## COMPLETION REPORT:

RAFT RIVER GEOTHERMAL EXPLORATORY HOLE NO. 1

RRGE-11

## OCTOBER 1975


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RAFT RIVER GEOTHERMAL EXPLORATORY HOLE NO. 1 (RRGE-1)

OCTOBER 1975

PREPARED BY REYNOLDS ELECTRICAL \& ENGINEERING CO., INC. LAS VEGAS, NEVADA

FOR
U. S. ENERGY RESEARCH \& DEVELOPMENT ADMINISTRATION NEVADA OPERATIONS OFFICE CONTRACT E (26-1)-410


The first geothermal exploratory hole is located in the Raft River Valley of Southern Idaho. Geothermal hol water is shown flowing into the fluid reserve pil from the ERDA drill rig.

Raft River Geothermal Exploratory Hole No. 1 (RRGE-1) is an exploratory hole drilled to a depth of 5,000 feet in intruded quartz monzonite basement rock of the Raft River valley of southeastern Idaho. The goal of the Raft River Geothermal ReD program is to determine the feasibility of developing and utilizing medium temperature ( $300^{\circ} \mathrm{F}$ ) geothermal resources for power generation and nonelectrical applications.

This well was drilled to obtain geological information and evaluate the deep geothermal reservoir system. This report describes the drilling and completion of RRGE-1 and includes the daily drilling reports, drill bit records, descriptions of the casing, cementing, logging and coring programs, and the containment techniques employed on RRGE-1. A subsequent report, 10010063 , will describe the planning, technology, and testing of RRGE-1.

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## I. INTROOUCTION

This report describes the drilling operation for the completion of the first deep geothermal exploratory hole drilled in the Raft River Valley of Southern Idaho. The operation is a part of the Idaho Geothermal R\&D Project. (See Figures 1, 2, and 3 for location.)

The Site for the Raft River Geothermal Exploratory Hole No. 1 (RRGE-1) was one of several considered after extensive surveys were conducted by the Aerojet Nuclear Company and the U.S. Geological Survey in the late fall of 1974. The RRGE-1 Well was designed to initially confirm the existence of hot water in quantities potentially suitable for commercial power applications. Drilling operations were started early in January 1975 and were completed at a total depth of about 5,000 feet on April 1, 1975. Limited flow testing and reinjection testing were performed before demobilizing the drill rig. A flow rate of approximately 600 gallons per minute was measured and a maximum downhole temperature of $292^{\circ} \mathrm{F}$ was recorded.

The drilling and completion work on RRGE-1 was performed by Reynolds Electrical \& Engineering $C_{0 .}$. Inc. (REECO), utilizing a drill rig and equipment mobilized to Idaho from an area in northwest Colorado. The U. S. Energy Research \& Development Administration (ERDA), Nevada Operations Office (NV) was responsible for all drill site activities through its on-site representative. Drilling program requirements were provided by the Aerojet Nuclear Company (ANC), a prime contrator to ERDA, Idaho Operations Office (ID). The Manager, ID, was responsible for the coordination of all project-related activities between NV/REECo and ANC and providing funding for the drilling operation. For the technical data obtained from this hole, refer to IDO 10063.


RRGE-1 - Well Flowing and Flashing at Surface near Shale Shaker.


Figure 1. Idaho Geothermal $R \& D$ Project Site Location


Fisure 2. Raft River Valley with Drill Sile Loration


Fisure 3. Location Survery and Coordinates

## EXPLORATORY HOLE DRILLING

## 1. DRILLING SUMMARY

The drill site with approximate dimensions of 300 feet by 300 feet was prepared in order to accommodate the drill rig and supporting equipment. Preparation included site leveling and grading, excavation of the fluid reserve pit and grading of road and storage surfaces adjoining the drill site. A domestic water well was drilled to approximately 200 feet using a water well drilling contractor.

A 42 -inch diameter hole was drilled to 40 feet (from ground level depth) and $30-i n c h$ diameter conductor pipe was set at 40 feet and cemented with 18 cubic yards of plant mix concrete. An 8 foot by 8 foot by 12 foot timberlined cellar was constructed around the conductor pipe.

A 15 -inch diameter hole was drilled with mud to 921 feet (RKB)* and reamed to 26 inches in diameter to 920 feet. A total of 22 joints of 20 -inch, $\mathrm{H}-40$, $94.0-1 b / f t$ casing was landed at 901 feet (GL - ground level) and was cemented to the surface in one stage with good cement returns to the surface.

A $121 / 4$-inch diameter hole was drilled with water to 4,495 feet. Core \#1 was cut with an 8 3/4-inch diamond bit from 4,495 feet to 4,555 feet with 23 feet of core recovered. The cored interval was reamed to $121 / 4$-inches and the same diameter hole was drilled from 4,555 feet to 4,650 feet. After circulating and while logging, the hole began to flow hot water at an inital rate of approximately 1,000 barrels per hour and a surface temperature of approximately $200^{\circ} \mathrm{F}$.

Efforts to stop the flow by injecting cold water were halted when this activity resulted in development of a major "thief zone," principally between 1600 feet and 1700 feet. The flow was successfully controlled by staging plugs of sand ( 862 feet), barite ( 12 feet), and cement ( 120 feet) pumped down the drill pipe. The top of the cement plug was tagged at 3,642 feet.

Based upon a 4-arm caliper log the average hole diameter from the 13 3/8-inch casing setting depth to the 20 -inch casing shoe was approximately 20 1/4 inches, with a maximum diameter of 25 inches and a minimum diameter of 16 1/2 inches. A 15 -inch diameter bit was run to the top of the cement plug at 3,642 feet to assure clearance and to circulate before running the 13 3/8-inch casing. A total of 92 joints of $133 / 8$-inch, 54.5 and $61.0-1 b / f t$ casing with float shoe and two differential fill float collars (see Section 4.2 Production Casing) were run and set at 3,623 feet (GL).

While cementing the first stage through the shoe with 454.5 barrels of cement displaced and 98 barrels of slurry remaining to be displaced, the casing parted at a coupling at approximately 240 feet $G L$ (seventh joint from the surface). The casing was successfully screwed back together, torqued and pressure tested. Before proceeding with the second stage, a cement bond log

* All depths (unless otherwise noted) are referenced to the rotary kelly bushing (RKB) which is 18 feet above ground level.
was run which indicated an annulus cement top at approximately 1,820 feet GL and the cement top inside the casing at 2,891 feet. The second cement stage was pumped through the casing head ports (Braden head) in accordance with the cementing program. A total of 407 barrels of cement slurry were pumped until the pumping pressure rise indicated the annular space was cemented. A cement bond $\log$ was run which confirmed the cement in place outside the casing from 1,820 feet $G L$ to the surface.

While drilling out the cement in the $133 / 8$-inch casing, collapsed casing zones were encountered at 3,325 feet and 3,584 feet. A total of 13 milling tool runs were made in addition to numerous runs with magnets (11 1/2-inch and 9 inch) and various junk baskets before drilling out of the $133 / 8$-inch casing shoe at 3,642 feet. The actual zones of casing collapse were determined to extend from 3,325 feet to 3,338 feet ( 13 feet) and from 3,584 feet to 3,591 feet (7 feet). These depths were determined from strapped drill pipe lengths and were at variance with the 4 -arm caliper log on April 6, 1975. Pressure tests of the casing to 300 psi were conducted during milling operations which indicated no leaks. The cement plug below the $133 / 8$-inch casing shoe was drilled out and the barite and sand plugs were circulated out of the hole to the previous total depth of 4,650 feet.

After drilling formation from 4,650 feet to 4,686 feet, Core \#2 was cut with an $83 / 4$-inch diamond bit from 4,686 feet to 4,698 feet with nine feet of core recovered. The cored interval was reamed to 11 inches and the same diameter hole drilled to 5,005 feet. A bottom hole core (\#3) was cut with an $83 / 4$-inch diamond bit from 5,005 to 5,007 feet with 2 feet of recovery.

Upon completion of the drilling and coring operations, a retrievable bridge plug was set in the $133 / 8$-inch casing at 1,380 feet to permit removal of the blowout equipment. A master gate valve was installed to allow for future flow tests and temperature measurements.

A summary of the daily drilling reports from mobilization through rig-down is presented as Appendix A.

Figure 4 depicts the Drilling and Operations Summary and Figure 5 reveals the current Subsurface We 11 Status of RRGE-1.

## 2. FORMATION TOPS

The following are the formation tops encountered in RRGE-T.

| Formation | Drilled <br> Depth (ft) | Sea Level <br> Depth (ft) |  |
| :--- | :---: | :---: | :---: |
|  |  |  |  |
| Alluvium | Surface |  | $+4,835$ |
| Raft River | 100 |  | $+4,735$ |
| Salt Lake | 820 | $+4,015$ |  |
| Contact Metamorphosed Zone | 4,595 |  | +240 |
| Elba Quartzite | 4,708 | +127 |  |
| Quartz Monzonite (Intermittent) | 4,928 | - | 93 |





Figure 5. Present Subsurface Well Status

## 3. SURFACE EQUIPMENT AND SERVICES

### 3.1 Wellhead

The wellhead configuration consisted of a 20 -inch by 14 -inch reduction spool with two 4 -inch flanged outlets from the 20 -inch surface casing head and a manually-operated, ASA Series 300 1b. Petrovalve master gate valve. This wellhead was installed after drilling operations were completed and the blowout preventer equipment was removed.

### 3.2 Flow Testing Manifold

A 6 -inch flow line was stabbed in the Hydril blowout preventer and secured with the pipe rams. This line extended across the rig floor when in use and was maneuvered with the rig cat line. Flow testing was also monitored through two 2-inch outlets from a spool under the blowout preventer equipment.

### 3.3 Mud Logging Services

A mud logging service monitoring drilling fluid and cutting returns was used from 900 feet (bottom of the 20 -inch surface casing) to a depth of 4,650 feet. This service monitored fluid temperatures (in and out), hydrogen sulfide and hydrocarbons. Lithologic characteristics were also determined by analyzing the drill cuttings at regular intervals.
3.4 Drilling Recorder

A Geolograph drilling recorder was used on the drill rig while drilling from the surface to the total depth. This multi-pen recorder continuously indicated depth, penetration rate, bit weight and pump pressure.

## 4. DOWNHOLE EQUIPMENT \& SERVICES

### 4.1 Surface Casing

Twenty-two joints of 20 -inch, $\mathrm{H}-40,94.0 \mathrm{lb} / \mathrm{ft} ., \mathrm{ST} \mathrm{\& C}$ casing totaling 921.08 feet was landed at 901 feet (GL). A float collar was positioned one joint ( 43 feet) above the guide shoe and centralizers were positioned on the collar of each joint of casing. Refer to Appendix B for the 20 -inch Casing Record.

### 4.2 Production Casing

Ninety-two joints of $133 / 8$-inch, 54.5 and $61.0-1 b / f t$ casing totaling $3,651.25$ feet were landed at 3,623 feet (GL). The $133 / 8$-inch casing string configuration was as follows:

| No. Jts. | Wall | Weight | Grade | Depth (GL) ${ }_{\text {Tom }}$ |  | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Thick(in) | Lb/Ft |  |  |  |  |
| 1 | 0.43 | 61.0 | K-55 | 0 | 11.81 | ST\&C 8RD |
| 41 | 0.38 | 54.5 | H-40 | 11.81 | 1646.65 | STAC 8RD |
| 49 | 0.43 | 61.0 | K-55 | 1646.65 | 3578.45 | ST\&C 8RD |
|  |  |  |  | 3578.45 | 3580.45 | Diff. Fill Float Collar |
| 1 | 0.43 | 61.0 | K-55 | 3589.45 | 3619.80 | STEC 8RD |
|  |  |  |  | 3619.80 | 3621.80 | Diff. Fill Float Collar |
|  |  |  |  | 3621.80 | 3623.00 | Cement Guide Shoe |

All casing ends were threaded and joined with couplings using power tongs and a torque recorder for registering specified torque. Refer to Appendix B for the 13,3/8-inch Casing Record.

### 4.3 Drill Bit Summary

The initial 42 -inch hole was drilled to 40 feet with a rat hole drill rig, and 30 -inch conductor pipe (CMP) was set and cemented to that depth.

The surface (pilot) hole was drilled from 40 feet to 920 feet with one 15 -inch mill tooth bit in $353 / 4$ rotating hours. The 15 -inch hole was reamed to 26 inches to a depth of 918 feet and 20 -inch casing was set and cemented to 901 feet GL. A $121 / 4$-inch hole was drilled with water from 901 feet to 4,650 feet in 147 1/4 rotating hours with eight 12 1/4inch mill tooth bits. A 15 -inch bit was run from 901 feet to 3,642 feet after the $121 / 4$-inch hole was plugged with sand, barite, and cement from 4,650 feet up to 3,642 feet. (The sand plugs were pumped in the well to shut off the flow of hot water until the $133 / 8$-inch casing was run and cemented.) Extensive milling operations were required to drill out two intervals of casing which collapsed during the first stage cementing operation. Appendix $C$ details the specialized milling and fishing tools used to mill to the bottom of the casing. After drilling again reached 4,650 feet, the ninth $121 / 4$-inch bit was used to drill to 4,686 feet. An 11-inch mill tooth bit was then used to drill from 4,686 feet to 5,005 feet in $341 / 4$ rotating hours.

Three cores were taken using two 8 3/4-inch diamond core bits (cores \#1 and \#3 were cut with bit \#1 and core \#2 with bit \#2). Details of the coring operation are depicted in the following Section 4.4.

The complete bit record is presented in Appendix $C$.

### 4.4 Coring

Three cores were cut using a $63 / 4$-inch by 4 -inch by 60 -foot core barrel as follows:

| Core No. | Zone Cut | Drilling Fluid | Core Bit Size | Core Recovered | Percent Recovered |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4,495-4,555 | Water-No Additives | 8-3/4 ${ }^{11}$ | $23^{\prime}$ | 38\% |
| 2 | 4,686-4,698 | Water-No Additives | $8-3 / 4^{11}$ | $9{ }^{\prime}$ | 75\% |
| 3 | $5,005-5,007$ | Water-No Additives | $8-3 / 4^{\prime \prime}$ | $2^{\prime}$ | 100\% |

### 4.5 Directional Control

A Sperry-Sun single-shot magnetic survey tool with a $6^{\circ}$ compass unit was used throughout the drilling operation. Surveys of the hole deviation were taken approximately every 90 feet. A summary of the deviations recorded has been tabulated in Appendix $D$.

### 4.6 Drilling Fluid Summary

A fresh water-based gel mud was used to drill and ream the surface hole to 918 feet. Mud weight was maintained at approximately 9.1 lbs. per gallon and viscosity of $48 \mathrm{sec} / 1000 \mathrm{cc}$. Plastic viscosity averaged 10 centipoises and sand content was maintained between 1 and 2 percent of total volume.

Fresh water containing no additives was used for all drilling and coring operations below 918 feet.

Overall drill fluid circulation throughout the drilling operation was good with the exception of the "thief zone" encountered between approximately 1,600-1,700 feet. Water loss to the formation, as a result of this "thief zone," averaged approximately 130 barrels per hour and necessitated the support of a 100 -barrel vacuum truck to haul water continually to the rig from the Raft River.

### 4.7 Samples

Four sets of samples of drill cuttings were taken at approximately every 10 feet by the mud logging representative between 900 feet to 4,650 feet, and below 4,650 feet by the drill crew. Samples were collected in sample sacks and were labeled and boxed for shipment to ANC, USGS, Standard American, Inc. and Boise State University.

### 4.8 Logging Program

Various logs were run in the RRGE-1 well to determine the condition of the hole at different stages of the drilling operations. A listing of the logs that were run, the logging interval, and the footage logged are displayed as follows:

| $\begin{aligned} & \text { Log } \\ & \text { Run No. } \end{aligned}$ | Type Log | $\begin{gathered} \text { Date } \\ \text { Log Run } \\ \hline \end{gathered}$ | Ground Logged (From) | Level <br> Interval <br> (TO) | Total Footage Logged |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Dual induction laterolog | 01-09-75 | 0 | 894 | 894 |
| 2 | Bore hole compensated-sonic-gamma ray | 01-09-75 |  | 865 | 865 |
| 3 | 4-arm caliber | 01-09-75 | 0 | 880 | 880 |
| 4 | Dual induction laterolog | 02-02-75 | 900 | 4,612 | 3,712 |
| 5 | 4 -arm caliper | 02-02-75 | 900 | 4,619 | 3,719 |
| 6 | High-resolution thermometer | 02-02-75 | 350 | 4,620 | 4,270 |
| 7 | Bore hole compensated-sonic-gamma ray | 02-02-75 | 900 | 4,610 | 3,710 |
| 8 | High-resolution thermaneter | 02-02-75 | 500 | 4,620 | 4,120 |
| 9 | Density-combination w/compensated neutron | 02-02-75 | 900 | 4,620 | 3,720 |
| 10 | Compensated neutron log-combination w/density GR | 02-02-75 | 900 | 4,620 | 3,720 |
| 11 | High-resolution thermometer | 02-03-75 | 800 | 4,620 | 3,820 |
| 12 | Continuous flow meter | 02-03-75 | 0 | Equipment | Failure |
| 13-15 | High-resolution thermometer (3 runs) | 02-09-75 | 900 | 4,610 | 11,130 |
| 16-21 | High-resolution thermometer (6 runs) | 02-09-75 | 900 | 4.610 | 22,260 |
| 22 | 4 -arm caliper | 02-09-75 | 900 | 4,616 | 3,716 |
| 23-26 | High-resolution thermometer (4 runs) | 02-10-75 | 900 | 4,616 | 14,864. |
| 27-28 | Acoustical cement bond log |  |  |  |  |
|  | lst Stage | 02-24-75 | 1,200 | 2,830 | 1,630 |
|  | 2nd Stage (after Braden head squeeze) | 02-25-75 |  | 2,000 | 2,000 |
| 29 | Bore hole compensated-sonic | 04-06-75 | 2,998 | 4,998 | 2,000 |
| 30 | High-resolution thermometer | 04-06-75 | 0 | 5,000 | 5,000 |
| 31 | 4-arm caliper | 04-06-75 | 3,000 | 5,000 | 2,000 |
| 32 | Density-combination w/compensated neutron GR | 04-07-75 | 3,000 | 4,992 | 1,992 |
| 33 | Compensated neutron $\log$ combination w/density GR | 04-07-75 | 3,000 | 4,992 | 1,992 |

### 4.9 Cementing

## Surface Casing

The 921.08 feet of 20 -inch, $94.0 \mathrm{lb} / \mathrm{ft}$ casing was cemented with 326 barrels ( 1,090 sacks) of $50 / 50$ poz-mix with 60 percent (by weight) silica flour and 3 percent (by weight) calcium chloride ( $\mathrm{CACL}_{2}$ ). Good circulation was maintained throughout the job although 30 barrels of circulation were slightly contaminated with mud.

## Production Casing

The $3,651.25$ feet of $133 / 8$-inch, 54.5 and $61.0 \mathrm{lb} / \mathrm{ft}$ casing was cemented in two primary stages as follows:

STAGE \#1 - 1,500 sacks of $50 / 50$ poz-mix, 60 percent (by weight) silica flour, $1 / 2$ of 1 percent (by weight) of HR-12, and 400 sacks of $50 / 50$ poz-mix. Total yield was 568 barrels of slurry. Lacking 98 barrels of having the plug pumped down, the casing parted at the seventh joint from the surface. The separated casing was screwed together with $2,000 \mathrm{ft} / 1 \mathrm{bs}$ of torque and pulled to 122,000 1bs. Halliburton applied 500 psi pressure on the casing and it held for a 5-minute test. A cement bond $\log$ was run to the cement top in the casing at 2,837 feet. This cement bond 10 g indicated cement outside the casing at 1,820 feet (GL).

Stage \#2 - Pumped through casing head ports down the annulus from the surface with 50 sacks of $50 / 50$ poz-mix with 4 percent calcium chloride and $25 \mathrm{lbs} /$ sack of gilsonite (lost circulation material) followed by 1,176 sacks of $50 / 50$ poz-mix with 60 percent silica flour. The total yield of 407 barrels of slurry were pumped until a pumping pressure rise occurred indicating annulus fill-up. A cement bond log confirmed cement from surface to 1,820 feet.

## 5. SAND, BARITE AND CEMENT PLUG

After unsuccessful attempts to control the hot water flowing from the well by pumping in cold water, the decision was made to install a temporary plug from total drilled depth to a point above the geothermal resource zone (see Figure 6).

The designed plug consisted of multiple stages of sand, followed by barite and topped by cement. The principle involved was to successively reduce the water flow with sand stages, further reduce percolation through the sand with barite, and finally seal off the flow with cement.

The sand used was of a gradation that would not be carried up hole by the flow and into the "thief zone," and the f111-up after each stage could be verified by setting down approximately $20,000 \mathrm{lbs}$. Weight on the sand stage top with the open ended drill pipe. The reduction in water percolation through each successive sand stage was also verified by the increased period of time the sand stage top would sustain the $20,000 \mathrm{lbs}$. drill pipe weight before the sand was eroded away by the velocity increase up the annulus around the drill pipe. This design was adopted because it was a method of shutting off the flow from the resource zone, would pemit the running and cementing of the $133 / 8$-inch production casing and would also permit drilling out the cement plug and circulating the barite and sand stages out of the hole without any damage to the resource zone formations.

### 5.1 Sand

Sand was provided from a local vendor and delivered in bulk to the location. Utilizing a Halliburton blender and pump truck, the sand was pumped down the hole through open-ended drill pipe in a total of nine stages which plugged 861 linear feet of hole. As each stage was completed, the rise of sand was monitored, tagged, and recorded. A total volume of approximately $1,575 \mathrm{cu}$. ft. of sand was pumped for this plug.

### 5.2 Barite

Continuing to utilize the Halliburton blender and pump truck, a plug of barite was placed in three stages which plugged an additional 8 linear feet of hole. A total of 120 sacks of barite was pumped in the hole. This material was used to cap the top of the sand plug thus allowing for the installation of the cement plug.

### 5.3 Cement

A 120 foot cement plug was then pumped in one stage with the Halliburton trucks. A total volumn of 153 barrels of slurry consisting of 115 sacks of Class $G$ Ideal cement was mixed to slurry weight at 16.8 ibs per gallon. Additives mixed with the cement included 108 sacks of CFR-2 at $1 \%$ by weight and 69 sacks of $H R-4$ at $0.6 \%$ by weight.


Figure 6. Sand, Barite, and Cement Plug Configuration

## 6. CONTAINMENT EQUIPMENT

### 6.1 Surface Hole

Containment equipment was not utilized while drilling the hor- for the 20 -inch surface casing from the bottom of the 30 -inch conduct $x$ pipe to the depth of 918 feet (RKB).

### 6.2 Production Hole

After the 20 -inch O.D. surface casing was installed and erer to the surface, it was cut off at ground level, and the 20 -inch casirg head was welded on the casing. Containment equipment was then install $d$ and utilized for the remainder of the drilling operation. The co tainment equipment (listed in order of installation above the casing hiky) was installed as follows:
a. Flanged Spool - size 20 -inch $\times 16$-inch; bolted onto easting head and included two, threaded two-inch outlets complete witn valves and connected to pipe for bleed-off to the reserve pit.
b. Rucker-Shaffer Double Gate LWS Blowout Preventer (BOP) - size 16-inch; bolted to the spool and equipped with $65 / 8$-inch drill pipe and blind rams.
C. Hydril Type GK Biowout Preventer - size 16-inch; bolted to the BOP. This Hydril was utilized until the $133 / 8$-inch production casing was installed and cemented. A 12-inch Hydril replaced this hydril for the remainder of the drilling operation.
d. Flanged Spool - size 16 -inch $\times 12$-inch; bolted to the Hydril and included two, flanged three-inch outlets with a companion flange, bull plug, double studded adapter and blind Flange. (Since this was the only spool available, it was necessary to close off the 3 -inch outlets). This spool was used while the 16 -inch Hydril was in the containment stack. After the 16 -inch Hydril was replaced with the 12-inch Hydril, this spool was deleted.
e. Grant Rotating Head - size 12-inch, 3000 1bs; bolted to the $16 \times 12$ spool - or to the 12 -inch hydril (after the spool was removed).

Figure 7 depicts the Containment Equipment as installed.


Figure 7. Containment Equipment

DAILY DRILLING REPORTS - RRGE-1

November 18, thru November 19, 1974

November 20, 1974

November 21, thru November 24, 1974

November 25, 1974

November 26, thru December 15, 1974

December 16, 1974

December 17, 1974

December 18, 1974

December 19, 1974

December 20, 1974

Began loading trucks at the RB-U-4 location in Colorado for shipment to the RRGE-1 drill site. Loaded and dispatched 11 trucks.

Unloaded 11 trucks beside the selected drill site from 8 a.m. to 6:30 pom. Commenced night watch on site.

Received and unloaded 32 trucks for a total of 43 loads from the RB-U-4 drill site.

Stacked drill pipe and miscellaneous equipment with the forklift for 8-1/2 hours.

Performed security watch during the site preparation activities. Sorted and arranged equipment to a limited degree pending hiring of the drill crew and start of the rig-up operations. The surface hole, rat and mouse holes were drilled during the period December 1 and 2, 1974. One joint of 30 -inch conductor pipe was set with the forklift and cemented with 18 cubic yards of plant mix cement on December 2 and 3, 1974. The 8 -foot by 8 -foot by 12 -foot cellar was excavated and lined with 3 -inch by 12 -inch boards on December 4, 1974.

9 hours - rigging up rotary tools with 20 men and two rig-up trucks. Set front of substructure in place.

10 hours - rigging up rotary tools with 20 men and two rig-up trucks. Finished setting in the substructure and assembled the derrick. Set in the mud tanks and mud pumps.

10 hours - continued rigging up with 20 men. Assembled A-frame for derrick and set the dog house and fuel tanks into place. Built the subdock and worked on mud pump liners and engines. Crane arrived on location today.

10 hours $=$ continued rigging up with 20 men, three rigup trucks and one crane. Set the derrick on the rig floor and pinned into the subbase. Set the crown end on the stand. Set the desander and desilter into position and set the compound and motor on the rig floor.

10 hours - continued rigging up with 20 men, two rig-up trucks and one crane. Set the draw works, A-frame and raising line in place. Set the three rig engines on the rig floor. Crane demobilized.

## DAILY DRILLING REPORTS - RRGE-1

December 21, 197410 hours - continued rigging up with 20 men and two rig-up trucks. Loaded seven 8 -inch drill collars and 50 joints of 6 5/8-inch drill pipe for transport to Drilco Machine Shop in Vernal, Utah, for inspection. Positioned compressor, water tank, and water line. Installed guardrail, engine shed frame, and curtains. Reieased rig-up trucks.

December 22, 19749 hours - continued general rig-up with 20 men. Approximately $85 \%$ rigged up.

December 23, 1974

December 24, thru December 26, 1974

December 27, 1974

December 28, 1974

December 29, thru
December 30, 1974
December 31, 1974

January 1, 1975
January 2, thru
January 4, 1975

8 hours - 19 men continued general rig-up operations. Started the rig engine. Raised the derrick, set in the rig floor, and installed the wind walls and all equipment lighting. Set the ramp and cat walk in place.

Secured for the Christmas holiday. Maintained a 24 -hour security watch at the location during this period.

8 hours - resumed general rig-up operations with 8 men and 1 welder. Tied off the bridle line, strung the air hoist, and extended the 30 -inch surface casing.

8 hours - continued general rig-up operations with 9 men and 1 welder. Dial-indicated the \#2 motor clutch and removed the cracked fluid coupling housing from the \#3 motor. Hung the rotary tong and set the rat hole. Commercial power was'connected to the rig panel.

Continued general rig-up with 9 men. Assisted with repairs to the draw works high-drum clutch.

8 hours - continued general rig-up with 8 men. Laid the water line from the shallow domestic well to the rig and trailer house. Unloaded line truck from NTS loaded with tubing and drill pipe, then reloaded same truck with 11 -inch drill collars and a 15 -inch reamer for return to the NTS. Continued to support the draw works repairs.

Secured for New Year's holiday. Maintained security watch.
Rigging up rotary tools and continued to assist in the repairs to the draw works. Constructed a shed around mud pumps. Ran $27 / 8$-inch tubing from the hot water well to the rig for the rig heaters. Filled pits with water, mixed spud mud, and picked up drilling tools.

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DAILY DRILLING REPORTS - RRGE-1
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January 5, 1975

January 6, 1975 . Drilled 15-inch hole from 301 feet to 787 feet in $141 / 2$ rotating hours. Electrician checked permanent power and rig generator. Mud VIS-48-54, WT-9.1. Sand content 1.5\%. Low temperature was $20^{\circ}$ at $5 \mathrm{a} . \mathrm{m}$.

January 7, 1975

January 8, 1975

January 9, 1975

January 10, 1975
Spudded the 15 -inch hole at 2 a.m. and drilled from 40 feet to 301 feet (RKB)* in $151 / 2$ hours. Bit \#1 is a Security, 3-cone mill tooth, type M4N. Mud VIS-55, WT-9.1. Worked 3 additional men to install the hot water line in the subbase. Low temperature was $20^{\circ} \mathrm{F}$ at 5 a.m.

Completed drilling the 15 -inch hole from 787 feet to 920 feet at 6 a.m. in $5-3 / 4$ rotating hours. Deviation survey: $1^{\circ}$ at 170 feet and $1^{\circ}$ at 295 feet. $51 / 2$ hours - laid down drill pipe and 11 -inch drill collars. 11-1/2 hours picked up 26 -inch hole opener ( $\mathrm{H}, \mathrm{O}$.) and float sub and reamed 15 -inch hole to 26 inches from 56 to 435 feet. Mud VIS-50, WT-9.1, plastic viscosity - 10, and sand content of $1 \%$.

Bit \#1. Security M4N, made 880 feet in $35-3 / 4$ hours.
Opened 15 -inch hole to 26 inches from 435 feet to 918 feet (total surface casing depth) in 17 hours. (Total rig time to ream the 15 -inch hole to 26 inches, including picking up the H.O., was $281 / 2$ hours.) 6 hours - circulated hole for logs. Mud VIS-48-52, WT-9.1.

7 hours - conditioned hole and tripped for logs. 5 hours logged with Schlumberger. (Loggers T.D. is 900 feet from ground level.) Logs run - 4-arm caliper, dual induction laterolog and bore hole compensated sonic. 11 hours tripped in with a 26 -inch H.O. to check for fill after logging - no fill. Tripped out and laid down 11-inch drill collars and hole opener. Rigged to run casing. Low temperature was $20^{\circ}$ and snowing.

1 hour - worked on high-drum clutch bearing in the draw works. 4 hours - made up shoe and float collar on shoe joint. $7-1 / 2$ hours - ran casing - 22 joints of 20 -inch, $94.0 \mathrm{ib} / \mathrm{ft}$, $\mathrm{H}-40$, ST\&C. Total length 921.08 feet of casing set at 901 feet ground level ( 919 feet RKB depth). The float collar was located 43 feet above the guide shoe on the first joint. Used 21 centralizers and 1 cement basket.
*All depths shown are referenced to the rotary kelly bushing (RKB) which is 18 feet greater than ground level.

| January 10, 1975 (Continued) | Circulated hole for 30 minutes with mud. Started cementing at 5 p.m. with 1,090 sacks of $50 / 50$ poz-mix with $60 \%$ silica flour and $3 \%$ CaCl ${ }^{2}$. Dropped plug at 6 p.m. and displaced with 311 barrels of mud and water. Pumped plug with 900 psi and cement in place (CIP) at 7 p.m. Good circulation throughout job. 5 hours - wait on cement (W.O.C.). Low temperature was $16^{\circ}$ with 40 mph winds. Bottom hole temperature was $109^{\circ} \mathrm{F}$. |
| :---: | :---: |
| January 11, 1975 | 24 hours - W.O.C. and clean rig floor. Released pressure on 20 -inch casing and cut off excess. Welded bradenhead on the 20 -inch casing. Nippled up the B.O.P. Low temperature was $4^{\circ}$ at midnight 1-11-75. |
| January 12, thru January 13, 1975 | 24 hours - W.O.C. and nippling up the B.O.P. Thawed mud and water lines. USGS on site to run a temperature survey in the 20 -inch casing. Worked 3 men dayshift to install the hot water system. |
|  | Nippling up B.O.P. and assisted mechanics from NTS in removal of guards from draw works for high-drum clutch bearing replacement. |
| January 14, thru January 17, 1975 | Supported draw works repairs. High-drum sprocket assembly removed by NTS mechanics and departed for Idaho Nuclear Engineering Laboratory Machine Shop. Cleaned and worked on other rig equipment. Continued work on the hot water blower system. Installed hot water line from the rig to the cattle pond to dispose of hot water after circulation through rig heating system. |
| January 18, 1975 | NTS mechanics installed the repaired high-drum clutch and bearing and shimmed in place at 8:30 p.m. Cleaned and worked on other rig equipment. |
| January 19, 1975 | 24 hours - completed rig repairs and finished chipping cement from under shaker tanks. Installed shaker screens, hooked up mud lines and started pump engines. |
| January 20, 1975 | $63 / 4$ hours - connected flow line, water line, and filled mud pits. $13 / 4$ hours - pressure tested B.O.P. to 300 lbs. - okay. Ran in one drill collar and one joint of $65 / 8$-inch drill pipe. Pressure tested pipe ram to 300 lbs - okay. Tripped in hole at 2 p.m. and tagged cement inside the 20 inch casing at 867 feet. 5 hours - drilled out the plug, cement and shoe with Bit \#2, a $121 / 4$-inch, Smith, type DTJ, mill tooth. Cleared shoe at 10 p.m. and drilled new hole from 918 feet to 975 feet in 2 hours. Drilling fluid is water with no additives. Placement of stabilizers is one-near bit, one-string at 35 feet up and one-string at 65 feet up. |

January 21, 1975

January 22, 1975

January 23, 1975

January 24, 1975

January 25, 1975

January 26, 1975
$153 / 4$ hours - drilled $121 / 4$-inch hole in sand and shale from 975 feet to 1,427 feet. $71 / 2$ hours - drained mud lines and changed head and liners in mud pump. Hole is taking about 100 barrels of water per hour. Temperature was $18^{\circ}$ at 5 a.m.

Drilled $121 / 4$-inch hole with water from 1,427 feet to 1,521 feet in $21 / 4$ hours. Hole is taking between 150 to 200 barrels of water per hour. Ran out of water at 5:15 a.m. Drained water and mud lines, desander, and mud pump. Connected hose from hot water line to pit. Waited on mud pits to fill, and filled rig tank. A 100 -barrel vacuum truck arrived on site from Duschesne, Utah to haul drilling water to the rig from the Raft River. 4 hours tripped for new bit while waiting on required water volume and went in hole with new Bit \#3, 12 1/4-inch Smith, type DTJ, mill tooth with jet nozzles - 2 14/32-inch and 1 15/32inch. (Bit \#2 made 603 feet in $173 / 4$ hours.) No fill encountered on trip to bottom. Drilled $121 / 4$-inch hole with Bit \#3 from 1,521 feet to 1,745 feet in 4 hours. Temperature was $11^{\circ}$ at 5 a.m.

Drilled $121 / 4$-inch hole in sand and shale from 1,745 feet to 2,142 feet in $111 / 2$ hours. Continuing to drill with water and no additives. Survey at 2,105 feet: $1^{\circ} 5$ minutes $S 82^{\circ} \mathrm{W}$. 6 hours - drained mud lines and tripped for new bit. (Bit \#3 made 621 feet in $151 / 2$ hours.) 18 feet of fill encountered in return trip with Bit \#4, a 12 //4-inch, Smith, type DTJ. Drilled 12-1/4-inch hole from 2,142 feet to 2,235 feet in 3-1/2 hours. Temperature was $22^{\circ}$ at 5 a.m.

Drilled $121 / 4$-inch hole with water in sand and shale from 2,235 feet to 2,635 feet in $14,3 / 4$ hours. Survey at 2,558 feet: $2^{\circ} 5$ minutes $S 74^{\circ} \mathrm{W} .21 / 2$ hours waited on drilling water, hooked up fill-up line and drained lines for trip. 2 hours - tripped out. (Bit \#4 made 493 feet in $181 / 4$ hours.

Pick up Bit \#5, Smith DTJ, mill tooth and tripped back in hole. 40 feet of fill encountered. Cleaned to bottom and drilled $121 / 4$-inch hole from 2,635 feet to 3,060 feet in $181 / 2$ hours.

Drilled 12 1/4-inch hole from 3,060 feet to 3,091 feet in $11 / 2$ hours. 3 hours - drained lines and tripped out of hole. 3 hours - dressed near bit stabilizer with new chert pin and blocks. (Bit \#5 drilled 456 feet in 20

January 26, 1975
(Continued)

January 27, 1975

January 28, 1975

January 29, 1975

January 30, 1975

January 31, 1975

February 1, 1975
hours.) $21 / 4$ hours - picked up the Smith Bit \#6, type DTJ and cleaned 55 feet of fill during trip to bottom. Drilled 12 //4-inch hole with water from 3,091 feet to 3,326 feet in $91 / 4$ hours. Temperature was $45^{\circ}$ at 5 a.m. with blowing snow.

Drilled $121 / 4$-inch hole with water from 3,326 feet to 3,533 feet in 11 1/2 hours. $21 / 4$ hours - tripped for new bit. (Bit \#6 drilled 442 feet in $203 / 4$ hours.) Picked up Bit ${ }^{H} 7$, a Smith DTJ mill tooth, and float sub. Tripped in the hole and cleaned 12 feet of fill. Drilled $121 / 4$-inch hole from 3,533 feet to 3,612 feet in 4 hours.

Drilled $121 / 4$-inch hole in volcanic tuff from 3,612 feet to 4,030 feet in 16 hours. Survey at 3,953 feet: $3^{\circ} 10$ minutes $\mathrm{N} 67^{\circ} \mathrm{W} .41 / 2$ hours - drained lines and tripped out of hole. (Bit $\# 7$ drilled 497 feet in 20 hours.) Hole is taking about 135 barrels of water per hour. Low temperature was $12^{\circ}$ at 4 a.m.

6 hours - finished trip out of hole and picked up Bit \#8, a Smith DTJ. Tripped in and cleaned 18 feet of fill. Drilled $\$ 21 / 4$-inch hole from 4,080 feet to 4,260 feet in $113 / 4$ hours. Hole continued to take approximately 130 barrels of water per hour. Low temperature was $8^{\circ}$ at 3 a.m.

Drilled 12 //4-inch hole from 4,260 feet to 4,495 feet in $81 / 4$ hours. Survey.at 4,356 feet: $2^{\circ} 45$ minutes $\mathrm{N} 85^{\circ} \mathrm{W} .3$ hours - circulate hole for \#1 core. 4 hours tripped out of hole. Hole is taking 130 barrels of water per hour. Low temperature was $9^{\circ}$ at $5 \mathrm{a} . \mathrm{m}$. (Bit \#8 drilled 465 feet in 21 hours.)

6 hours - picked up and serviced the core barrel and worked on compressors. $31 / 2$ hours - tripped in hole for Core \#1 with an $83 / 4$-inch diamond core bit. $41 / 4$ hours - cut Core \#1 from 4,495 feet to 4,555 feet and recovered 23 feet of core (38\%). 7 1/4 hours - laid down core barrel and USGS ran temperature survey. Hole still taking approximately 135 barrels of water per hour.

USGS temperature survey line broke and left the instrument and 1,100 feet of line in the hole. Reamed core hole to $121 / 4$-inches from 4,495 feet to 4,555 feet and drilled from 4,555 feet to 4,650 feet in 14 hours. Circulated hole for logs. Low temperature was $26^{\circ}$ at 5 a.m.





February 2, 1975

February 3, 19755 hours - completed logging and rigged down logging equipment. 19 hours - closed B.O.P. blind rams at 6 a.m. and pumped cold water in the hole with 100 psi in an attempt to kill the flow. 2,000 barrels pumped in hole and monitored well head pressure rise from 47 lbs. to 58 lbs.

February 4, 1975 B.O.P. shut-in. Continually monitored pressure on the well head - pressure ranged from 48 psi to 58 psi. Pump pressure while trying to kill well was 150 psi at 35 strokes. per minute. 800 barrels of cold water injected today.

February 5, 1975

February 6, 1975

February 7, 1975

February 8, 1975

February 9, 1975
Waited on Grant rotating head from NTS. Changed oil in one rig engine and pump engine and performed other general maintenance. Well head pressure ranged from 55 psi to 60 psi. Set in the rotating head, rotary table and floor. Ran two drill collars, one joint of pipe and kelly in hole to circulate. .

Pulled drilling tools out of the hole. 6 hours - tripped in hole and tagged fill at 4,631 feet. 8 hours - pumped cold water in the hole - 1,300 barrels today. Off loaded 4 -inch aluminum pipe and ran line from Raft River to the rig. Well head pressure ranged from 45 psi to 70 psi.

21 1/2 hours - pumped cold water in the hole through drill pipe at 28 to 40 strokes per minute (S.P.M.) with pipe rams ciosed.

24 hours - continued pumping cold water in hole through drill pipe. Ran the Amarada temperature bomb on 100-foot stations and on 271-foot stations. Tripped out of the hole to log.

24 hours - logged with Schlumberger and continuously pumped cold water at 16 S.P.M. While logging. Ran the caliper $\log$ to 4,616 feet and the temperature survey to 4,610 feet.

February 10, 1975 Tripped in hole to 3,798 feet. Rigged up 2-inch return line from Braden head to mud pits. Continued pumping water down drill pipe. Rigged up and ran the Schlumberger temperature survey. Shut the well in at 6 p.m. and shut off pump at 7 p.m. Waited on orders.

February 11, 197517 hours - continued to circulate hot water out of the hole with cold water. 2 hours - repaired the trash pump used for pumping from the river. 7 hours - tripped out of the hole; made up the otis sub and plug and tripped in the hole in preparation for setting the sand plug. Drill string open-ended at 4,399 feet.

February 12, 19754 hours - picked up 4 joints of drill pipe and ran in to $4,399.26$ feet. Picked up kelly, filled drill pipe with water and rigged up Halliburton to set the sand plug. Tried to pull the Otis plug with the wireline no success.

February 13, 197510 hours - tripped out of hole and waited on Otis plug parts. Serviced the rig. 6 hours - picked up a crossover sub and float sub, a single joint of drill pipe and put on the rotating head. The float sub connection leaked. Broke the float sub off, picked up one stand of drill collars, installed the rotating head and tripped in hole to 4,404 feet. Halliburton primed the pumps and started pumping sand in the hole at 4 p.m. Stage \#1 - 4, 632 feet to 4,528 feet, 104 feet of fill-up. Stage \#2 - 4,528 feet to 4, 398 feet, 130 feet of fill-up. Pumped in Stage ${ }^{*} 3$ with the pipe set at 4,216 feet.

February 14, 1975 Halliburton continued pumping the sand plug. Finished Stage \#3 - 4, 398 feet to 4,328 feet - 70 feet of fill-up; Stage \#4 - 4,328 feet to 4,168 feet -160 feet of fill-up; and Stage \#5-4,768 feet to 4,077 feet - 91 feet of fillup. Pulled pipe up to 3,876 feet. Pumped Stage \#6-4,077 feet to 3,983 feet - 94 feet of fill-up.

February 15, 1975 Continued to monitor the sand rise after pumping Stage \#6. Pulled up to 3,783 feet. Started pumping Stage \#7 at 4 a.m. Stage \#7 - 3,983 feet to 3,877 feet - 106 feet of fill-up. (Used approximately 50,000 lbs. of sand in 7 stages.) Plugged the drill pipe when trying to displace sand with water in Stage \#8 with the drill pipe hung at 3,660 feet. Tripped out and unplugged 6 stands and 1 single joint of drill pipe. Tripped in the hole and tagged the top of Stage \#8 at 3,840 feet - 37 feet of fill-up. Started pumping sand Stage \#9 at 9:10 p.m. with the drill pipe hung at 3,628 feet. Tagged top of Stage \#9 at 3,770 feet - 70 feet of fill-up.

February 16, 1975

February 17, 1975

February 18, 1975

February 19, 1975

February 20, thru February 21, 1974

3 hours - pressure tested for water flow. 3 hours pumped 30 sacks of barite as Stage \#10, tagged top of plug at 3,770 feet - no fill-up. Pumped Stage \#11, an additional 30 sacks of barite with the drill pipe hung at 3,750 feet. 12 hours - continued to tag the top of the barite Stage \#11. Final tag at 5:45 p.m. was 3,769 feet - 1 foot fill-up. Pumped 60 sacks of barite Stage \#12 with drill pipe hung at 3,752 feet. Stage \#12-3,769 feet to 3,763 feet -6 feet of fill-up. Plug held 20,000 lbs. weight for 10 minutes.

Final tag on barite plug (Stage \#12) at 12:05 a.m. was 3,762 feet. Laid down a single joint of drill pipe. Pumped a cement plug (Stage \#13) in hole and pulled the drill pipe up the hole to clear the cement plug. Stage \#13-115 sacks of Class $G$ cement, slurry weight - 16.8 1bs./gal. and volume was 1.02 feet $3 /$ sack with 4.0 gals. of water per sack. C.I.P. at 1:05 a.m. 8 hours -W.O.C. Tripped in the hole and tagged the top of cement Stage \#13 at 3,642 feet - 120 feet of fill-up. Checked pressure on the well and tripped out of the hole. Set out the floor and rotary table. Changed out the 13 3/8-inch Hydril BOP to a 16-inch Hydril BOP and bolted on the rotating head.

Welder rebuilt the flow line and changed out a 6 -inch valve in the line. Serviced the rig and tripped in the hole. Filled the drill pipe with water, started the desander and jetted the pits. $81 / 4$ hours - ran the Amarada temperature bomb and concurrently flow tested the well through the 6 -inch flow valve. Temperatures recorded: 3,100 feet, $231^{\circ} ; 3,300$ feet, 239ㅇ 3,600 feet, $239^{\circ}$. $21 / 2$ hours - pulled temperature bomb out of the hole and started to trip out of the hole to pick up a 15 -inch bit.

5 hours - tripped out of hole and picked up Bit \#10, a 15inch Smith, DSJ mill tooth. Reamed $121 / 2$-inch hole to 15 inches with tight spot encountered between 3,167 feet to 3,257 feet. (The 15 -inch bit was run only to assure clearance for the $133 / 8$-inch casing string, since the average eroded bore hole diameter after drilling the $121 / 4$-inch hole with water was 20 inches.) $111 / 2$ hours - attempted to level rig. Moved drill pipe from front of rig and spread sand around jack pad.

Waited on rig leveling equipment and attempted to level rig. (Ground-thaw settlement caused rig to settle to the southeast. The attempt proved unsuccessfu1.) Thawed and drained the 4inch water line to the rig from the river and serviced the rig and equipment.

February 22, $1975 \quad 121 / 2$ hours - continued to attempt to level the rig and rigged down the leveling equipment. $23 / 4$ hours tripped out of the hole to run casing. 5 1/4 hours rigged to run casing, ( $133 / 8$-inch, $\mathrm{H}-40,54.5$ and 61.0 los./ft.) 3 hours - running casing - picked up and ran 20 joints on the hook.

February 23, 19756 hours - finished running $133 / 8$-inch casing; total of 3,651 feet on the hook. Rigged up to cement and circulated out fill from 3,621 feet to 3,642 feet. Started cementing Stage \#1 at 12:30 p.m. with bottom of casing set at 3,623 feet (GL). $31 / 4$ hours - cementing with Halliburton. Stage \#1 - 1,500 sacks of $50 / 50$ poz-mix, $60 \%$ silica flour and $1 / 2$ of $1 \%$ of HR-12 and 400 sacks of $50 / 50$ poz-mix yielded 568 barrels of slurry. The casing parted approximately 7 joints down while displacing the cement at 2:45 p.m. Screwed back into casing and torqued to 2,000 ft/lbs. Pulled the casing string to 122,000 lbs. Hooked up the Halliburton lines and put 500 lbs . pressure on the casing - held okay. Low temperature was $12^{\circ}$ at 5 a.m.

February 24, 197516 hours - wait on cement (W.O.C.) Dresser-Atlas ran a cement bond log which stopped at 2,837 feet. Cleared area around rig during W.O.C. period. $31 / 4$ hours - rigged up and cemented Stage \#2 at 5:45 p.m. Cemented from the top and down the annulus with 50 sacks of $50 / 50$ poz-mix with $60 \%$ silica flour: 250 sacks of $50 / 50$ poz-mix with $4 \%$ gel, $2 \% \mathrm{CACL}_{2}$ and 25 lbs ./sack of gilsonite and 1,176 sacks of 50/50 poz-mix with $60 \%$ silica flour - yielded 407 barrels of slurry. Drained water pump and water lines. Drained the kelly hose, stand pipe, and the \#1 pump while W.O.C.

February 25, 1975

February 26, 1975

8 hours - W.O.C. Cut off $133 / 8$-inch casing and rigged up Dresser-Atlas for running the cement bond log. Ran the bond log at 10 a.m. $61 / 2$ hours - cleared the rig floor of cementing and casing tools, picked up Bit \#11, a Smith 12 1/4-inch DTJ and tripped in hole. Tagged cement at 2,835 feet. 4 hours - drilled plug and cement from 2,835 feet to 2,937 feet. Low temperature was $18^{\circ}$ at 6 a.m.
$71 / 2$ hours - drilled cement out of 13 3/8-inch casing from 2,937 feet to 3,328 feet. Drill pipe torquing up at 3,325 feet. $31 / 2$ hours - drilled on junk - tripped out of the hole to pick up a $97 / 8$-inch bit. (Bit \#11 drilled 493 feet of cement in 11 1/2 hours.) $41 / 2$ hours - picked up a $97 / 8$ inch security mill tooth bit, tripped in the hole and drilled on junk. $81 / 2$ hours - tripped out of hole and pressure tested casing to 300 psi. Picked up $43 / 4$-inch collars, bit sub and 5 3/4-inch Gruner mill tooth bit. Picked up a pin-box float sub.
DAILY DRILLING REPORTS - RRGE-1

February 27, 1975

February 28, 1975

March 1, 1975

March 2, 1975

March 3, 1975

March 4, 1975

24 hours - layed down the 5 3/4-inch tools and picked up an $113 / 4$-inch Globe junk basket. Tripped in the hole and milled the collapsed casing from 3,325 feet to 3,331 feet. Serviced the rig and equipment intermittently during the day.
$151 / 2$ hours - tripped out after milling and left the float sub ( 1.82 feet), junk sub ( 2.81 feet), and mill (1.91 feet) in the hole. Waited on overshot for fishing operation. $81 / 2$ hours - made up the fishing tools and tripped in the hole with the overshot. Fished for 1 hour with no recovery. Tripped out and used welder to hard face the bit guide.

24 hours - fished with the overshot. Recovered the fish at 8:30 p.m., tripped out of the hole and laid down the fishing tools.

24 hours - cleared rig floor of fishing equipment and picked up a dual milling assembly, a $121 / 4$-inch clusterite mill behind an $113 / 4$-inch mill. Milled 2 inches and tripped out - the $121 / 4$-inch mill was out of gauge $11 / 4$-inches. 5 hours - slipped and cut 88 feet of drilling line and picked up 6 -inch drill collars and an $81 / 2$-inch Security bit, type M44N. 11-hours - tripped in the hole (tight spot at 3,325 feet) and drilled on junk at 3,329 feet. Tripped out to check bit after no penetration and found the center teeth worn completely off. Picked up $93 / 8$-inch globe basket and tools and tripped in the hole. The tools would not get past a tight spot at 3,325 feet. Tripped out of the hole for a mill.

24 hours - laid down the globe basket and picked up milling tools. Milled on collapsed casing with $123 / 8$-inch clusterite mill and $121 / 4$ concave and taper mills from 3,325 feet to 3,335 feet.

7 hours - milled with 12 1/4-inch (concave) tapered Mill \#5 from 3,335 feet to 3,338 feet. Tripped out to check the mill. The junk sub skirt was torn off and the mill was worn out. 9 hours - picked up Mill \#6, a 12 1/4-inch flat-bottom concave mill, tripped in and milled from 3,332 feet to 3,338 feet. Tripped out - $121 / 4$-inch mill was worn out and $1 / 2$-inch out of gauge. 8 hours - off-loaded Servco mills and pressure tested the casing for 15 minutes to 300 lbs. Tripped in the hole with a 9 -inch magnet and worked the magnet from 3,336 feet to 3,338 feet. Tripped out and recovered the junk sub skirt pieces and other junk steel.

March 5, 1975

March 6, 1975

March 7, 1975

March 8, 1975

March 9, 1975

March 10, 1975

5 hours - worked in the hole with a 9 -inch magnet. Recovered additional pieces of the junk sub skirt and other steel. 11 hours - laid down the magnet and picked up Mill \#7, an $81 / 2$-inch tapered mill. Milled from 3,338 feet to 3,370 feet and tripped out of the hole. 8 hours picked up Mill \#8, an 8 3/4-inch mill and milled on junk and cement from 3,370 feet to 3,435 feet.
$61 / 2$ hours - drilled cement out of $133 / 8$-inch casing from 3,435 feet to 3,585 feet. $81 / 2$ hours - tripped out of the hole, broke down the milling tools and cleared the rig floor of all fishing tools. Pressure tested the $133 / 8$-inch casing to 300 lbs. for 30 minutes. 9 hours picked up Mill \#9, a $121 / 4$-inch tapered mill and tripped in the hole. Milled on junk and cement from 3,571 feet to 3,584 feet. Started to trip out of the hole.

4 hours - finished the trip out of the hole with Mill \#9. Picked up an 11 1/4-inch 0.D. Globe basket and float sub and tripped in the hole to fish for junk. Fished for junk for $23 / 4$ hours. Tripped out of the hole and tool joints were tight after pulling 3 stands of drill pipe. Serviced the rig. Picked up a 9 -inch magnet and subs and tripped in the hole. 11-3/4 hours - fished with the magnet and tripped out of hole 3 times and recovered a full basket of junk each time.

17 1/4 hours - made magnet runs Numbers 5, 6, and 7 and recovered junk each time. 6 hours - laid down the 9 -inch magnet and subs and picked up a 12 1/4-inch Smith bit (a rerun of \#5). Tripped in and tried to get past junk at 3,585 feet. Tripped out to pick up a magnet. 1 hour picked up and started to trip in hole for a 9 -inch magnet run \#8.

2 3/4 hours - fished with the 9 -inch magnet and tripped out with $1 / 2$ basket of junk. $71 / 4$ hours - broke down the magnet and subs and picked up a 12 1/4-inch bit (rerun of \#3). Tripped in and drilled on junk at 3,586 feet. 6 hours - tripped out and picked up a 9 -inch magnet. Tripped in and fished with magnet run \#9 and recovered a full basket of small junk. Picked up an 11 1/2-inch magnet, tripped in and recovered small junk. Picked up an 11 1/2-inch flat-bottom mill, tripped in and milled from 3,586 feet to 3,587 feet.
$31 / 2$ hours - milled from 3,586 feet to 3,590 feet. $61 / 2$ hours - tripped out to check mill. The junk sub skirt was pushed in and split and the mill was worn out. Picked up an 11 1/2-inch magnet and clusterite shoe and

March 10, 1975 (Continued)

March 11, 1975

March 12, 1975

March 13, 1975

March 14, 1975

March 15, 1975
tripped in the hole to 3,587 feet. Drilled down with magnet to 3,589 feet and pulled out of the hole. $81 / 2$ hours - picked up a 12 -inch concave mill and milled to 3,590 feet. $41 / 2$ hours - tripped out and picked up an 11 1/2-inch magnet. Tripped in, fished from 3,587 feet to 3,590 feet and recovered 1 1/2 cups of junk.

8 hours - fished with 11 1/2-inch magnet and recovered a full cup of junk at 3,590 feet. Tripped out, picked up 6 -inch collars and an $83 / 4$-inch tapered mill. 8 hours - tripped in and milled on junk from 3,587 feet to 3,591 feet. Tripped out, laid down tools and repaired the rotating head. 8 hours - picked up a $93 / 4$-inch tapered mill and milled junk and cement from 3,591 feet to 3,617 feet.

16 hours - milled junk and cement to 3,631 feet and tripped out for a $121 / 2$-inch mill and picked up a staged $93 / 4$-inch and $121 / 4$-inch mill and milled to 3,631 feet. 8 hours - made up an 11 1/2-inch magnet assembly, worked on the B.O.P. and accumulators and tripped in with magnet run \#14.

10 1/2 hours' - tripped out with magnet run \#14 and recovered a large piece of junk casing ( 2 feet, 7 inches long and 7 inches wide). Two additional magnet runs (\#15 and \#16) recovered numerous pieces of casing, a nose cone from a mill and other small junk. 9 1/2 hours - worked on the blowout equipment and picked up a. 12 1/4-inch drilling assembly with Bit \#14, a Smith, mill tooth, type DGHT. Tripped in the hole to 3,632 feet and drilled out the float collar and shoe, the Halliburton cement barite and sand plugs to 3,752 feet with water.

24 hours - drilled out the sand plug from 3,752 feet to 4,613 feet with water in $16 \mathrm{l} / 2$ rotating hours circulated hole and jetted pits every 120 feet.

24 hours - finished drilling sand plug to 4,645 feet and encountered junk. Tripped out of the hole and installed a new rotating head. Pumped water down the drill pipe to kill the flow for 6 hours. Pumped water down the annulus for 10 hours while a welder hooked up the $65 / 8$-inch flow test manifold. Used backhoe to bury a reserve pit drain line.

March 16; 1975

March 17, thru March 18, 1975

March 19, 1975

March 20, thru
March 21, 1975

March 22, 1975

March 23, 1975

March 24, 1975

24 hours - worked on the flow test system and flow tested the well. The well flowed approximately 700 to 900 gallons per minute at surface temperatures ranging from $110^{\circ}$ to $236^{\circ} \mathrm{F}$. Tested the flow by pumping cool water down $133 / 8$-inch casing and gauging flow rates back into mud pits. Hot water is flashing at the surface.

Injected cool water and flow tested. Wellhead pressure during flow test was 25 lbs. (max.) and when the well was shut in was 150 lbs. Welder worked on flow test manifold. The maximum flow rate and surface temperature recorded was $1,000 \mathrm{gpm}$ at $265^{\circ} \mathrm{F}$. The drill crew serviced equipment and cleaned the location.

12 1/2 hours - continued to flow test the well. 11 1/2 hours - rigged down the test line at 12:30 p.m. for a trip in the hole. Ran 29 stands and 1 single joint in the hole and laid down drill pipe in preparation for leveling the rig.

24 hours - laid down 6 5/8-inch drill pipe and drill collars and moved out some equipment to allow for rig leveling. Off-loaded leveling equipment at 9 a.m. (shipped from NTS). Leveled the rig and reloaded the leveling equipment by 8 p.m. on March 20.

Moved equipment in and reassembled the equipment around the subbase area. Nippled up the blowout equipment, worked on the flow test manifold system and prepared to go in the hole with fishing tools.

24 hours - finished picking up the 12 1/4-inch Globe basket, drill collars and $65 / 8$-inch drill pipe. Fished for junk and bit cone at 4,645 feet.

Completed trip out with Globe basket and recovered the bit cone and a piece of formation. Tripped back in the hole and recovered 2 pieces of formation. Picked up an 11-inch magnet, tripped in and fished with the magnet at 4,651 feet. Started out of hole with magnet and pumped down annulus because float was not holding.

2 hours - finished trip out of hole and recovered 17 bearings and 7 stripper rubber bolts. 12 hours - picked up a 12 1/4-inch Smith DGAT bit (Bit \#15) and drilled from 4,651 feet to 4,686 feet in $41 / 2$ hours. Conditioned hole for a core and tripped out of the hole. 10 hours - picked up a Christensen core barrel and $83 / 4$-inch and 4 -inch core

## DAILY DRILLING REPORTS - RRGE-1

March 24, 1975 (continued)

March 25, 1975

March 26, thru March 27, 1975

March 28, 1975

March 29, 1975

March 30, 1975

March 31, 1975

April 1, thru April 3, 1975
bit. Tripped in and cut Core \#2 from 4,686 feet to 4,690 feet. Coring at $35 \mathrm{rmp}, 12,000 \mathrm{lbs}$. on the bit, 575 psi pump pressure at 23 strokes per minute.

10 hours - completed cutting Core \#2 from 4,690 feet to 4,698 feet. Tripped out, serviced the core barrel and recovered 9 feet of core. 14 hours - laid down core assembly and jetted pits to flow test. Worked on B.O.P. for 2 1/4 hours.

Tried to pressure test the well but pipe rams would not hold. Worked on the B.O.P. and accumulator. 17 hours - drained and thawed water lines. Low temperature was $10^{\circ}$ at 5 a.m. with high winds. Detected an earthquake at 8:30 p.m. The crews serviced equipment and cleaned up around the drill site. Flow testing 600 G.P.M. at $207^{\circ}$ F.

23 hours - repaired water pump and ran injection test. Repaired Schaffer B.O.P. - $31 / 2$ hours. 1 hour - made up the junk sub and Bit \#16, a Security 11-inch button, type M-88.

6 hours - repaired Hydril accumulator and tripped in the hole to 4,686 feet. 1 hour - reamed $83 / 4$-inch core hole to 11 inches from 4,686 feet to 4,698 feet. Drilled new formation with 11 -inch bit from 4,698 feet to 4,825 feet with water in $121 / 4$ hours.

Drilled 11 -inch hole with Bit \#16 from 4,825 feet to 4,995 feet in 21 rotating hours. $13 / 4$ hours - repaired mud line and pumped cool water in annulus for connections.

Drilled the 11 -inch hole from 4,995 feet to 5,005 feet (TD) in 1 hour. Conditioned hole for 2 hours for Core \#3. 21 hours - tripped out with Bit \#16. (The 11-inch Bit \#16 drilled 307 feet in $341 / 2$ hours.) Picked up the Christensen core barrel and Core Bit \#3, an 8 3/4inch by 4-inch type MC2O, and tripped in the hole. Cut Core \#3 from 5,005 feet to 5,007 feet. Coring was at $42 \mathrm{rpm}, 15$ to 20,000 lbs. on bit, 800 psi pump pressure at 20 strokes per minute. Pulled out of hole and recovered 2 feet of core.

Rigged up and performed flow tests through 6-inch flow line and two 2-inch lines. Crew worked on equipment and sorted spare parts in bins.

Picked up and ran the Amarada temperature bomb. Picked up water sampler and took 2 water samples at 2,000 feet.

## DAILY DRILLING REPORTS - RRGE-1

April 10, 1975 Commenced rigging down on graveyard shift. Laid down

Apri1 4, 1975

April 5, 1975

April 6, 1975

April 7, 1975

April 8, 1975

Apri1 9, 1975

April 17, 1975

April 12, 1975
$111 / 2$ hours - laid down 101 joints of $65 / 8$-inch drill pipe and thirteen 8 -inch drill collars. 12 1/2 hours ran the Amarada temperature bomb to 1,000 feet and flow tested the well. Maximum recorded temperature and flow rate was $255^{\circ} \mathrm{F}$ and 425 gpm .

Took well pressure readings with the well shut-in. Ran the Amarada temperature bomb and flow tested the well through the 6 -inch flow line and two 2 -inch lines.

Continued to take well head pressure readings while waiting for Schlumberger to arrive on location. Rigged up to log at 9:30 a.m. Schlumberger ran the temperature $\log$ and sonic $\log$ to 5,000 feet and the 4 -arm caliper $\log$ from 5,000 feet to 3,000 feet. Maximum bottom hole temperature was $292^{\circ} \mathrm{F}$.

Finished running caliper and density logs at 5:30 a.m. and rigged down Schlumberger. Picked up kelly and a single joint of drill pipe for tests. Tested well for flow temperature and flow rate. Shut the well in and pumped cool water in the hole at 20 s.p.m.

Pumped cool water in the hole and waited for valves and spools. Picked up the Halliburton retrievable packer and set the packer in the $133 / 8$-inch casing at 1,380 feet to stop flow. Installed the 20 -inch by 14 -inch spools two-inch valves and pressure tested to 575 psi. No leaks were observed.

Broke down tools and B.O.P. equipment. Nippled up the 14 -inch master gate valve and spools, Hydril, rotating head and 6 -inch flow line. Laid down 45 joints of drill pipe. Broke out the water line from Raft River. Crews worked on equipment and cleaned location. kelly, rat and mouse holes and steam blowers. Worked 2 crews - 10 men during day shift for rig down operations.

Rigged down for 8 hours on day shift with 3 crews ( 15 men).

Rigged down for 8 hours on day shift with 3 crews ( 14 men ). Stacked and prepared $133 / 8$-inch casing, 30-inch casing, drill collars, drill pipe and subs for inspection.

April 13, 1975 Rigged down for 8 hours on day shift with 3 crews (14 men). Worked with the forklift in the yard and broke out the water well line to the rig. Lowered mast on the stand at 3:15 p.m.

April 14, 1975 Rigged down for 8 hours on day shift with 3 crews (14 men). Drained the draw works drum and changed liners in mud pumps.

April 15, 1975 Rigged down for 8 hours on day shift with 3 crews ( 15 men). Unbolted subbase and cleaned and painted the derrick.

April 16, thru Apri1 18, 1975

Rigged down for 8 hours on day shift with 3 crews ( 15 men). Worked with casing inspectors and offloaded $133 / 8$-inch casing ( 3 loads). Worked on the B.O.P. Rigged down the desilter and mud pits. Cleaned and painted some equipment and loaded tools in junk boxes while waiting on trucks. Trucks will be on site tomorrow morning (April 19) to start the move to RRGE-2.

| Apri] 13, 1975 | Rigged down for 8 hours on day shift with 3 crews (14 men). Worked with the forklift in the yard and broke out the water well line to the rig. Lowered mast on the stand at 3:15 p.m. |
| :---: | :---: |
| April 14, 1975 | Rigged down for 8 hours on day shift with 3 crews (14 men). Drained the draw works drum and changed liners in mud pumps. |
| April 15, 1975 | Rigged down for 8 hours on day shift with 3 crews ( 15 men). Unbolted subbase and cleaned and painted the derrick. |
| April 16, thru April 18, 1975 | Rigged down for 8 hours on day shift with 3 crews (15 men). Worked with casing inspectors and offloaded $133 / 8$-inch casing ( 3 loads). Worked on the B.O.P. Rigged down the desilter and mud pits. Cleaned and painted some equipment and loaded tools in junk boxes while waiting on trucks. Trucks will be on site tomorrow morning (April 19) to start the move to RRGE-2 |

REYNOLDS ELECTRICAL \& ENGineering co., inc.
CASING RECORD
RRGE-1 - SURFACE CASING - 20 INCH O.D., 94 1b/ft, H-40 DATE INSTALLED - JANUARY 10, 1975
Joint
No.

Cumulative Length (ft.)
2.20
45.72
47.62
86.95
129.96
173.26
211.70
254.62
297.53
339.75
381.98
418.35
461.69
504.43
547.23
590.05
631.80
674.69
717.47
757.20
796.85
837.65
877.63
921.08

Remarks
Float Shoe
Centralizer located 30 up
Float Collar
Centralizer on collar
Centralizer on collar
Centralizer on collar
Centralizer on collar
Centralizer on collar
Centralizer on collar
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Centralizer on collar

Total casing length: 921.08 feet
Casing setting depth: 901.00 feet (G.L.)

REYNOLDS ELECTRICAL \& ENGINEERING CO., INC.

## CASING RECORD

RRGE-1 - PRODUCTION CASING - 13 3/8-INCH O.D. DATE INSTALLED - FEBRUARY 22, 1975

| Joint | Weight | Measured Length (ft.) | $\begin{aligned} & \text { Cumulative } \\ & \text { Length (ft.) } \end{aligned}$ | Remarks |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 1.20 | 1.20 | Float Shoe |
|  |  | 2.00 | 3.20 | Float Collar |
| 1 | 61 1b/ft | 39.35 | 42.55 | Centralizer |
|  |  | 2.00 | 44.55 | Float Collar |
| 2 | $61 \mathrm{lb} / \mathrm{ft}$ | 39.83 | 84.38 | Float Coltar |
| 3 | $61 \mathrm{lb} / \mathrm{ft}$ | 39.32 | 123.70 | Centralizer |
| 4 | $61 \mathrm{lb} / \mathrm{ft}$ | 41.15 | 164.85 | Centratizer |
| 5 | $61 \mathrm{lb} / \mathrm{ft}$ | 41.10 | 205.95 |  |
| 6 | $61 \mathrm{lb} / \mathrm{ft}$ | 37.75 | 243.70 |  |
| 7 | $61 \mathrm{lb} / \mathrm{ft}$ | 40.41 | 284.11 | Centralizer |
| 8 | $61 \mathrm{lb} / \mathrm{ft}$ | 39.27 | 323.38 |  |
| 9 | $61 \mathrm{lb} / \mathrm{ft}$ | 37.26 | 360.64 | Centralizer |
| 10 | $61 \mathrm{lb} / \mathrm{ft}$ | 37.05 | 397.69 | Centralizer |
| 11 | $61 \mathrm{lb} / \mathrm{ft}$ | 37.82 | 435.51 | Cement basket |
| 12 | $61 \mathrm{lb} / \mathrm{ft}$ | 38.69 | 474.20 | Centralizer |
| 13 | $61 \mathrm{lb} / \mathrm{ft}$ | 37.94 | 512.14 |  |
| 14 | $61 \mathrm{lb} / \mathrm{ft}$ | 40.15 | 552.29 |  |
| 15 16 | $61 \mathrm{lb} / \mathrm{ft}$ | 39.71 | 592.00 | Centralizer |
| 16 | $61 \mathrm{lb} / \mathrm{ft}$ | 38.79 | 630.79 |  |
| 17 | $61 \mathrm{lb} / \mathrm{ft}$ | 29.34 | 670.13 |  |
| 18 | $61 \mathrm{lb} / \mathrm{ft}$ | 41.72 | 711.85 | Centralizer |
| 19 | 61 1b/ft | 37.20 | 749.05 | Centralizer |
| 20 | $61 \mathrm{lb} / \mathrm{ft}$ | 39.09 | 788.14 |  |
| 21 | $61 \mathrm{lb} / \mathrm{ft}$ | 38.34 | 826.48 | Centralizer |
| 22 | $61 \mathrm{lb} / \mathrm{ft}$ | 39.14 | 865.62 | Centralizer |
| 23 24 | $61 \mathrm{lb} / \mathrm{ft}$ $61 \mathrm{lb} / \mathrm{ft}$ | 37.72 41.02 | 903.34 | Cement basket |
| 25 | 61 1b/ft | 36.87 | 981.23 | Centralizer |
| 26 | 61 1b/ft | 40.43 | 1,021.66 |  |
| 27 | $61 \mathrm{lb} / \mathrm{ft}$ | 40.58 | 1,062.24 | Centraizer |
| 28 | $61 \mathrm{lb} / \mathrm{ft}$ | 38.98 | 1,101.22 | Centraizer |
| 29 | $61 \mathrm{1b} / \mathrm{ft}$ | 38.15 | 1,139.37 |  |
| 30 | $61 \mathrm{lb} / \mathrm{ft}$ | 41.11 | 1,180.48 |  |
| 31 | $61 \mathrm{lb} / \mathrm{ft}$ | 41.27 | 1,221.55 |  |
| 32 | $61 \mathrm{lb} / \mathrm{ft}$ | 39.13 | 1,260.58 |  |
| 33 34 | $61 \mathrm{lb} / \mathrm{ft}$ | 38.59 | 1,299.27 |  |
| 34 35 | $61 \mathrm{lb} / \mathrm{ft}$ | 39.78 | 1,339.05 | Cement basket |
| 36 | $6110 / f t$ | 41.43 40.60 | 1,380.48 |  |
| 37 | 61 1b/ft | 40.08 | 1,461.16 | Centralizer |
| 38 | $61 \mathrm{lb} / \mathrm{ft}$ | 39.65 | 1,500.81 |  |
| 49 | $611 \mathrm{l} / \mathrm{ft}$ | 38.64 | 1,539.45 | Centralizer |
| 40 | 61 1b/ft | 36.91 | 1,596.36 |  |
| 42 | $611 \mathrm{~b} / \mathrm{ft}$ $611 \mathrm{f} / \mathrm{ft}$ | 37.22 39.32 | $1,613.58$ $1,652.90$ |  |
| 43 | $61 \mathrm{lb} / \mathrm{ft}$ | 38.26 | $1,691.16$ | Centralizer |
| 44 | $61 \mathrm{lb} / \mathrm{ft}$ | 39.29 | $1,730.45$ |  |
| 45 | $61 \mathrm{lb} / \mathrm{ft}$ | 41.21 | 1,771.66 | Centralizer |
| 46 | $61 \mathrm{lb} / \mathrm{ft}$ | 41.18 | 1,812.84 | Cement basket |

REYNOLDS ELECTRICAL \& ENGINEERING CO., INC.
Page 2 of 2
CASING RECORD
RRGE-1 - PRODUCTION CASING - 13 3/8-INCH 0.D. DATE INSTALLED - FEBRUARY 22, 1975

heymolds electrical a emgineering co., imc.
paft river geotherul exploratory hole mo.
RRGE I
RIT
RECORO




| $\begin{aligned} & \text { JETS } \\ & 32 n d \text { In } \end{aligned}$ | Sertal | $\begin{aligned} & \text { Depth Out } \\ & (8 \times B) \end{aligned}$ $(8 \times B)$ | Feet | Hours | $\begin{aligned} & \text { ht. } \\ & \text { yu0. } \\ & \text { los. } \\ & \text { los. } \end{aligned}$ | APM | $\begin{aligned} & \text { Puspe } \\ & \text { Press } \end{aligned}$ | SP监 |  | $\frac{411 .}{8 / G}$ | $\frac{\text { Cond. }}{\text { 6/ Other }}$ | Forgation Reparks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opar | 1607 | $\text { OPEA } 15^{\circ}$ | $864$ | $\begin{aligned} & 35-3 / 4 \\ & 26060 \end{aligned}$ | 5100 | 5 | 200 | 62 | 6 | 1 |  | Bud Helght 9.8 , yis, -45 Ren $200^{4}$ cassing to 918 ! |
| $19.14-15$ | AP835 | 1,521 | 603 | 17-3/4 | 5/10 | 60 | 1,200 | 62 | 5 | 2 | 0 0 $3 / 16^{\circ}$ |  |
| 14-14-15 | Ap854 | 2.142 | 621 | $16-1 / 2$ | 5/10. | 80 | 1,250 | 52 | 5 | 3 | $01 / 8^{\circ}$ |  |
| $14+16-15$ | Pp756 | 2.535 | 493 | $18.1 / 8$ | $5 / 10$ | 9 | 1,300 | St | \$ | 2 | $0 \quad 173^{\circ}$ |  |
| 14-14-15 | AP224 | 3,091 | 456 | 20 | 6/10 | 80 | 1,350 | 62 | 5 | 3 | Q 3/8* |  |
| 14-14-15 | A8875 | 3.573 | 442 | $20-3 / 4$ | 10/16 | 80 | 1,400 | 62 | 4 | , | 0. $3 / 16^{\circ}$ |  |
| 18-14-15 | AP791 | 4,030 | 497 | 20 | 5/10 | 80 | 1,900 | 62 | 3 | 4 | 0 1/8* |  |
| 14-14-15 | AP703 | 4,495 | 665 | 1 | $5 / 10$ | 80 | 1,400 | 62 | 3 |  | $91 / 8^{\prime \prime}$ |  |
| Diceond | 4545257 | 4,555 | 60 | 4-1/4 | $10 / 15$ | 60 | 500 | 30 |  |  |  | Rec. 23 ' core |
| 14-14-15 | AP876 | 4.5850 | 155 | 14 | 20 | 85 | 1,400 | 52 | 0 | 8 | 0 | 1 cona missing; all bearlings missing. |

Open 12-1/4" hole to $15^{\prime \prime}$ from $918^{\prime}$ to $3,642^{\prime \prime}$
Ap894 Drilled out cement 2, a35' to 3,325' junk e 3,325

(Used) Drill $2^{\prime \prime}$ of collapsed casing ${ }^{3,325^{+}}$
Hilled collapsed $13-3 / 8^{\prime \prime}$ casing from $3,325^{\prime}$ to $3,331^{1}$
Hilled collapsed $13-3 / 8^{\prime \prime}$ casing from $3,325^{\prime}$ to
Hilled out $11-3 / 4^{4}$ hole from $3,325^{\prime}$ to $3,331^{\prime}$
Run in on junk and collapsed casfing o 3.325:
Hilled from $3,283^{\prime}$ to $3,285^{\prime} ; 3,325^{\prime}$ to $3,325-1 / 2^{\prime \prime}$
Milled, casing from 3,328' to 3,333'
Hilled casing from 3,320' to 3,338
Recovered-metal (2 big pieces looked like junk sub skirt)
Hilled casing from 3,332 'to $3,338^{\prime}$
Hilled casing
Milled cement out of casing from $3,370^{\prime}$ to $3,585^{\circ}$
Hilled cement and junk from 3,571 'to $3,584^{\prime}$
Cored from $3,5844^{\prime}$ to 3,585 ' no recovery
Made 7 runs and recovered about two-2 1 b . cans full
Try to get by junk a 3.585'-could not-broke § teath off -got jugk in sub
Rec 'd 2 cups of junk
Iry to get by junk e 3,585.50' -could nat
Rec'd full shoe of junk
Rec 'd cup full of junk
Milled on junk 3,586' to $3,590^{\prime}$--junk sub skirt torn up
Rec'd $1 / 2$ cup of junk
milled from 3,587' to $3,590^{\prime}$
Rec 'd full cup junk from tagnet; 2 cups fron junk sub
Rec'd yery little junk from Magnet or junk sub
milled thru junk from 3,587' to 3,590' and cenent 3.590 to 3,591
Hilled thru bottom Plug, diff. float collar/and cement from 3,591' to 3,631'
milled thru $3.587^{\circ}$, diff. float collars and cenent in casing to $3.631^{\prime}$
Rec'd piece of casing $2^{\prime} 7^{\prime \prime}$ long $7^{\prime \prime}$ wide; pleces of junk in sub e 3,629 '
Rec'd $12-1 / 4^{\prime \prime}$ and $8-3 / 4^{\prime \prime}$ nill nose cone and ten-1" pieces of junk 3.631.73
Rec'd 4 pleces of Junk in magnet, 1 cup cement and 2 pieces aluminum junk in basket
4,645 25-1/4 $\quad 3$
4,645 Recov. 1 bit cone
4,645 Recov. 2 pleces formation
4,651 Recov. 17 bearings; 7 bolts
AB899
$\begin{array}{lllll}4,686 & 36 & 4-1 / 2 & 20 & 65\end{array}$
4545520, 4686-4698
4581198.

05030
$\begin{array}{ccc}6-1 / 2 & 18 & 65 \\ 34-1 / 4 & 20 \quad 45\end{array}$
$1,400 \quad 64$
Pulled to core


