214650	2282.07				09/12/75	224800				2271.99
09/12/75	214660	2282.07				09/12/75	224850				2271.90
09/12/75	214670	2282.07				09/12/75	224900				2271.81
09/12/75	214680	2282.07				09/12/75	224950				2271.71
09/12/75	214690	2282.07				09/12/75	225000				2271.62
09/12/75	214700	2282.07				09/12/75	225050				2271.53
09/12/75	214710	2282.07				09/12/75	225100				2271.44
09/12/75	214720	2282.07				09/12/75	225150				2271.35
09/12/75	214730	2282.07				09/12/75	225200				2271.26
09/12/75	214740	2282.07				09/12/75	225250				2271.17
09/12/75	214750	2282.07				09/12/75	225300				2271.08
09/12/75	214760	2282.07				09/12/75	225350				2270.99
09/12/75	214770	2282.07				09/12/75	225400				2270.90
09/12/75	214780	2282.07				09/12/75	225450				2270.81
09/12/75	214790	2282.07				09/12/75	225500				2270.71
09/12/75	214800	2282.07				09/12/75	225550				2270.62
09/12/75	214810	2282.07				09/12/75	225600				2270.53
09/12/75	214820	2282.07				09/12/75	225650				2270.44
09/12/75	214830	2282.07				09/12/75	225700				2270.35
09/12/75	214840	2282.07				09/12/75	225750				2270.26
09/12/75	214850	2282.07				09/12/75	225800				2270.17
09/12/75	214860	2282.07				09/12/75	225850				2270.08
09/12/75	214870	2282.07				09/12/75	225900				2270.00
09/12/75	214880	2282.07				09/12/75	225950				2269.91
09/12/75	214890	2282.07				09/12/75	226000				2269.82
09/12/75	214900	2282.07				09/12/75	226050				2269.73
09/12/75	214910	2282.07				09/12/75	226100				2269.64
09/12/75	214920	2282.07				09/12/75	226150				2269.55
09/12/75	214930	2282.07				09/12/75	226200				2269.46
09/12/75	214940	2282.07				09/12/75	226250				2269.37
09/12/75	214950	2282.07				09/12/75	226300				2269.28
09/12/75	214960	2282.07				09/12/75	226350				2269.19
09/12/75	214970	2282.07				09/12/75	226400				2269.10
09/12/75	214980	2282.07				09/12/75	226450				2269.01
09/12/75	214990	2282.07				09/12/75	226500				2268.92
09/12/75	215000	2282.07				09/12/75	226550				2268.83
09/12/75	215010	2282.07				09/12/75	226600				2268.74
09/12/75	215020	2282.07				09/12/75	226650				2268.65
09/12/75	215030	2282.07				09/12/75	226700				2268.56
09/12/75	215040	2282.07				09/12/75	226750				2268.47
09/12/75	215050	2282.07				09/12/75	226800				2268.38
09/12/75	215060	2282.07				09/12/75	226850				2268.29
09/12/75	215070	2282.07				09/12/75	226900				2268.20
09/12/75	215080	2282.07				09/12/75	226950				2268.11
09/12/75	215090	2282.07				09/12/75	227000				2268.02
09/12/75	215100	2282.07				09/12/75	227050				2267.93
09/12/75	215110	2282.07				09/12/75	227100				2267.84
09/12/75	215120	2282.07				09/12/75	227150				2267.75
09/12/75	215130	2282.07				09/12/75	227200				2267.66
09/12/75	215140	2282.07				09/12/75	227250				2267.57
09/12/75	215150	2282.07				09/12/75	227300				2267.48
09/12/75	215160	2282.07				09/12/75	227350				2267.39
09/12/75	215170	2282.07				09/12/75	227400				2267.30
09/12/75	215180	2282.07				09/12/75	227450				2267.21
09/12/75	215190	2282.07				09/12/75	227500				2267.12
09/12/75	215200	2282.07				09/12/75	227550				2267.03
09/12/75	215210	2282.07				09/12/75	227600				2266.94
09/12/75	215220	2282.07				09/12/75	227650				2266.85
09/12/75	215230	2282.07				09/12/75	227700				2266.76
09/12/75	215240	2282.07				09/12/75	227750				2266.67
09/12/75	21										

LOG 2 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE	TIME	FLOW RATE (GPM)	DOWNHOLE / WELL HEAD / PRESSURE / PRESSURE / (PSIA) / (PSIA) /	REMARKS	DATE	TIME	FLOW RATE (GPM)	DOWNHOLE / WELL HEAD / PRESSURE / PRESSURE / (PSIA) / (PSIA) /	REMARKS
09/13/75	122910	2273.13			09/13/75	133700			2282.45
09/13/75	122920	2273.21			09/13/75	133830			2282.53
09/13/75	122930	2273.27			09/13/75	133900			2282.58
09/13/75	122940	2273.30			09/13/75	134000			2282.62
09/13/75	122950	2273.63			09/13/75	134100			2282.70
09/13/75	123000	2273.56			09/13/75	134200			2282.76
09/13/75	123010	2273.59			09/13/75	134300			2282.85
09/13/75	123020	2273.60			09/13/75	134400			2282.89
09/13/75	123030	2273.76			09/13/75	134500			2282.93
09/13/75	123040	2273.82			09/13/75	134600			2282.98
09/13/75	123050	2273.80			09/13/75	134700			2283.06
09/13/75	123100	2273.76			09/13/75	134800			2283.12
09/13/75	123110	2273.70			09/13/75	134900			2283.16
09/13/75	123120	2274.17			09/13/75	135000			2283.19
09/13/75	123130	2274.69			09/13/75	135100			2283.23
09/13/75	123140	2275.02			09/13/75	135200			2283.31
09/13/75	123150	2275.11			09/13/75	135300			2283.37
09/13/75	123160	2275.22			09/13/75	135400			2283.43
09/13/75	123170	2275.77			09/13/75	135500			2283.49
09/13/75	123180	2276.02			09/13/75	135600			2283.52
09/13/75	123190	2276.28			09/13/75	135700			2283.60
09/13/75	124000	2276.40			09/13/75	135800			2283.63
09/13/75	124100	2276.59			09/13/75	135900			2283.64
09/13/75	124200	2276.78			09/13/75	140000			2283.68
09/13/75	124300	2276.96			09/13/75	140100			2283.76
09/13/75	124400	2277.13			09/13/75	140200			2283.81
09/13/75	124500	2277.83			09/13/75	140300			2283.80
09/13/75	124600	2278.17			09/13/75	140400			2283.92
09/13/75	124700	2278.36			09/13/75	140441			2283.95
09/13/75	124800	2278.36							
09/13/75	125400	2278.61							
09/13/75	125500	2278.80							
09/13/75	125600	2279.12							
09/13/75	125700	2279.38							
09/13/75	125800	2279.47							
09/13/75	130200	2279.59							
09/13/75	130300	2279.70							
09/13/75	130400	2279.82							
09/13/75	130500	2279.95							
09/13/75	130600	2280.04							
09/13/75	130700	2280.17							
09/13/75	130800	2280.22							
09/13/75	130900	2280.32							
09/13/75	131036	2280.40							
09/13/75	131100	2280.49							
09/13/75	131200	2280.56							
09/13/75	131300	2280.67							
09/13/75	131400	2280.77							
09/13/75	131500	2280.86							
09/13/75	131600	2280.94							
09/13/75	131700	2281.02							
09/13/75	131800	2281.10							
09/13/75	131900	2281.17							
09/13/75	132000	2281.24							
09/13/75	132100	2281.33							
09/13/75	132200	2281.43							
09/13/75	132300	2281.50							
09/13/75	132400	2281.57							
09/13/75	132500	2281.63							
09/13/75	132600	2281.70							
09/13/75	132700	2281.80							
09/13/75	132800	2281.86							
09/13/75	132900	2281.92							
09/13/75	133000	2282.01							
09/13/75	133100	2282.07							
09/13/75	133200	2282.14							
09/13/75	133300	2282.20							
09/13/75	133400	2282.24							
09/13/75	133500	2282.31							
09/13/75	133600	2282.35							

END OF DATA

APPENDIX 2

RRGE 1 INTERFERENCE TEST DATA.

RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

RACE 1 INTERFERENCE TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / BELL HEAD / PRESSURE / (PSIA) /	REMARKS	DATE / /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / BELL HEAD / PRESSURE / (PSIA) /	REMARKS
9/15/75	1720	575	82	150-405	9/15/75	2120	450	575-036	
9/15/75	1730	575	86		9/15/75	2200	450	575-024	
9/15/75	1740	575	86		9/15/75	2200	450	575-017	
9/15/75	1750	575	86		9/15/75	2300	450	575-005	
9/15/75	1800	575	89		9/15/75	0000	450	575-010	.681
9/15/75	1810	575	86		9/15/75	0300	450	575-008	
9/15/75	1820	575	86		9/15/75	0400	450	575-011	
9/15/75	1830	575	86		9/15/75	0130	450	575-002	
9/15/75	1840	575	86		9/15/75	0200	450	575-001	
9/15/75	1850	575	83		9/15/75	0830	450	575-005	
9/15/75	1900	575	820		9/15/75	0300	450	575-010	
9/15/75	1910	575	820		9/15/75	0330	450	575-016	
9/15/75	1920	575	825		9/15/75	0400	450	575-009	
				PRODUCTION STOPPED AT	9/15/75	0630	450	574-905	
9/15/75	1930	575	822		9/15/75	0900	450	574-986	
9/15/75	2000	575	785		9/15/75	0930	450	574-972	
9/15/75	2030	575	752		9/15/75	0800	450	574-956	
9/15/75	2110	575	752		9/15/75	0830	450	574-932	
9/15/75	2130	575	752		9/15/75	0700	450	574-906	
9/15/75	2140	575	729		9/15/75	0230	450	574-890	
9/15/75	2200	575	706		9/15/75	0300	453	574-851	.427
9/15/75	2230	575	713		9/15/75	0330	453	574-830	
9/15/75	2300	575	683		9/15/75	0900	453	574-822	
9/15/75	2308	575	683		9/15/75	0930	453	574-792	
9/15/75	2330	575	712		9/15/75	1000	453	574-779	
9/15/75	0000	575	685		9/15/75	1030	453	574-757	.368
9/15/75	0030	575	659		9/15/75	1100	453	574-747	
9/15/75	0100	575	646		9/15/75	1130	453	574-734	
9/15/75	0110	575	630		9/15/75	1200	453	574-737	.373
9/15/75	0200	575	622		9/15/75	1300	453	574-728	
9/15/75	0230	575	600		9/15/75	1330	453	574-733	.449
9/15/75	0300	575	593		9/15/75	1400	453	574-732	
9/15/75	0330	575	581		9/15/75	1430	453	574-708	
9/15/75	0400	575	565		9/15/75	1500	453	574-759	
9/15/75	0430	575	545		9/15/75	1530	453	574-751	.487
9/15/75	0500	575	518		9/15/75	1600	453	574-745	
9/15/75	0530	575	493		9/15/75	1630	453	574-747	.492
9/15/75	0600	575	471		9/15/75	1700	453	574-752	1.49-4.605
9/15/75	0630	575	437		9/15/75	1730	453	574-756	
9/15/75	0700	575	387		9/15/75	1800	453	574-732	.422
9/15/75	0800	575	354		9/15/75	1830	453	574-715	
9/15/75	0830	575	337		9/15/75	1900	453	574-698	
9/15/75	0900	575	303		9/15/75	2000	453	574-687	.314
9/15/75	0930	575	283		9/15/75	2030	437	574-661	
9/15/75	1000	575	253		9/15/75	2100	437	574-642	
9/15/75	1030	575	249		9/15/75	2130	437	574-628	
9/15/75	1100	575	236		9/15/75	2200	442	574-616	
9/15/75	1130	575	224		9/15/75	2300	442	574-602	.211
9/15/75	1200	575	216		9/15/75	2330	442	574-588	.166
9/15/75	1230	575	212		9/15/75	2300	442	574-575	
9/15/75	1300	575	210		9/15/75	0300	442	574-562	
9/15/75	1330	575	203		9/15/75	0330	442	574-552	
9/15/75	1400	575	200		9/15/75	0400	442	574-500	
9/15/75	1430	575	214		9/15/75	0430	442	574-507	
9/15/75	1500	575	210		9/15/75	0500	442	574-506	
9/15/75	1530	575	208		9/15/75	0530	442	574-506	
9/15/75	1600	575	206	1.49-0.892	9/15/75	0600	442	574-500	
9/15/75	1630	575	206		9/15/75	0630	442	574-500	
9/15/75	1700	575	195		9/15/75	0600	442	574-502	.033
9/15/75	1730	575	186		9/15/75	0630	442	574-502	
9/15/75	1800	575	172		9/15/75	0700	442	574-503	
9/15/75	1830	575	155		9/15/75	0730	442	574-523	
9/15/75	1900	575	145		9/15/75	0800	442	574-503	.049
9/15/75	1930	575	127						
9/15/75	2000	575	96						
9/15/75	2030	575	86						
9/15/75	2100	575	83	.757					
9/15/75	2130	575	83						

PRODUCTION STOPPED AT

ORGE 2

.394

AT 2310 HRS. LEAKAGE IN

FLANGE STOPPED (MP).

.232

1.49-0.951

.849

1.49-0.892

.757

RAGE 1 INTERFERENCE TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / TIME / FLOW RATE / ODHOLE / WELL HEAD / REMARKS				DATE / TIME / FLOW RATE / ODHOLE / WELL HEAD / REMARKS							
DATE	TIME	FLOW RATE / (GPM)	ODHOLE / (PSIA)	WELL HEAD / (PSIA)	REMARKS	DATE	TIME	FLOW RATE / (GPM)	ODHOLE / (PSIA)	WELL HEAD / (PSIA)	REMARKS
9/17/75	0430	442	574.472			9/17/75	2130	437	574.319		
9/17/75	0900	437	574.455			9/17/75	2156	437	574.318		
9/17/75	0930	437	574.429		.811	9/17/75	2156	437	574.322		146.941
9/17/75	1000	437	574.399			9/17/75	2200	437	574.315		
9/17/75	1030	437	574.383			9/17/75	2210	437	574.300		
9/17/75	1100	437	574.360			9/17/75	2220	437	574.303		
9/17/75	1130	437	574.356			9/17/75	2230	437	574.295		
9/17/75	1200	437	574.351		148.979	9/17/75	2240	437	574.291		
9/17/75	1300	437	574.347			9/17/75	2250	437	574.287		
9/17/75	1300	437	574.346			9/17/75	2300	437	574.285		146.795
9/17/75	1330	437	574.340			9/17/75	2300	437	574.280		
9/17/75	1400	437	574.333		149.086	9/18/75	0700	437	574.250		
9/17/75	1430	437	574.328			9/18/75	0730	437	574.249		
9/17/75	1500	437	574.324		.109	9/18/75	0800	437	574.248		
9/17/75	1530	437	574.316			9/18/75	0100	437	574.203		
9/17/75	1600	437	574.313			9/18/75	0130	437	574.216		
9/17/75	1630	437	574.308		.116	9/18/75	0200	437	574.339		
9/17/75	1700	437	574.309		.109	9/18/75	0230	437	574.319		
9/17/75	1730	437	574.301		.098	9/18/75	0300	437	574.379		
9/17/75	1800	437	574.302		.082	9/18/75	0330	437	574.402		
9/17/75	1800	437	574.302			9/18/75	0400	437	574.420		
9/17/75	1900	437	574.302		.482RAGE 2 SHUT IN. 20 SEC SHUT IN TIME.	9/18/75	0430	437	574.420		
9/17/75	1801	437	574.300			9/18/75	0500	437	574.435		.995
9/17/75	1802	437	574.301		149.076	9/18/75	0530	437	574.450		.930
9/17/75	1803	437	574.300			9/18/75	0600	437	574.457		.963
9/17/75	1804	437	574.300			9/18/75	0630	437	574.467		.966
9/17/75	1805	437	574.300			9/18/75	0700	437	574.461		
9/17/75	1806	437	574.300			9/18/75	0730	437	574.429		.966
9/17/75	1807	437	574.300			9/18/75	0800	437	574.418		.979
9/17/75	1808	437	574.300			9/18/75	0830	437	574.399		
9/17/75	1809	437	574.300			9/18/75	0900	437	574.391		
9/17/75	1810	437	574.300			9/18/75	0930	437	574.377		.995
9/17/75	1811	437	574.300		149.076	9/18/75	1000	437	574.366		.930
9/17/75	1812	437	574.300			9/18/75	1030	437	574.357		.963
9/17/75	1813	437	574.300			9/18/75	1100	437	574.336		.963
9/17/75	1814	437	574.300			9/18/75	1130	437	574.323		.966
9/17/75	1815	437	574.300			9/18/75	1200	437	574.319		.966
9/17/75	1816	437	574.300			9/18/75	1230	437	574.325		.979
9/17/75	1817	437	574.300			9/18/75	1300	437	574.347		
9/17/75	1818	437	574.300			9/18/75	1330	437	574.396		
9/17/75	1819	437	574.300			9/18/75	1400	437	574.372		
9/17/75	1820	437	574.301			9/18/75	1430	437	574.379		149.090
9/17/75	1821	437	574.301			9/18/75	1500	437	574.386		.141
9/17/75	1822	437	574.301			9/18/75	1530	437	574.448		.141
9/17/75	1823	437	574.301		.405	9/18/75	1530	437	574.448		.141
9/17/75	1824	437	574.300			9/18/75	1600	437	574.451		
9/17/75	1825	437	574.300			9/18/75	1630	437	574.460		
9/17/75	1826	437	574.300			9/18/75	1700	437	574.467		.173
9/17/75	1827	437	574.300			9/18/75	1730	437	574.499		
9/17/75	1905	437	574.305			9/18/75	1800	437	574.509		.190
9/17/75	1910	437	574.366			9/18/75	1830	437	574.517		
9/17/75	1915	437	574.367			9/18/75	1900	437	574.519		
9/17/75	1920	437	574.359			9/18/75	1930	437	574.510		
9/17/75	1925	437	574.362			9/18/75	2000	437	574.500		
9/17/75	1930	437	574.364			9/18/75	2030	437	574.483		
9/17/75	1935	437	574.363			9/18/75	2100	437	574.466		.071
9/17/75	1940	437	574.359			9/18/75	2130	437	574.478		.033
9/17/75	1945	437	574.360			9/18/75	2200	437	574.453		.038
9/17/75	1950	437	574.356			9/18/75	2230	437	574.455		.076
9/17/75	2000	437	574.351			9/18/75	2300	437	574.445		
9/17/75	2010	437	574.347			9/18/75	2330	437	574.445		.049
9/17/75	2020	437	574.346			9/19/75	0000	437	574.435		
9/17/75	2030	437	574.342			9/19/75	0030	437	574.444		
9/17/75	2040	437	574.329			9/19/75	0100	437	574.462		
9/17/75	2050	437	574.332			9/19/75	0130	437	574.472		
9/17/75	2100	437	574.329			9/19/75	0200	437	574.469		
9/17/75	2110	437	574.336			9/19/75	0230	437	574.508		
9/17/75	2120	437	574.336			9/19/75	0300	437	574.517		
9/17/75	2130	437	574.332			9/19/75	0330	437	574.549		

A 20 MIN. SHUTDOWN.

.141 FIRST DATA POINT AFTER MP GAGE WAS TURNED ON AFTER

ARGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / TIME	FLOW RATE / (GPH)	DOWNHOLE / PRESSURE / (PSIA)	WELL HEAD / PRESSURE / (PSIA)	REMARKS	DATE / TIME	FLOW RATE / (GPH)	DOWNHOLE / PRESSURE / (PSIA)	WELL HEAD / PRESSURE / (PSIA)	REMARKS
9/23/75	0640	386	573.656		9/25/75	1450	398	573.796	
9/23/75	0610	386	573.678		9/25/75	1450	398	573.774	
9/23/75	0640	386	573.407		9/25/75	1320	386	573.771	.358
9/23/75	0640	386	573.684	.849	9/25/75	1350	386	573.781	
9/23/75	0640	386	573.658		9/25/75	1350	386	573.742	.341
9/23/75	0710	386	573.699		9/25/75	1420	386	573.732	
9/23/75	0610	386	573.253	.071	9/25/75	1450	386	573.723	.352
9/23/75	0640	386	573.257		9/25/75	1520	404	573.715	
9/23/75	0610	386	573.686		9/25/75	1550	404	573.711	.352
9/23/75	0940	386	573.674		9/25/75	1828	404	573.709	
9/23/75	1010	386	573.630	.085	9/25/75	1690	404	573.711	
9/23/75	1040	386	573.635		9/25/75	1720	398	573.705	.341
9/23/75	1110	386	573.426		9/25/75	1750	398	573.713	
9/23/75	1140	386	573.381		9/25/75	1820	398	573.716	
9/23/75	1210	386	573.380		9/25/75	1890	398	573.725	.320
9/23/75	1240	386	573.382		9/25/75	1920	386	573.721	
9/23/75	1310	386	573.375	.055	9/25/75	1950	386	573.721	.393
9/23/75	1340	386	573.389		9/25/75	2020	386	573.724	.277
9/23/75	1410	421	573.339	.076	9/25/75	2058	386	573.715	
9/23/75	1440	421	573.337		9/25/75	2128	386	573.712	
9/23/75	1510	421	573.336		9/25/75	2150	386	573.710	.228
9/23/75	1540	421	573.338	.055	9/25/75	2220	404	573.696	
9/23/75	1610	409	573.318	.065	9/25/75	2250	404	573.685	.163
9/23/75	1730	386	573.339	.080	9/25/75	2320	404	573.672	
9/23/75	1900	386	573.372	.060	9/25/75	2390	404	573.650	
9/23/75	1930	386	573.365	.044	9/26/75	0020	404	573.629	.125
9/23/75	2030	386	573.385		9/26/75	0050	404	573.615	
9/23/75	2220	386	573.351	.730	9/26/75	0120	404	573.599	
9/23/75	2243	386	573.388	.703	9/26/75	0150	404	573.579	
9/23/75	2243	386	573.388		9/26/75	0220	404	573.567	144.061
9/24/75	1400	409	576.514	.783MP GAGE FAILED-PULLED OUT OF WELL FOR CHECKING AND REPAIR.	9/26/75	0250	404	573.558	
9/24/75	1400	409	576.514	.783MP GAGE LOWERED INTO ARGE	9/26/75	0320	404	573.539	
9/24/75	1430	409	576.043	1 AND SET AT 1800 FT.	9/26/75	0350	398	573.533	.012
9/24/75	1530	409	576.013		9/26/75	0620	398	573.546	167.990
9/24/75	1600	409	576.017		9/26/75	0650	398	573.540	
9/24/75	1630	409	575.990		9/26/75	0720	398	573.570	
9/24/75	1700	409	575.993	.666	9/26/75	0750	398	573.577	144.033
9/24/75	1820	404	576.011		9/26/75	0820	398	573.597	.05
9/24/75	1900	404	575.999		9/26/75	0850	398	573.583	.055
9/24/75	1930	404	575.995	144.606	9/26/75	0920	398	573.588	
9/24/75	2000	404	576.002		9/26/75	0950	398	573.597	
9/24/75	2030	404	576.017		9/26/75	1020	398	573.585	.066
9/24/75	2100	404	576.066		9/26/75	1050	398	573.581	
9/24/75	2130	404	576.036		9/26/75	1120	398	573.576	
9/24/75	2200	404	576.073	.666	9/26/75	1150	398	573.564	.000
9/24/75	2230	404	576.175		9/26/75	1220	404	573.559	
9/24/75	2320	404	576.112	.466	9/26/75	1250	404	573.553	.077
9/24/75	0020	404	575.975	.466	9/26/75	1320	404	573.550	
9/24/75	0120	404	575.933		9/26/75	1350	404	573.532	.077
9/25/75	0220	404	575.877		9/26/75	1420	404	573.513	
9/25/75	0320	404	575.865		9/26/75	1490	404	573.509	
9/25/75	0358	404	575.833	.358	9/26/75	1520	404	573.498	.066
9/25/75	0428	404	575.857		9/26/75	1550	404	573.497	.071
9/25/75	0528	404	575.857		9/26/75	1620	404	573.492	.061
9/25/75	0620	404	573.831	.347	9/26/75	1690	404	573.493	
9/25/75	0720	404	573.855		9/26/75	1720	404	573.489	.050
9/25/75	0750	404	573.857	.368	9/26/75	1850	404	573.492	
9/25/75	0820	398	573.854		9/26/75	1920	404	573.495	.028
9/25/75	0850	398	573.849		9/26/75	1950	404	573.497	
9/25/75	0920	398	573.846		9/26/75	2020	398	573.496	.017
9/25/75	0950	398	573.840		9/26/75	2050	398	573.500	147.969
9/25/75	1050	386	573.831	.305	9/26/75	2120	398	573.500	
9/25/75	1080	386	573.822		9/26/75	2150	409	573.495	
9/25/75	1120	386	573.806		9/26/75	2220	409	573.480	.942

ARCE 1 INTERFERENCE TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPM)	DOWNHOLE PRESSURE / (PSIA)	WELL HEAD PRESSURE / (PSIA)	REMARKS
9/29/75	2220	404	572.326		.385
9/29/75	2250	406	572.320		
9/29/75	2300	406	572.331		
9/29/75	2350	406	572.331		.369
9/30/75	0050	406	572.335		
9/30/75	0050	406	572.337		
9/30/75	0120	406	572.342		.367
9/30/75	0150	404	572.345		
9/30/75	0220	406	572.342		
9/30/75	0250	406	572.337		
9/30/75	0320	406	572.360		
9/30/75	0350	406	572.325		
9/30/75	0420	406	572.316		.326
9/30/75	0450	406	572.305		
9/30/75	0520	406	572.293		
9/30/75	0550	406	572.283		
9/30/75	0620	406	572.270		.304
9/30/75	0650	398	572.267		
9/30/75	0720	398	572.237		.283
9/30/75	0750	398	572.216		
9/30/75	0820	398	572.200		
9/30/75	0850	398	572.199		
9/30/75	0920	398	572.190		
9/30/75	0950	398	572.185		.180
9/30/75	1020	398	572.186		
9/30/75	1050	404	572.184		.259
9/30/75	1120	406	572.189		
9/30/75	1150	406	572.191		.268
9/30/75	1220	406	572.211		.320
9/30/75	1250	406	572.211		.353
9/30/75	1320	406	572.220		
9/30/75	1350	406	572.220		.360
9/30/75	1420	406	572.231		
9/30/75	1450	406	572.226		.445
9/30/75	1520	406	572.226		.439
9/30/75	1550	406	572.226		.423
9/30/75	1620	406	572.226		.407
9/30/75	1650	404	572.246		.365
9/30/75	1720	406	572.253		.364
9/30/75	1750	406	572.263		.357
9/30/75	1820	406	572.239		.320
9/30/75	1850	406	572.220		
9/30/75	1920	406	572.216		
9/30/75	1950	406	572.216		.277
9/30/75	2020	406	572.216		.261
9/30/75	2050	409	572.183		.239
9/30/75	2120	409	572.187		.223
9/30/75	2150	409	572.189		.216
9/30/75	2220	409	572.189		.207
9/30/75	2250	409	572.189		.216
9/30/75	2320	409	572.187		.229
9/30/75	2350	409	572.187		.180
10/01/75	0050	409	572.176		.287
10/01/75	0120	409	572.186		.282
10/01/75	0150	409	572.191		.216
10/01/75	0220	409	572.202		.229
10/01/75	0250	409	572.195		.234
10/01/75	0320	409	572.226		.229
10/01/75	0350	409	572.203		.223
10/01/75	0420	409	572.202		.229
10/01/75	0450	409	572.205		.212
10/01/75	0520	409	572.184		.202
10/01/75	0550	409	572.166		.184
10/01/75	0620	409	572.156		.164
10/01/75	0650	409	572.130		.142
10/01/75	0720	409	572.108		.120
10/01/75	0750	409	572.890		.099
10/01/75	0820	409	572.861		.077
10/01/75	0850	409	572.850		.062
10/01/75	0920	409	572.861		.066
10/01/75	0950	409	572.861		.066
10/01/75	1020	409	572.861		.066
10/01/75	1050	409	572.861		.066
10/01/75	1120	409	572.861		.066
10/01/75	1150	409	572.861		.066
10/01/75	1220	409	572.861		.066
10/01/75	1250	409	572.861		.066
10/01/75	1320	409	572.861		.066
10/01/75	1350	409	572.861		.066
10/01/75	1420	409	572.861		.066
10/01/75	1450	409	572.861		.066
10/01/75	1520	409	572.861		.066
10/01/75	1550	409	572.861		.066
10/01/75	1620	409	572.861		.066
10/01/75	1650	409	572.861		.066
10/01/75	1720	409	572.861		.066
10/01/75	1750	409	572.861		.066
10/01/75	1820	409	572.861		.066
10/01/75	1850	409	572.861		.066
10/01/75	1920	409	572.861		.066
10/01/75	1950	409	572.861		.066
10/01/75	2020	409	572.861		.066
10/01/75	2050	409	572.861		.066
10/01/75	2120	409	572.861		.066
10/01/75	2150	409	572.861		.066
10/01/75	2220	409	572.861		.066
10/01/75	2250	409	572.861		.066
10/01/75	2320	409	572.861		.066
10/01/75	2350	409	572.861		.066
10/01/75	2420	409	572.861		.066
10/01/75	2450	409	572.861		.066
10/01/75	2520	409	572.861		.066
10/01/75	2550	409	572.861		.066
10/01/75	2620	409	572.861		.066
10/01/75	2650	409	572.861		.066
10/01/75	2720	409	572.861		.066
10/01/75	2750	409	572.861		.066
10/01/75	2820	409	572.861		.066
10/01/75	2850	409	572.861		.066
10/01/75	2920	409	572.861		.066
10/01/75	2950	409	572.861		.066
10/01/75	3020	409	572.861		.066
10/01/75	3050	409	572.861		.066
10/01/75	3120	409	572.861		.066
10/01/75	3150	409	572.861		.066
10/01/75	3220	409	572.861		.066
10/01/75	3250	409	572.861		.066
10/01/75	3320	409	572.861		.066
10/01/75	3350	409	572.861		.066
10/01/75	3420	409	572.861		.066
10/01/75	3450	409	572.861		.066
10/01/75	3520	409	572.861		.066
10/01/75	3550	409	572.861		.066
10/01/75	3620	409	572.861		.066
10/01/75	3650	409	572.861		.066
10/01/75	3720	409	572.861		.066
10/01/75	3750	409	572.861		.066
10/01/75	3820	409	572.861		.066
10/01/75	3850	409	572.861		.066
10/01/75	3920	409	572.861		.066
10/01/75	3950	409	572.861		.066
10/01/75	4020	409	572.861		.066
10/01/75	4050	409	572.861		.066
10/01/75	4120	409	572.861		.066
10/01/75	4150	409	572.861		.066
10/01/75	4220	409	572.861		.066
10/01/75	4250	409	572.861		.066
10/01/75	4320	409	572.861		.066
10/01/75	4350	409	572.861		.066
10/01/75	4420	409	572.861		.066
10/01/75	4450	409	572.861		.066
10/01/75	4520	409	572.861		.066
10/01/75	4550	409	572.861		.066
10/01/75	4620	409	572.861		.066
10/01/75	4650	409	572.861		.066
10/01/75	4720	409	572.861		.066
10/01/75	4750	409	572.861		.066
10/01/75	4820	409	572.861		.066
10/01/75	4850	409	572.861		.066
10/01/75	4920	409	572.861		.066
10/01/75	4950	409	572.861		.066
10/01/75	5020	409	572.861		.066
10/01/75	5050	409	572.861		.066
10/01/75	5120	409	572.861		.066
10/01/75	5150	409	572.861		.066
10/01/75	5220	409	572.861		.066
10/01/75	5250	409	572.861		.066
10/01/75	5320	409	572.861		.066
10/01/75	5350	409	572.861		.066
10/01/75	5420	409	572.861		.066
10/01/75	5450	409	572.861		.066
10/01/75	5520	409	572.861		.066
10/01/75	5550	409	572.861		.066
10/01/75	5620	409	572.861		.066
10/01/75	5650	409	572.861		.066
10/01/75	5720	409	572.861		.066
10/01/75	5750	409	572.861		.066
10/01/75	5820	409	572.861		.066
10/01/75	5850	409	572.861		.066
10/01/75	5920	409	572.861		.066
10/01/75	5950	409	572.861		.066
10/01/75	6020	409	572.861		.066
10/01/75	6050	409	572.861		.066
10/01/75	6120	409	572.861		.066
10/01/75	6150	409	572.861		.066
10/01/75	6220	409	572.861		.066
10/01/75	6250	409	572.861		.066
10/01/75	6320	409	572.861		.066
10/01/75	6350	409	572.861		.066
10/01/75	6420	409	572.861		.066
10/01/75	6450	409	572.861		.066
10/01/75	6520	409	572.861		.066
10/01/75	6550	409	572.861		.066
10/01/75	6620	409	572.861		.066
10/01/75	6650	409	572.861		.066
10/01/75	6720	409	572.861		.066
10/01/75	6750	409	572.861		.066
10/01/75	6820	409	572.861		.066
10/01/75	6850	409	572.861		.066
10/01/75	6920	409	572.861		.066
10/01/75	6950	409	572.861		.066
10/01/75	7020	409	572.861		.066
10/01/75	7050	409	572.861		.066
10/01/75	7120	409	572.861		.066
10/01/75	7150	409	572.861		.066
10/01/75	7220	409	572.861		.066
10/01/75	7250	409	572.861		.066
10/01/75	7320	409	572.861		.066
10/01/75	7350	409	572.861		.066
10/01/75	7420	409	572.861		.066
10/01/75	7450	409	572.861		.066
10/01/75	7520	409	572.861		.066
10/01/75	7550	409	572.861		.066
10/01/75	7620	409	572.861		.066
10/01/75	7650	409	572.861		.066
10/01/75	7720	409	572.861		.066
10/01/75	7750	409	572.861		.066
10/01/75	7820	409	572.861		.066
10/01/75	7850	409			

SARGE 1 INTERFERENCE TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE	TIME	FLOW RATE (GPM)	DOWNHOLE PRESSURE (PSIA)	WELL HEAD PRESSURE (PSIA)	REMARKS
9/29/75	2220	404	572.326	.385	
9/29/75	2250	404	572.320		
9/29/75	2320	404	572.331		
9/29/75	2350	404	572.331	.369	
9/29/75	0020	404	572.335		
9/30/75	0050	404	572.337		
9/30/75	0120	404	572.349		
9/30/75	0150	404	572.345		
9/30/75	0220	404	572.345	.367	
9/30/75	0250	404	572.337		
9/30/75	0320	404	572.348		
9/30/75	0350	404	572.323		
9/30/75	0420	404	572.310		
9/30/75	0450	404	572.310	.326	
9/30/75	0520	404	572.293		
9/30/75	0550	404	572.293		
9/30/75	0620	404	572.270	.304	
9/30/75	0650	398	572.267		
9/30/75	0720	398	572.237	.283	
9/30/75	0750	398	572.216		
9/30/75	0820	398	572.200		
9/30/75	0850	398	572.186	.180	
9/30/75	0920	398	572.189		
9/30/75	0950	398	572.190		
9/30/75	1020	398	572.185	.180	
9/30/75	1050	404	572.186	.205	
9/30/75	1120	404	572.186		
9/30/75	1150	404	572.191	.200	
9/30/75	1220	404	572.211	.326	
9/30/75	1250	404	572.211	.353	
9/30/75	1320	404	572.220	.300	
9/30/75	1350	404	572.231	.445	
9/30/75	1420	404	572.226	.439	
9/30/75	1450	404	572.240	.423	
9/30/75	1520	404	572.246	.407	
9/30/75	1550	404	572.240	.385	
9/30/75	1620	404	572.233	.364	
9/30/75	1650	404	572.243	.347	
9/30/75	1720	404	572.243	.320	
9/30/75	1750	404	572.228		
9/30/75	1820	404	572.216		
9/30/75	1850	404	572.215		
9/30/75	1920	404	572.194		
9/30/75	1950	404	572.185	.167.299	
9/30/75	2020	404	572.178	.277	
9/30/75	2050	404	572.163	.261	
9/30/75	2120	409	572.154	.239	
9/30/75	2150	409	572.137	.223	
9/30/75	2220	409	572.149	.212	
9/30/75	2250	409	572.150	.196	
9/30/75	2320	409	572.157		
9/30/75	2350	409	572.157	.180	
10/01/75	0050	409	572.176	.207	
10/01/75	0120	409	572.146	.212	
10/01/75	0150	409	572.191	.210	
10/01/75	0220	409	572.202	.229	
10/01/75	0250	409	572.195	.236	
10/01/75	0320	409	572.216	.236	
10/01/75	0350	409	572.203	.223	
10/01/75	0420	409	572.202	.223	
10/01/75	0450	409	572.205	.212	
10/01/75	0520	409	572.184	.202	
10/01/75	0550	409	572.166	.180	
10/01/75	0620	409	572.156	.184	
10/01/75	0650	409	572.150	.162	
10/01/75	0720	409	572.108	.120	
10/01/75	0750	409	572.090	.098	
10/01/75	0820	409	572.061	.072	
10/01/75	0850	409	572.050	.072	
10/01/75	0920	409	572.041	.066	
10/01/75	0950	409	572.032		
10/01/75	1020	409	572.022		
10/01/75	1050	409	572.016		
10/01/75	1120	409	572.016	.086	
10/01/75	1150	409	572.016	.099	
10/01/75	1220	409	572.020	.126	
10/01/75	1250	409	572.022	.158	
10/01/75	1320	409	572.034	.200	
10/01/75	1350	409	572.039	.212	
10/01/75	1420	409	572.053	.234	
10/01/75	1450	409	572.075	.266	
10/01/75	1520	409	572.086	.293	
10/01/75	1550	409	572.091	.324	
10/01/75	1620	409	572.099	.356	
10/01/75	1650	409	572.103	.380	
10/01/75	1720	409	572.116	.412	
10/01/75	1750	409	572.133	.450	
10/01/75	1820	409	572.146	.487	
10/01/75	1850	409	572.166	.527	
10/01/75	1920	409	572.184	.564	
10/01/75	1950	409	572.201	.601	
10/01/75	2020	409	572.218	.638	
10/01/75	2050	409	572.234	.675	
10/01/75	2120	409	572.251	.712	
10/01/75	2150	409	572.268	.749	
10/01/75	2220	409	572.285	.786	
10/01/75	2250	409	572.302	.823	
10/01/75	2320	409	572.319	.860	
10/01/75	2350	409	572.336	.897	
10/01/75	2420	409	572.353	.934	
10/01/75	2450	409	572.370	.971	
10/01/75	2520	409	572.387	1.008	
10/01/75	2550	409	572.404	1.045	
10/01/75	2620	409	572.421	1.082	
10/01/75	2650	409	572.438	1.119	
10/01/75	2720	409	572.455	1.156	
10/01/75	2750	409	572.472	1.193	
10/01/75	2820	409	572.489	1.230	
10/01/75	2850	409	572.506	1.267	
10/01/75	2920	409	572.523	1.304	
10/01/75	2950	409	572.540	1.341	
10/01/75	3020	409	572.557	1.378	
10/01/75	3050	409	572.574	1.415	
10/01/75	3120	409	572.591	1.452	
10/01/75	3150	409	572.608	1.489	
10/01/75	3220	409	572.625	1.526	
10/01/75	3250	409	572.642	1.563	
10/01/75	3320	409	572.659	1.600	
10/01/75	3350	409	572.676	1.637	
10/01/75	3420	409	572.693	1.674	
10/01/75	3450	409	572.710	1.711	
10/01/75	3520	409	572.727	1.748	
10/01/75	3550	409	572.744	1.785	
10/01/75	3620	409	572.761	1.822	
10/01/75	3650	409	572.778	1.859	
10/01/75	3720	409	572.795	1.896	
10/01/75	3750	409	572.812	1.933	
10/01/75	3820	409	572.829	1.970	
10/01/75	3850	409	572.846	2.007	
10/01/75	3920	409	572.863	2.044	
10/01/75	3950	409	572.880	2.081	
10/01/75	4020	409	572.897	2.118	
10/01/75	4050	409	572.914	2.155	
10/01/75	4120	409	572.931	2.192	
10/01/75	4150	409	572.948	2.229	
10/01/75	4220	409	572.965	2.266	
10/01/75	4250	409	572.982	2.303	
10/01/75	4320	409	572.999	2.340	
10/01/75	4350	409	573.016	2.377	
10/01/75	4420	409	573.033	2.414	
10/01/75	4450	409	573.050	2.451	
10/01/75	4520	409	573.067	2.488	
10/01/75	4550	409	573.084	2.525	
10/01/75	4620	409	573.101	2.562	
10/01/75	4650	409	573.118	2.599	
10/01/75	4720	409	573.135	2.636	
10/01/75	4750	409	573.152	2.673	
10/01/75	4820	409	573.169	2.710	
10/01/75	4850	409	573.186	2.747	
10/01/75	4920	409	573.203	2.784	
10/01/75	4950	409	573.220	2.821	
10/01/75	5020	409	573.237	2.858	
10/01/75	5050	409	573.254	2.895	
10/01/75	5120	409	573.271	2.932	
10/01/75	5150	409	573.288	2.969	
10/01/75	5220	409	573.305	3.006	
10/01/75	5250	409	573.322	3.043	
10/01/75	5320	409	573.339	3.080	
10/01/75	5350	409	573.356	3.117	
10/01/75	5420	409	573.373	3.154	
10/01/75	5450	409	573.390	3.191	
10/01/75	5520	409	573.407	3.228	
10/01/75	5550	409	573.424	3.265	
10/01/75	5620	409	573.441	3.302	
10/01/75	5650	409	573.458	3.339	
10/01/75	5720	409	573.475	3.376	
10/01/75	5750	409	573.492	3.413	
10/01/75	5820	409	573.509	3.450	
10/01/75	5850	409	573.526	3.487	
10/01/75	5920	409	573.543	3.524	
10/01/75	5950	409	573.560	3.561	
10/01/75	6020	409	573.577	3.598	
10/01/75	6050	409	573.594	3.635	
10/01/75	6120	409	573.611	3.672	
10/01/75	6150	409	573.628	3.709	
10/01/75	6220	409	573.645	3.746	
10/01/75	6250	409	573.662	3.783	
10/01/75	6320	409	573.679	3.820	
10/01/75	6350	409	573.696	3.857	
10/01/75	6420	409	573.713	3.894	
10/01/75	6450	409	573.730	3.931	
10/01/75	6520	409	573.747	3.968	
10/01/75	6550	409	573.764	4.005	
10/01/75	6620	409	573.781	4.042	
10/01/75	6650	409	573.798	4.079	
10/01/75	6720	409	573.815	4.116	
10/01/75	6750	409	573.832	4.153	
10/01/75	6820	409	573.849	4.190	
10/01/75	6850	409	573.866	4.227	
10/01/75	6920	409	573.883	4.264	
10/01/75	6950	409	573.900	4.301	
10/01/75	7020	409	573.917	4.338	
10/01/75	7050	409	573.934	4.375	
10/01/75	7120	409	573.951	4.412	
10/01/75	7150	409	573.968	4.449	
10/01/75	7220	409	573.985	4.486	
10/01/75	7250	409	574.002	4.523	
10/01/75	7320	409	574.019	4.560	
10/01/75	7350	409	574.036	4.597	
10/01/75	7420	409	574.053	4.634	
10/01/75	7450	409	574.070	4.671	
10/01/75	7520	409	574.087	4.708	
10/01/75	7550	409	574.104	4.745	
10/01/75	7620	409	574.121	4.782	
10/01/75	7650	409	574.138	4.819	
10/01/75	7720				

RANGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE	TIME	FLOW RATE / (GPM)	DOMMHOLE / PRESSURE / (PSIA)	WELL HEAD / REMARKS	DATE	TIME	FLOW RATE / (GPM)	DOMMHOLE / PRESSURE / (PSIA)	WELL HEAD / REMARKS
10/05/75	1850	606	571.667	.710	10/07/75	0550	606	571.351	.326
10/05/75	1920	606	571.631	.699	10/07/75	0620	606	571.376	.337
10/05/75	1950	606	571.690	.683	10/07/75	0650	606	571.401	.348
10/05/75	2020	606	571.617	.696	10/07/75	0720	606	571.404	.356
10/05/75	2050	606	571.610	.693	10/07/75	0750	606	571.396	.391
10/05/75	2120	606	571.585	.698	10/07/75	0820	606	571.409	.391
10/05/75	2150	606	571.531	.699	10/07/75	0850	606	571.465	.386
10/05/75	2220	606	571.527	.691	10/07/75	0920	606	571.397	.380
10/05/75	2250	606	571.502	.691	10/07/75	0950	606	571.436	.370
10/05/75	2320	606	571.470	.666	10/07/75	1020	606	566.792	.321
10/05/75	2350	606	571.466	.629	10/07/75	1050	606	506.	.651
10/05/75	0020	606	571.424	.366	10/07/75	1120	606	586.	.624
10/05/75	0050	606	571.417	.397	10/07/75	1150	606	2003.763	.618
10/05/75	0120	606	571.405	.413	10/07/75	1220	606	2003.720	1.66-.402
10/05/75	0150	606	571.375	.423	10/07/75	1250	606	2003.697	.397
10/05/75	0220	606	571.360	.463	10/07/75	1320	606	2003.667	.375
10/05/75	0250	606	571.322	.661	10/07/75	1350	606	2003.660	.375
10/05/75	0320	606	571.326	.661	10/07/75	1420	606	2003.651	.359
10/05/75	0350	606	571.317	.699	10/07/75	1450	606	2003.649	.368
10/05/75	0420	606	571.353	.521	10/07/75	1520	606	2003.668	.353
10/05/75	0450	606	571.360	.537	10/07/75	1550	606	2003.656	.380
10/05/75	0520	606	571.370	.532	10/07/75	1620	606	2003.655	.366
10/05/75	0550	606	571.398	.542	10/07/75	1650	606	2003.659	.387
10/05/75	0620	606	571.367	.532	10/07/75	1720	606	2003.664	.397
10/05/75	0650	606	571.350	.521	10/07/75	1750	606	2003.664	.397
10/05/75	0720	606	571.365	1.66.516	10/07/75	1820	606	2003.669	.397
10/05/75	0750	606	571.362	.505	10/07/75	1850	606	2003.682	.402
10/05/75	0820	606	571.326	.496	10/07/75	1920	606	2003.679	.429
10/05/75	0850	606	571.349	.493	10/07/75	1950	606	2003.675	.426
10/05/75	0920	606	571.349	.482	10/07/75	2020	606	2003.666	.
10/05/75	0950	606	571.364	.496	10/07/75	2050	606	2003.653	.191
10/05/75	1020	606	571.436	.466	10/07/75	2150	606	2003.601	.375
10/05/75	1050	606	571.430	.466	10/07/75	2220	606	2003.601	.353
10/05/75	1080	606	571.400	.466	10/07/75	2250	606	2003.582	.326
10/05/75	1120	606	571.420	.466	10/07/75	2320	606	2003.549	.310
10/05/75	1150	606	571.430	.466	10/07/75	2350	606	2003.530	.283
10/05/75	1220	606	571.436	.466	10/07/75	0020	606	2003.496	.296
10/05/75	1250	606	571.421	.461	10/07/75	0050	606	2003.466	.234
10/05/75	1320	606	571.462	.466	10/07/75	0080	606	571.316	.234MP GAGE MALFUNCTION.
10/05/75	1350	606	571.469	.466	10/07/75	0130	606	571.316	MP GAGE REPAIRED.
10/05/75	1420	606	571.461	.505	10/09/75	1920	606	571.391	
10/05/75	1450	606	571.478	.510	10/09/75	2000	606	571.336	
10/05/75	1520	606	571.498	.510	10/09/75	2050	606	571.352	
10/05/75	1550	606	571.523	.510	10/09/75	2140	606	571.330	
10/05/75	1620	606	571.509	.510	10/09/75	2220	606	571.320	
10/05/75	1650	606	571.471	.591	10/09/75	2250	606	571.326	
10/05/75	1720	606	571.487	.678	10/09/75	2320	606	571.279	
10/05/75	1750	606	571.456	.661	10/10/75	0000	606	571.195	.261
10/05/75	1820	606	571.456	.629	10/10/75	0100	606	571.161	.351
10/05/75	1850	606	571.418	.482	10/10/75	0200	606	571.199	.326
10/05/75	1920	606	571.394	.378	10/10/75	0300	606	571.190	.282
10/05/75	1950	606	571.354	.371	10/10/75	0400	606	571.199	.175
10/05/75	2020	606	571.318	.266	10/10/75	0500	606	571.170	.175
10/05/75	2050	606	571.317	.287	10/10/75	0600	606	571.161	.186
10/05/75	2120	606	571.291	.251	10/10/75	0700	606	571.165	.207
10/05/75	2150	606	571.250	.268	10/10/75	0800	606	571.168	.218
10/05/75	2220	606	571.261	.213	10/10/75	0900	606	571.	.218MP GAGE MALFUNCTION
10/05/75	2250	606	571.264	.213	10/10/75	1000	606	571.291	.378
10/05/75	2320	606	571.260	.210	10/10/75	1600	606	571.290	.356
10/05/75	2350	606	571.281	.213	10/10/75	1700	606	571.290	
10/05/75	0020	606	571.287	.256	10/10/75	1800	606	571.277	.240
10/05/75	0050	606	571.307	.287	10/10/75	1900	606	571.241	.229
10/05/75	0080	606	571.327	.278	10/10/75	2000	606	571.209	.218
10/05/75	0120	606	571.326	.266	10/10/75	2100	606	571.217	.207
10/05/75	0150	606	571.326	.266	10/10/75	2200	606	571.150	.175

RAGE 1 INTERFERENCE TEST DATA - RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE	TIME	FLOW RATE / (GPM)	DOWNHOLE / PRESSURE / (PSIA)	WELL HEAD / PRESSURE / (PSIA)	REMARKS
10/06/75	1850	406	571.667	710	
10/06/75	1920	406	571.631	699	
10/06/75	1950	406	571.640	683	
10/06/75	2020	406	571.617	668	
10/06/75	2050	406	571.610	654	
10/06/75	2150	406	571.560	596	
10/06/75	2150	406	571.531	559	
10/06/75	2220	406	571.527	521	
10/06/75	2250	406	571.502	491	
10/06/75	2350	406	571.470	458	
10/06/75	2350	406	571.460	429	
10/06/75	0030	406	571.429	413	
10/06/75	0120	406	571.405	391	
10/06/75	0150	406	571.406	350	
10/06/75	0220	406	571.424	306	
10/06/75	0250	406	571.417	297	
10/06/75	0320	406	571.439	413	
10/06/75	0350	406	571.454	469	
10/06/75	0420	406	571.475	485	
10/06/75	0450	406	571.522	661	
10/06/75	0520	406	571.526	660	
10/06/75	0550	406	571.534	699	
10/06/75	0620	406	571.553	521	
10/06/75	0650	406	571.560	537	
10/06/75	0720	406	571.570	532	
10/06/75	0750	406	571.569	542	
10/06/75	0820	392	571.567	532	
10/06/75	0850	406	571.596	512	
10/06/75	0920	406	571.565	166.519	
10/06/75	0950	406	571.562	505	
10/06/75	1020	406	571.516	496	
10/06/75	1050	406	571.516	483	
10/06/75	1120	406	571.463	472	
10/06/75	1150	406	571.464	456	
10/06/75	1220	406	571.436	450	
10/06/75	1320	406	571.430	446	
10/06/75	1350	406	571.420	460	
10/06/75	1420	406	571.438	460	
10/06/75	1450	406	571.432	456	
10/06/75	1520	406	571.421	461	
10/06/75	1550	406	571.432	466	
10/06/75	1620	406	571.464	478	
10/06/75	1650	406	571.469	468	
10/06/75	1720	406	571.461	585	
10/06/75	1750	406	571.470	510	
10/06/75	1820	406	571.450	510	
10/06/75	1850	406	571.425	510	
10/06/75	1920	406	571.409	510	
10/06/75	1950	406	571.471	581	
10/06/75	2020	406	571.487	678	
10/06/75	2050	406	571.456	661	
10/06/75	2120	406	571.454	449	
10/06/75	2150	406	571.416	462	
10/06/75	2220	406	571.396	375	
10/06/75	2250	406	571.366	346	
10/06/75	2320	406	571.396	321	
10/06/75	2350	406	571.310	280	
10/06/75	0020	406	571.317	267	
10/06/75	0050	406	571.291	251	
10/06/75	0120	406	571.230	280	
10/06/75	0150	406	571.261	213	
10/06/75	0220	406	571.200	219	
10/06/75	0250	406	571.200	219	
10/06/75	0320	406	571.201	213	
10/06/75	0350	406	571.207	256	
10/06/75	0420	406	571.307	267	
10/06/75	0450	406	571.327	278	
10/06/75	0520	406	571.326	280	
10/06/75	0550	406	571.326	280	
10/06/75	0620	406	571.326	280	
10/06/75	0650	406	571.326	280	
10/06/75	0720	406	571.326	280	
10/06/75	0750	406	571.326	280	
10/06/75	0820	406	571.326	280	
10/06/75	0850	406	571.326	280	
10/06/75	0920	406	571.326	280	
10/06/75	0950	406	571.326	280	
10/06/75	1020	406	571.326	280	
10/06/75	1050	406	571.326	280	
10/06/75	1120	406	571.326	280	
10/06/75	1150	406	571.326	280	
10/06/75	1220	406	571.326	280	
10/06/75	1250	406	571.326	280	
10/06/75	1320	406	571.326	280	
10/06/75	1350	406	571.326	280	
10/06/75	1420	406	571.326	280	
10/06/75	1450	406	571.326	280	
10/06/75	1520	406	571.326	280	
10/06/75	1550	406	571.326	280	
10/06/75	1620	406	571.326	280	
10/06/75	1650	406	571.326	280	
10/06/75	1720	406	571.326	280	
10/06/75	1750	406	571.326	280	
10/06/75	1820	406	571.326	280	
10/06/75	1850	406	571.326	280	
10/06/75	1920	406	571.326	280	
10/06/75	1950	406	571.326	280	
10/06/75	2020	406	571.326	280	
10/06/75	2050	406	571.326	280	
10/06/75	2120	406	571.326	280	
10/06/75	2150	406	571.326	280	
10/06/75	2220	406	571.326	280	
10/06/75	2250	406	571.326	280	
10/06/75	2320	406	571.326	280	
10/06/75	2350	406	571.326	280	
10/06/75	0020	406	571.326	280	
10/06/75	0050	406	571.326	280	
10/06/75	0120	406	571.326	280	
10/06/75	0150	406	571.326	280	
10/06/75	0220	406	571.326	280	
10/06/75	0250	406	571.326	280	
10/06/75	0320	406	571.326	280	
10/06/75	0350	406	571.326	280	
10/06/75	0420	406	571.326	280	
10/06/75	0450	406	571.326	280	
10/06/75	0520	406	571.326	280	
10/06/75	0550	406	571.326	280	
10/06/75	0620	406	571.326	280	
10/06/75	0650	406	571.326	280	
10/06/75	0720	406	571.326	280	
10/06/75	0750	406	571.326	280	
10/06/75	0820	406	571.326	280	
10/06/75	0850	406	571.326	280	
10/06/75	0920	406	571.326	280	
10/06/75	0950	406	571.326	280	
10/06/75	1020	406	571.326	280	
10/06/75	1050	406	571.326	280	
10/06/75	1120	406	571.326	280	
10/06/75	1150	406	571.326	280	
10/06/75	1220	406	571.326	280	
10/06/75	1250	406	571.326	280	
10/06/75	1320	406	571.326	280	
10/06/75	1350	406	571.326	280	
10/06/75	1420	406	571.326	280	
10/06/75	1450	406	571.326	280	
10/06/75	1520	406	571.326	280	
10/06/75	1550	406	571.326	280	
10/06/75	1620	406	571.326	280	
10/06/75	1650	406	571.326	280	
10/06/75	1720	406	571.326	280	
10/06/75	1750	406	571.326	280	
10/06/75	1820	406	571.326	280	
10/06/75	1850	406	571.326	280	
10/06/75	1920	406	571.326	280	
10/06/75	1950	406	571.326	280	
10/06/75	2020	406	571.326	280	
10/06/75	2050	406	571.326	280	
10/06/75	2120	406	571.326	280	
10/06/75	2150	406	571.326	280	
10/06/75	2220	406	571.326	280	
10/06/75	2250	406	571.326	280	
10/06/75	2320	406	571.326	280	
10/06/75	2350	406	571.326	280	
10/06/75	0020	406	571.326	280	
10/06/75	0050	406	571.326	280	
10/06/75	0120	406	571.326	280	
10/06/75	0150	406	571.326	280	
10/06/75	0220	406	571.326	280	
10/06/75	0250	406	571.326	280	
10/06/75	0320	406	571.326	280	
10/06/75	0350	406	571.326	280	
10/06/75	0420	406	571.326	280	
10/06/75	0450	406	571.326	280	
10/06/75	0520	406	571.326	280	
10/06/75	0550	406	571.326	280	
10/06/75	0620	406	571.326	280	
10/06/75	0650	406	571.326	280	
10/06/75	0720	406	571.326	280	
10/06/75	0750	406	571.326	280	
10/06/75	0820	406	571.326	280	
10/06/75	0850	406	571.326	280	
10/06/75	0920	406	571.326	280	
10/06/75	0950	406	571.326	280	
10/06/75	1020	406	571.326	280	
10/06/75	1050	406	571.326	280	
10/06/75	1120	406	571.326	280	
10/06/75	1150	406	571.326	280	
10/06/75	1220	406	571.326	280	
10/06/75	1250	406	571.326	280	
10/06/75	1320	406	571.326	280	
10/06/75	1350	406	571.326	280	
10/06/75	1420	406	571.326	280	
10/06/75	1450	406	571.326	280	
10/06/75	1520	406	571.326	280	
10/06/75	1550	406	571.326	280	
10/06/75	1620	406	571.326	280	
10/06/75	1650	406	571.326	280	
10/06/75	1720	406	571.326	280	
10/06/75	1750	406	571.326	280	
10/06/75	1820	406	571.326	280	
10/06/75	1850	406	571.326	280	
10/06/75	1920	406	571.326	280	
10/06/75	1950	406	571.326	280	
10/06/75	2020	406	571.326	280	
10/06/75	2050	406	571.326	280	
10/06/75	2120	406	571.326	280	
10/06/75	2150	406	571.326	280	
10/06/75	2220	406	571.326	280	
10/06/75	2250	406	571.326	280	
10/06/75	2320	406	571.326	280	
10/06/75	2350	406	571.326	280	
10/06/75	0020	406	571.326	280	
10/06/75	0050	406	571.326	280	
10/06/75	0120	406	571.326	280	
10/06/75	0150	406	571.326	280	
10/06/75	0220	406	571.326	280	
10/06/75	0				

ARCE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IOANO

DATE	TIME	FLOW RATE (GPH)	DOWNHOLE / WELL HEAD PRESSURE / (PSIA)	REMARKS	DATE	TIME	FLOW RATE (GPH)	DOWNHOLE / WELL HEAD PRESSURE / (PSIA)	REMARKS
10/20/75	0130		.680		10/21/75	1230			.180
10/20/75	0200		.710		10/21/75	1300			.190
10/20/75	0230		.730		10/21/75	1330			.190
10/20/75	0300		.760		10/21/75	1400			.210
10/20/75	0330		.780		10/21/75	1430			.220
10/20/75	0400		.810		10/21/75	1500			.240
10/20/75	0430		.820		10/21/75	1560			.260
10/20/75	0500		.860		10/21/75	1600			147-.280
10/20/75	0600		.910		10/21/75	1630			.290
10/20/75	0630		.930		10/21/75	1700			.310
10/20/75	0700		.940		10/21/75	1730			.320
10/20/75	0730		.950		10/21/75	1800			.330
10/20/75	0800		.950		10/21/75	1800			.330
10/20/75	0830		.950		10/21/75	1830			.350
10/20/75	0900		.980		10/21/75	1900			.320
10/20/75	0930		.940		10/21/75	2000			.310
10/20/75	1000		.940		10/21/75	2030			.290
10/20/75	1030		.940		10/21/75	2100			.270
10/20/75	1100		.940		10/21/75	2130			.260
10/20/75	1130		.900		10/21/75	2200			.220
10/20/75	1200		.900		10/21/75	2230			.210
10/20/75	1230		.870		10/21/75	2300			.190
10/20/75	1300		.800		10/21/75	0000			.170
10/20/75	1330		.800		10/21/75	0030			.160
10/20/75	1400		.950		10/22/75	0100			.180
10/20/75	1430		.920		10/22/75	0130			.150
10/20/75	1500		.920		10/22/75	0200			.150
10/20/75	1530		.840		10/22/75	0230			.160
10/20/75	1600		.870		10/22/75	0300			.170
10/20/75	1630		.880		10/22/75	0330			.330
10/20/75	1700		.880		10/22/75	0400			.320
10/20/75	1730		.870		10/22/75	0430			.370
10/20/75	1800		.860		10/22/75	0460			.390
10/20/75	1830		.830		10/22/75	0500			.390
10/20/75	1900		.810		10/22/75	0530			.310
10/20/75	1930		.800		10/22/75	0600			.330
10/20/75	2000		.800		10/22/75	0630			.350
10/20/75	2030		.800		10/22/75	0660			.370
10/20/75	2100		.830		10/22/75	0700			.390
10/20/75	2130		.810		10/22/75	0730			.400
10/20/75	2200		.800		10/22/75	0800			.400
10/20/75	2230		.800		10/22/75	0830			.420
10/20/75	2300		.930		10/22/75	0900			.420
10/20/75	2330		.950		10/22/75	0930			.420
10/21/75	0000		.950		10/22/75	1000			.360
10/21/75	0030		.910		10/22/75	1030			.410
10/21/75	0100		.940		10/22/75	1100			.440
10/21/75	0130		.940		10/22/75	1130			.390
10/21/75	0200		.960		10/22/75	1200			.390
10/21/75	0230		.960		10/22/75	1230			.390
10/21/75	0300		.960		10/22/75	1300			.360
10/21/75	0330		.970		10/22/75	1330			.380
10/21/75	0400		.980		10/22/75	1400			.380
10/21/75	0430		.980		10/22/75	1430			.400
10/21/75	0500		.980		10/22/75	1500			.400
10/21/75	0530		.980		10/22/75	1530			.450
10/21/75	0600		.980		10/22/75	1600			.450
10/21/75	0630		.980		10/22/75	1630			.450
10/21/75	0700		.980		10/22/75	1700			.450
10/21/75	0730		.980		10/22/75	1730			.510
10/21/75	0800		.980		10/22/75	1800			.530
10/21/75	0830		.980		10/22/75	1830			.560
10/21/75	0900		.980		10/22/75	1900			.560
10/21/75	0930		.980		10/22/75	1930			147-.540
10/21/75	1000		.980		10/22/75	2000			.540
10/21/75	1030		.980		10/22/75	2030			.530
10/21/75	1100		.980		10/22/75	2100			.560
10/21/75	1130		.980		10/22/75	2130			.560
10/21/75	1200		.980		10/22/75	2200			.580
10/21/75	1230		.980		10/22/75	2230			.490
10/21/75	1300		.980		10/22/75	2300			.490

ARCE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE	TIME	FLOW RATE / (GPM)	DOWNHOLE / PRESSURE / (PSIA)	WELL HEAD / PRESSURE / (PSIA)	REMARKS
10/25/75	2130			.800	
10/25/75	2200			.846	
10/25/75	2300			1.64-0.00	
10/25/75	2330			.870	
10/26/75	0000			.800	
10/26/75	0030			.823	
10/26/75	0100			.887	
10/26/75	0130			.881	
10/26/75	0200			1.67-0.00	
10/26/75	0230			.905	
10/26/75	0300			.969	
10/26/75	0330			.963	
10/26/75	0400			.969	
10/26/75	0430			1.67-0.00	
10/26/75	0500			.903	
10/26/75	0500			.958	
10/26/75	0530			.963	
10/26/75	0600			.978	
10/26/75	0700			.990	
10/26/75	0730			.996	
10/26/75	0800			1.68-0.07	
10/26/75	0830			.836	
10/26/75	0900			.866	
10/26/75	0930			.861	
10/26/75	1000			.871	
10/26/75	1030			.888	
10/26/75	1100			.890	
10/26/75	1130			.889	
10/26/75	1200			.813	
10/26/75	1230			.831	
10/26/75	1300			.836	
10/26/75	1330			.862	
10/26/75	1400			.867	
10/26/75	1430			.862	
10/26/75	1500			.882	
10/26/75	1530			.882	
10/26/75	1600			.842	
10/26/75	1700			.867	
10/26/75	1800			.852	
10/26/75	1830			.852	
10/26/75	1900			.850	
10/26/75	1930			.876	
10/26/75	2000			.874	
10/26/75	2030			.865	
10/26/75	2100			.865	
10/26/75	2130			.861	
10/26/75	2200			.861	
10/26/75	2230			.861	
10/26/75	2300			.861	
10/26/75	2330			.885	
10/26/75	0000			.881	
10/26/75	0030			.896	
10/26/75	0100			.891	
10/26/75	0130			.891	
10/26/75	0200			.891	
10/26/75	0230			.896	
10/26/75	0300			.896	
10/26/75	0330			.885	
10/26/75	0400			.885	
10/26/75	0430			.860	
10/26/75	0500			.868	
10/26/75	0530			.863	
10/26/75	0600			.858	
10/26/75	0630			.850	
10/26/75	0700			.867	
10/26/75	0730			.867	
10/26/75	0800			.858	
10/26/75	0830			.858	
10/26/75	0900			.874	
10/26/75	0930			.895	
10/26/75	1000			.895	
10/26/75	1030			.895	
10/26/75	1100			.895	
10/26/75	1130			.895	
10/26/75	1200			.895	
10/26/75	1230			.895	
10/26/75	1300			.895	
10/26/75	1330			.895	
10/26/75	1400			.895	
10/26/75	1430			.895	
10/26/75	1500			.895	
10/26/75	1530			.895	
10/26/75	1600			.895	
10/26/75	1630			.895	
10/26/75	1700			.895	
10/26/75	1730			.895	
10/26/75	1800			.895	
10/26/75	1830			.895	
10/26/75	1900			.895	
10/26/75	1930			.895	
10/26/75	2000			.895	
10/26/75	2030			.895	
10/26/75	2100			.895	
10/26/75	2130			.895	
10/26/75	2200			.895	
10/26/75	2230			.895	
10/26/75	2300			.895	
10/26/75	2330			.895	
10/27/75	0000			.895	
10/27/75	0030			.895	
10/27/75	0100			.895	
10/27/75	0130			.895	
10/27/75	0200			.895	
10/27/75	0230			.895	
10/27/75	0300			.895	
10/27/75	0330			.895	
10/27/75	0400			.895	
10/27/75	0430			.895	
10/27/75	0500			.895	
10/27/75	0530			.895	
10/27/75	0600			.895	
10/27/75	0630			.895	
10/27/75	0700			.895	
10/27/75	0730			.895	
10/27/75	0800			.895	
10/27/75	0830			.895	
10/27/75	0900			.895	
10/27/75	0930			.895	
10/27/75	1000			.895	
10/27/75	1030			.895	
10/27/75	1100			.895	
10/27/75	1130			.895	
10/27/75	1200			.895	
10/27/75	1230			.895	
10/27/75	1300			.895	
10/27/75	1330			.895	
10/27/75	1400			.895	
10/27/75	1430			.895	
10/27/75	1500			.895	
10/27/75	1530			.895	
10/27/75	1600			.895	
10/27/75	1630			.895	
10/27/75	1700			.895	
10/27/75	1730			.895	
10/27/75	1800			.895	
10/27/75	1830			.895	
10/27/75	1900			.895	
10/27/75	1930			.895	

ARCE 1 INTERFERENCE TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / TIME	FLOW RATE / (GPM)	DOWNHOLE / PRESSURE / (PSIA)	WELL HEAD / PRESSURE / (PSIA)	REMARKS
10/25/75	2130		.080	
10/25/75	2200		.080	
10/25/75	2230			
10/25/75	2300	140.000		
10/25/75	2330	.070		
10/26/75	0000		.060	
10/26/75	0030		.033	
10/26/75	0100		.007	
10/26/75	0130		.001	
10/26/75	0200	147.500		
10/26/75	0230		.005	
10/26/75	0300		.009	
10/26/75	0330		.049	
10/26/75	0400	147.500		
10/26/75	0430		.003	
10/26/75	0500		.000	
10/26/75	0600		.001	
10/26/75	0630		.001	
10/26/75	0700		.000	
10/26/75	0730		.000	
10/26/75	0800	146.007		
10/26/75	0830		.034	
10/26/75	0900		.046	
10/26/75	0930		.061	
10/26/75	1000		.071	
10/26/75	1030		.000	
10/26/75	1100		.000	
10/26/75	1130		.009	
10/26/75	1200		.009	
10/26/75	1230		.111	
10/26/75	1300		.116	
10/26/75	1330		.112	
10/26/75	1400		.117	
10/26/75	1430		.117	
10/26/75	1500		.162	
10/26/75	1530		.167	
10/26/75	1600		.182	
10/26/75	1630		.187	
10/26/75	1700		.212	
10/26/75	1730		.167	
10/26/75	1800		.182	
10/26/75	1830		.182	
10/26/75	1900		.182	
10/26/75	1930		.176	
10/26/75	2000		.176	
10/26/75	2030		.185	
10/26/75	2100		.201	
10/26/75	2130		.201	
10/26/75	2200		.200	
10/26/75	2230		.201	
10/26/75	2300		.201	
10/26/75	2330		.200	
10/26/75	2400		.200	
10/26/75	2430		.201	
10/26/75	2500		.200	
10/26/75	2530		.201	
10/26/75	2600		.200	
10/26/75	2630		.201	
10/26/75	2700		.200	
10/26/75	2730		.200	
10/26/75	2800		.200	
10/26/75	2830		.200	
10/26/75	2900		.200	
10/26/75	2930		.200	
10/26/75	3000		.200	
10/26/75	3030		.200	
10/26/75	3100		.200	
10/26/75	3130		.200	
10/26/75	3200		.200	
10/26/75	3230		.200	
10/26/75	3300		.200	
10/26/75	3330		.200	
10/26/75	3400		.200	
10/26/75	3430		.200	
10/26/75	3500		.200	
10/26/75	3530		.200	
10/26/75	3600		.200	
10/26/75	3630		.200	
10/26/75	3700		.200	
10/26/75	3730		.200	
10/26/75	3800		.200	
10/26/75	3830		.200	
10/26/75	3900		.200	
10/26/75	3930		.200	
10/26/75	4000		.200	
10/26/75	4030		.200	
10/26/75	4100		.200	
10/26/75	4130		.200	
10/26/75	4200		.200	
10/26/75	4230		.200	
10/26/75	4300		.200	
10/26/75	4330		.200	
10/26/75	4400		.200	
10/26/75	4430		.200	
10/26/75	4500		.200	
10/26/75	4530		.200	
10/26/75	4600		.200	
10/26/75	4630		.200	
10/26/75	4700		.200	
10/26/75	4730		.200	
10/26/75	4800		.200	
10/26/75	4830		.200	
10/26/75	4900		.200	
10/26/75	4930		.200	
10/26/75	5000		.200	
10/26/75	5030		.200	
10/26/75	5100		.200	
10/26/75	5130		.200	
10/26/75	5200		.200	
10/26/75	5230		.200	
10/26/75	5300		.200	
10/26/75	5330		.200	
10/26/75	5400		.200	
10/26/75	5430		.200	
10/26/75	5500		.200	
10/26/75	5530		.200	
10/26/75	5600		.200	
10/26/75	5630		.200	
10/26/75	5700		.200	
10/26/75	5730		.200	
10/26/75	5800		.200	
10/26/75	5830		.200	
10/26/75	5900		.200	
10/26/75	5930		.200	
10/26/75	6000		.200	
10/26/75	6030		.200	
10/26/75	6100		.200	
10/26/75	6130		.200	
10/26/75	6200		.200	
10/26/75	6230		.200	
10/26/75	6300		.200	
10/26/75	6330		.200	
10/26/75	6400		.200	
10/26/75	6430		.200	
10/26/75	6500		.200	
10/26/75	6530		.200	
10/26/75	6600		.200	
10/26/75	6630		.200	
10/26/75	6700		.200	
10/26/75	6730		.200	
10/26/75	6800		.200	
10/26/75	6830		.200	
10/26/75	6900		.200	
10/26/75	6930		.200	
10/26/75	7000		.200	
10/26/75	7030		.200	
10/26/75	7100		.200	
10/26/75	7130		.200	
10/26/75	7200		.200	
10/26/75	7230		.200	
10/26/75	7300		.200	
10/26/75	7330		.200	
10/26/75	7400		.200	
10/26/75	7430		.200	
10/26/75	7500		.200	
10/26/75	7530		.200	
10/26/75	7600		.200	
10/26/75	7630		.200	
10/26/75	7700		.200	
10/26/75	7730		.200	
10/26/75	7800		.200	
10/26/75	7830		.200	
10/26/75	7900		.200	
10/26/75	7930		.200	
10/26/75	8000		.200	
10/26/75	8030		.200	
10/26/75	8100		.200	
10/26/75	8130		.200	
10/26/75	8200		.200	
10/26/75	8230		.200	
10/26/75	8300		.200	
10/26/75	8330		.200	
10/26/75	8400		.200	
10/26/75	8430		.200	
10/26/75	8500		.200	
10/26/75	8530		.200	
10/26/75	8600		.200	
10/26/75	8630		.200	
10/26/75	8700		.200	
10/26/75	8730		.200	
10/26/75	8800		.200	
10/26/75	8830		.200	
10/26/75	8900		.200	
10/26/75	8930		.200	
10/26/75	9000		.200	
10/26/75	9030		.200	
10/26/75	9100		.200	
10/26/75	9130		.200	
10/26/75	9200		.200	
10/26/75	9230		.200	
10/26/75	9300		.200	
10/26/75	9330		.200	
10/26/75	9400		.200	
10/26/75	9430		.200	
10/26/75	9500		.200	
10/26/75	9530		.200	
10/26/75	9600		.200	
10/26/75	9630		.200	
10/26/75	9700		.200	
10/26/75	9730		.200	
10/26/75	9800		.200	
10/26/75	9830		.200	
10/26/75	9900		.200	
10/26/75	9930		.200	
10/26/75	10000		.200	
10/26/75	10030		.200	
10/26/75	10100		.200	
10/26/75	10130		.200	
10/26/75	10200		.200	
10/26/75	10230		.200	
10/26/75	10300		.200	
10/26/75	10330		.200	
10/26/75	10400		.200	
10/26/75	10430		.200	
10/26/75	10500		.200	
10/26/75	10530		.200	
10/26/75	10600		.200	
10/26/75	10630		.200	
10/26/75	10700		.200	
10/26/75	10730		.200	
10/26/75	10800		.200	
10/26/75	10830		.200	
10/26/75	10900		.200	
10/26/75	10930		.200	
10/26/75	11000		.200	
10/26/75	11030		.200	
10/26/75	11100		.200	
10/26/75	11130		.200	
10/26/75	11200		.200	
10/26/75	11230		.200	
10/26/75	11300		.200	
10/26/75	11330		.200	
10/26/75	11400		.200	
10/26/75	11430		.200	
10/26/75	11500		.200	
10/26/75	11530		.200	
10/26/75	11600		.200	
10/26/75	11630		.200	
10/26/75	11700		.200	
10/26/75	11730		.200	
10/26/75	11800		.200	
10/26/75	11830		.200	
10/26/75	11900		.200	
10/26/75	11930		.200	
10/26/75	12000		.200	
10/26/75	12030		.200	
10/26/75	12100		.200	
10/26/75	12130		.200	
10/26/75	12200		.200	
10/26/75	12230		.200	
10/26/75	12300		.200	
10/26/75	12330		.200	
10/26/75	12400		.200	
10/26/75	12430		.200	
10/26/75	12500		.200	
10/26/75	12530		.200	
10/26/75	12600		.200	
10/26/75	12630		.200	
10/26/75	12700		.200	
10/26/75	12730		.200	
10/26/75	12800		.200	
10/26/75	12830		.200	
10/26/75	12900		.200	
10/26/75	12930		.200	
10/26/75	13000		.200	
10/26/75	13030		.200	
10/26/75	13100		.200	
10/26/75	13130		.200	
10/26/75	13200		.200	
10/26/75	13230		.200	
10/26/75	13300		.200	
10/26/75	13330		.200	
10/26/75	13400		.200	
10/26/75	13430		.200	
10/26/75	13500		.200	
10/26/75	13530		.200	
10/26/75	13600		.200	
10/26/75	13630		.200	
10/26/75	13700		.200	
10/26/75	13730		.200	
10/26/75	13800		.200	
10/26				

APPENDIX 3

RRGE 1 SHORT-TERM TEST DATA.

RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

APPENDIX 3

RRGE 1 SHORT-TERM TEST DATA.

RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

ARGE 1 SHORT-TERM TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDMC

DATE	TIME	FLOW RATE / (GPM)	DOWNHOLE / PRESSURE / (PSIA)	WELL HEAD / PRESSURE / (PSIA)	REMARKS
11/06/75	170000		2082.392		
11/06/75	171000		2082.394		
11/06/75	172000		2082.395		
11/06/75	173000		2082.379		
11/06/75	174000		2082.373		
11/06/75	175000		2082.399		
11/06/75	180000		2082.395		
11/06/75	181000		2082.417		
11/06/75	182000		2082.395		
11/06/75	183000		2082.380		
11/06/75	184000		2082.380		
11/06/75	185000		2082.403		
11/06/75	190000		2082.409		
11/06/75	191000		2082.387		
11/06/75	192000		2082.419		
11/06/75	193000		2082.413		
11/06/75	194000		2082.384		
11/06/75	195000		2082.355		
11/06/75	200000		2082.323		
11/06/75	201000		2082.363		
11/06/75	202000		2082.390		
11/06/75	203000		2082.351		
11/06/75	204000		2082.342		
11/06/75	205000		2082.351		
11/06/75	210000		2082.341		
11/06/75	211000		2082.333		
11/06/75	212000		2082.324		
11/06/75	213000		2082.337		
11/06/75	214000		2082.285		
11/06/75	215000		2082.267		
11/06/75	220000		2082.297		
11/06/75	221000		2082.258		
11/06/75	222000		2082.295		
11/06/75	223000		2082.234		
11/06/75	224000		2082.286		
11/06/75	225000		2082.244		
11/06/75	230000		2082.215		
11/06/75	231000		2082.213		
11/06/75	232000		2082.212		
11/06/75	233000		2082.236		
11/06/75	234000		2082.237		
11/06/75	235000		2082.189		
11/05/75	000000		2082.244		
11/05/75	001000		2082.239		
11/05/75	002000		2082.229		
11/05/75	003000		2082.201		
11/05/75	004000		2082.192		
11/05/75	005000		2082.244		
11/05/75	010000		2082.169		
11/05/75	011000		2082.208		
11/05/75	012000		2082.197		
11/05/75	013000		2082.202		
11/05/75	014000		2082.223		
11/05/75	015000		2082.200		
11/05/75	020000		2082.248		
11/05/75	021000		2082.251		
11/05/75	022000		2082.251		
11/05/75	023000		2082.233		
11/05/75	024000		2082.239		
11/05/75	025000		2082.244		
11/05/75	030000		2082.273		
11/05/75	031000		2082.247		
11/05/75	032000		2082.289		
11/05/75	033000		2082.259		
11/05/75	034000		2082.272		
11/05/75	035000		2082.268		
11/05/75	040000		2082.279		
11/05/75	041000		2082.281		
11/05/75	042000		2082.336		
11/05/75	043000		2082.305		
11/05/75	044000		2082.300		
11/05/75	045000		2081.578		
11/05/75	046000		2081.573		
11/05/75	047000		2081.598		
11/05/75	048000		2081.591		
11/05/75	049000		2081.583		
11/05/75	050000		2081.578		
11/05/75	051000		2081.596		
11/05/75	052000		2082.371		
11/05/75	053000		2082.396		
11/05/75	054000		2082.410		
11/05/75	055000		2082.394		
11/05/75	056000		2082.392		
11/05/75	057000		2082.368		
11/05/75	058000		2082.381		
11/05/75	059000		2082.423		
11/05/75	060000		2082.419		
11/05/75	070000		2082.429		
11/05/75	071000		2082.429		
11/05/75	072000		2082.429		
11/05/75	073000		2082.429		
11/05/75	074000		2082.429		
11/05/75	075000		2082.429		
11/05/75	076000		2082.429		
11/05/75	077000		2082.429		
11/05/75	078000		2082.429		
11/05/75	079000		2082.429		
11/05/75	080000		2082.429		
11/05/75	081000		2082.429		
11/05/75	082000		2082.429		
11/05/75	083000		2082.429		
11/05/75	084000		2082.429		
11/05/75	085000		2082.429		
11/05/75	086000		2082.429		
11/05/75	087000		2082.429		
11/05/75	088000		2082.429		
11/05/75	089000		2082.429		
11/05/75	090000		2082.429		
11/05/75	091000		2082.429		
11/05/75	092000		2082.429		
11/05/75	093000		2082.429		
11/05/75	094000		2082.429		
11/05/75	095000		2082.429		
11/05/75	096000		2082.429		
11/05/75	097000		2082.429		
11/05/75	098000		2082.429		
11/05/75	099000		2082.429		
11/05/75	100000		2082.429		
11/05/75	101000		2082.429		
11/05/75	102000		2082.429		
11/05/75	103000		2082.429		
11/05/75	104000		2082.429		
11/05/75	105000		2082.429		
11/05/75	106000		2082.429		
11/05/75	107000		2082.429		
11/05/75	108000		2082.429		
11/05/75	109000		2082.429		
11/05/75	110000		2082.429		
11/05/75	111000		2082.429		
11/05/75	112000		2082.429		
11/05/75	113000		2082.429		
11/05/75	114000		2082.429		
11/05/75	115000		2082.429		
11/05/75	116000		2082.429		
11/05/75	117000		2082.429		
11/05/75	118000		2082.429		
11/05/75	119000		2082.429		
11/05/75	120000		2082.429		
11/05/75	121000		2082.429		
11/05/75	122000		2082.429		
11/05/75	123000		2082.429		
11/05/75	124000		2082.429		
11/05/75	125000		2082.429		
11/05/75	126000		2082.429		
11/05/75	127000		2082.429		
11/05/75	128000		2082.429		
11/05/75	129000		2082.429		
11/05/75	130000		2082.429		
11/05/75	131000		2082.429		
11/05/75	132000		2082.429		
11/05/75	133000		2082.429		
11/05/75	134000		2082.429		
11/05/75	135000		2082.429		
11/05/75	136000		2082.429		
11/05/75	137000		2082.429		
11/05/75	138000		2082.429		
11/05/75	139000		2082.429		
11/05/75	140000		2082.429		
11/05/75	141000		2082.429		
11/05/75	142000		2082.429		
11/05/75	143000		2082.429		
11/05/75	144000		2082.429		
11/05/75	145000		2082.429		
11/05/75	146000		2082.429		
11/05/75	147000		2082.429		
11/05/75	148000		2082.429		
11/05/75	149000		2082.429		
11/05/75	150000		2082.429		
11/05/75	151000		2082.429		
11/05/75	152000		2082.429		
11/05/75	153000		2082.429		
11/05/75	154000		2082.429		
11/05/75	155000		2082.429		
11/05/75	156000		2082.429		
11/05/75	157000		2082.429		
11/05/75	158000		2082.429		
11/05/75	159000		2082.429		
11/05/75	160000		2082.429		
11/05/75	161000		2082.429		
11/05/75	162000		2082.429		
11/05/75	163000		2082.429		
11/05/75	164000		2082.429		
11/05/75	165000		2082.429		
11/05/75	166000		2082.429		
11/05/75	167000		2082.429		
11/05/75	168000		2082.429		
11/05/75	169000		2082.429		
11/05/75	170000		2082.429		
11/05/75	171000		2082.429		
11/05/75	172000		2082.429		
11/05/75	173000		2082.429		
11/05/75	174000		2082.429		
11/05/75	175000		2082.429		
11/05/75	176000		2082.429		
11/05/75	177000		2082.429		
11/05/75	178000		2082.429		
11/05/75	179000		2082.429		
11/05/75	180000		2082.429		
11/05/75	181000		2082.429		
11/05/75	182000		2082.429		
11/05/75	183000		2082.429		
11/05/75	184000		2082.429		
11/05/75	185000		2082.429		
11/05/75	186000		2082.429		
11/05/75	187000		2082.429		
11/05/75	188000		2082.429		
11/05/75	189000		2082.429		
11/05/75	190000		2082.429		
11/05/75	191000		2082.429		
11/05/75	192000		2082.429		
11/05/75	193000		2082.429		
11/05/75	194000		2082.429		
11/05/75	195000		2082.429		
11/05/75	196000		2082.429		
11/05/75	197000		2082.429		
11/05/75	198000		2082.429		
11/05/75	199000		2082.429		
11/05/75	200000		2082.429		
11/05/75	201000		2082.429		
11/05/75	202000		2082.429		
11/05/75	203000		2082.429		
11/05/75	204000		2082.429		
11/05/75	205000		2082.429		
11/05/75	206000		2082.429		
11/05/75	207000		2082.429		
11/05/75	208000				

RRGE 1 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / TIME / FLOW RATE / DOWNHOLE / WELL HEAD / REMARKS	DATE / TIME / FLOW RATE / DOWNHOLE / WELL HEAD / REMARKS
/ / (GPM) / PRESSURE / PRESSURE /	/ / (GPM) / PRESSURE / PRESSURE /
/ / (PSIA) / (PSIA) /	/ / (PSIA) / (PSIA) /
11/05/75 084820 2081.567	11/05/75 090000 2081.462
11/05/75 084830 2081.564	11/05/75 090200 2081.452
11/05/75 084840 2081.557	11/05/75 090400 2081.463
11/05/75 084850 2081.556	11/05/75 090600 2081.467
11/05/75 084900 2081.622	11/05/75 090800 2081.439
11/05/75 084910 2081.546	11/05/75 091000 2081.435
11/05/75 084920 2081.542	11/05/75 091200 2081.424
11/05/75 084930 2081.538	11/05/75 091400 2081.411
11/05/75 084940 2081.537	11/05/75 091600 2081.415
11/05/75 084950 2081.533	11/05/75 091800 2081.419
11/05/75 085000 2081.532	11/05/75 092000 2081.415
11/05/75 085010 2081.530	11/05/75 092200 2081.407
11/05/75 085020 2081.529	11/05/75 092400 2081.403
11/05/75 085030 2081.528	11/05/75 092600 2081.397
11/05/75 085040 2081.527	11/05/75 092800 2081.398
11/05/75 085050 2081.525	11/05/75 093000 2081.430
11/05/75 085100 2081.524	11/05/75 093200 2081.430
11/05/75 085110 2081.521	11/05/75 093400 2081.431
11/05/75 085120 2081.517	11/05/75 093600 2081.395
11/05/75 085130 2081.515	11/05/75 093800 2081.432
11/05/75 085140 2081.515	11/05/75 094000 2081.407
11/05/75 085150 2081.515	11/05/75 094200 2081.401
11/05/75 085200 2081.513	11/05/75 094400 2081.402
11/05/75 085210 2081.511	11/05/75 094600 2081.406
11/05/75 085220 2081.505	11/05/75 094800 2081.411
11/05/75 085230 2081.500	11/05/75 095000 2081.421
11/05/75 085240 2081.495	11/05/75 095200 2081.414
11/05/75 085250 2081.491	11/05/75 095400 2081.412
11/05/75 085300 2081.492	11/05/75 095600 2081.408
11/05/75 085310 2081.493	11/05/75 095800 2081.398
11/05/75 085320 2081.494	11/05/75 096000 2081.377
11/05/75 085330 2081.497	11/05/75 096200 2081.376
11/05/75 085340 2081.500	11/05/75 096400 2081.379
11/05/75 085350 2081.500	11/05/75 096600 2081.377
11/05/75 085400 2081.503	11/05/75 096800 2081.368
11/05/75 085410 2081.503	11/05/75 097000 2081.362
11/05/75 085420 2081.503	11/05/75 097200 2081.374
11/05/75 085430 2081.504	11/05/75 097400 2081.373
11/05/75 085440 2081.503	11/05/75 097600 2081.372
11/05/75 085450 2081.500	11/05/75 097800 2081.372
11/05/75 085500 2081.497	11/05/75 098000 2081.381
11/05/75 085510 2081.500	11/05/75 098200 2081.380
11/05/75 085520 2081.499	11/05/75 098400 2081.377
11/05/75 085530 2081.496	11/05/75 098600 2081.368
11/05/75 085540 2081.494	11/05/75 098800 2081.377
11/05/75 085550 2081.494	11/05/75 099000 2081.391
11/05/75 085600 2081.494	11/05/75 099200 2081.406
11/05/75 085610 2081.491	11/05/75 099400 2081.406
11/05/75 085620 2081.491	11/05/75 099600 2081.394
11/05/75 085630 2081.490	11/05/75 099800 2081.390
11/05/75 085640 2081.489	11/05/75 100000 2081.389
11/05/75 085650 2081.485	11/05/75 099500 2081.372
11/05/75 085700 2081.484	11/05/75 099700 2081.359
11/05/75 085710 2081.485	11/05/75 099900 2081.345
11/05/75 085720 2081.485	11/05/75 100100 2081.333
11/05/75 085730 2081.481	11/05/75 100300 2081.340
11/05/75 085740 2081.479	11/05/75 100500 2081.342
11/05/75 085750 2081.478	11/05/75 100700 2081.339
11/05/75 085800 2081.472	11/05/75 100900 2081.329
11/05/75 085810 2081.471	11/05/75 101100 2081.322
11/05/75 085820 2081.473	11/05/75 101300 2081.322
11/05/75 085830 2081.469	11/05/75 101500 2081.320
11/05/75 085840 2081.469	11/05/75 101700 2081.325
11/05/75 085850 2081.470	11/05/75 101900 2081.311
11/05/75 085900 2081.467	11/05/75 102100 2081.311
11/05/75 085910 2081.466	11/05/75 102300 2081.306
11/05/75 085920 2081.465	11/05/75 102500 2081.306
11/05/75 085930 2081.464	11/05/75 102700 2081.303
11/05/75 085940 2081.465	11/05/75 102900 2081.300
11/05/75 085950 2081.464	11/05/75 103100 2081.292
	11/05/75 103300 2081.297

RAGE 1 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, 104M7

DATE / TIME /	FLOW RATE / (GPM) /	WELL HEAD / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS	DATE / TIME /	FLOW RATE / (GPM) /	WELL HEAD / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
11/06/75	064000		2081.200		11/06/75	144319		2081.14	
11/06/75	065000		2081.202		11/06/75	144320		2081.14	
11/06/75	070000		2081.231		11/06/75	144321		2081.13	
11/06/75	071000		2081.104		11/06/75	144322		2081.13	
11/06/75	072000		2081.212		11/06/75	144323		2081.13	
11/06/75	073000		2081.213		11/06/75	144324		2081.14	
11/06/75	074000		2081.185		11/06/75	144325		2081.14	
11/06/75	075000		2081.225		11/06/75	144326		2081.14	
11/06/75	080000		2081.235		11/06/75	144327		2081.14	
11/06/75	081000		2081.208		11/06/75	144328		2081.14	
11/06/75	082000		2081.162		11/06/75	144329		2081.14	
11/06/75	083000		2081.274		11/06/75	144330		2081.15	
11/06/75	084000		2081.268		11/06/75	144331		2081.14	
11/06/75	085000		2081.214		11/06/75	144332		2081.13	
11/06/75	090000		2081.137		11/06/75	144334		2081.14	
11/06/75	091000		2081.206		11/06/75	144335		2081.14	
11/06/75	092000		2081.245		11/06/75	144336		2081.14	
11/06/75	093000		2081.211		11/06/75	144337		2081.14	
11/06/75	094000		2081.245		11/06/75	144338		2081.15	
11/06/75	095000		2081.228		11/06/75	144339		2081.15	
11/06/75	100000		2081.196		11/06/75	144340		2081.14	
11/06/75	101000		2081.215		11/06/75	144342		2081.14	
11/06/75	102000		2081.257		11/06/75	144343		2081.15	
11/06/75	103000		2081.248		11/06/75	144344		2081.14	
11/06/75	104000		2081.209		11/06/75	144345		2081.14	
11/06/75	105000		2081.206		11/06/75	144346		2081.15	
11/06/75	110000		2081.160		11/06/75	144347		2081.15	
11/06/75	111000		2081.181		11/06/75	144348		2081.15	
11/06/75	112000		2081.164		11/06/75	144350		2081.15	
11/06/75	113000		2081.206		11/06/75	144351		2081.14	
11/06/75	114000		2081.267		11/06/75	144352		2081.15	
11/06/75	115000		2081.208		11/06/75	144353		2081.15	
11/06/75	120000		2081.217		11/06/75	144354		2081.15	
11/06/75	121000		2081.268		11/06/75	144355		2081.14	
11/06/75	122000		2081.124		11/06/75	144356		2081.15	
11/06/75	123000		2081.164		11/06/75	144358		2081.16	
11/06/75	124000		2081.146		11/06/75	144359		2081.15	
11/06/75	125000		2081.139		11/06/75	144400		2081.15	
11/06/75	130000		2081.144		11/06/75	144401		2081.17	
11/06/75	131000		2081.108		11/06/75	144402		2081.15	
11/06/75	132000		2081.076		11/06/75	144403		2081.15	
11/06/75	133000		2081.188		11/06/75	144404		2081.15	
11/06/75	134000		2081.185		11/06/75	144406		2081.16	
11/06/75	135000		2081.188		11/06/75	144407		2081.16	
11/06/75	140000		2081.120		11/06/75	144408		2081.15	
11/06/75	141000		2081.207		11/06/75	144409		2081.15	
11/06/75	142000		2081.127		11/06/75	144410		2081.15	
11/06/75	143000		2081.09		11/06/75	144411		2081.16	
11/06/75	143600		2081.11		11/06/75	144412		2081.15	
11/06/75	143700		2081.13		11/06/75	144414		2081.15	
11/06/75	143800		2081.15		11/06/75	144415		2081.16	
11/06/75	143900		2081.14		11/06/75	144416		2081.15	
11/06/75	144000		2081.13		11/06/75	144417		2081.16	
11/06/75	144100		2081.13		11/06/75	144418		2081.16	
11/06/75	144259		2081.15		11/06/75	144419		2081.17	
11/06/75	144301		2081.14		11/06/75	144420		2081.16	
11/06/75	144302		2081.14		11/06/75	144422		2081.16	
11/06/75	144303		2081.15		11/06/75	144423		2081.17	
11/06/75	144304		2081.14		11/06/75	144424		2081.16	
11/06/75	144305		2081.13		11/06/75	144425		2081.15	
11/06/75	144306		2081.14		11/06/75	144426		2081.16	
11/06/75	144308		2081.15		11/06/75	144427		2081.17	
11/06/75	144310		2081.14		11/06/75	144428		2081.16	
11/06/75	144311		2081.14		11/06/75	144430		2081.15	
11/06/75	144312		2081.13		11/06/75	144431		2081.17	
11/06/75	144313		2081.15		11/06/75	144432		2081.16	
11/06/75	144314		2081.15		11/06/75	144433		2081.16	
11/06/75	144315		2081.14		11/06/75	144434		2081.16	
11/06/75	144316		2081.14		11/06/75	144435		2081.17	
11/06/75	144318		2081.14		11/06/75	144436		2081.16	

TABLE 1 SHORT-TERM TEST DATA, PUMP TESTS IN THE GEOTHERMAL FIELD, 1975

DATE	TIME	FLOW RATE / (GPM)	DOWNHOLE / PRESSURE / (PSIA)	WELL HEAD / PRESSURE / (PSIA)	REMARKS
11/05/75	064000		2081.200		
11/05/75	064300		2081.202		
11/05/75	071000		2081.201		
11/06/75	075000		2081.109		
11/06/75	072000		2081.212		
11/06/75	073000		2081.213		
11/06/75	074000		2081.185		
11/06/75	075000		2081.225		
11/06/75	080000		2081.225		
11/06/75	081000		2081.208		
11/06/75	082000		2081.162		
11/05/75	083000		2081.276		
11/06/75	084000		2081.258		
11/06/75	085000		2081.214		
11/06/75	090000		2081.197		
11/06/75	091000		2081.236		
11/06/75	092000		2081.245		
11/06/75	093000		2081.211		
11/06/75	094000		2081.245		
11/06/75	095000		2081.228		
11/06/75	100000		2081.196		
11/06/75	101000		2081.215		
11/06/75	102000		2081.257		
11/06/75	103000		2081.248		
11/06/75	104000		2081.209		
11/06/75	105000		2081.206		
11/06/75	110000		2081.160		
11/06/75	111000		2081.181		
11/06/75	112000		2081.164		
11/06/75	113000		2081.236		
11/06/75	114000		2081.267		
11/06/75	115000		2081.208		
11/06/75	120000		2081.217		
11/06/75	121000		2081.268		
11/06/75	122000		2081.124		
11/06/75	123000		2081.164		
11/06/75	124000		2081.146		
11/06/75	125000		2081.139		
11/06/75	130000		2081.144		
11/06/75	131000		2081.108		
11/06/75	132000		2081.076		
11/06/75	133000		2081.188		
11/06/75	134000		2081.185		
11/06/75	135000		2081.188		
11/06/75	140000		2081.120		
11/06/75	141000		2081.207		
11/06/75	142000		2081.127		
11/06/75	143000		2081.09		
11/06/75	143600		2081.11		
11/06/75	143700		2081.13		
11/06/75	143800		2081.15		
11/06/75	143900		2081.14		
11/06/75	144000		2081.13		
11/06/75	144100		2081.13		
11/06/75	144259		2081.15		
11/06/75	144301		2081.14		
11/06/75	144302		2081.14		
11/06/75	144303		2081.15		
11/06/75	144304		2081.14		
11/06/75	144305		2081.13		
11/06/75	144306		2081.14		
11/06/75	144308		2081.15		
11/06/75	144310		2081.14		
11/06/75	144311		2081.14		
11/06/75	144312		2081.13		
11/06/75	144313		2081.15		
11/06/75	144314		2081.15		
11/06/75	144315		2081.14		
11/06/75	144316		2081.14		
11/06/75	144318		2081.14		
11/06/75	144319		2081.14		
11/06/75	144320		2081.14		
11/06/75	144321		2081.14		
11/06/75	144322		2081.14		
11/06/75	144327		2081.14		
11/06/75	144328		2081.14		
11/06/75	144329		2081.14		
11/06/75	144330		2081.15		
11/06/75	144331		2081.14		
11/06/75	144332		2081.13		
11/06/75	144334		2081.13		
11/06/75	144335		2081.14		
11/06/75	144336		2081.15		
11/06/75	144337		2081.14		
11/06/75	144338		2081.14		
11/06/75	144339		2081.15		
11/06/75	144340		2081.14		
11/06/75	144342		2081.14		
11/06/75	144343		2081.15		
11/06/75	144344		2081.14		
11/06/75	144345		2081.14		
11/06/75	144346		2081.15		
11/06/75	144347		2081.15		
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11/06/75	144352		2081.15		
11/06/75	144353		2081.15		
11/06/75	144354		2081.15		
11/06/75	144355		2081.14		
11/06/75	144356		2081.15		
11/06/75	144358		2081.16		
11/06/75	144359		2081.15		
11/06/75	144400		2081.15		
11/06/75	144401		2081.17		
11/06/75	144402		2081.15		
11/06/75	144403		2081.15		
11/06/75	144404		2081.15		
11/06/75	144406		2081.16		
11/06/75	144407		2081.16		
11/06/75	144408		2081.15		
11/06/75	144409		2081.15		
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11/06/75	144411		2081.16		
11/06/75	144412		2081.15		
11/06/75	144414		2081.15		
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11/06/75	144416		2081.15		
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11/06/75	144432		2081.16		
11/06/75	144433		2081.16		
11/06/75	144434		2081.16		
11/06/75	144435		2081.17		
11/06/75	144436		2081.16		

RRGE I SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

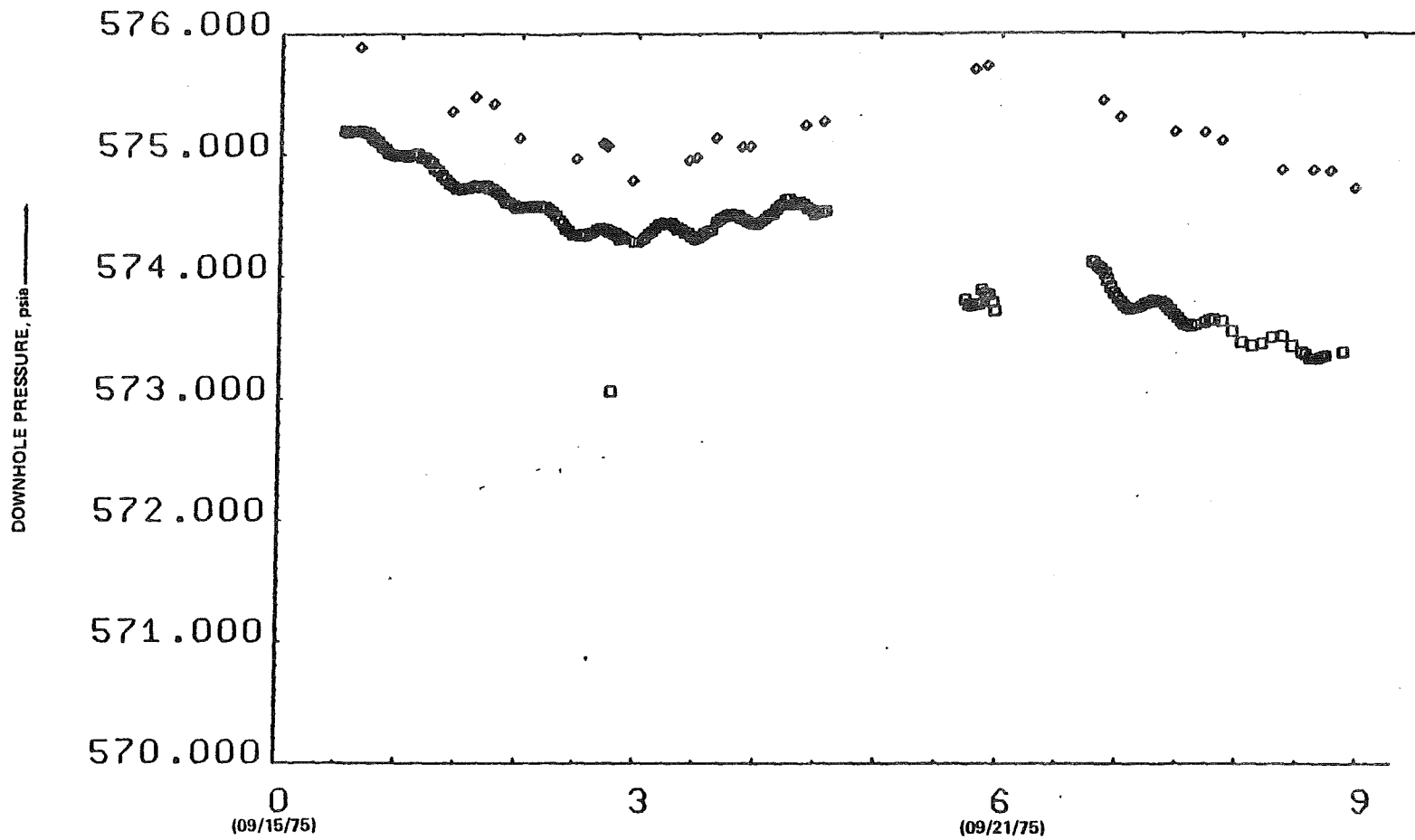
DATE / / /	TIME /	FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS	DATE / / /	TIME /	FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS
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11/06/75	144442		2081.16			11/06/75	144600		2082.02		
11/06/75	144443		2081.17			11/06/75	144601		2082.02		
11/06/75	144444		2081.17			11/06/75	144602		2082.03		
11/06/75	144446		2081.16			11/06/75	144603		2082.03		
11/06/75	144447		2081.18			11/06/75	144604		2082.03		
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11/06/75	144448		2081.17			11/06/75	144607		2082.04		
11/06/75	144449		2081.17			11/06/75	144608		2082.03		
11/06/75	144450		2081.17			11/06/75	144609		2082.03		
11/06/75	144451		2081.17			11/06/75	144610		2082.04		
11/06/75	144452		2081.17			11/06/75	144611		2082.04		
11/06/75	144454		2081.17			11/06/75	144612		2082.04		
11/06/75	144455		2081.18			11/06/75	144614		2082.05		
11/06/75	144456		2081.17			11/06/75	144615		2082.05		
11/06/75	144457		2081.17			11/06/75	144616		2082.05		
11/06/75	144458		2081.17			11/06/75	144617		2082.05		
11/06/75	144459		2081.17			11/06/75	144618		2082.06		
11/06/75	144500		2081.17		FLOW SHUT IN. ASSUME ZERO TIME FOR BUILD UP	11/06/75	144619		2082.06		
11/06/75	144502		2081.18			11/06/75	144620		2082.06		
11/06/75	144503		2081.19			11/06/75	144622		2082.06		
11/06/75	144504		2081.28			11/06/75	144623		2082.07		
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11/06/75	144506		2081.53			11/06/75	144625		2082.07		
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11/06/75	144508		2081.58			11/06/75	144627		2082.07		
11/06/75	144510		2081.66			11/06/75	144628		2082.07		
11/06/75	144511		2081.67			11/06/75	144630		2082.07		
11/06/75	144512		2081.67			11/06/75	144631		2082.08		
11/06/75	144513		2081.74			11/06/75	144632		2082.07		
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11/06/75	144516		2081.78			11/06/75	144635		2082.09		
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11/06/75	144519		2081.80			11/06/75	144638		2082.09		
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11/06/75	144521		2081.83			11/06/75	144640		2082.09		
11/06/75	144522		2081.85			11/06/75	144641		2082.09		
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11/06/75	144527		2081.88			11/06/75	144646		2082.09		
11/06/75	144528		2081.88			11/06/75	144647		2082.10		
11/06/75	144529		2081.90			11/06/75	144648		2082.10		
11/06/75	144530		2081.92			11/06/75	144649		2082.10		
11/06/75	144531		2081.91			11/06/75	144650		2082.11		
11/06/75	144532		2081.92			11/06/75	144651		2082.11		
11/06/75	144534		2081.94			11/06/75	144652		2082.10		
11/06/75	144535		2081.93			11/06/75	144654		2082.11		
11/06/75	144536		2081.94			11/06/75	144655		2082.11		
11/06/75	144537		2081.95			11/06/75	144656		2082.10		
11/06/75	144538		2081.95			11/06/75	144657		2082.11		
11/06/75	144539		2081.95			11/06/75	144658		2082.12		
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11/06/75	144542		2081.97			11/06/75	144700		2082.11		
11/06/75	144543		2081.97			11/06/75	144702		2082.12		
11/06/75	144544		2081.97			11/06/75	144703		2082.12		
11/06/75	144545		2081.98			11/06/75	144704		2082.11		
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11/06/75	144548		2081.99			11/06/75	144707		2082.12		
11/06/75	144550		2082.00			11/06/75	144708		2082.12		
11/06/75	144551		2082.00			11/06/75	144710		2082.12		
11/06/75	144552		2082.00			11/06/75	144711		2082.13		
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11/06/75	144554		2082.00			11/06/75	144713		2082.13		
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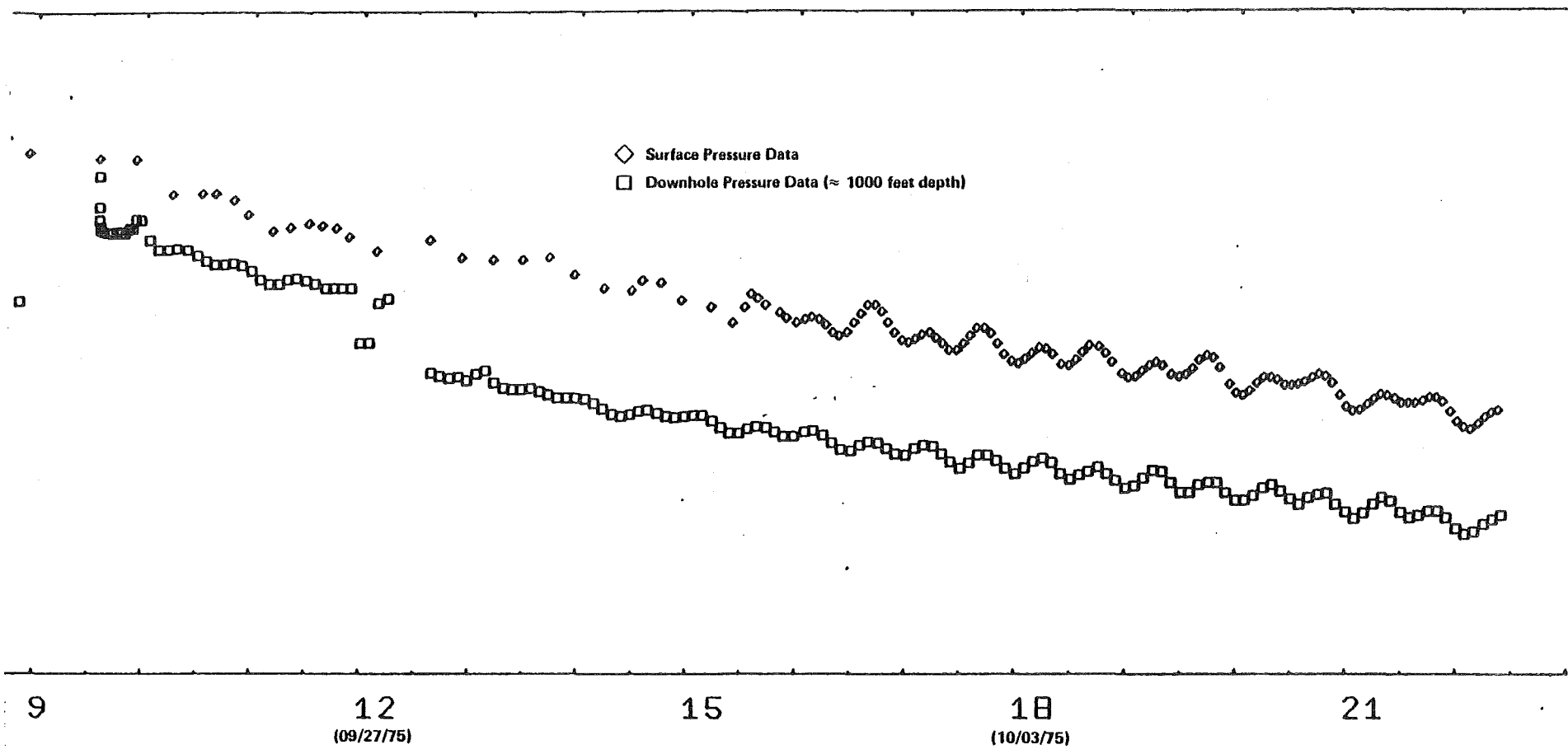
RAGE 1 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME /	/FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS	DATE / /	TIME /	/FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS
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11/06/75	144718		2082.13			11/06/75	144838		2082.17		
11/06/75	144719		2082.13			11/06/75	144839		2082.16		
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11/06/75	144721		2082.13			11/06/75	144841		2082.17		
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11/06/75	144723		2082.13			11/06/75	144843		2082.17		
11/06/75	144724		2082.15			11/06/75	144844		2082.13		
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11/06/75	144729		2082.14			11/06/75	144849		2082.17		
11/06/75	144730		2082.15			11/06/75	144850		2082.16		
11/06/75	144731		2082.14			11/06/75	144851		2082.17		
11/06/75	144732		2082.14			11/06/75	144852		2082.17		
11/06/75	144734		2082.15			11/06/75	144854		2082.17		
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11/06/75	144737		2082.14			11/06/75	144857		2082.17		
11/06/75	144738		2082.15			11/06/75	144858		2082.16		
11/06/75	144739		2082.15			11/06/75	144859		2082.17		
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11/06/75	144743		2082.15			11/06/75	144903		2082.17		
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11/06/75	144753		2082.15			11/06/75	144913		2082.17		
11/06/75	144754		2082.16			11/06/75	144914		2082.17		
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11/06/75	144756		2082.16			11/06/75	144916		2082.18		
11/06/75	144758		2082.16			11/06/75	144918		2082.17		
11/06/75	144759		2082.16			11/06/75	144919		2082.17		
11/06/75	144800		2082.17			11/06/75	144920		2082.18		
11/06/75	144801		2082.16			11/06/75	144921		2082.17		
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11/06/75	144807		2082.17			11/06/75	144927		2082.18		
11/06/75	144808		2082.17			11/06/75	144928		2082.18		
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11/06/75	144828		2082.16			11/06/75	144948		2082.17		
11/06/75	144830		2082.16			11/06/75	144950		2082.17		
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11/06/75	144832		2082.16			11/06/75	144952		2082.17		
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11/06/75	144834		2082.18			11/06/75	144954		2082.15		

RRGE 1 SHORT-TERM TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS	DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
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11/06/75	144958		2082.17			11/06/75	152800		2082.187		
11/06/75	144959		2082.17			11/06/75	152900		2082.195		
11/06/75	145000		2082.17			11/06/75	153000		2082.193		
11/06/75	145010		2082.18			11/06/75	154000		2082.171		
11/06/75	145020		2082.17			11/06/75	155000		2082.228		
11/06/75	145030		2082.17			11/06/75	160000		2082.206		
11/06/75	145040		2082.17			11/06/75	161000		2082.248		
11/06/75	145050		2082.17			11/06/75	162000		2082.281		
11/06/75	145100		2082.17			11/06/75	163000		2082.284		
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11/06/75	145120		2082.17			11/06/75	165000		2082.258		
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11/06/75	145530		2082.15			11/06/75	204000		2082.341		
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11/06/75	145630		2082.17			11/06/75	210000		2082.292		
11/06/75	145700		2082.17			11/06/75	211000		2082.319		
11/06/75	145730		2082.18			11/06/75	212000		2082.293		
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11/06/75	145900		2082.19			11/06/75	215000		2082.279		
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11/06/75	150000		2082.122			11/06/75	221000		2082.294		
11/06/75	150100		2082.198			11/06/75	222000		2082.289		
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11/06/75	150700		2082.142			11/06/75	232000		2082.237		
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11/06/75	150900		2082.157			11/06/75	234000		2082.223		
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11/06/75	151100		2082.160			11/07/75	000000		2082.199		
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11/06/75	151300		2082.193			11/07/75	002000		2082.198		
11/06/75	151400		2082.192			11/07/75	003000		2082.228		
11/06/75	151500		2082.195			11/07/75	004000		2082.216		
11/06/75	151600		2082.191			11/07/75	005000		2082.204		
11/06/75	151700		2082.185			11/07/75	010000		2082.189		
11/06/75	151800		2082.173			11/07/75	011000		2082.179		
11/06/75	151900		2082.171			11/07/75	012000		2082.201		
11/06/75	152000		2082.167			11/07/75	013000		2082.214		
11/06/75	152100		2082.164			11/07/75	014000		2082.237		
11/06/75	152200		2082.172			11/07/75	015000		2082.191		
11/06/75	152300		2082.181			11/07/75	020000		2082.245		
11/06/75	152400		2082.193			11/07/75	021000		2082.162		
11/06/75	152500		2082.186			11/07/75	022000		2082.198		





RRGE 1 INTERFERENCE TEST DATA.

DOWNHOLE PRESSURE, psia

2299.000
2295.000
2291.000
2287.000
2283.000
2279.000
2275.000
2271.000
2267.000
2263.000
2259.000

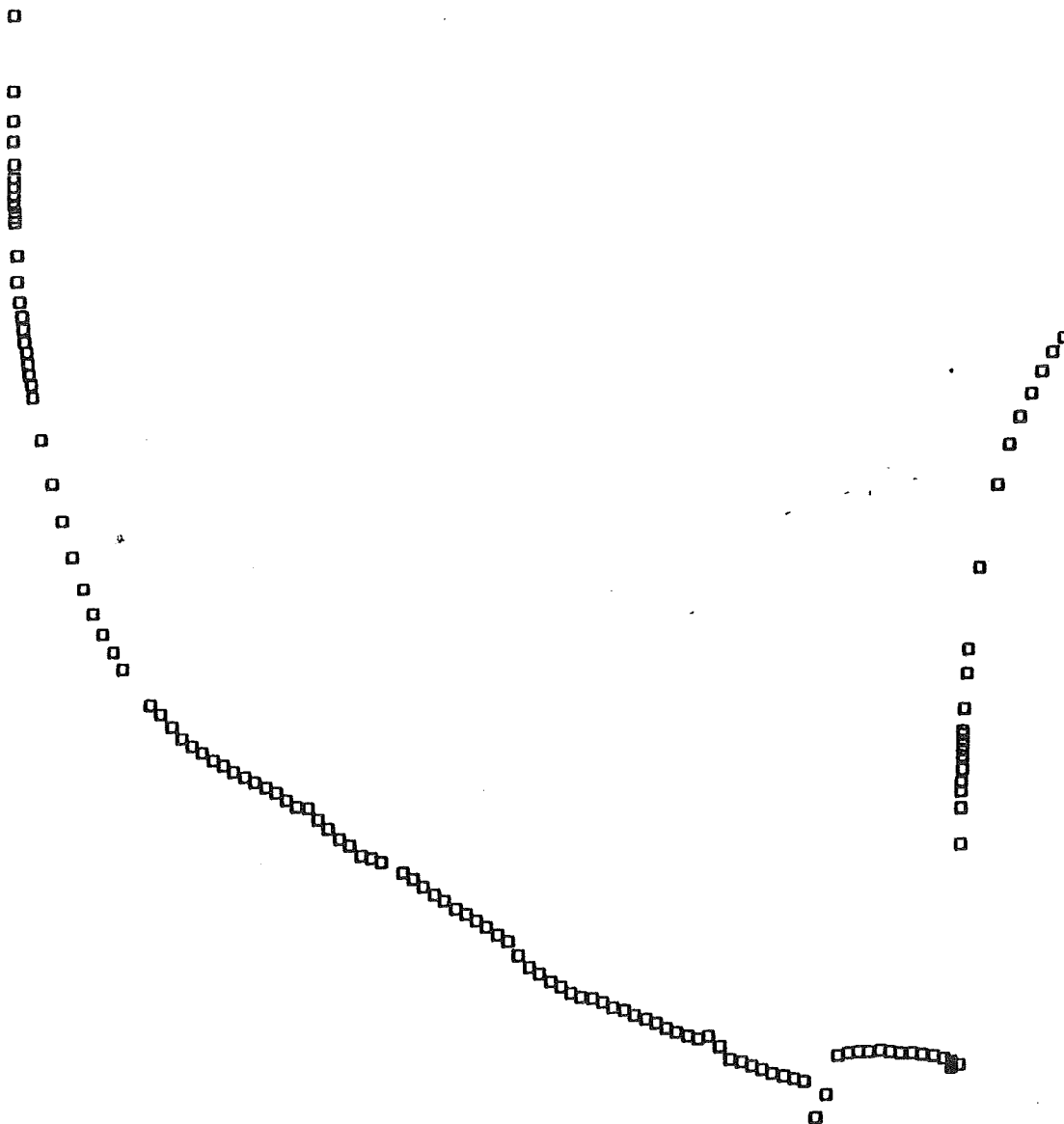
0

DAYS

RR6E 2 SHORT-TERM TEST DATA. R

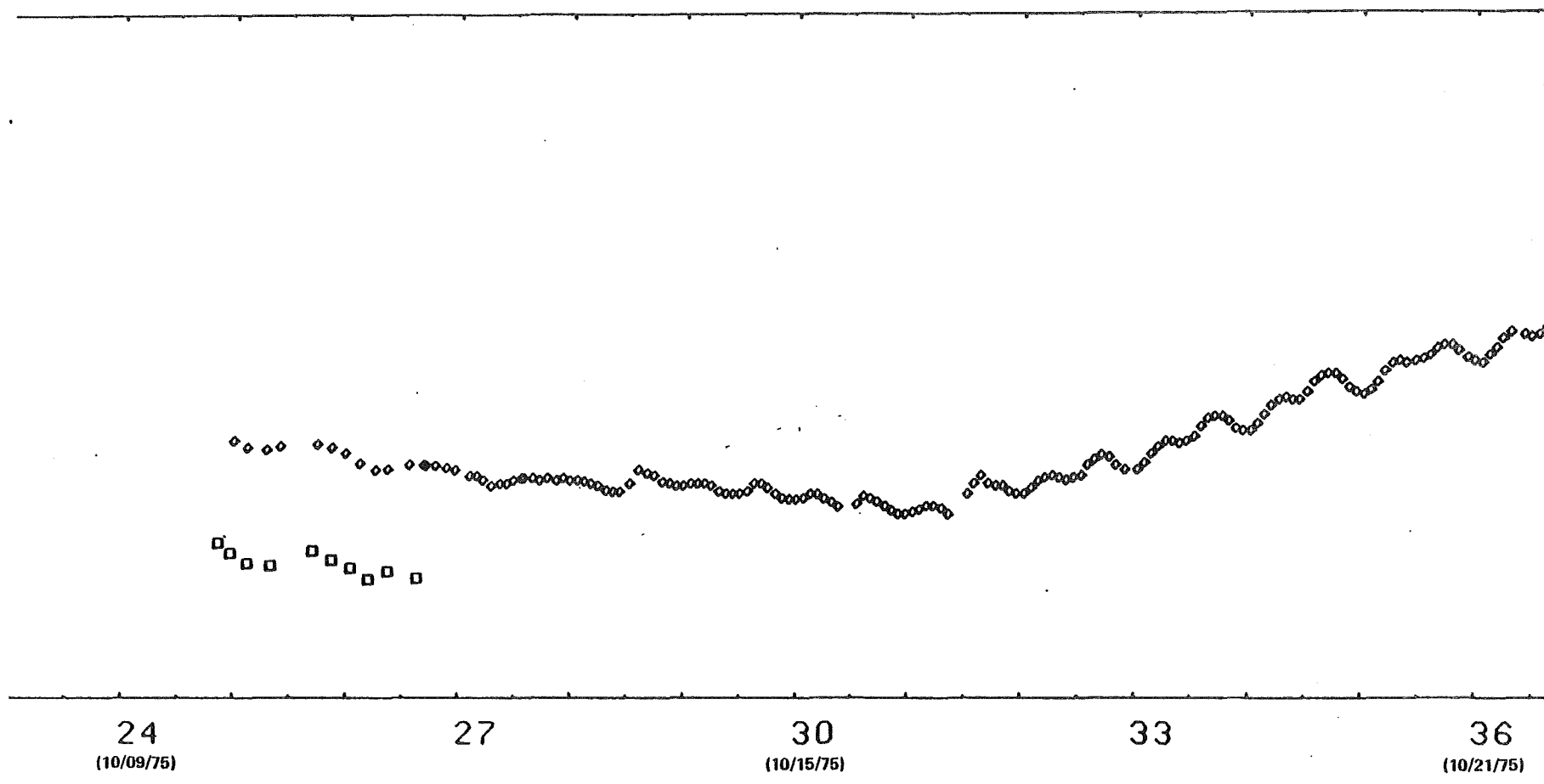
(09/12/75)

PRESSURE GAGE
AT 5200 ft.



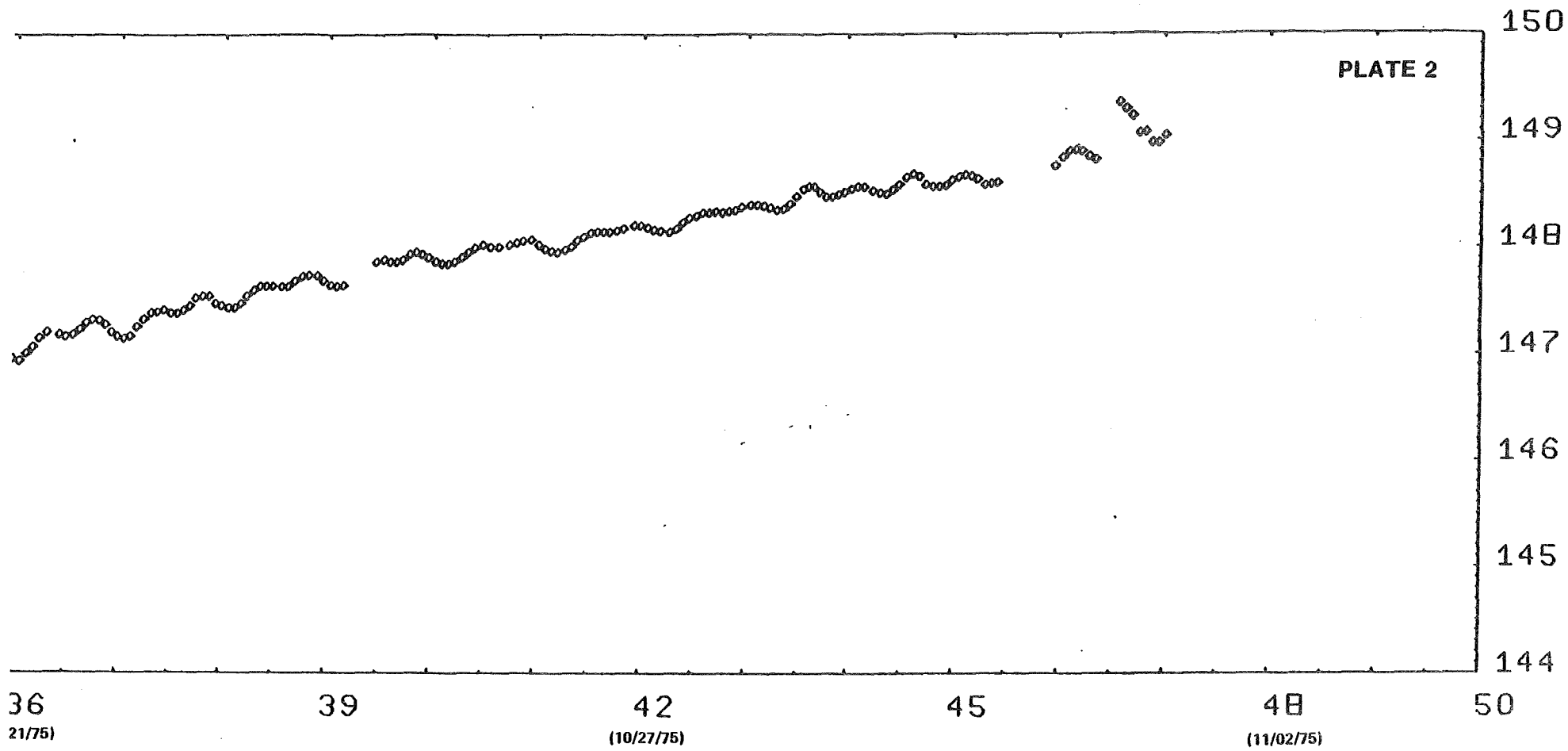
1

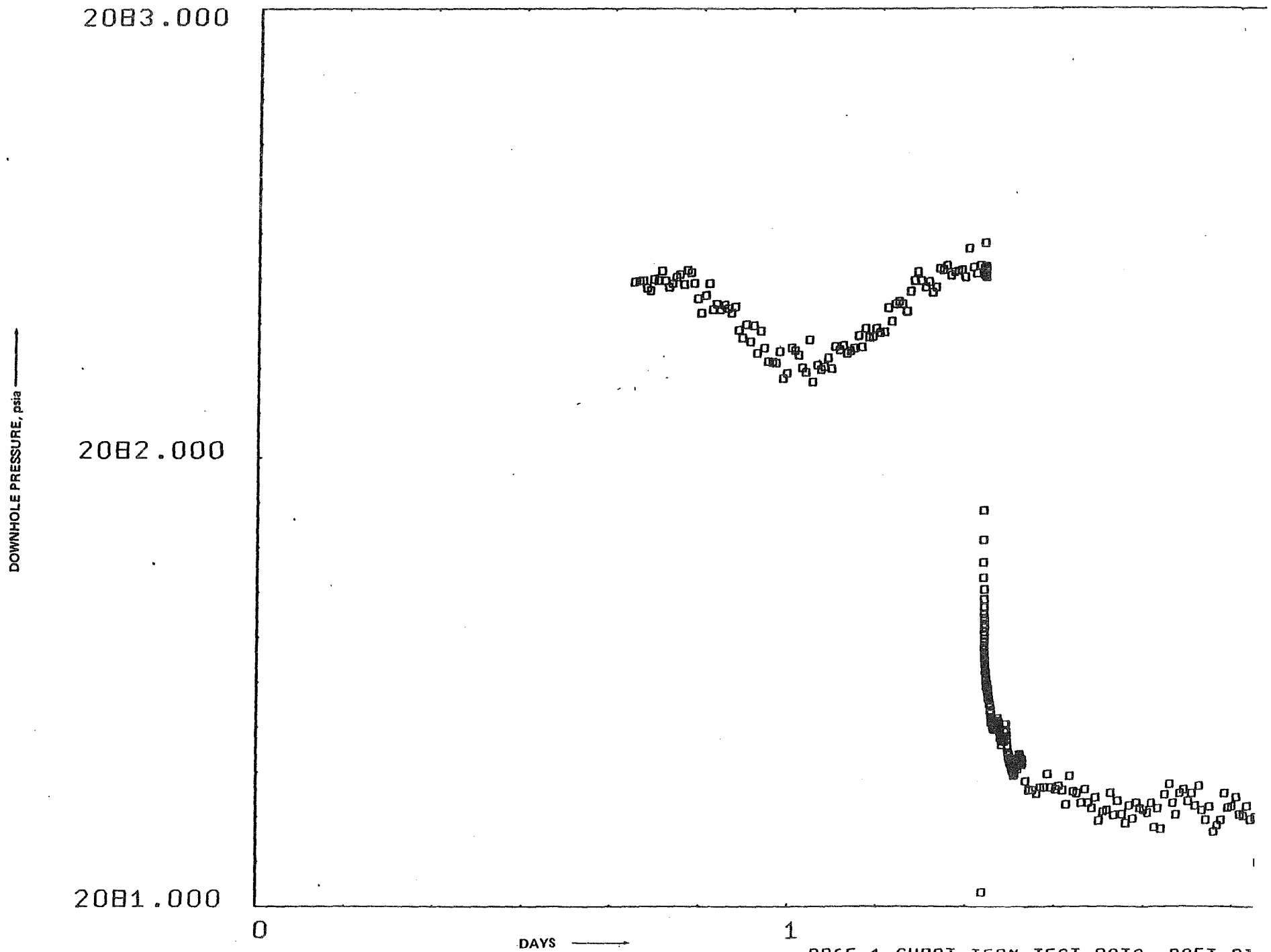
2



DAYS →

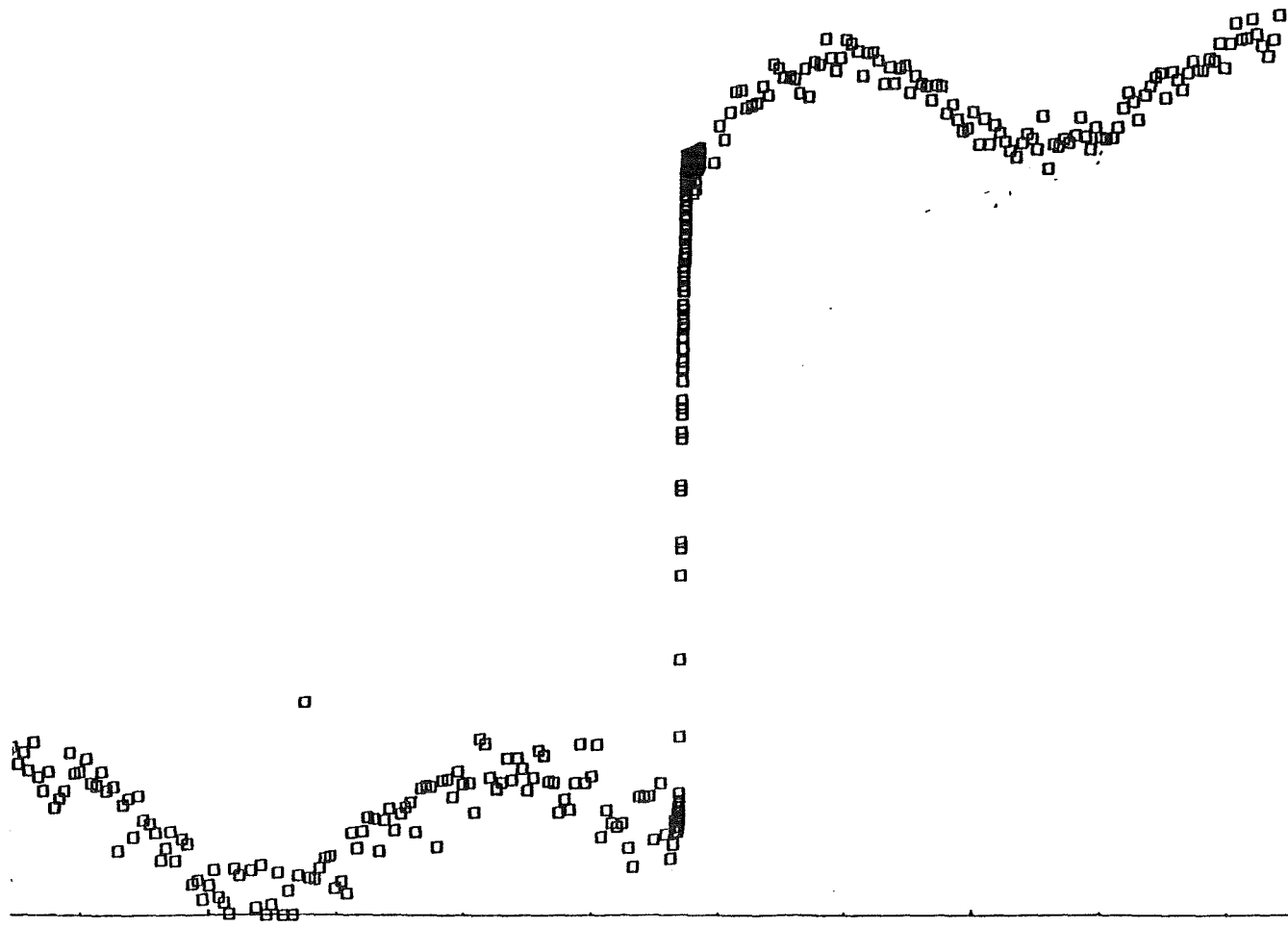
RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO





(11/04/75)

RRGE 1 SHORT-TERM TEST DATA. RAFT R1



2
AFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO
(11/06/75)

3

4