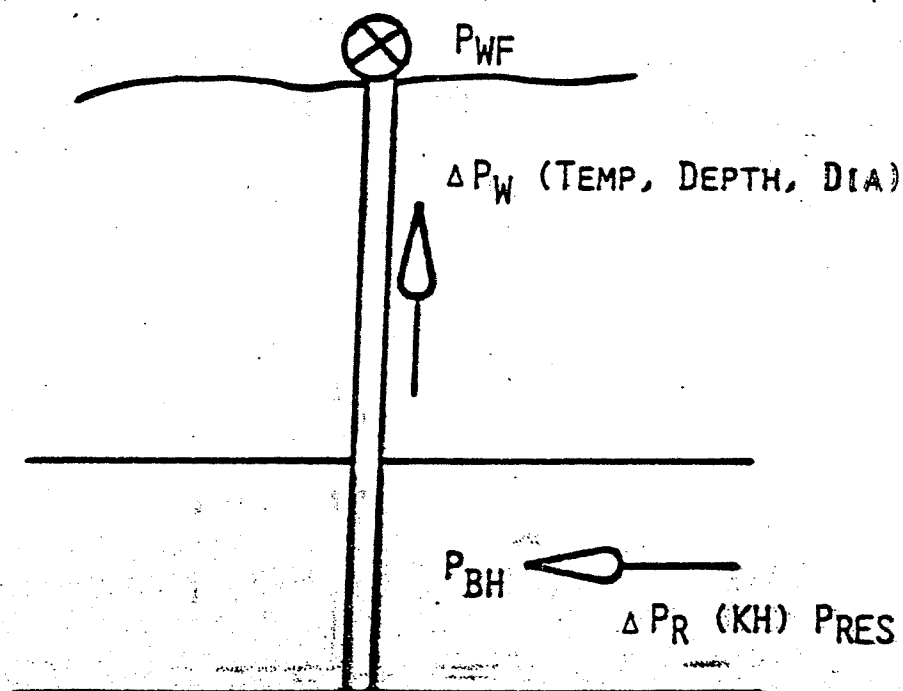


IMPORTANT PARAMETERS IN A FLOWING GEOTHERMAL WELL

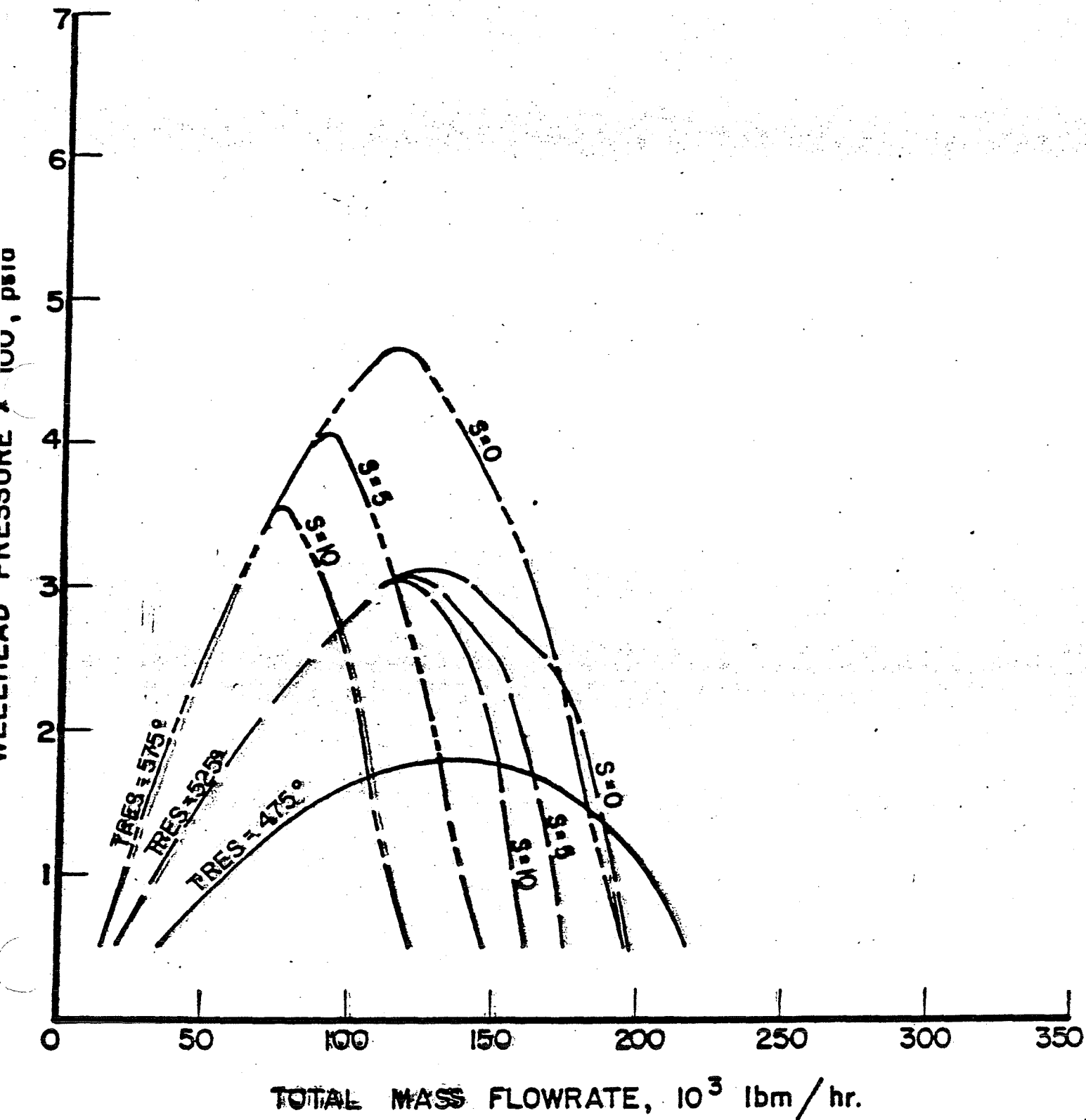


FOUR KEY PARAMETERS:

1. RESERVOIR PRESSURE
2. POROSITY-THICKNESS PRODUCT
3. PERMEABILITY-THICKNESS PRODUCT
4. TEMPERATURE

THEORETICAL DELIVERABILITY CURVES

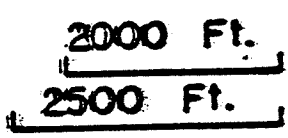
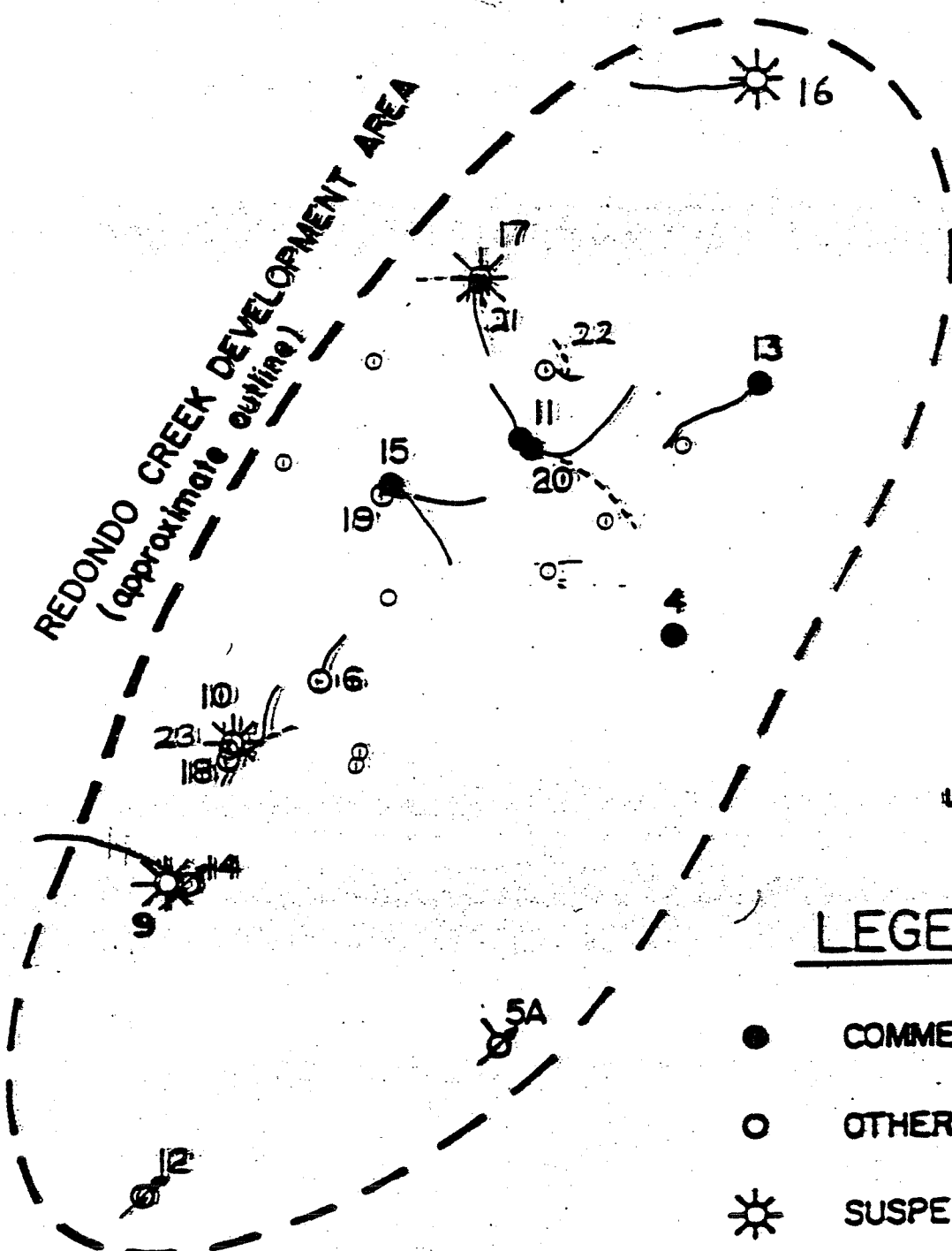
Mechanical Configuration and Reservoir
Pressure Corresponding to Boca 19
 $kh = 2500$ md-ft.



A COMPARISON OF KEY PARAMETERS
IN VARIOUS GEOTHERMAL SYSTEMS

FIELD	AVERAGE KH, MD-FT	AVERAGE ΦH, FT	INITIAL PRESSURE AT 3000' BELOW SURFACE	TEMPERATURE AT 3000' ° F.
TIWI	50,000	500	1320	500 +
BULALO	20,000	250	1270	500 +
BRAWLEY	20,000	250	1300	500 +
WEBER	130,000	130	1300	350 +
GEYERS	100,000	200	500	470 +
BACA	6,000	90	610	500 +

REDONDO CREEK DEVELOPMENT AREA
(approximate outline)



LEGEND

- COMMERICAL PRODUCERS
- OTHER
- ☀ SUSPENDED
- ⊕ WATER DISPOSAL
- Future Locations

SUMMARY OF RESERVOIR ENGINEERING AT BACA - 1978 - PRESENT

<u>Date</u>	<u>Well</u>	<u>Test</u>	<u>Results</u>
5/79 5/9/79 -5/11/79	B-18 <i>- data available (58-511) last survey 6/30/79 (514)</i>	Injectivity (32 hr)	Injectivity increased from 0.5 to 2.2 gpm during test Pressure falloff dominated by wellbore storage
10/79	Alamo Canyon #1	26 hr Flowtest and subsequent pressure buildup	kh = 1800 md-ft Skin = +12.7
2/80	Alamo Canyon #1	22 hr Injection test	Most of the liquid enters the formation below 5400'. Major fluid entry at 6500' ± 100' Pressure falloff dominated by wellbore and thermal effects (kh) and skin not determined
2/80	Alamo Canyon #1	7 day Flowtest and subsequent pressure buildup	kh = 1350 md-ft Skin = +11.0 Pressure buildup behavior indicates the well is 500 to 1000' away from two perpendicular highly productive faults.

<u>Date</u>	<u>Well</u>	<u>Test</u>	<u>Results</u>
11/79	B-19	12 day Flowtest - downhole wireline surveys Pressure buildup	Production cycling due to liquid loading and unloading in wellbore kh = 2360 md-ft Skin = +12.6
12/79	B-19	Low rate injectivity (22 hrs) High rate injectivity (11 hrs) Schlumberger spinner and temperature suveys during injection Pressure falloff	Pressure falloff dominated by thermal effects (estimated kh = 2000 md-ft, Skin = 3.5) 56% of flow exiting between 5170 and 5180' 81% of flow exiting below 5000' Injection test terminated prematurely due to surface equipment failure. (estimated kh = 2510 md-ft, Skin = 2.0)
3/80 5/80	B-19	44 day flowtest and pressure buildup	kh = 2990 md-ft Skin = +15.8

*last sum. (11/79)
(Buildup
S 4)
flow data?*

S12 (Pressure fall off)

missing

B17 (fall off)

*buildup
data S34
flow data?*

<u>Date</u>	<u>Well</u>	<u>Test</u>	<u>Results</u>
5/80	B-12	34 hr Injectivity test	Injection terminated prematurely due to lack of water. Wellbore storage dominated pressure fall-off
6/80	B-14	68 hr Injectivity test	kh = 4760 md-ft Skin = 3.8 Calculated injectivity only 50% of that in DOE proposal
9/80- 1/81	B-20	102 day flowtest	Deliverability at 125 psig separator pressure = 27,000 lb/hr steam, with 54% flash Steam rate declined at an annual rate of 50-70%
1/81	B-20	Pressure buildup test	Two-phase reservoir effects mask buildup behavior.

<u>Date</u>	<u>Well</u>	<u>Test</u>	<u>Results</u>
2/81- 3/81	B-21	46 day Flowtest	Commercial deliverability questionable
		Pressure buildup test	In progress. First 2 days of behavior indicate linear flow near wellbore
9/80- 3/81	B-4	Sperry Sun pressure interference monitoring	No clear response
1/81- 3/81	B-6	Sperry Sun pressure interference monitoring	No clear response
9/80- 3/81	B-13	Sperry Sun pressure interference monitoring	No clear response

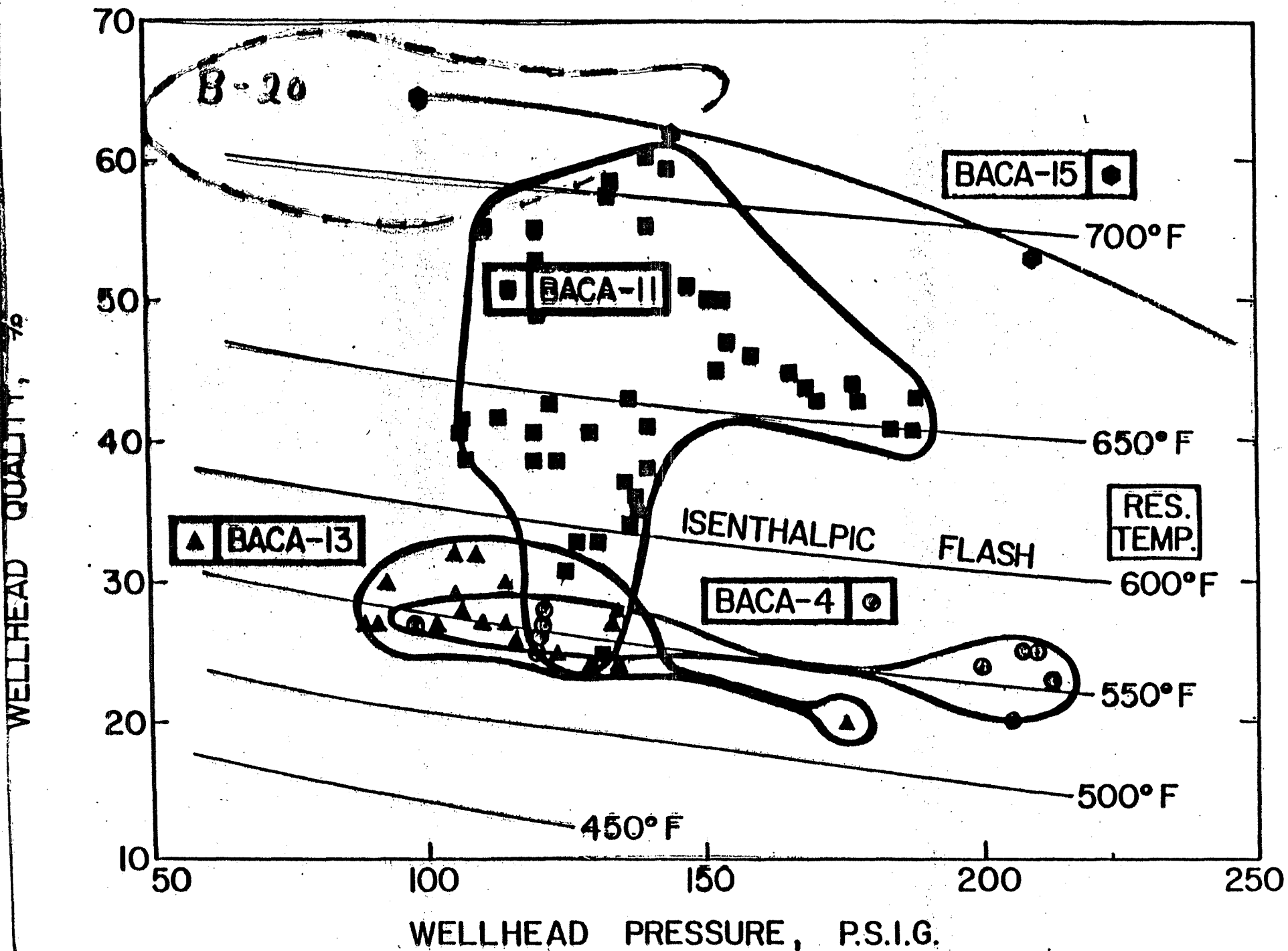
PRODUCTIVITY DATA FOR BACA WELLS

DELIVERABILITY

<u>WELL NO.</u>	<u>KH, MD=FT</u>	<u>SKIN</u>	<u>TEMP., °F</u>	<u>RATE, MLB/HR</u>		<u>P_{WH} PSIG</u>	<u>FLASH</u>
				<u>TOTAL</u>	<u>STEAM</u>		
11	3450	- 4	550	265	117	140	44%
15	≥ 5500	- 3	510	175	105	140	60%
13	2020	+ 4	500	200	54	140	27%
4 (PREVIOUSLY)	4200	+15	550	172	45	140	27%
(CURRENT)			550	54	25	140	27%
20			540	51	27	140	50%
6 (BRIDGED)	6400	+10	510	150	33	95	22%
10	5100	+43	500	(126)	43	16	(34%)
19	2360	+ 9	490	(120)	(30)	22	(25%)
(INJECTIVITY)	2510	= 2					
A.C.#1	1850	+13	550	(130)	(65)	40	(50%)

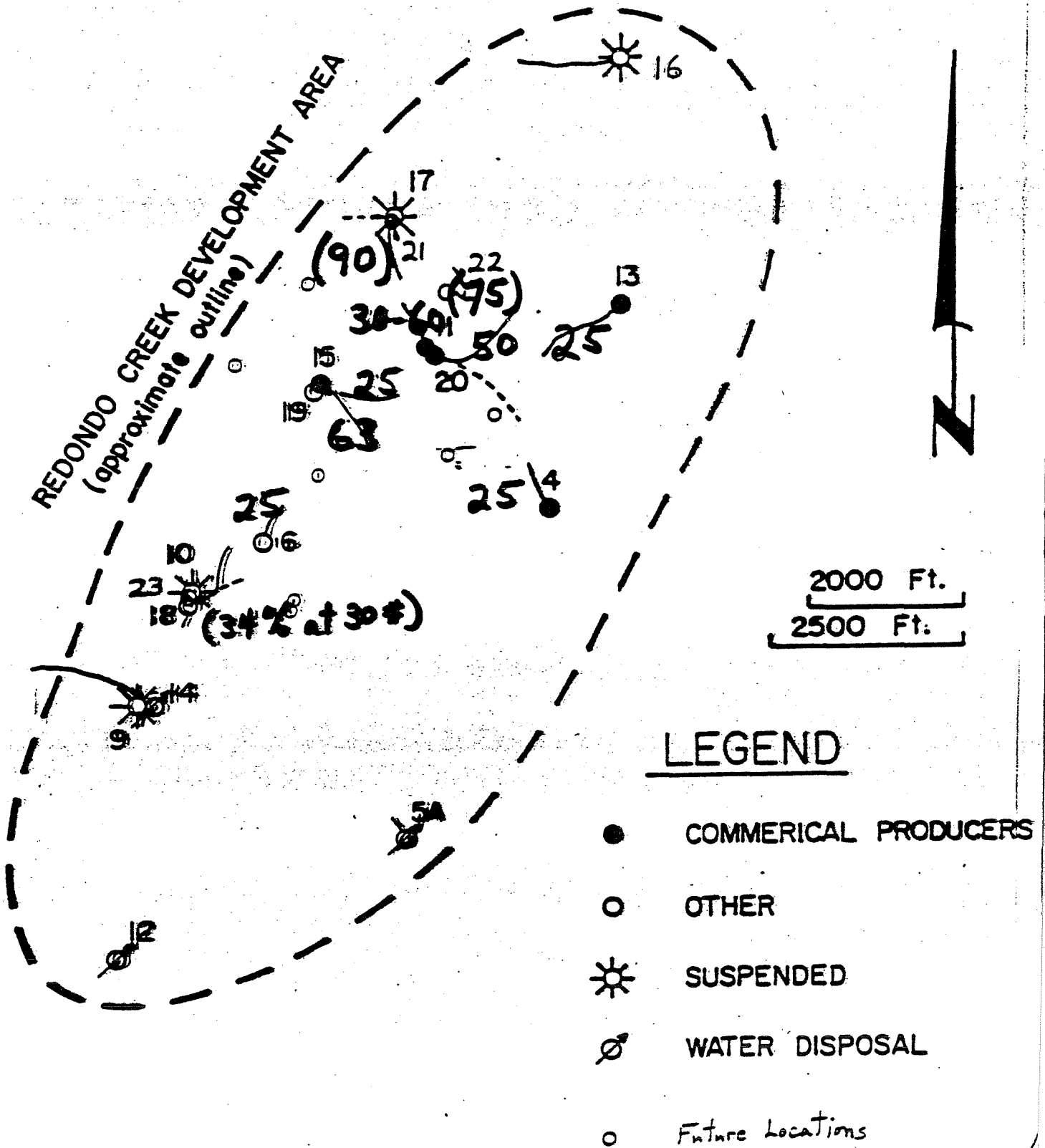
(): ESTIMATED RATES AND FLASH

PRODUCING WELLHEAD QUALITY AT BACA



SURFACE FLASH (%) AT 150 PSI WHP

() : estimated

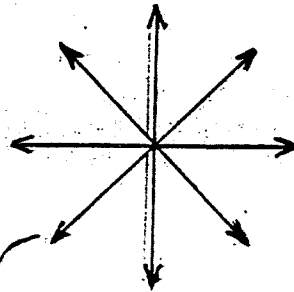


1975-76 INTERFERENCE DATA ANALYSIS

USING NEW FLOW GEOMETRIES

RADIAL-ISOTROPIC

PERMEABILITY SAME
IN EVERY DIRECTION

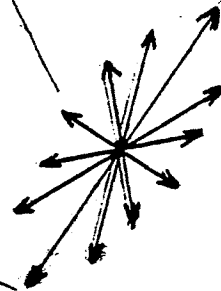


magnitude and direction of k

RADIAL-ANISOTROPIC

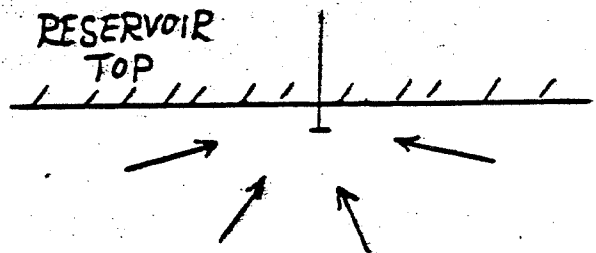
PERMEABILITY VARIES
WITH DIRECTION

MAJOR PERMEABILITY



HEMISPHERICAL

RESERVOIR HAS
NO BOTTOM



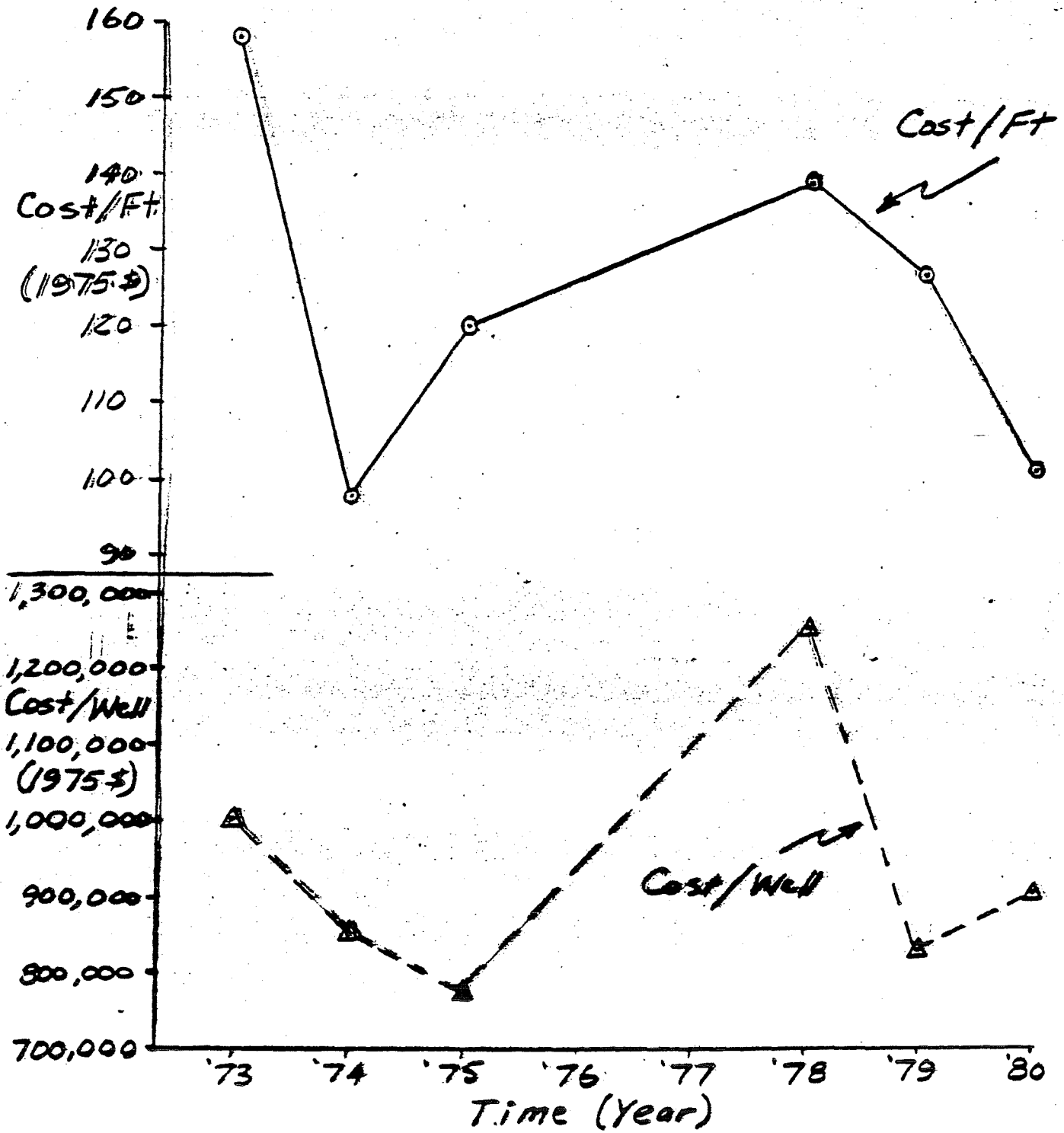
Fluid Flow Lines

BACA 10 INTERFERENCE DATA ANALYSIS
USING NEW FLOW GEOMETRIES

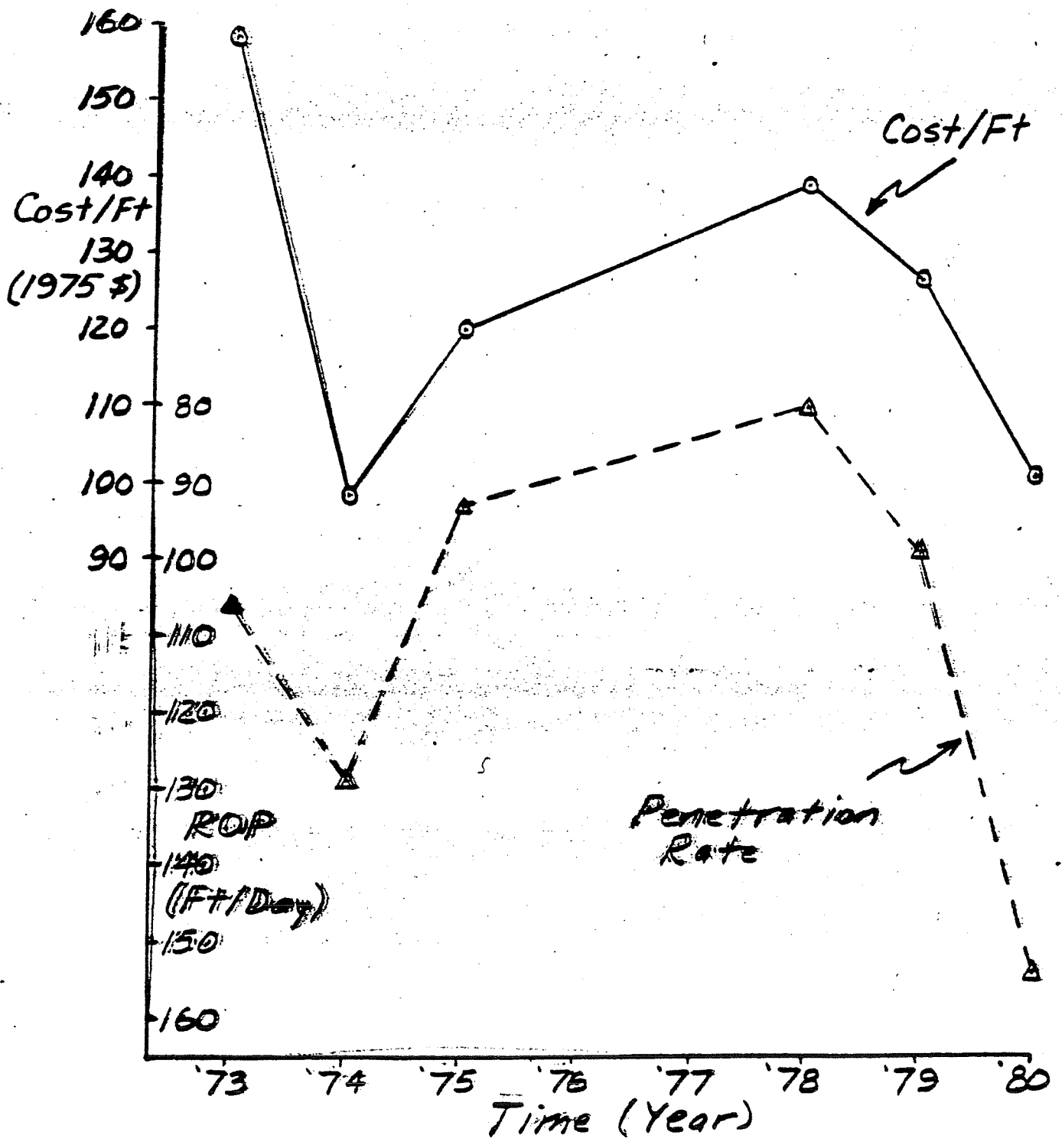
<u>FLOW GEOMETRY</u>	<u>OPTIMUM MATCH</u>	<u>E₀ PSI/PT</u>
<u>PURE RADIAL</u>	(KH) = 6.4 D-FT ϕ _H = 107 FT	6.1
<u>ANISOTROPIC RADIAL</u>		
	$\left. \begin{array}{l} (KH)_{MAX} = 105 \text{ D-FT}, (KH)_{MIN} = 1 \text{ D-FT} \\ (\phi_H) = 15 \text{ FT}, (KH)_{MAX} \text{ ORIENTED N80W}^{(*)} \end{array} \right\}$	4.5
	ϕ _H = 100 SPECIFIED:	
	$\left. \begin{array}{l} (KH)_{MAX} = 20 \text{ D-FT}, (KH)_{MIN} = 5 \text{ D-FT} \\ (KH)_{MAX} \text{ ORIENTED N80W} \end{array} \right\}$	5.3
<u>HEMISPHERICAL</u>	K = 4.9 MD ϕ = 0.05	6.9

(*) N80W IS PERPENDICULAR TO REDONDO CREEK

COST PER FOOT + COST PER WELL
vs TIME BACA 1973-1980



COST PER FOOT + PENETRATION RATE
 VS TIME BACA 1973-1980



BACA 23 STIMULATION

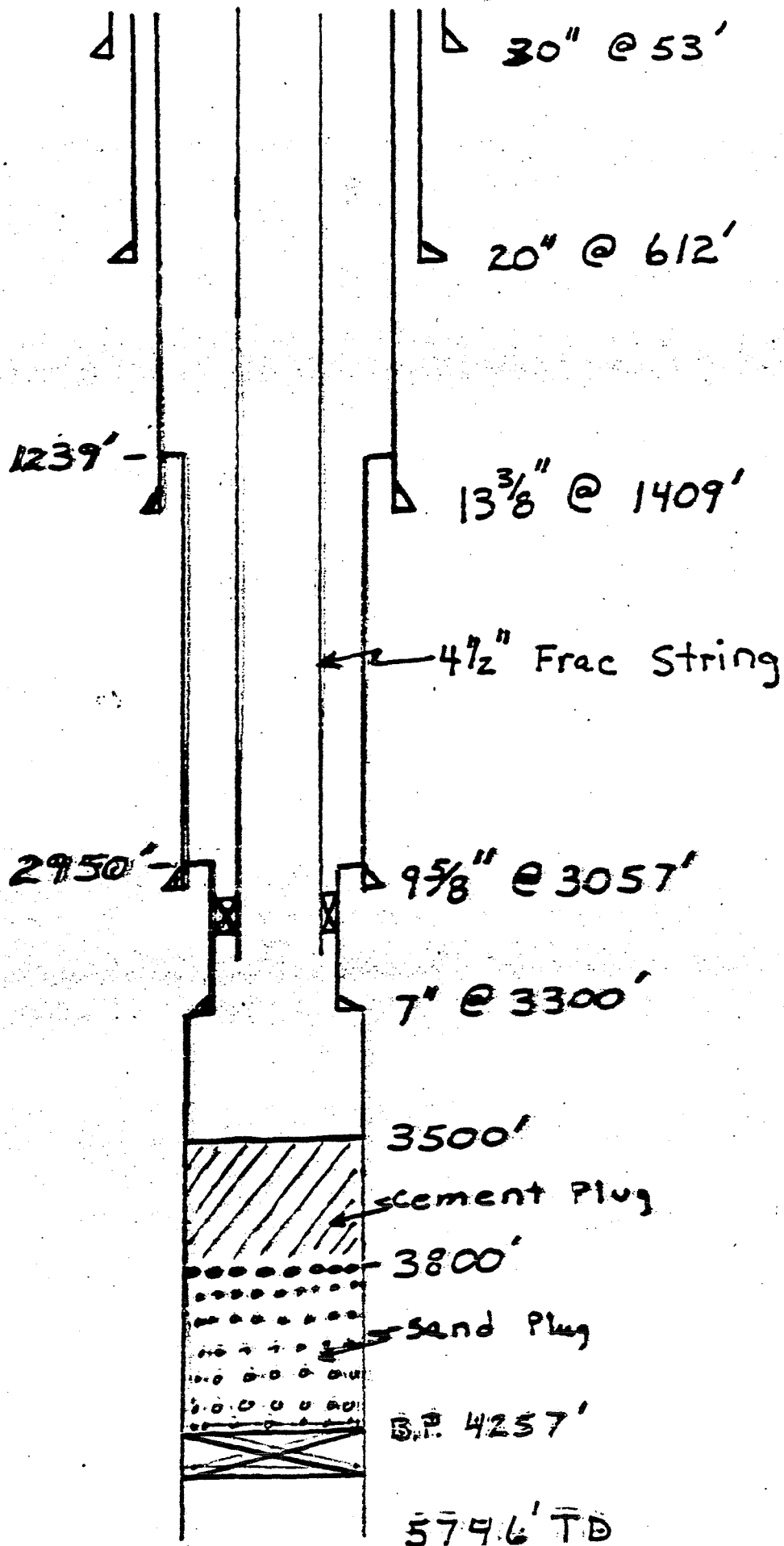


TABLE 1

PUMPING SCHEDULE FOR FRACTURE TREATMENT

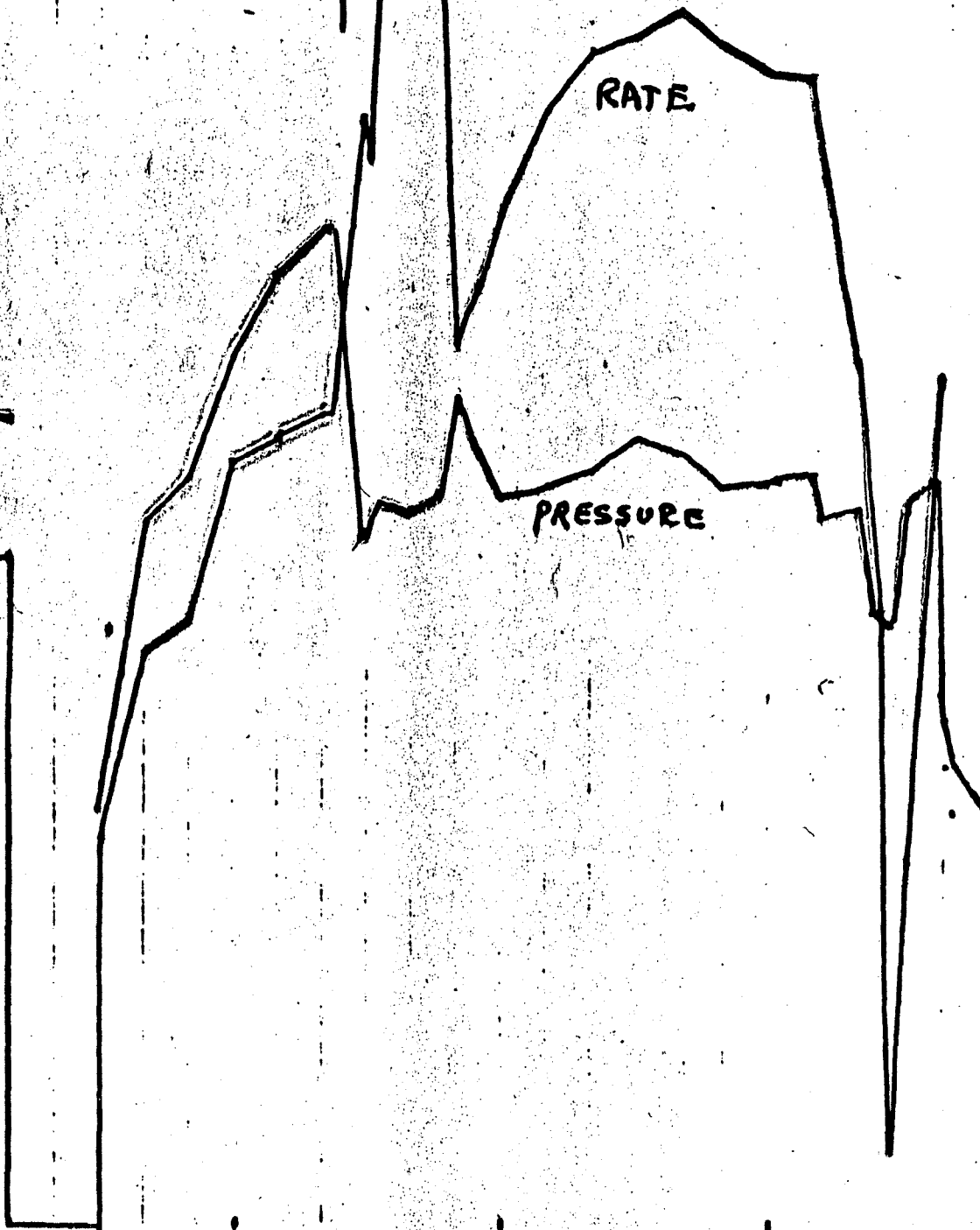
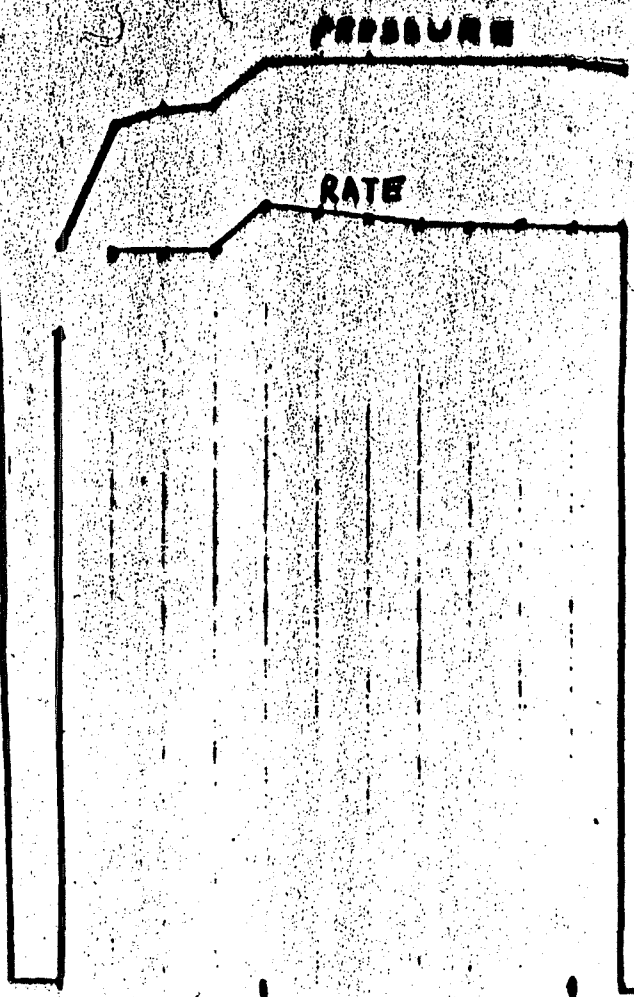
BACA 18

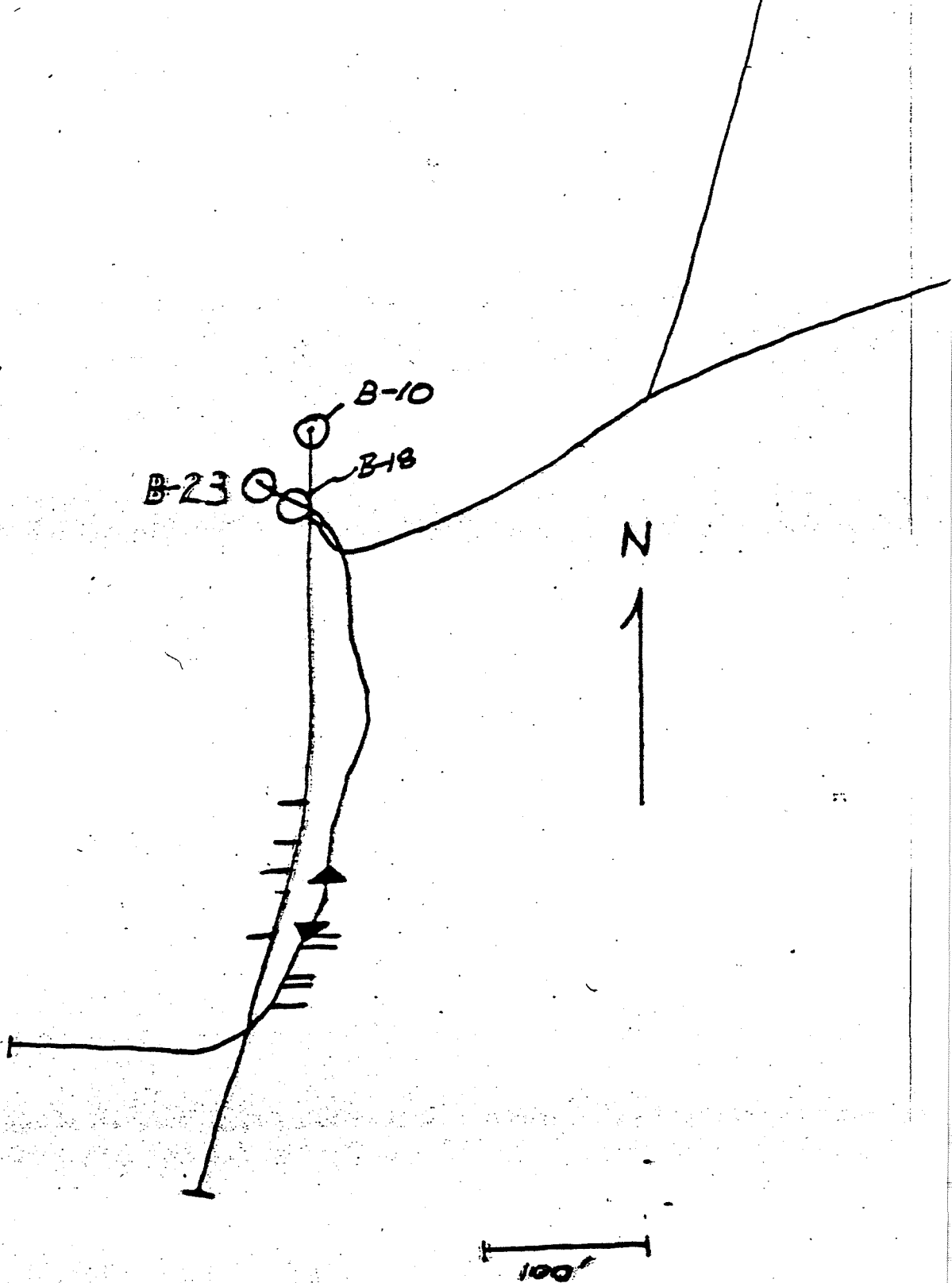
<u>EVENT NO.</u>	<u>FLUID VOLUME (bbls)</u>		<u>PROPPANT</u>		
	<u>INCR.</u>	<u>CUM.</u>	<u>lbs/gal</u>	<u>SIZE</u>	<u>FLUID</u>
1	4,000	4,000	-	-	Prepad - water with FLA at maximum rate up to 80 BPM.
2	500	4,500	-	-	Pad - gelled water with FLA at 80 BPM
3	500	5,000	2	100	" " "
4	400	5,400	-	-	" " "
5	900	6,300	1	20/40	Proppant transport - same as Pad except <u>no FLA.</u> 80 BPM
6	1,000	7,300	2	20/40	" " "
7	600	7,900	3	20/40	" " "

STAGE 1

12
-75
-70
-65
-60
-55
-50
-45
-40
-35
-30
-25
-20
-15
-10
0

2 | 3 | 4 | 5 | 6 | 7 | 8





PLAN VIEW

PRODUCTION RESULTS

1315 PUMPED AIR AND WATER THROUGH BIT (6-1/8") IN THE 7" LINER
1325 GOT RETURNS
1544 SHUT OFF AIR AND MUD PUMP
1952 KILLED WELL

AVERAGE RATE TO PIT 135,170 LBS WATER/HR - UNABLE TO
RECORD STEAM OR WATER RATE TO THE SUMP

RAN LINER

RAN TEST WELL - FLOWING INSIDE DRILL PIPE, LIFTING WITH
NITROGEN THROUGH COILED TUBING AT 2500 FT, PUMPING 300
SCF

FLOWED (N₂ ASSISTED) FOR 5 HRS AT 21,580 LB/HR
SURFACE TEMPERATURE 150°F, MAXIMUM BHT - 341° F
PRESSURE DRAWDOWN 42 PSI

PTI = 5000 LBS/HR/PSI

PRESSURED WELL - DID NOT FLOW

PRESSURED WELL UNTIL 8 AM SATURDAY - WELL FLOWED

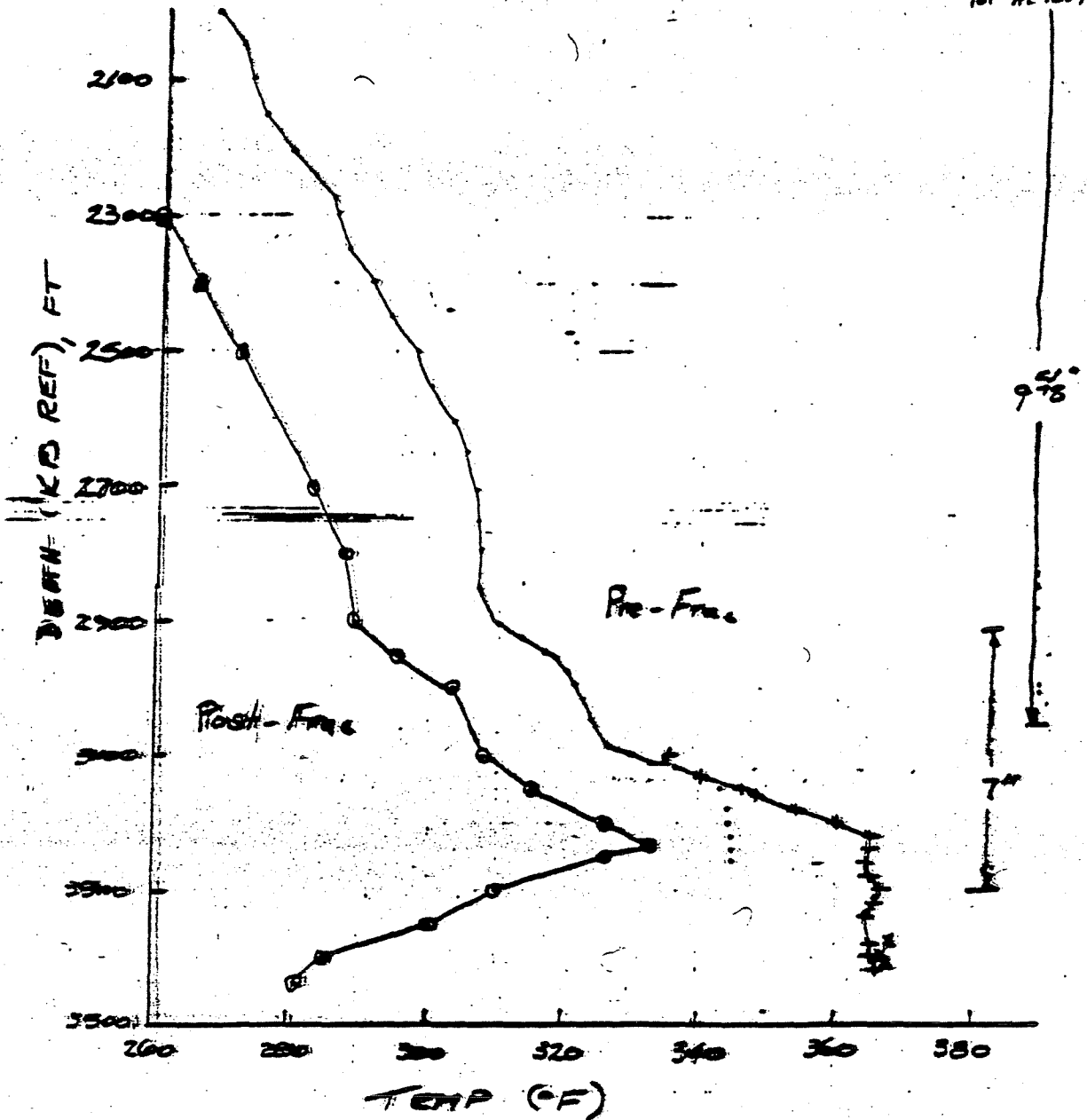
MONDAY AT 0500 HRS FLOWING 48,400 LB/HR STEAM, 120,900 LBS/HR

MASS AT AN ASSURED 40% FLASH

Denver Research
Institute

3/22/81

TOP AT 1239'



RB

BACA 0A

BACA 09
BACA 14

BACA 10

BACA 08

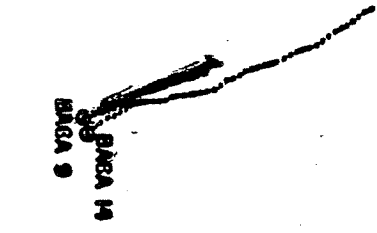
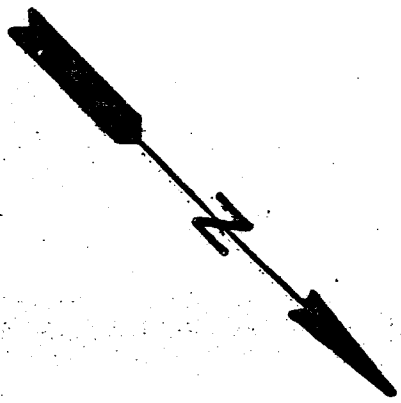
BACA 13

BACA 11

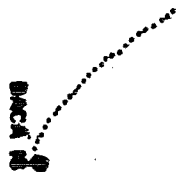
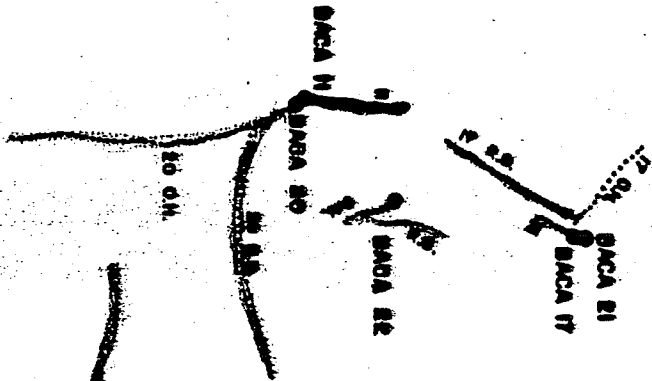
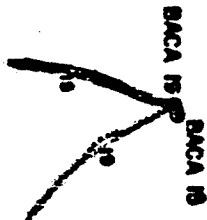
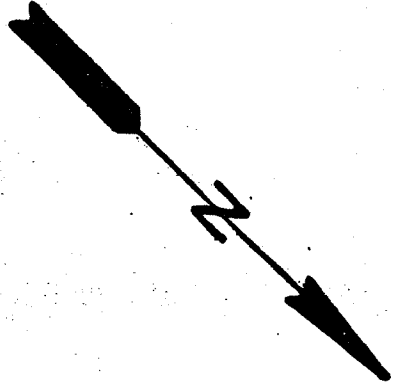
BACA 07

BACA 12

BACA 15



BACA 0A



BACA-12

CALDERA

20"

9-5/8"

13-3/8"

BANDELIER TUFF

9-5/8"

ANDESITE

ALBUQUERQUE

ABO

9212' TD
7"

LIMESTONE

GRANITE

10,300' T.D.
5 1/2"

BACA-24

CALDERA

20"

9-5/8"

13-3/8"

BANDELIER TUFF

ANDESITE

SANTA FE

ABO

LIMESTONE

GRANITE

9-5/8"
8500' TD
7"

BACA-16

CALDERA

20"

RHYOLITE

13-3/8"

9-5/8"

BANDELIER TUFF

9-5/8"

ANDESITE

SANTA FE

ABO

LIMESTONE

GRANITE

7002' TD

8-3/4"
HOLE

7"

10,000' TD
5 1/2"

1981 PROPOSED RIG SCHEDULE

<u>WELL</u>	<u>PROGRAM</u>	<u>TIMING</u>	<u>COST</u>
BACA - 24	NEW WELL (L.S. TEST)	65 DAYS	\$1,750,000
BACA - 19	FRAC BOTTOM 300'	23 DAYS	\$1,100,000
BACA - 12	DEEPEN (L.S. TEST)	60 DAYS	\$1,250,000
BACA - 22	FRAC 200' INTERVAL	23 DAYS	\$1,100,000
BACA - 16	DEEPEN (L.S. TEST)	42 DAYS	\$1,200,000

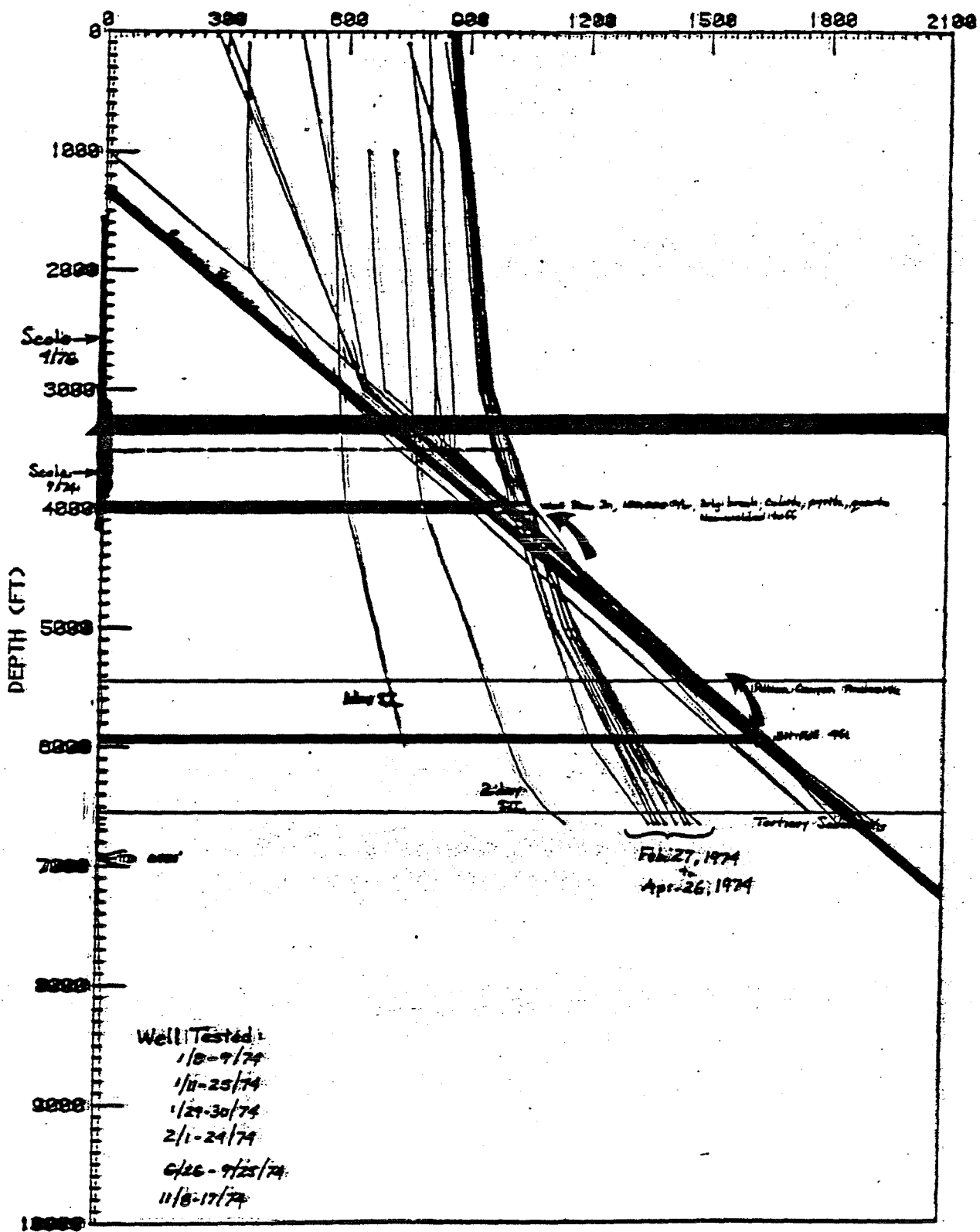
(IF SUCCESS IS INDICATED BY ABOVE RIG WORK)

BACA - 21	DEEPEN THROUGH ANDESITE	30 DAYS	\$ 500,000
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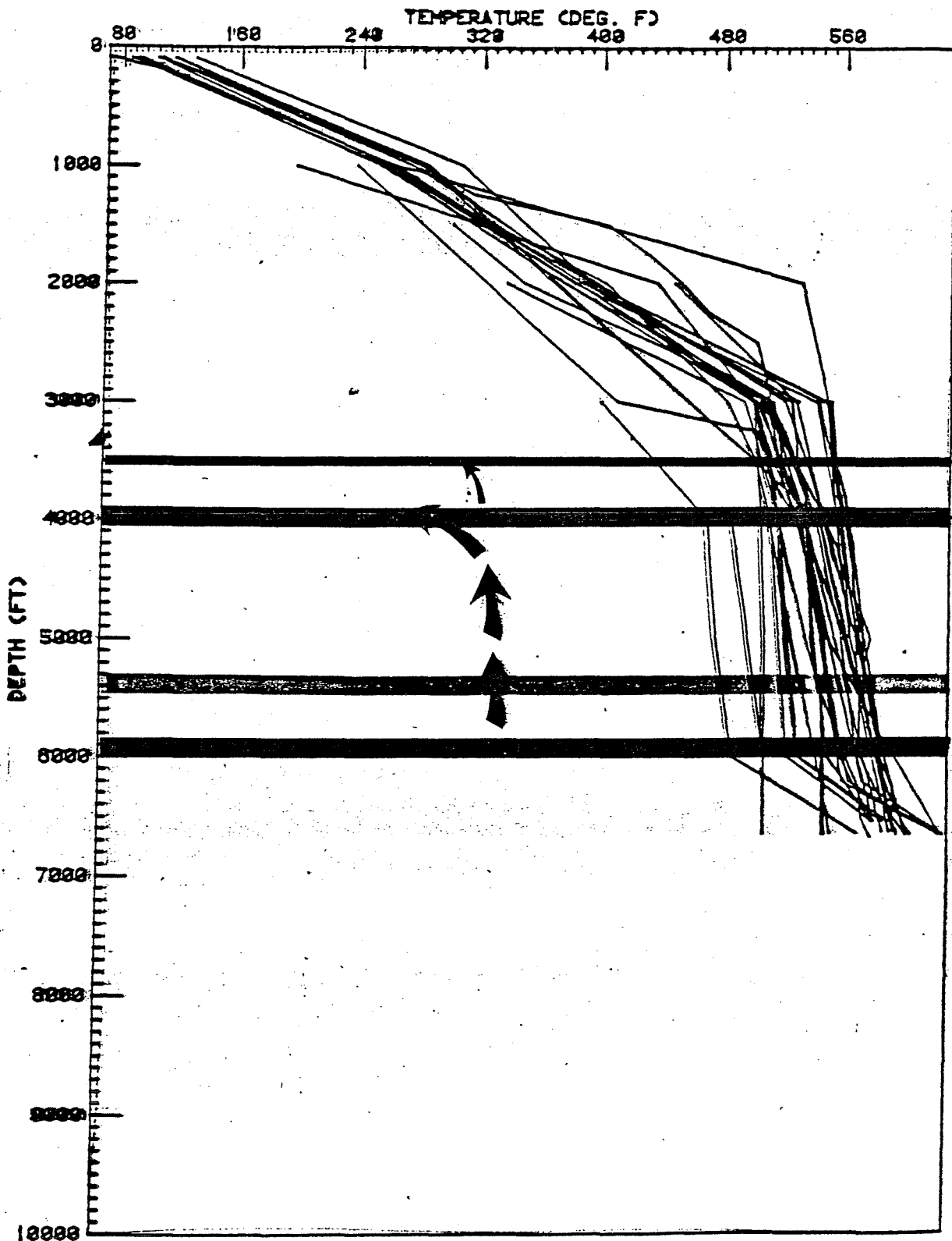
1982

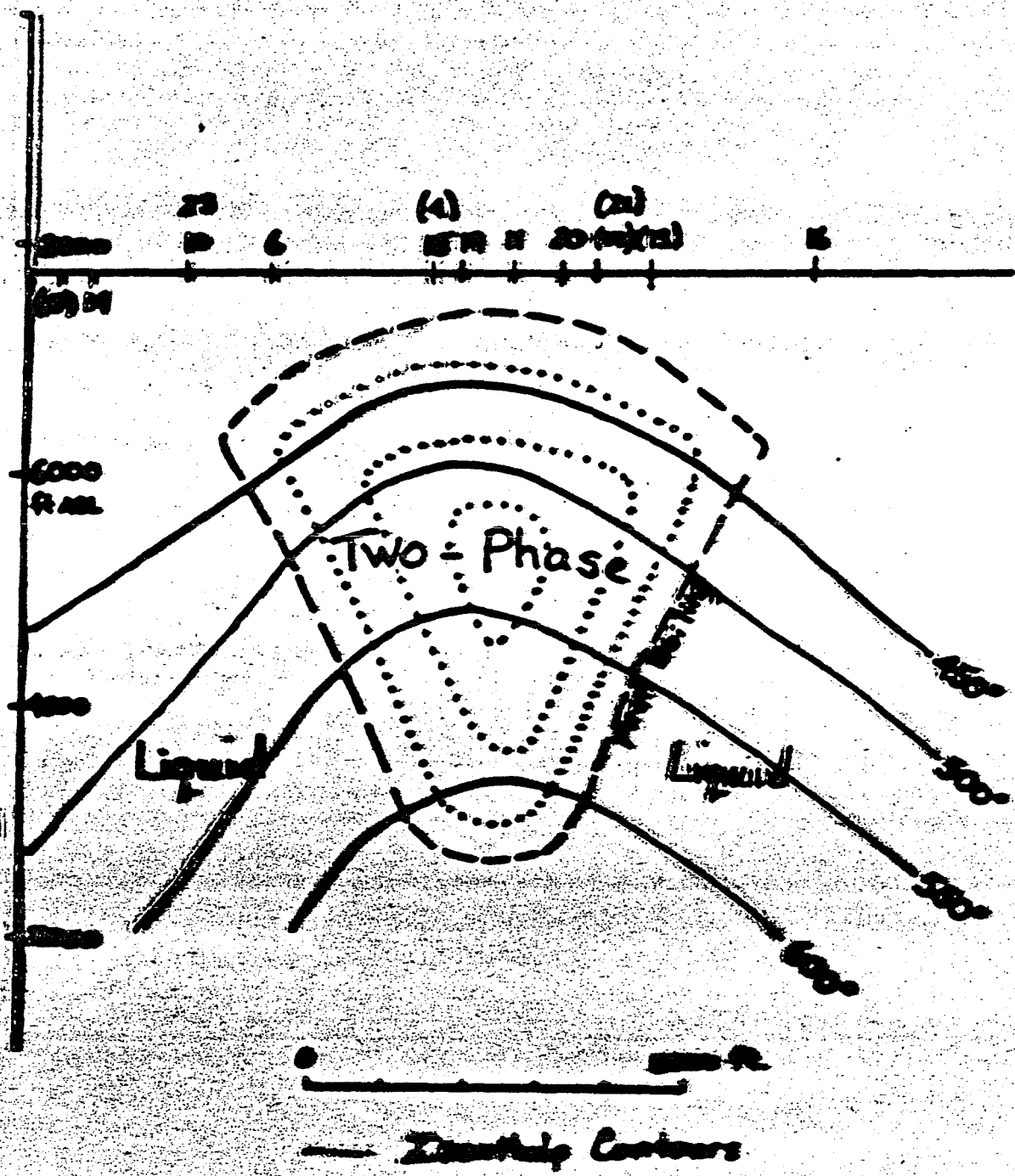
BACA - 18	FRAC OR REDRILL	23-30 DAYS	\$667,000 - 1,055,000
BACA - 25	NEW WELL (L.S. TEST)	65 DAYS	\$1,750,000

BAGA 11 PRESSURE PROFILES

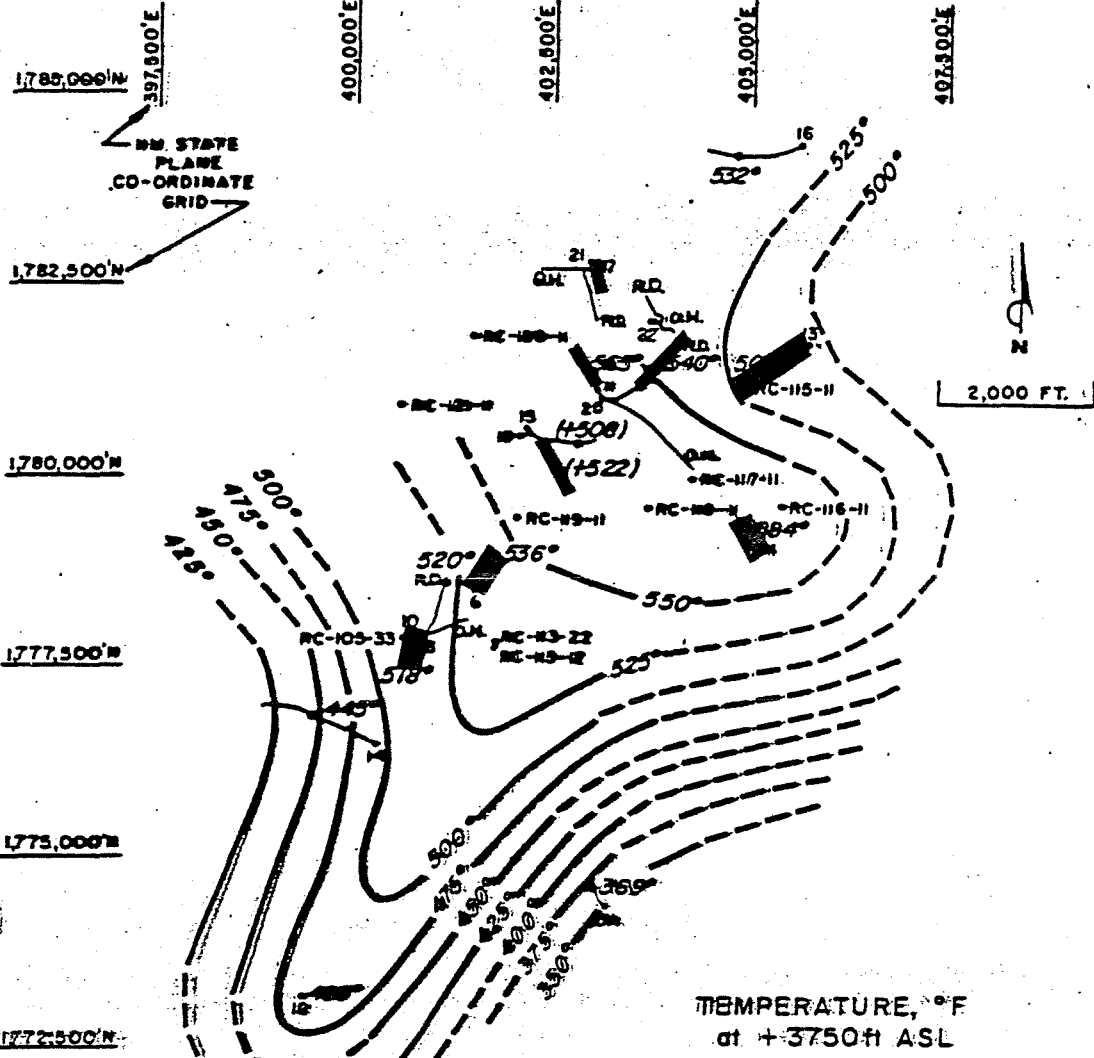


BACA 11 TEMPERATURE PROFILES





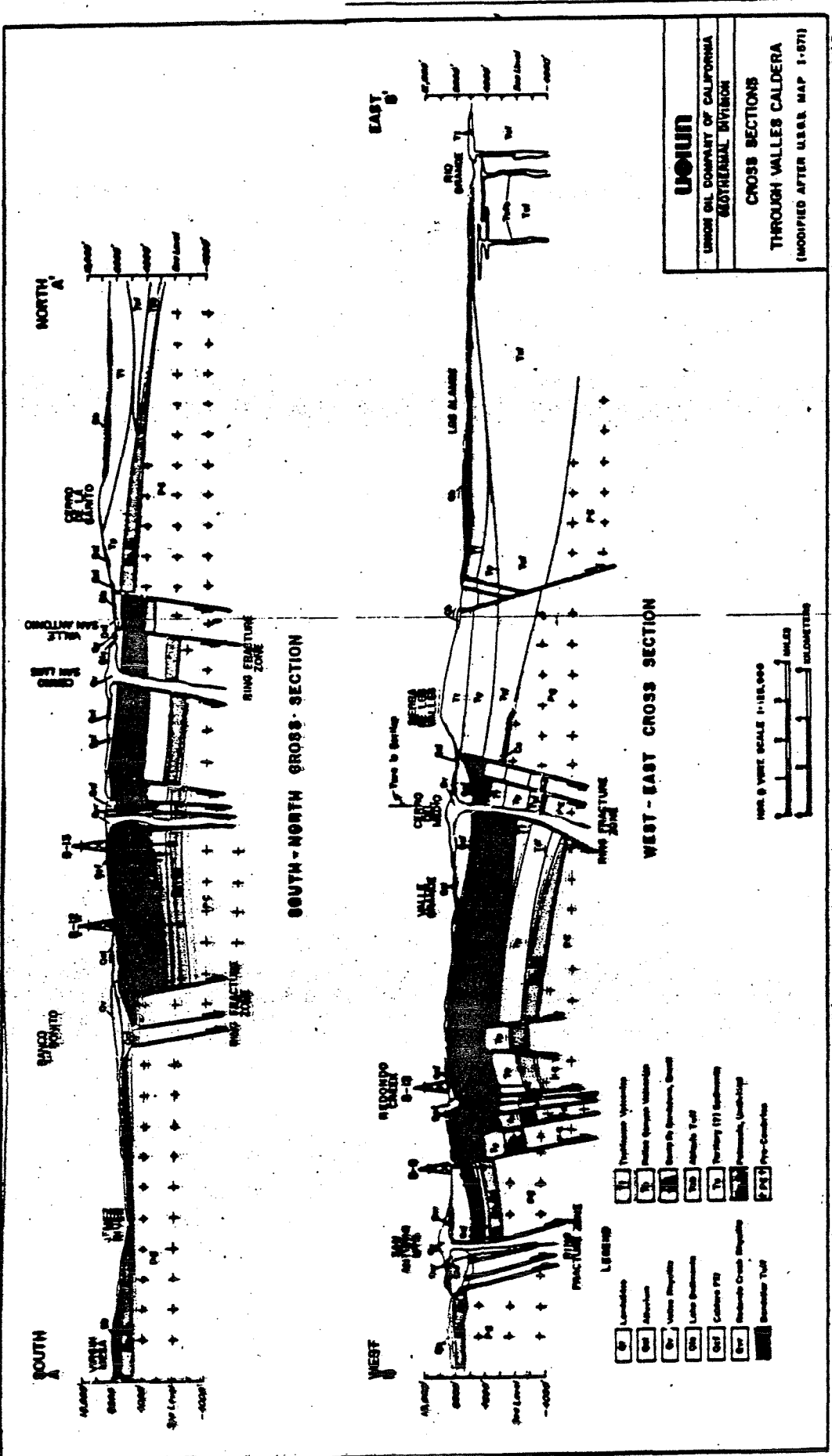
REVISIONS				
REV	DESCRIPTION	DATE	BY	APP'D
A	ISSUED	5-16-80		



TEMPERATURE, °F
at +3750ft ASL

- () NOT STABLE BECAUSE OF FLUID
- 1) Injection or
- 2) Flushing in Formation

UNION 76		Union Geothermal Company of New Mexico		
REDONDO CREEK DEVELOPMENT AREA				
DESIGN		SIZE ARE NO.	DWG. NO.	REV
DRAWN		A	RC-L-20K-101a	A
CHECK		SCALE: NOTED	SHEET	1 OF 1
DATE				



SOUTH

NORTH

SOUTH-NORTH CROSS SECTION

WEST-EAST CROSS SECTION

WEST

EAST

UNION
 UNION OIL COMPANY OF CALIFORNIA
 GEOTHERMAL DIVISION
CROSS SECTIONS
 THROUGH VALLES CALDERA
 (MODIFIED AFTER U.S.G.S. MAP 1-571)

- LEGEND**
- Limestone
 - Sandstone
 - Volcanic Deposits
 - Lava
 - Caldera Fill
 - Residual Crustal Deposits
 - Quaternary Tuff
 - Tertiary Volcanics
 - Paleozoic Metamorphic
 - Deeply Dissected, Erosion
 - Alluvial Tuff
 - Primary HTI Sediments
 - Paleozoic Metamorphic
 - Pre-Cambrian

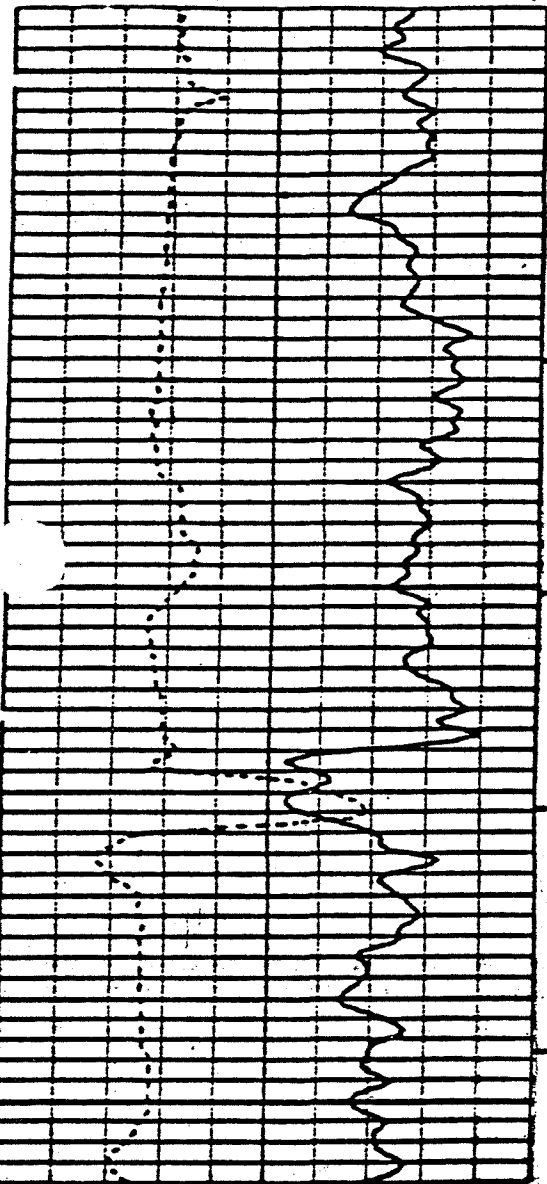


1.1.2

Caliper

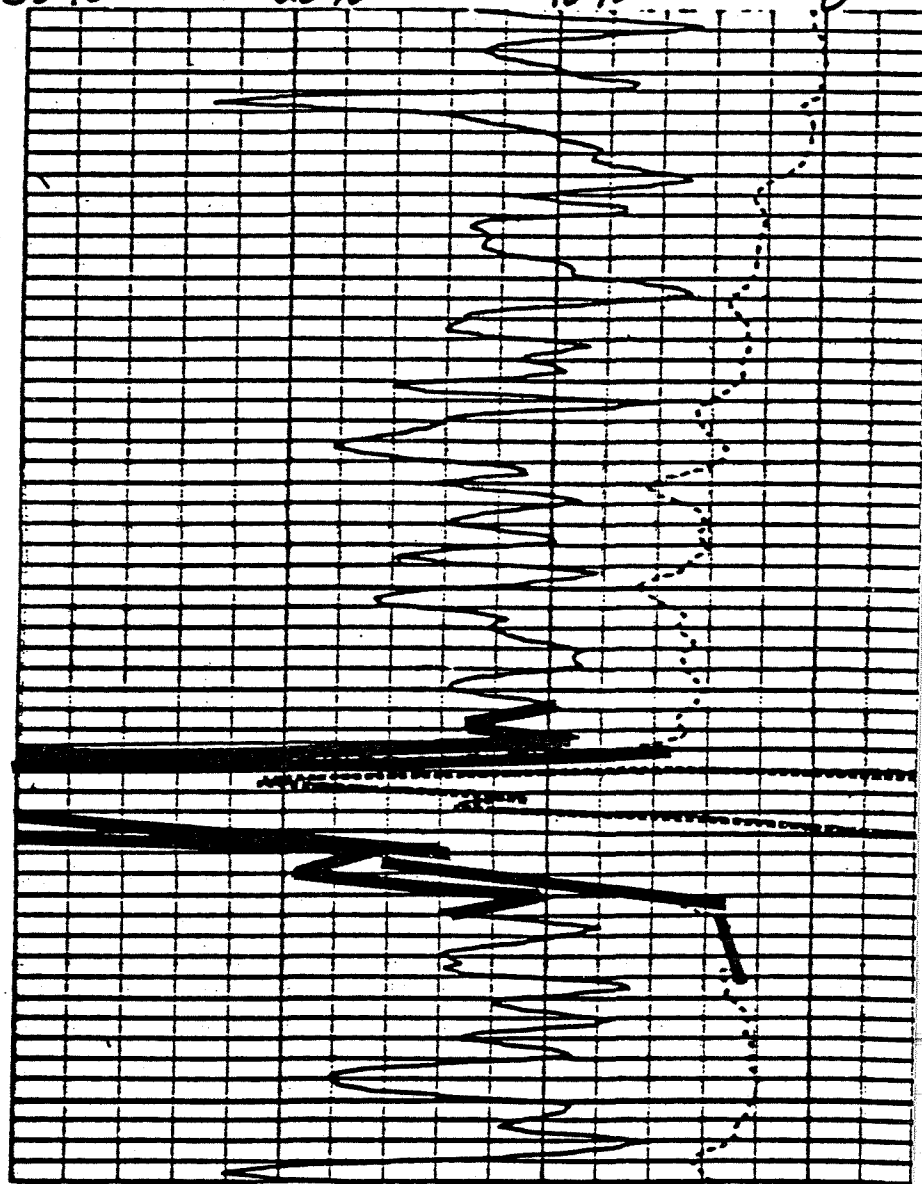
G. R.

30% 20% Porosity 10% 0



2700

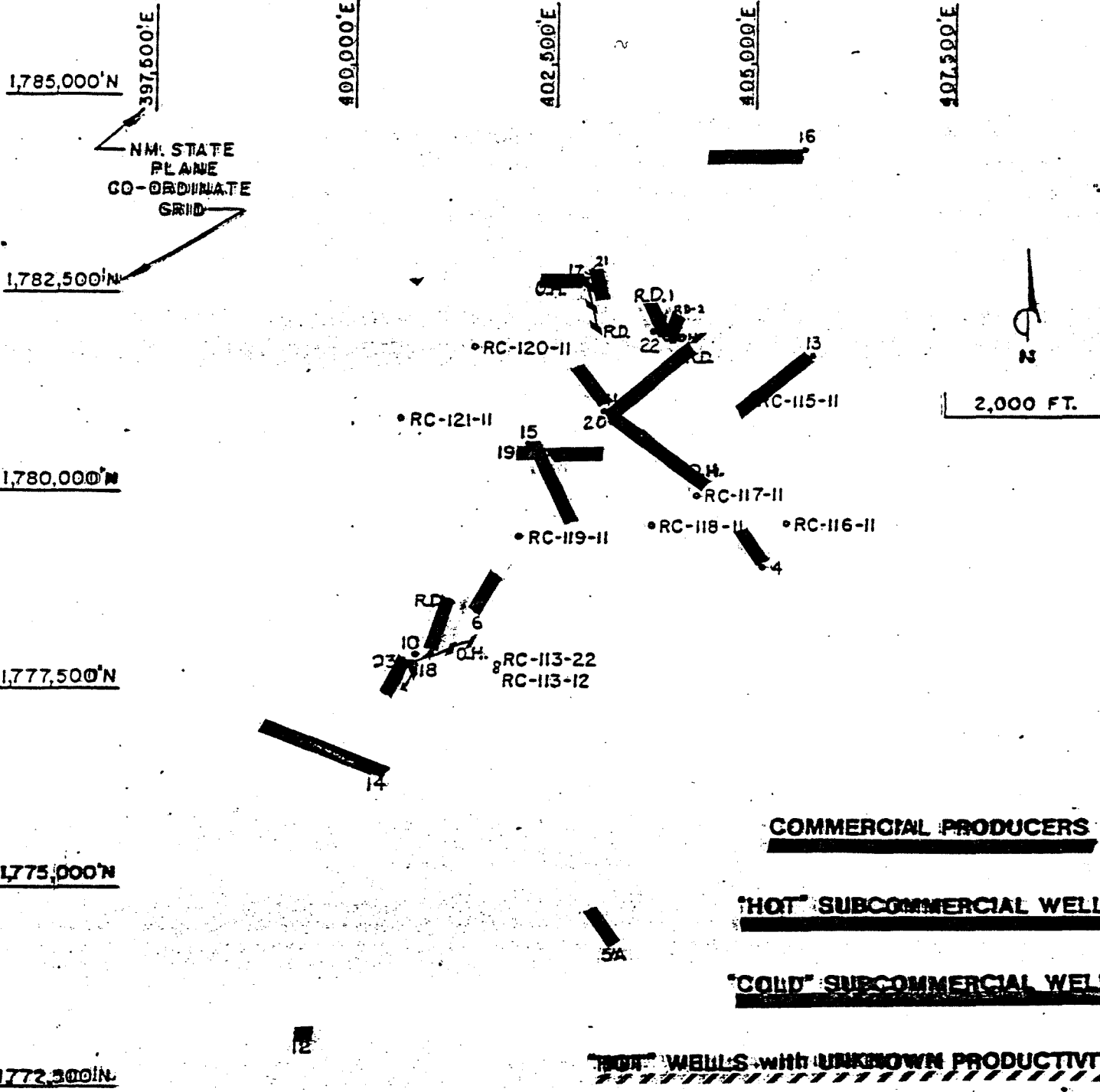
2800



Density Porosity —————

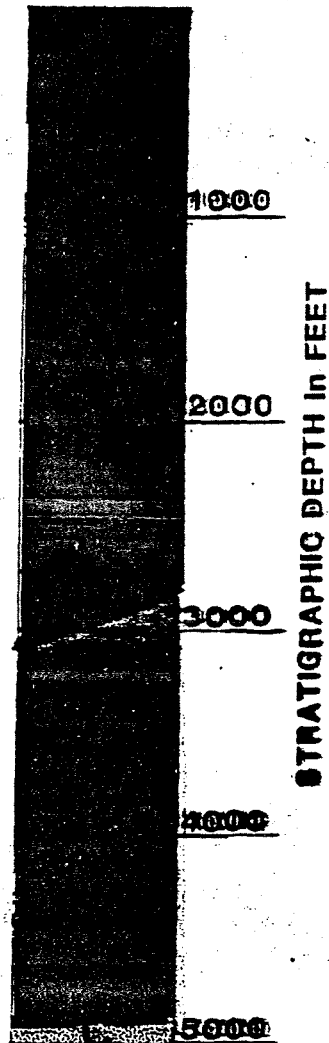
Neutron Porosity —————

A	ISSUED	5-16-80	L.
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		Union Geothermal Company of New Mexico	
		REDONDO CREEK DEVELOPMENT AREA	
DESIGN	RD		
DRAWN	E. G. Smith		

PRELIMINARY STRATIGRAPHY BANDELIER TUFF



A1 ZONE:

MODERATELY TO WEAKLY WELDED.
COMMON KAOLINITE ALTERATION.

A2 ZONE:

STRONGLY WELDED.
DENSE, HARD, VITRIFIC

A3 ZONE

MODERATELY TO STRONGLY WELDED.
VARIABLELY VITRIFIC AND DEVITRIFIED.
MORE ABUNDANT PHENOCRYSTS THAN IN A2

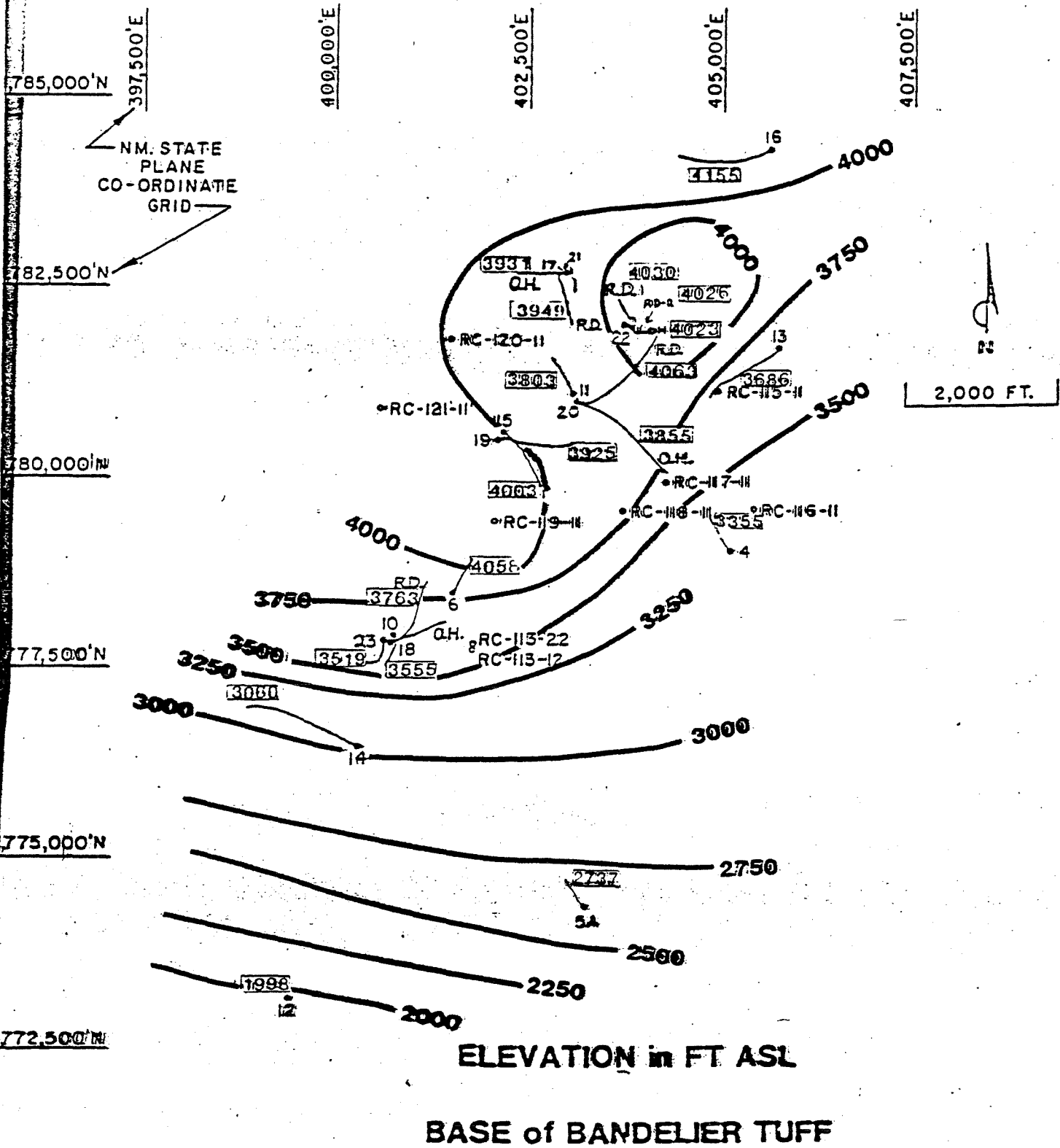
B ZONE

VISUALLY SIMILAR TO A3.
CHARACTERIZED ON LOGS BY
SIGNIFICANT INCREASES IN
POROSITY & CONDUCTIVITY

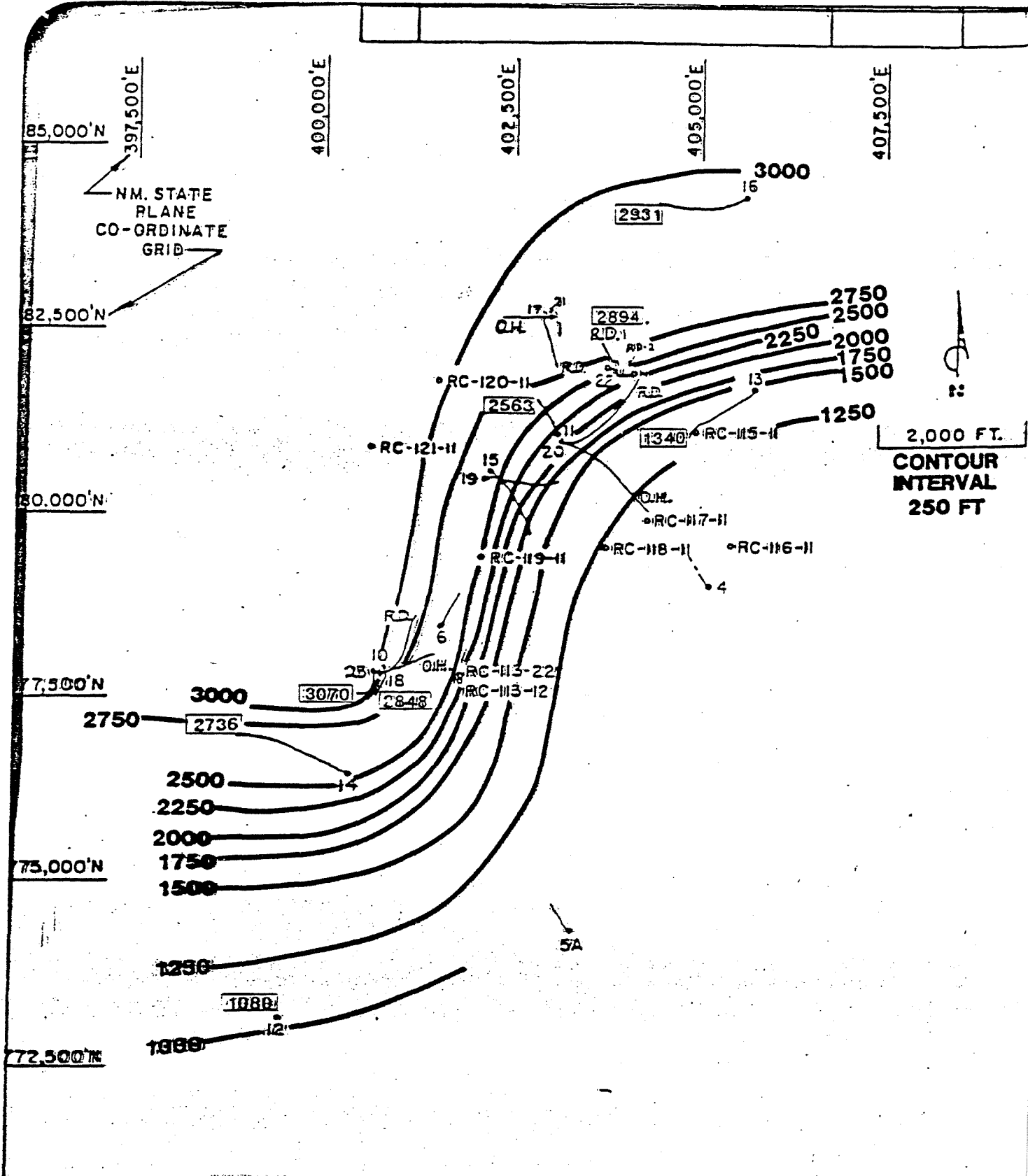
C ZONE

BASAL PUMICE.
WEAKLY WELDED.
HIGHLY ALTERED.

REV	DESCRIPTION	DATE	BY	APP
A	ISSUED	5-16-80		



UNION <small>76</small>	Union Geothermal Company of New Mexico
REDONDO CREEK DEVELOPMENT AREA	
DESIGN: <i>R.D.</i>	
DRAWN: <i>G. ...</i>	



Union Geothermal Company of New Mex

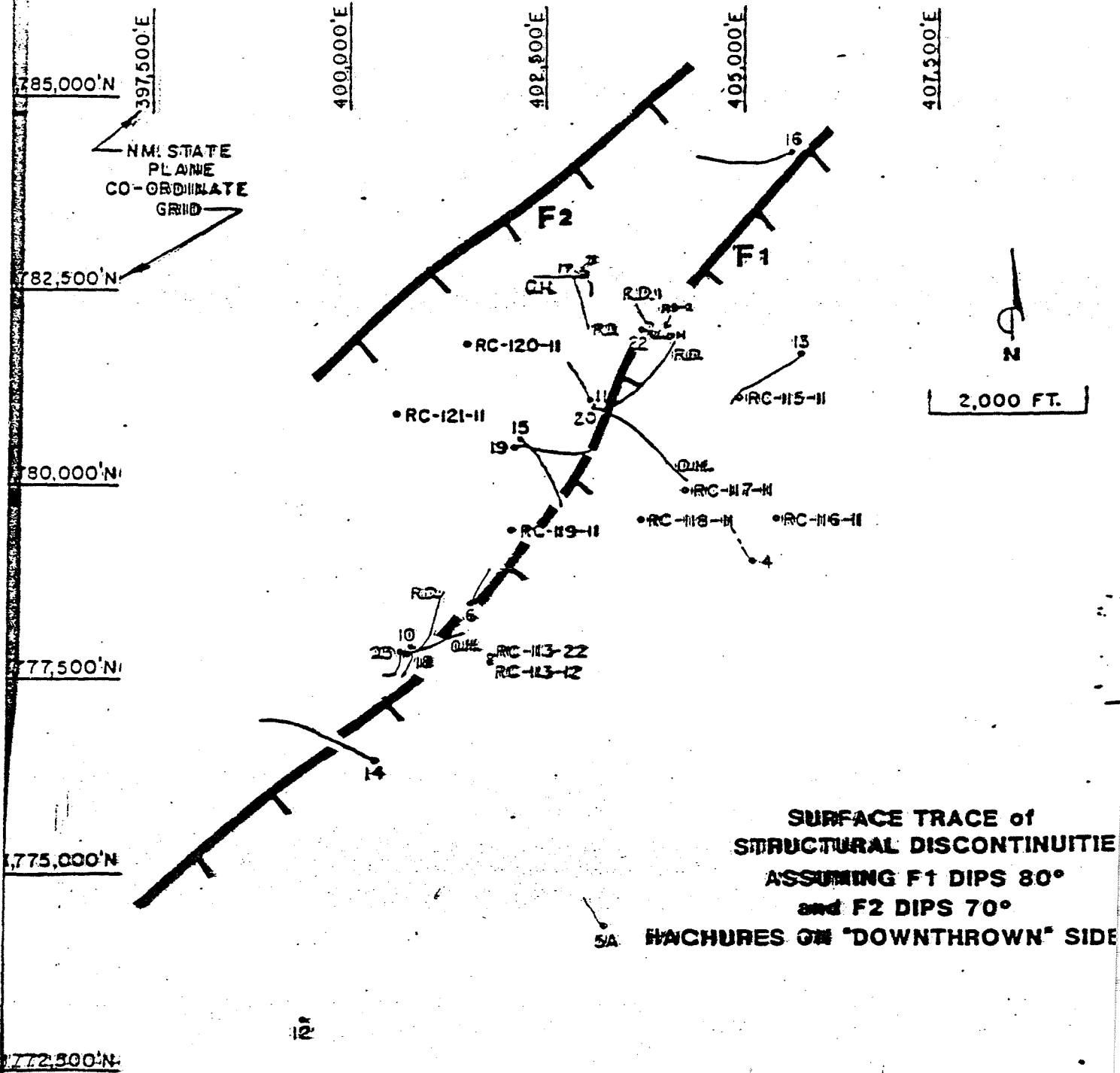
REDONDO CREEK DEVELOPMENT AREA
ELEVATION in FT ASL
BASE of PALIZA CANYON FM

DESIGN	10
DRAWN	S. FENZAK, R.
CHECK	AT

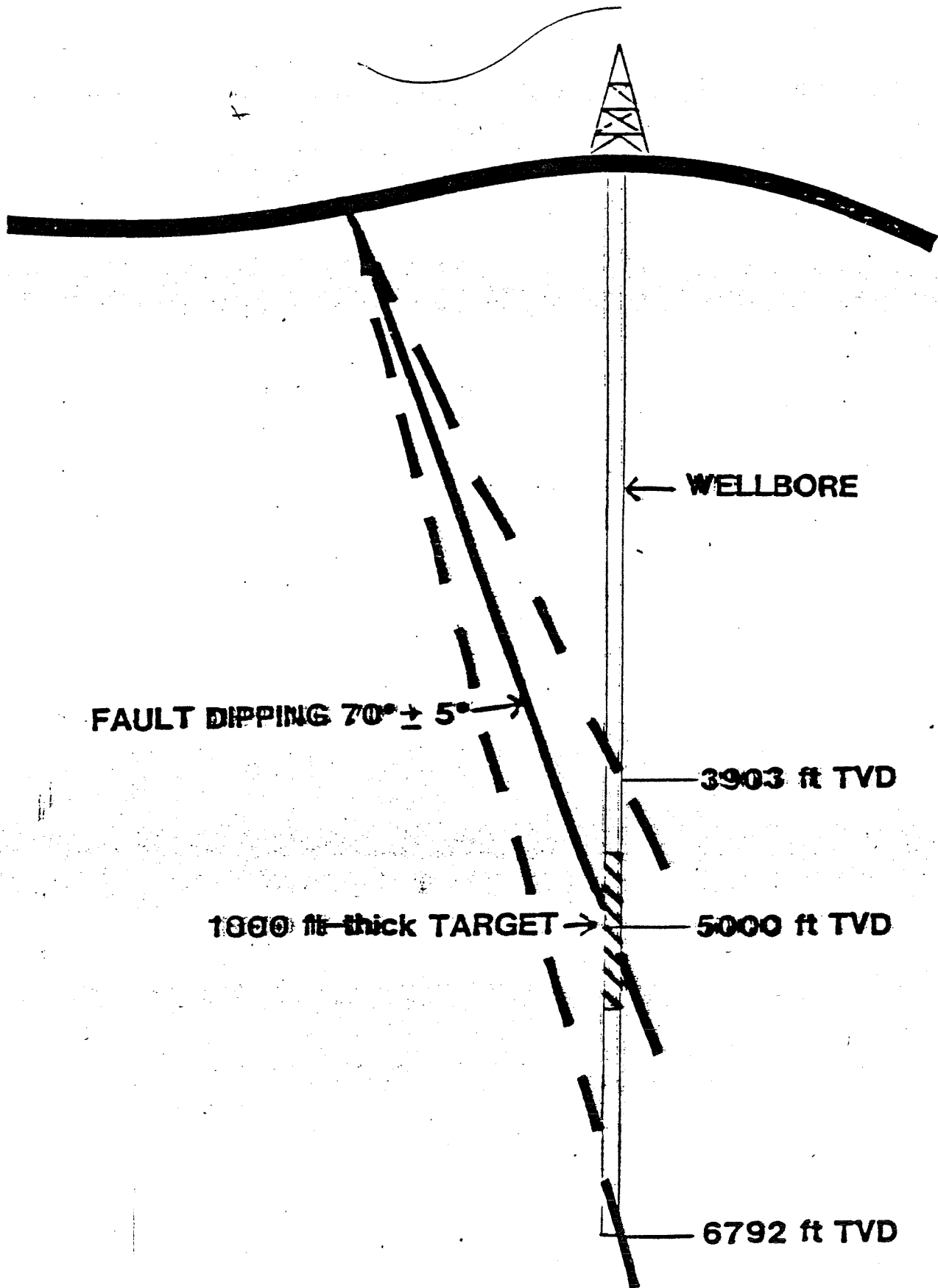
SIZE/A FE NO.
A

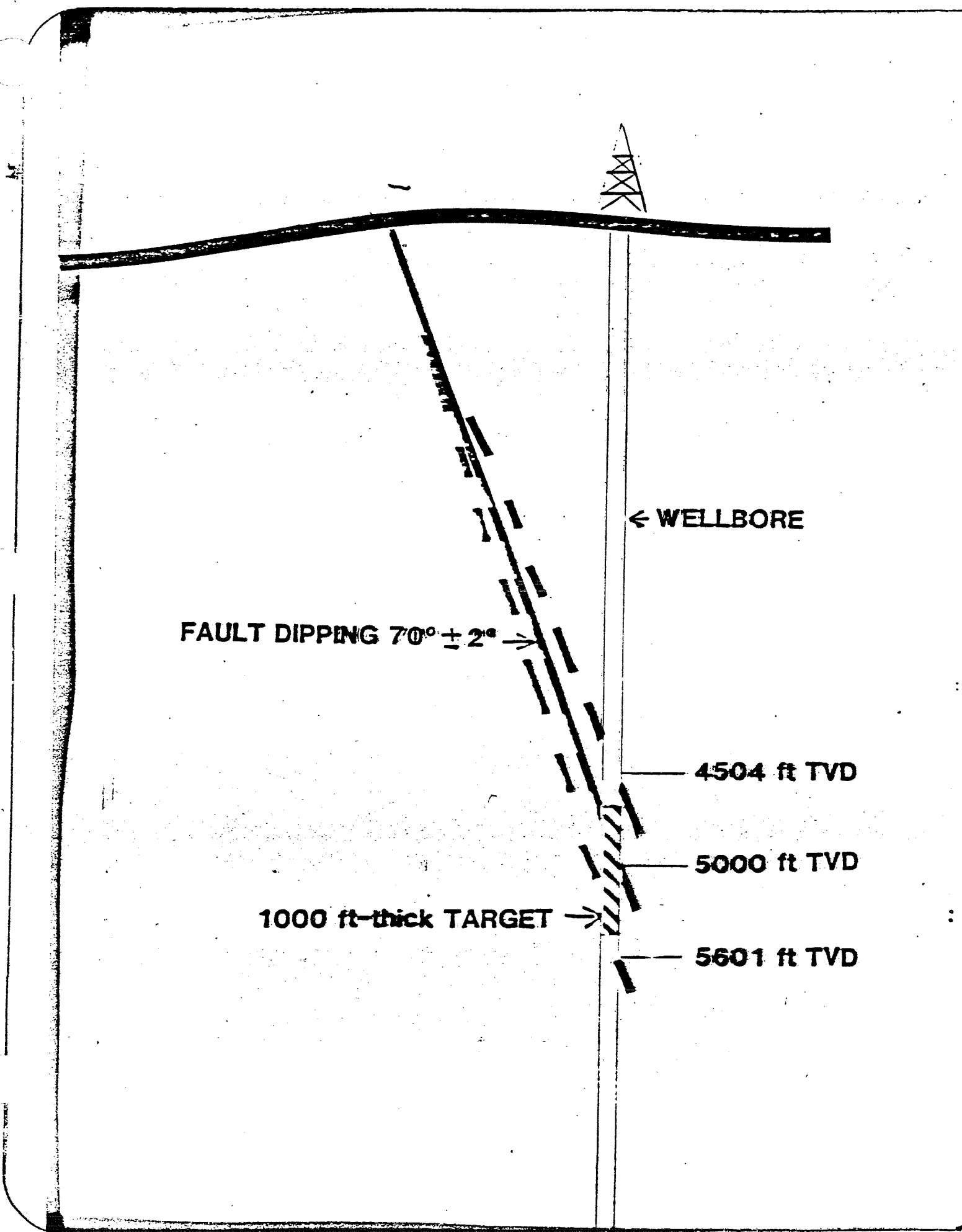
DWG. NO.
RC-L-24K-101a

REVISIONS				
REV	DESCRIPTION	DATE	BY	AP
A	ISSUED	5-16-80		



	Union Geothermal Company of New Mexico
	REDONDO CREEK DEVELOPMENT AREA
DESIGN - <i>R.D.</i>	





← WELLBORE

FAULT DIPPING $70^\circ \pm 2^\circ$ →

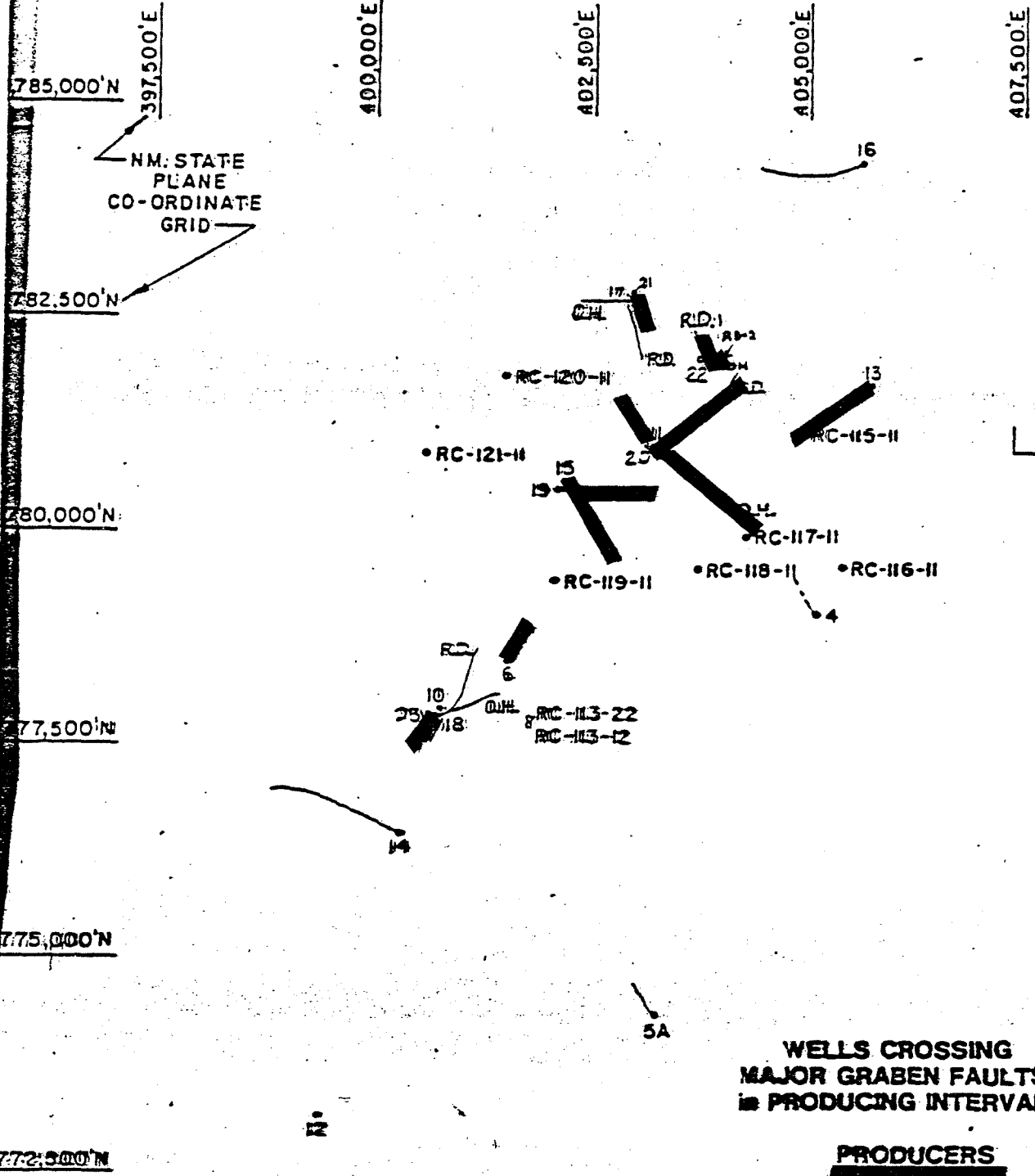
4504 ft TVD

5000 ft TVD

1000 ft-thick TARGET →

5601 ft TVD

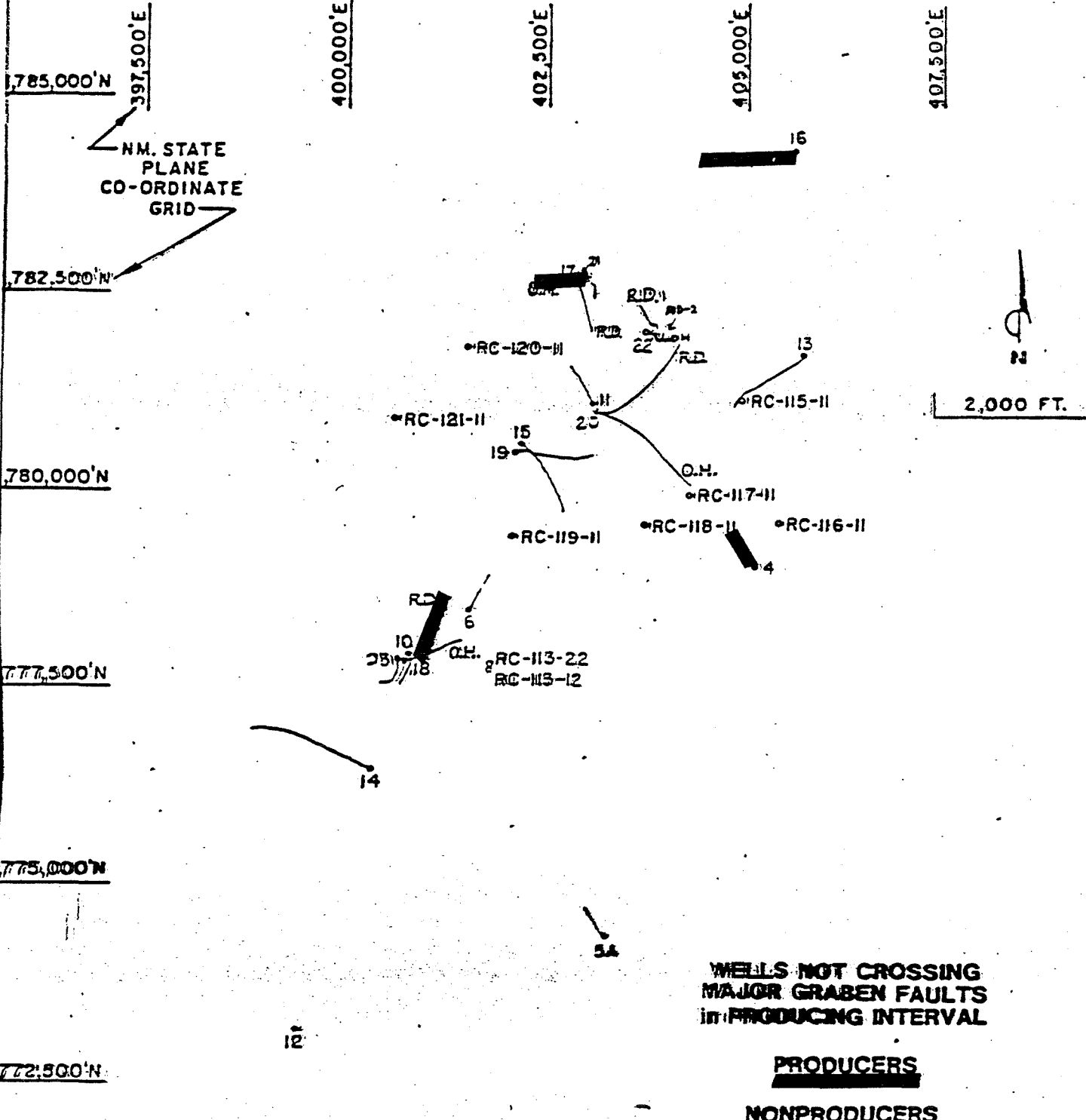
A	ISSUED	5-15-80	Z.	.
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WELLS CROSSING
MAJOR GRABEN FAULTS
IN PRODUCING INTERVAL

PRODUCERS
NON-PRODUCERS

Union 76		Union Geothermal Company of New Mexico	
REDONDO CREEK DEVELOPMENT AREA			
DESIGN	R.D.	SIZE/A FE NO.	DWG. NO.
DRAWN	S. FEUZAKER		RC-L-24K-101a
CHECKED			



WELLS NOT CROSSING
MAJOR GRABEN FAULTS
in PRODUCING INTERVAL

PRODUCERS
NONPRODUCERS

Union		Union Geothermal Company of New Mexico	
		REDONDO CREEK DEVELOPMENT AREA	
DESIGN	RD	SIZE	A
DRAWN	S. FELZAK-R.	AFE NO.	
CHECK	RD	DWG. NO.	RC-L-24K-101a

1,785,000'N

397,500'E

400,000'E

402,500'E

405,000'E

407,500'E

NM. STATE
PLANE
CO-ORDINATE
GRID

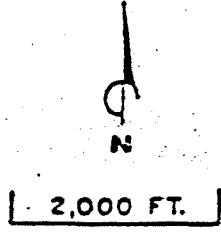
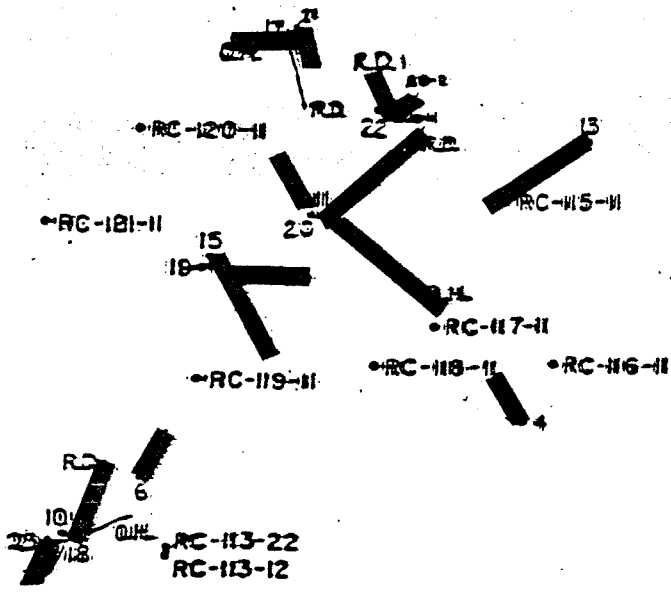
1,782,500'N

1,780,000'N

1,777,500'N

1,775,000'N

1,772,500'N



WELLCOURSES IN STUDY 15

WELLS AGREEING WITH HYPOTHESIS 8(53%)

WELLS DISAGREEING WITH HYPOTHESIS 7(47%)

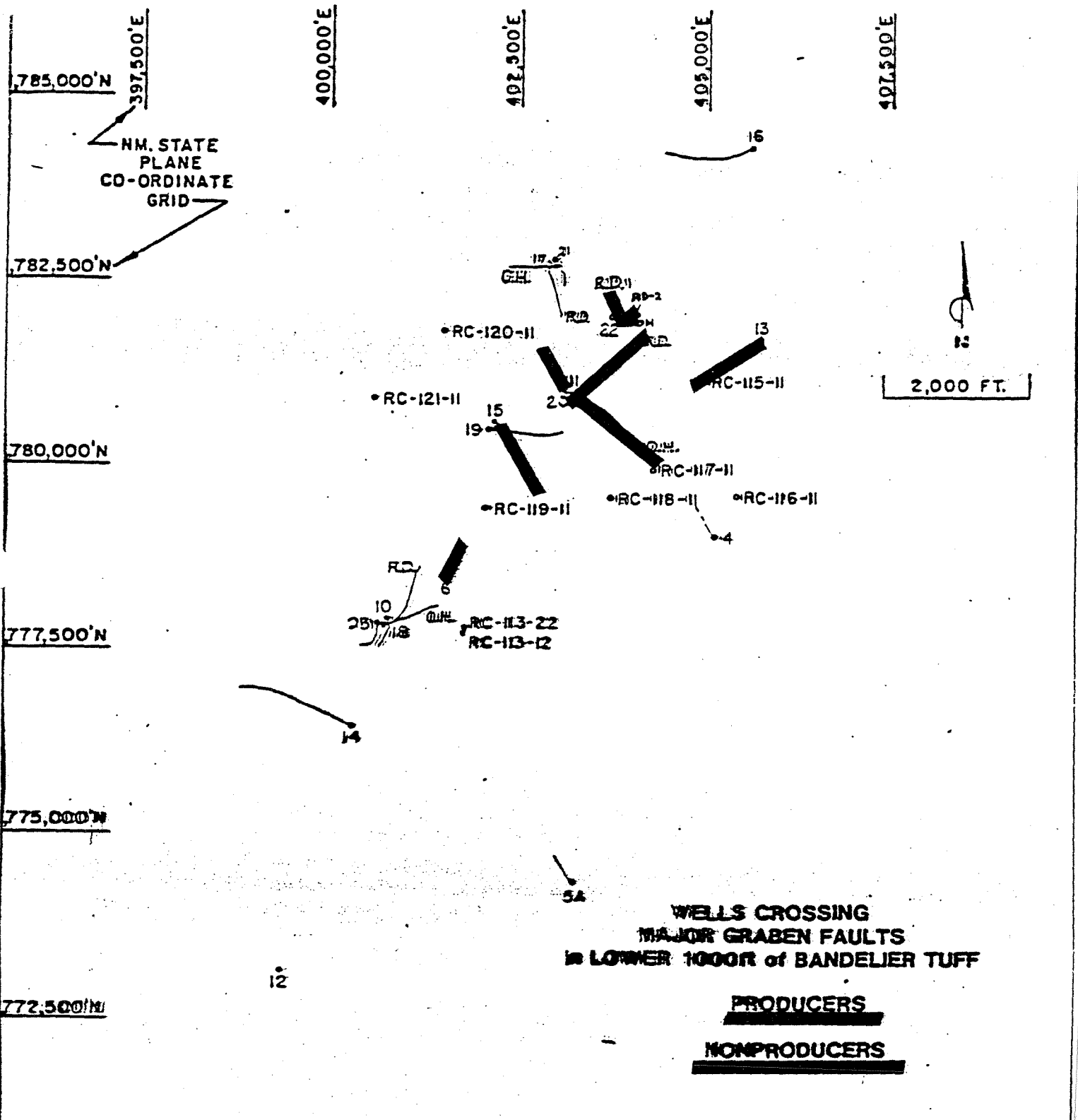


Union Geothermal Company of New Mexico

REDONDO CREEK DEVELOPMENT AREA

DESIGN	RD
DRAWN	S. FEUZAKER

SIZE/AFE NO.	DWG. NO.	RF
--------------	----------	----



WELLS CROSSING
 MAJOR GRABEN FAULTS
 IN LOWER 1000' OF BANDELIER TUFF

PRODUCERS
NONPRODUCERS

Union		Union Geothermal Company of New Mexico	
		REDONDO CREEK DEVELOPMENT AREA	
DESIGN	W.D.	SIZE/AFE NO.	DWG: NO.
DRAWN	S. FEYZAKER.		RC-L-24K-101a
CHECK			

REV	DESCRIPTION	DATE	BY	AP
A	ISSUED	5-15-80		

785,000'N 397,500'E
 400,000'E
 402,500'E
 405,000'E
 407,500'E

NM. STATE
 PLANE
 CO-ORDINATE
 GRID

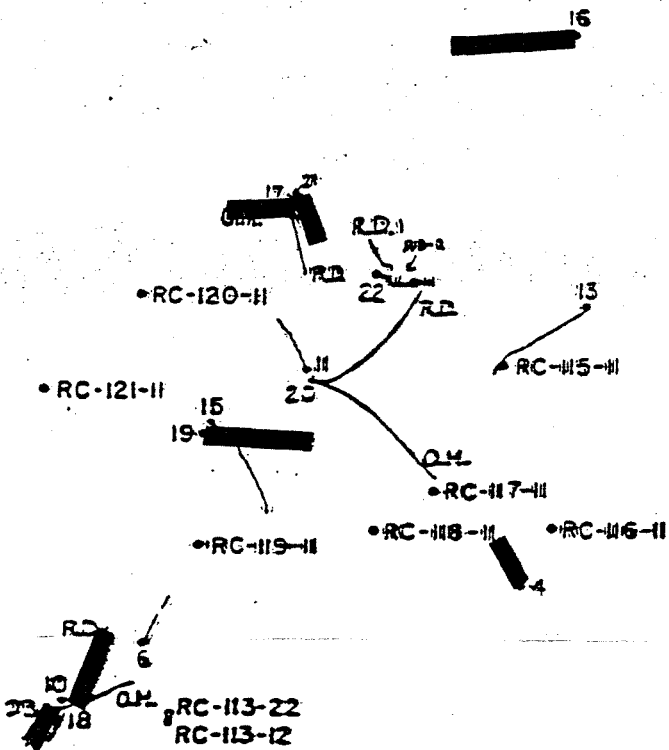
782,500'N

780,000'N

777,500'N

775,000'N

772,500'N



WELLS NOT CROSSING
 MAJOR GRABEN FAULTS
 IN LOWER 1000' of BANDELIER TUFF

PRODUCERS

NON-PRODUCERS

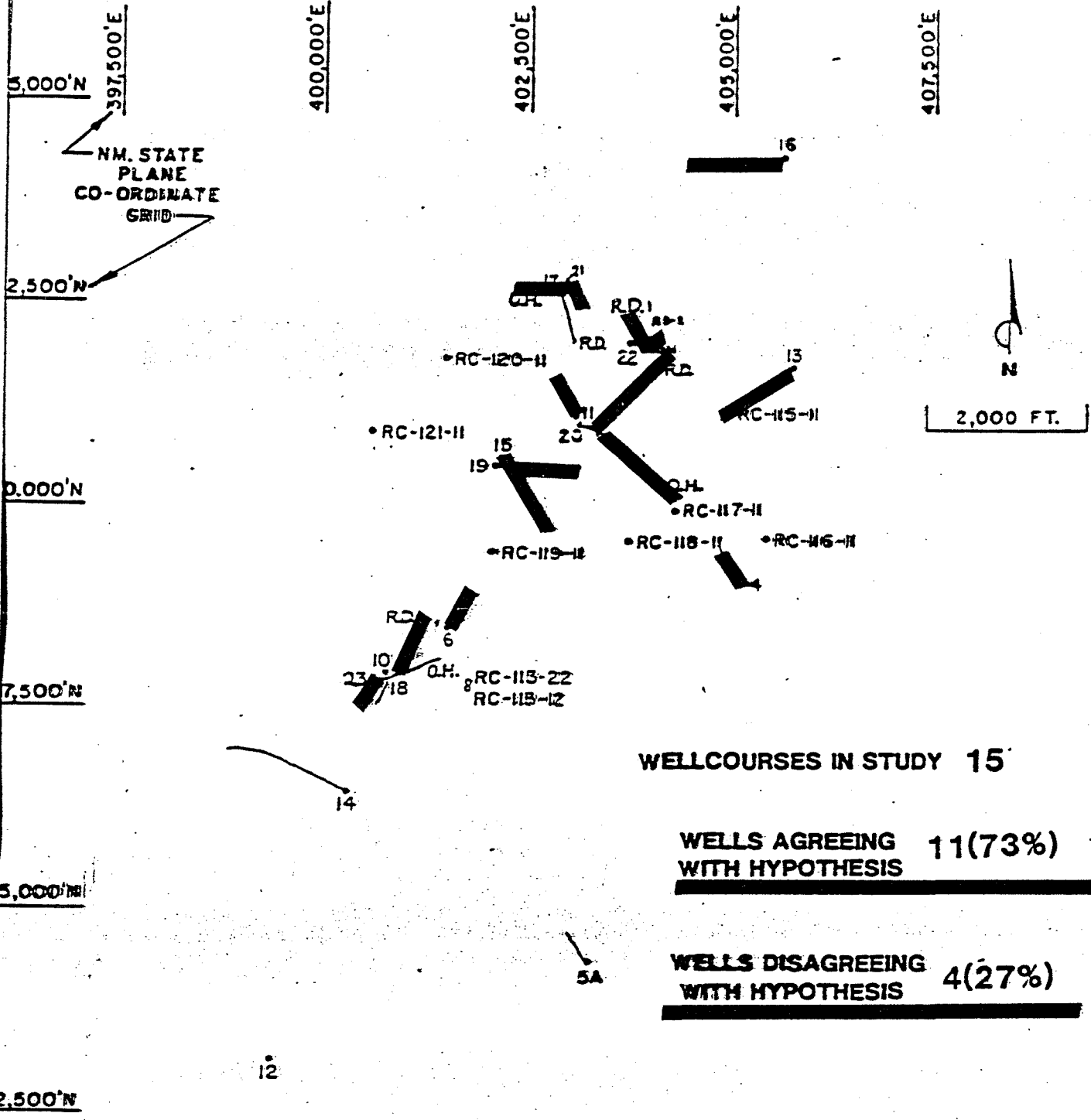


Union Geothermal Company of New Mexico

REDONDO CREEK DEVELOPMENT AREA

DESIGN . L.D.

REV.	DESCRIPTION	DATE	BY	APP.
A	ISSUED	5-10-80		



WELLCOURSES IN STUDY 15

WELLS AGREEING WITH HYPOTHESIS 11(73%)

WELLS DISAGREEING WITH HYPOTHESIS 4(27%)

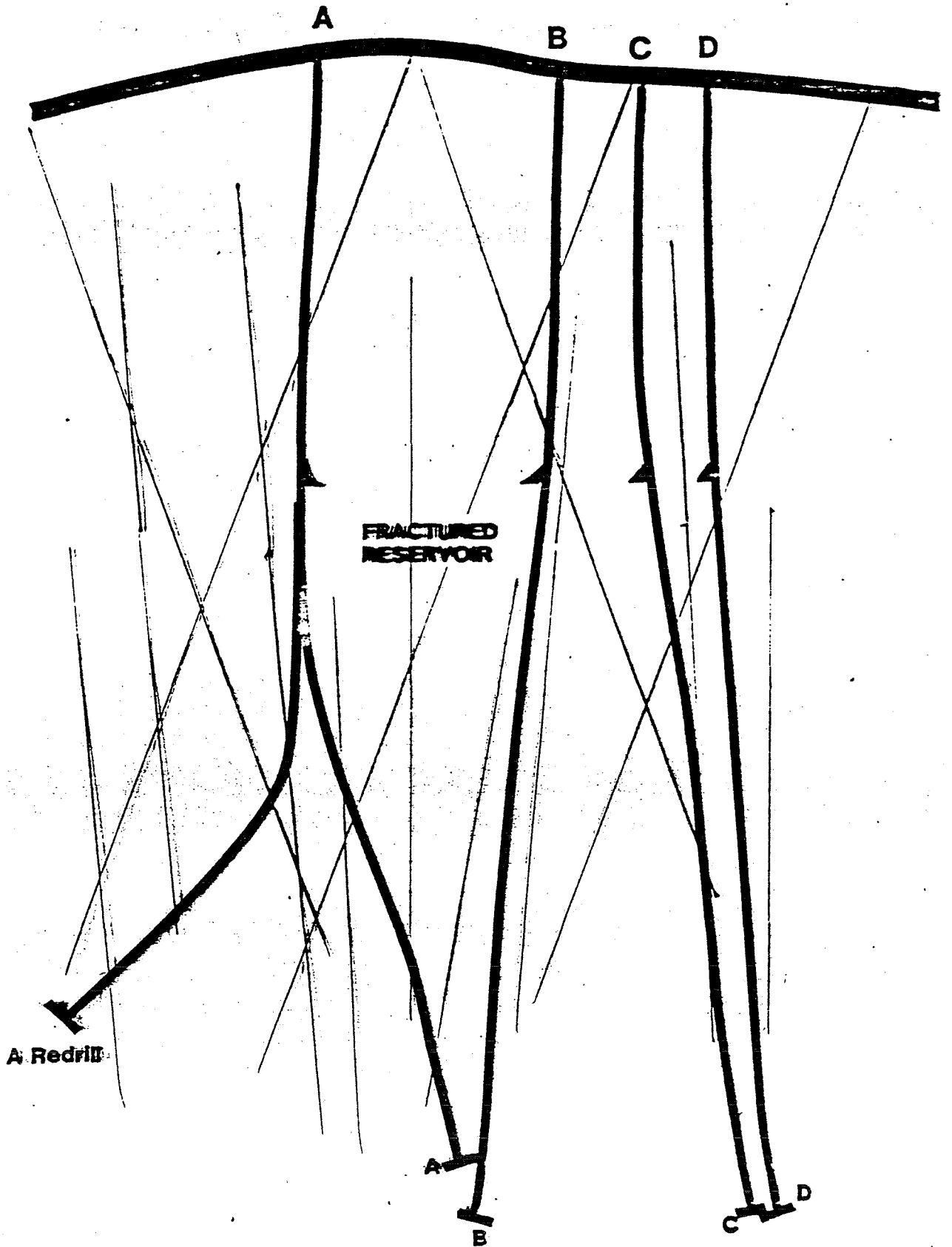


Union Geothermal Company of New Mexico

REDONDO CREEK DEVELOPMENT AREA

DESIGN	A.D.
DRAWN	E. PEWZAK R.

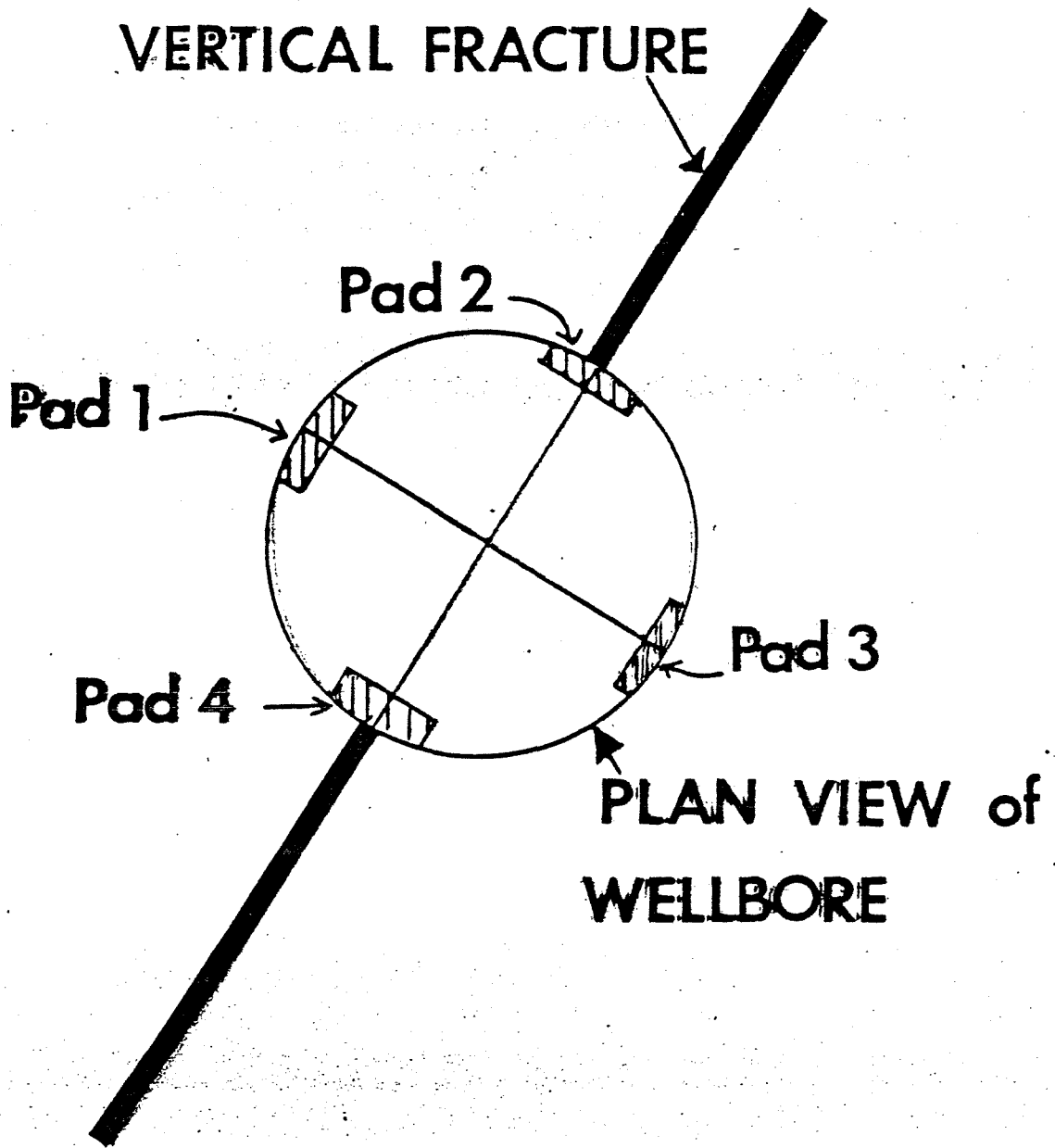
CROSS SECTIONAL VIEW



FRACTURED RESERVOIR

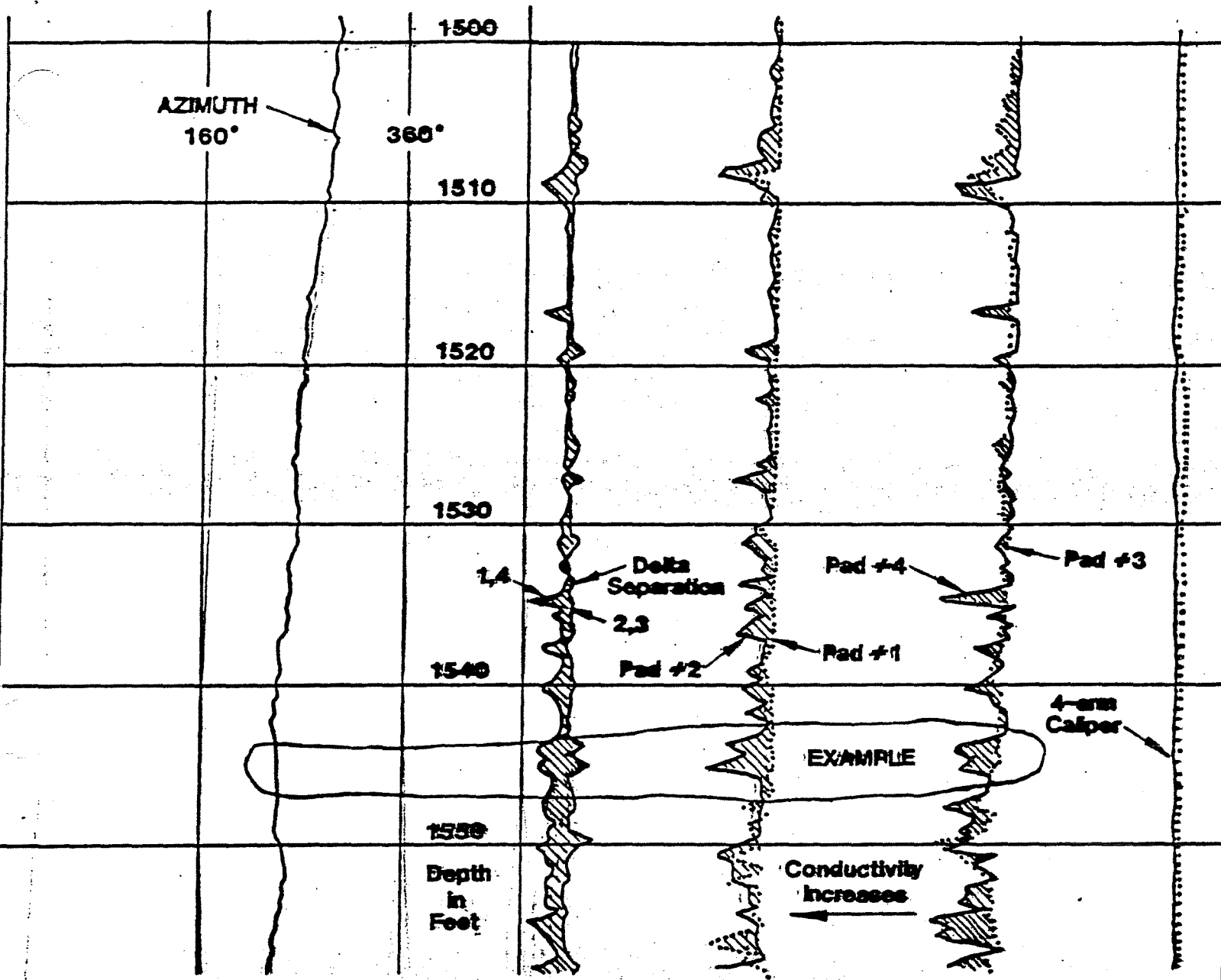
A Redrill

**TRACE of
VERTICAL FRACTURE**



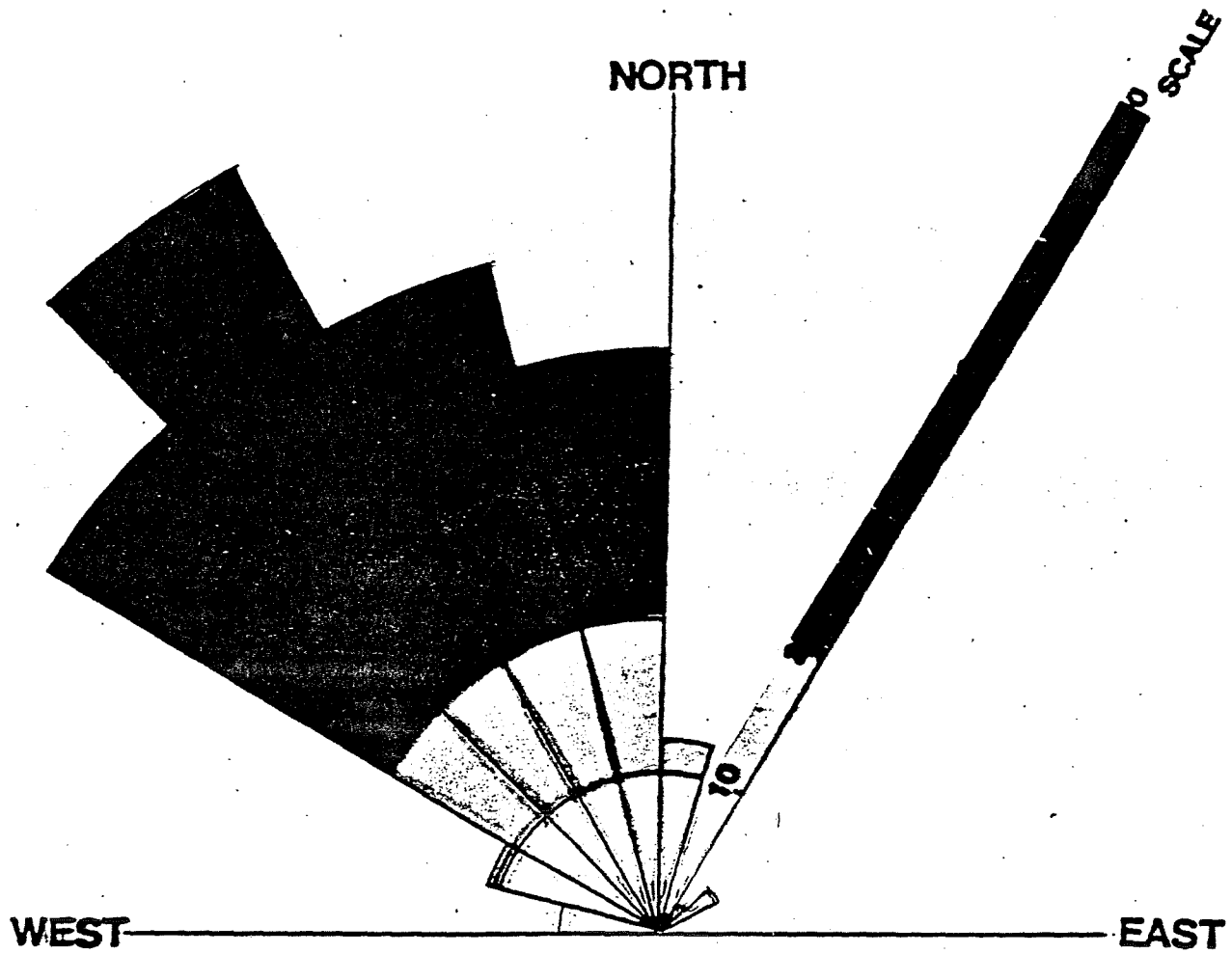
PADS 2 & 4 SEE FRACTURE

PADS 1 & 3 (at 90° to fracture) DO NOT



FRACTURE IDENTIFICATION LOG BACA 18

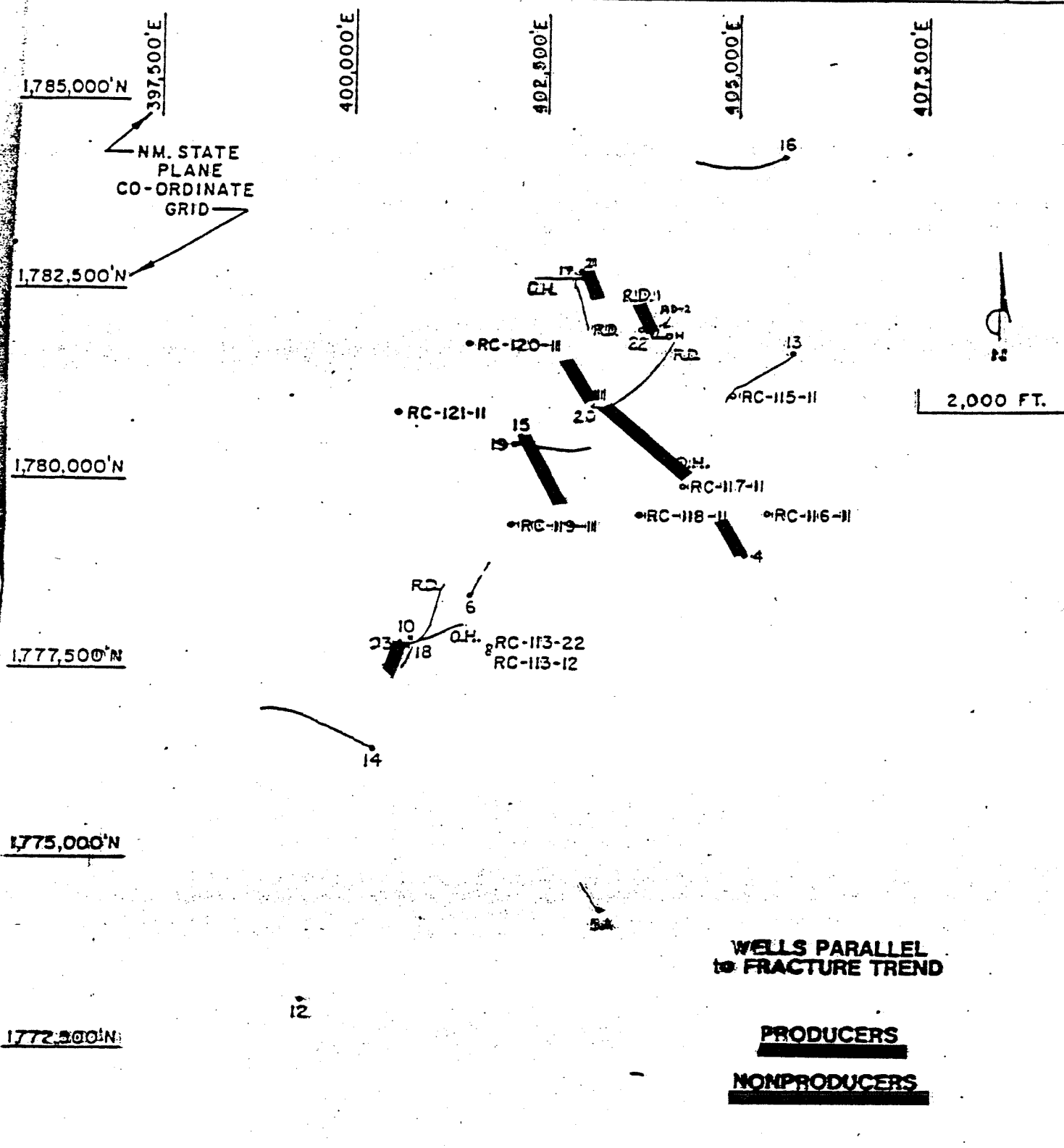
Depth: 1,545 ft
 Observed azimuth 248° Magnetic Declination 12° E
 True azimuth & position of Pad 1: 252 or S 72 W
 Pads Observing Fracture: 2 and 4
 Fracture Strike : 342 or N 18 W




FRACTURE STRIKES ALL WELLS

NUMBER of FRACTURES	220
MEAN DIRECTION	N 31 W
STD DEV	27 deg

A	ISSUED	5-15-80	2.
---	--------	---------	----



	Union Geothermal Company of New Mexico
	REDONDO CREEK DEVELOPMENT AREA
DESIGN: <i>W.D.</i>	

785,000'N
397,500'E

400,000'E

402,500'E

405,000'E

407,500'E

NM. STATE
PLANE
CO-ORDINATE
GRID

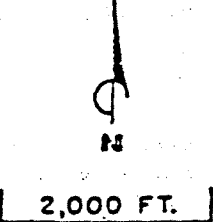
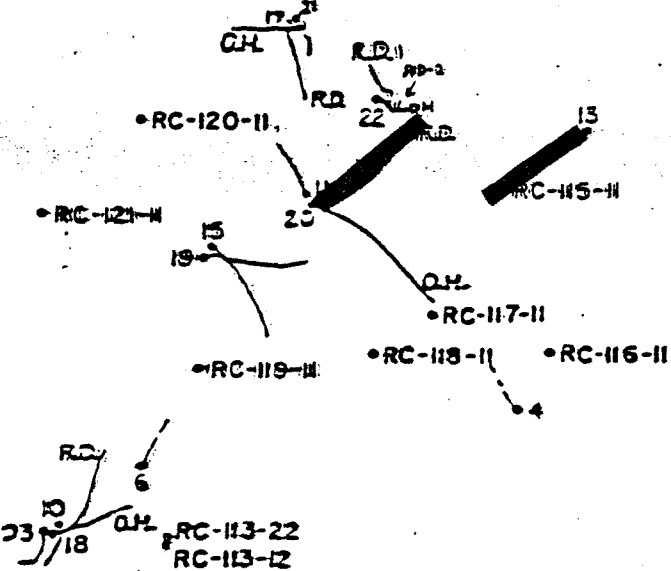
782,500'N

780,000'N

777,500'N

775,000'N

772,500'N



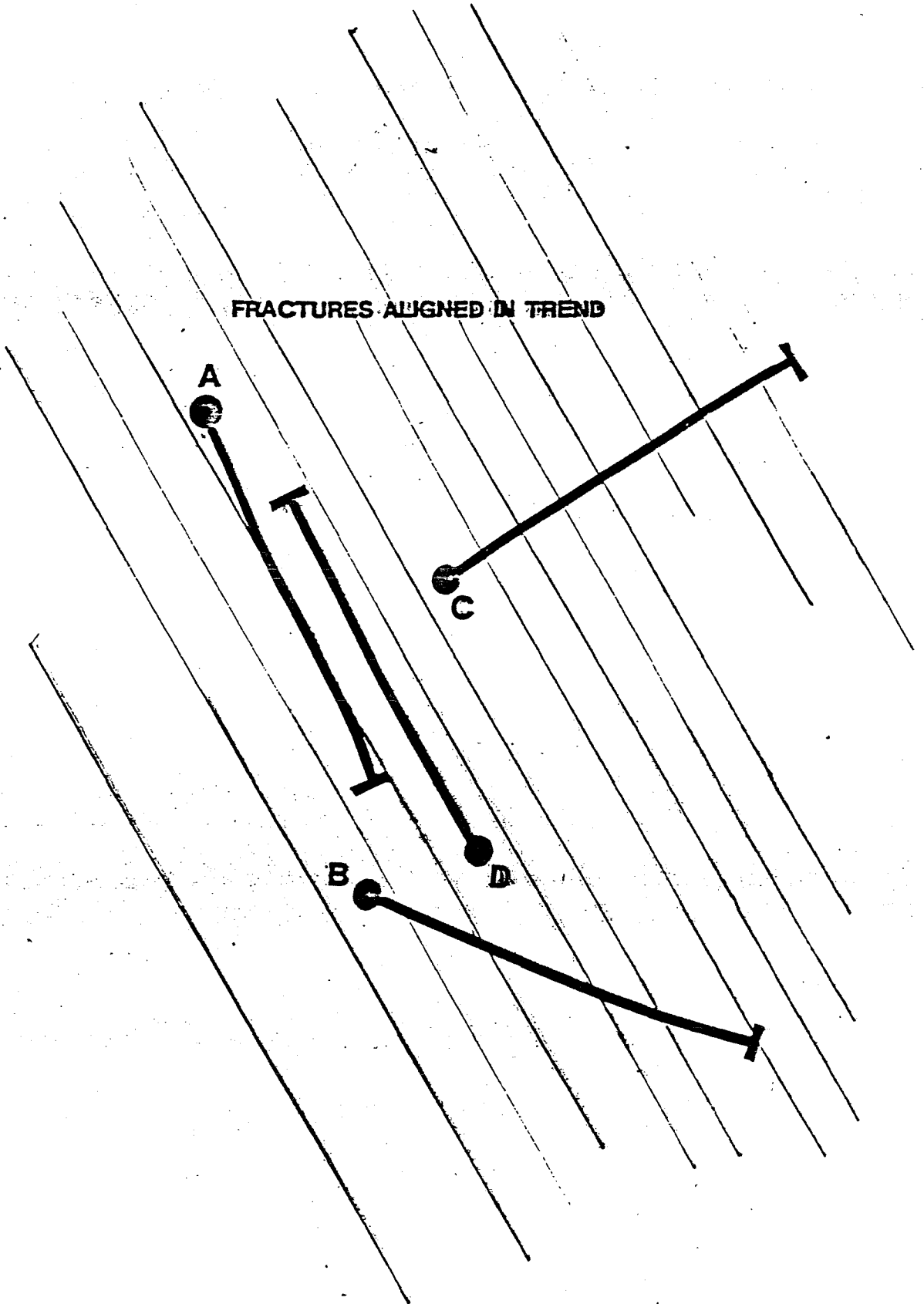
WELLS PERPENDICULAR
to FRACTURE TREND

PRODUCERS
NONPRODUCERS

UNION 76		Union Geothermal Company of New Mexico	
REDONDO CREEK DEVELOPMENT AREA			
DESIGN	E.D.	SIZE AFE NO.	DWG. NO.
DRAWN	E. FELZKA R.		RC-L-24K-101a
CHECK			

MAP VIEW

FRACTURES ALIGNED IN TREND



785,000'N
397,500'E

400,000'E

402,500'E

405,000'E

407,500'E

NM. STATE
PLANE
CO-ORDINATE
GRID

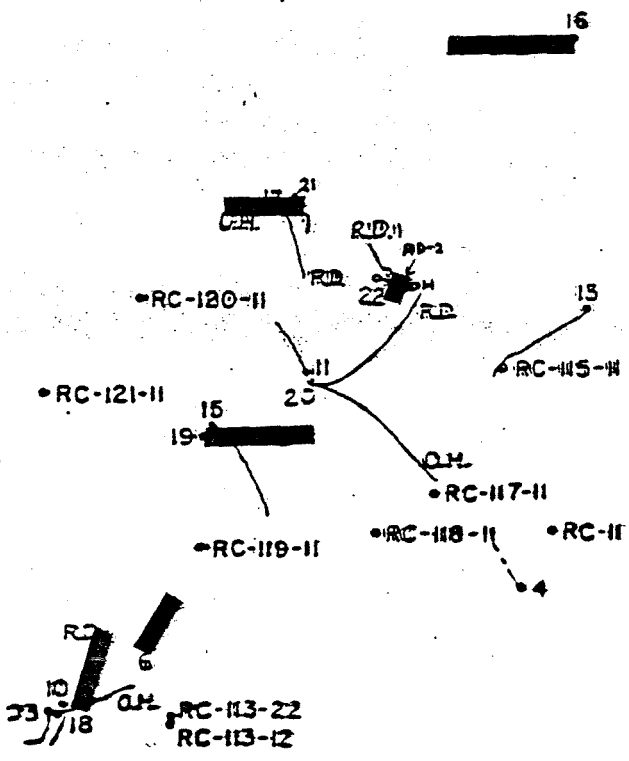
782,500'N

780,000'N

777,500'N

775,000'N

772,500'N



WELLS NEITHER
PARALLEL NOR PERPENDICULAR
TO FRACTURE TREND

PRODUCERS
NONPRODUCERS

Union 76		Union Geothermal Company of New Mexico	
REDONDO CREEK DEVELOPMENT AREA			
DESIGN	P.D.	SIZE/AFE NO.	DWG. NO.
DRAWN	E. FELIZAKA		RC-L-24K-101a
CHECK			

1,785,000'N 397,500'E
 400,000'E
 402,500'E
 405,000'E
 407,500'E

NM. STATE
 PLANE
 CO-ORDINATE
 GRID

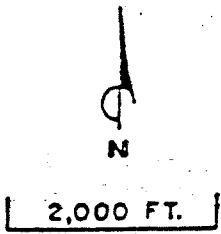
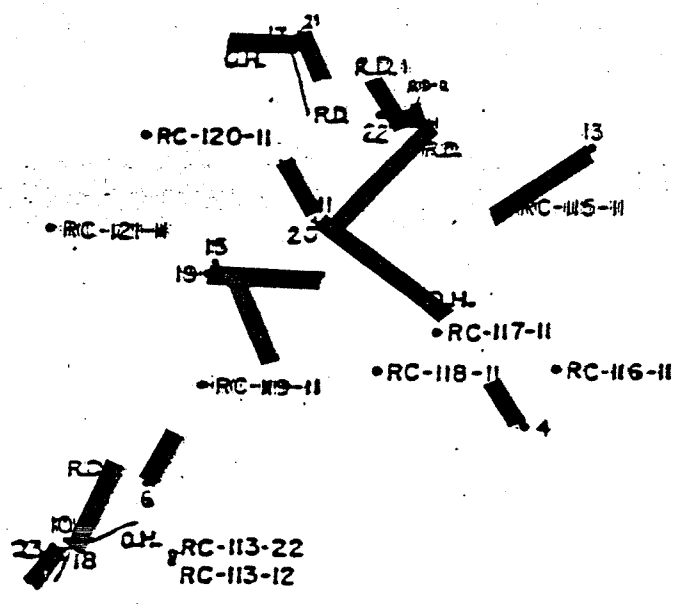
1,782,500'N

1,780,000'N

1,777,500'N

1,775,000'N

1,772,500'N



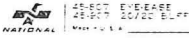
WELLCOURSES IN STUDY 15

WELLS AGREEING WITH HYPOTHESIS 14(93%)

WELLS DISAGREEING WITH HYPOTHESIS 1(7%)

UNION		Union Geothermal Company of New Mexico	
		REDONDO CREEK DEVELOPMENT AREA	
DESIGN	LD	SIZE	A FE NO.
DRAWN	E. FEUZAKER.	DWG. NO.	RC-1-24K-101a

Initials	Date
Prepared By	
Approved By	



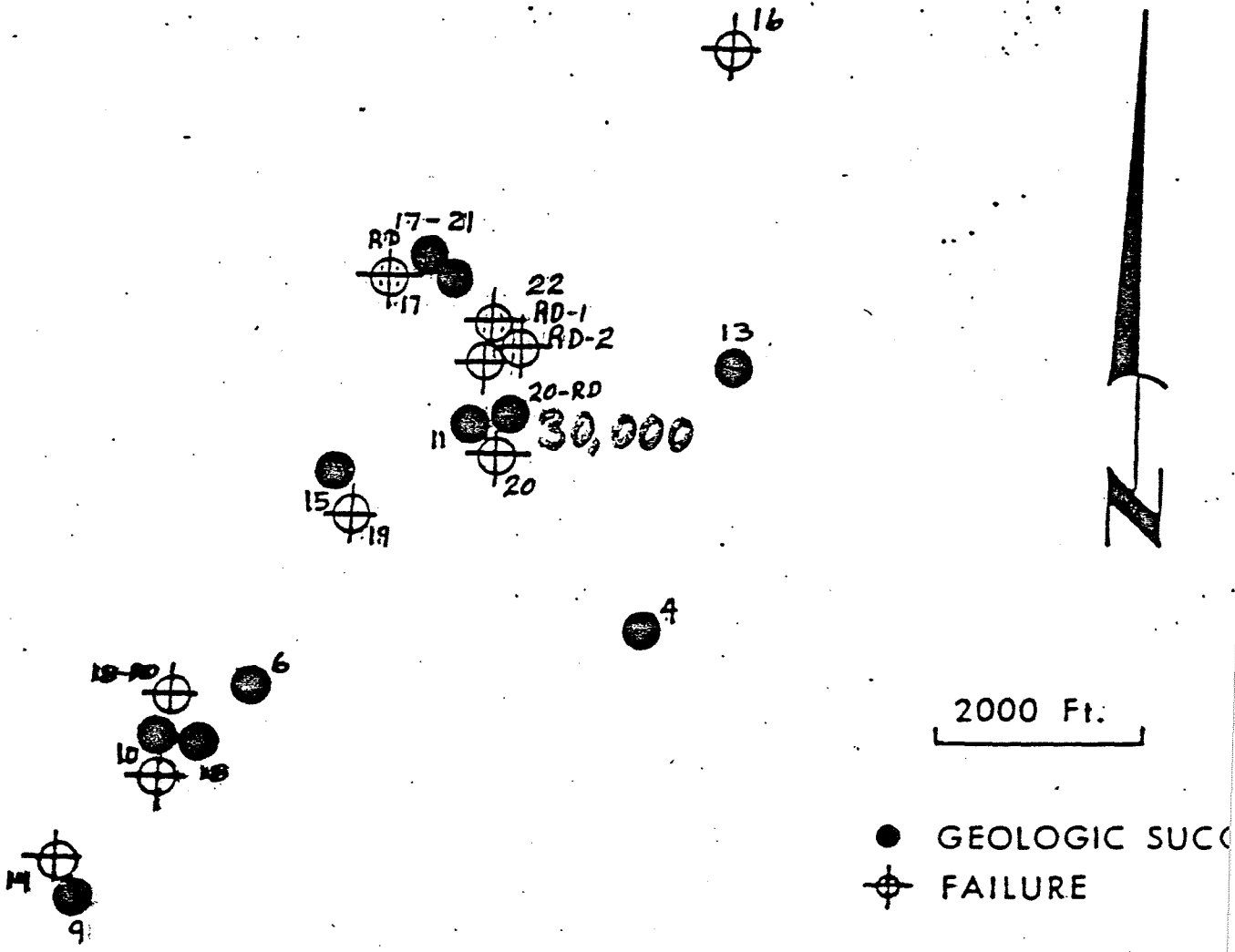
Well	Date Start	Date Finish	Total Depth (ft)	Union Presentation to Review Com Cook (000)	Union Proposal Dec 16	Steam d/h
4			6378			45,000
5A			6973			
6 RD			4810			
7	7-26-72	8-15-72	5532			
8	8-16-72	9-13-72	4384			
9	9-15-72	10-13-72	5303	333		
10	7-5-73	9-18-73	6001	635		
11	9-26-73	11-13-73	6931	425		116,000
12	6-19-74	8-19-74	9212	542		
13	8-23-74	10-27-74	8228	718		54,000
14	11-15-74	2-24-75	6824	908		
15	4-20-75	6-12-75	5505	610		105,000
16	6-19-75	8-21-75	7002	557		
17	8-13-78	10-15-78	5791	914	812	
17 RD	10-18-78	12-4-78	6254	733		
18	12-16-78	2-4-79	4597	996	1586	
18 RD	?		5250	447		
19	9-24-80	11-3-80	5610	999	1039	
20	6-27-80	8-2-80	6863	905	11698	
20 RD	8-3-80	8-20-80	6374	797		30,000
21			3000	875	876	
22			6017	1263		
22 RD1			6485	400		
22 RD2			6006	531		
23			5746	1261		
23 RD			3515	602		30,000

PRE - DOE WELLS

<u>WELL</u>	<u>T.D.</u>	<u>COST</u> (\$000)	<u>STATUS</u>	<u>STEAM</u> (AT LINE PRESSURE)
BACA 4	6378'		COMMERCIAL	45,000 LBS/HR
BACA 5A	6973'		WATER INJECTOR	
BACA 6	4810' (3455' BRIDGE)		INITIALLY COMMERCIAL NOW BRIDGED @ 9-5/8" COLLAPSED	(33,000)
BACA 9	5303'	333	P&A	
BACA 10	6001'	635	MECHANICAL PROBLEMS	
BACA 11	6931'	425	COMMERCIAL	116,000 LBS/HR
BACA 12	9212'	542	WATER INJECTOR	
BACA 13	8228'	718	COMMERCIAL	54,000 LBS/HR
BACA 14	6824' (5780' GMT.)	908	WATER INJECTOR	
BACA 15	5505'	610	COMMERCIAL	105,000 LBS/HR
BACA 16	7002'	557	NON-PRODUCTIVE	
			TOTAL:	----- 320,000 LBS/HR

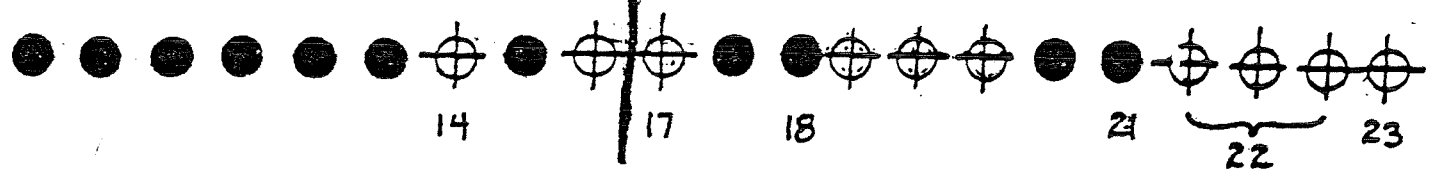
POST - DE WELLS

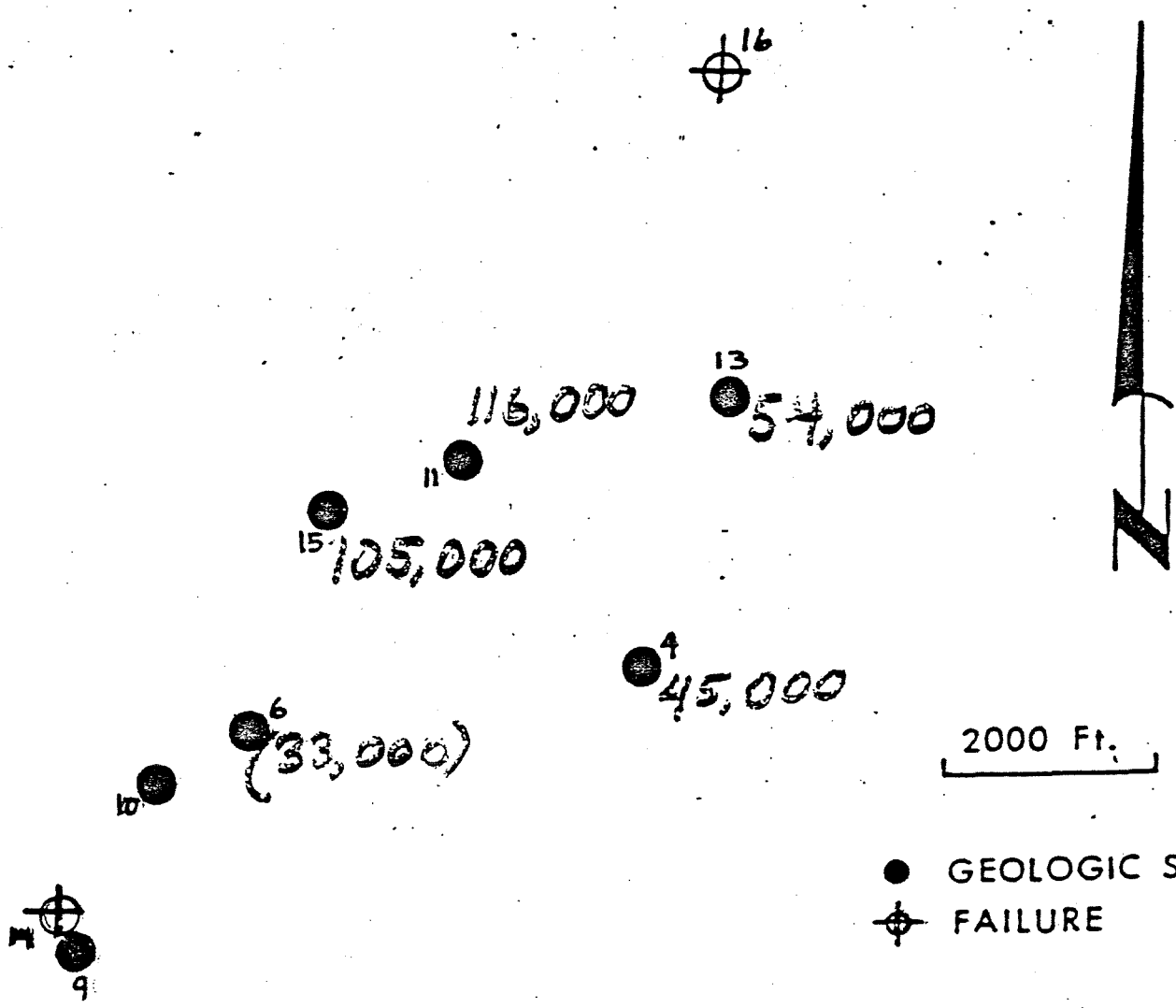
<u>WELL</u>	<u>T.D.</u>	<u>COST</u> (\$000)	<u>STATUS</u>	<u>STEAM</u>
BACA 17	OH 5791'	914	NON-PRODUCTIVE	
	RD 6254'	733	INITIALLY PRODUCTIVE,	
		\$1,647	MECHANICAL PROBLEMS	
BACA 18	OH 4597'	996	POT. PRODUCTIVE,	
	RD 5250'	477	LOST HOLE	
		\$1,473	NON-PRODUCTIVE	
BACA 19	5610'	\$ 999	SUB-COMMERCIAL	(32,000 @ 10 PSI)
BACA 20	OH 6863'	905	NON-PRODUCTIVE	
		791	COMMERCIAL	30,000 LBS/HR
		\$1,696		
BACA 21	3000'	\$ 875	SUB-COMMERCIAL	(34,000 @ 75 PSI)
BACA 22	OH 6017'	1,263	POT. PRODUCTIVE,	
			LOST HOLE	
	RD1 6485'	400	SUB-COMMERCIAL	(41,000 @ 45 PSI)
	RD2 6006'	531	SUB-COMMERCIAL	(20,000 @ 8 PSI)
		\$2,194		
BACA 23	TD 5746'	1,261	NON-PRODUCTIVE	
	RECPL. 3515'	602	POSSIBLY COMMERCIAL	(48,000 @ 5L PSI)
		\$1,863		
TOTAL:				30,000 LBS/HR



PRE DOE POST DOE

SEQUENCE





SEQUENCE





2000 Ft.

- GEOLOGIC SUCCES
- ⊕ FAILURE

III

4

6

10

9

SEQUENCE





2000 Ft.

- GEOLOGIC SUCCES
- ⊕ FAILURE

6

4

SEQUENCE





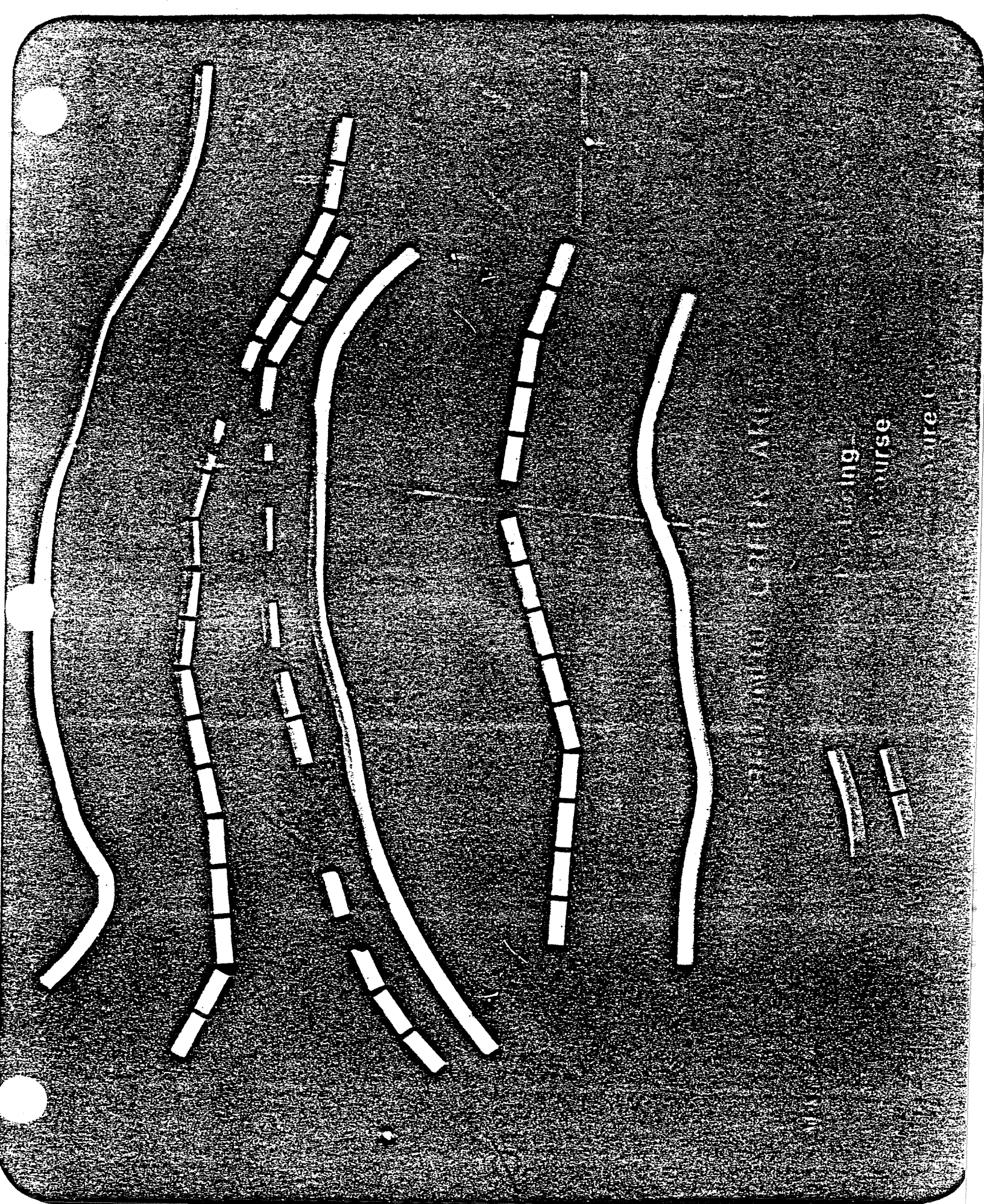
4

2000 Ft.

- GEOLOGIC SUCCESS
- ⊕ FAILURE

SEQUENCE





ST. PAUL, MINN. 55101

Producting
course

Source Co.



GEOHERMAL DIVISION

BACA PROSPECT

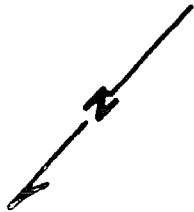
BRINE ANALYSIS

(UNCORRECTED FOR FLASH)

pH	7.2	
T.D.S.	6093	Mg/l
SiO ₂	599	
CO ₃	19	
HCO ₃	127	
SO ₄	64	
Cl	3061	
Na	1749	
K	370	
Ca	15	
Mg	0.3	
Ba	0.05	
B	23	
F	6	
As	3	

ALAMO CANYON-1

533°



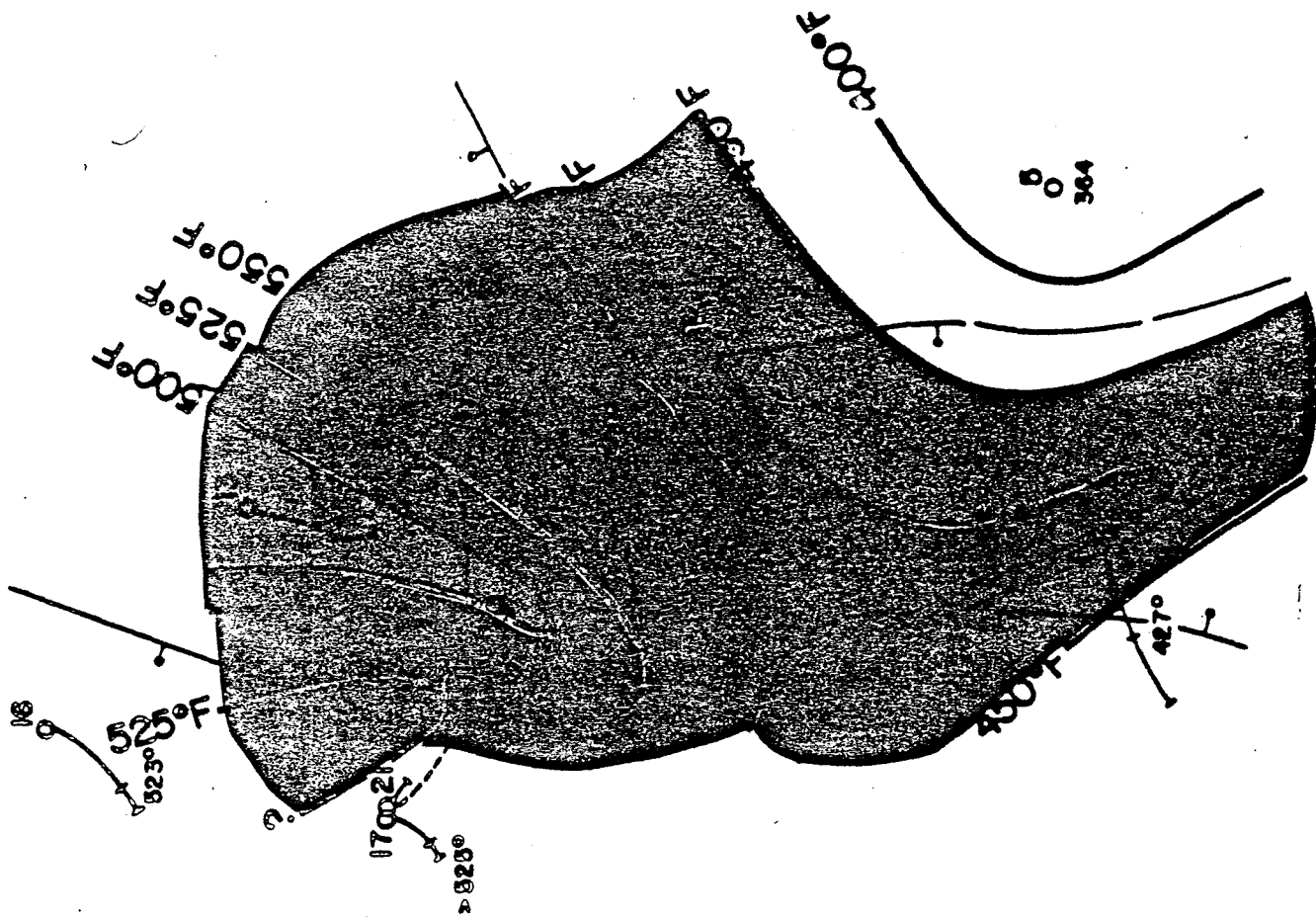
--- PRODUCER

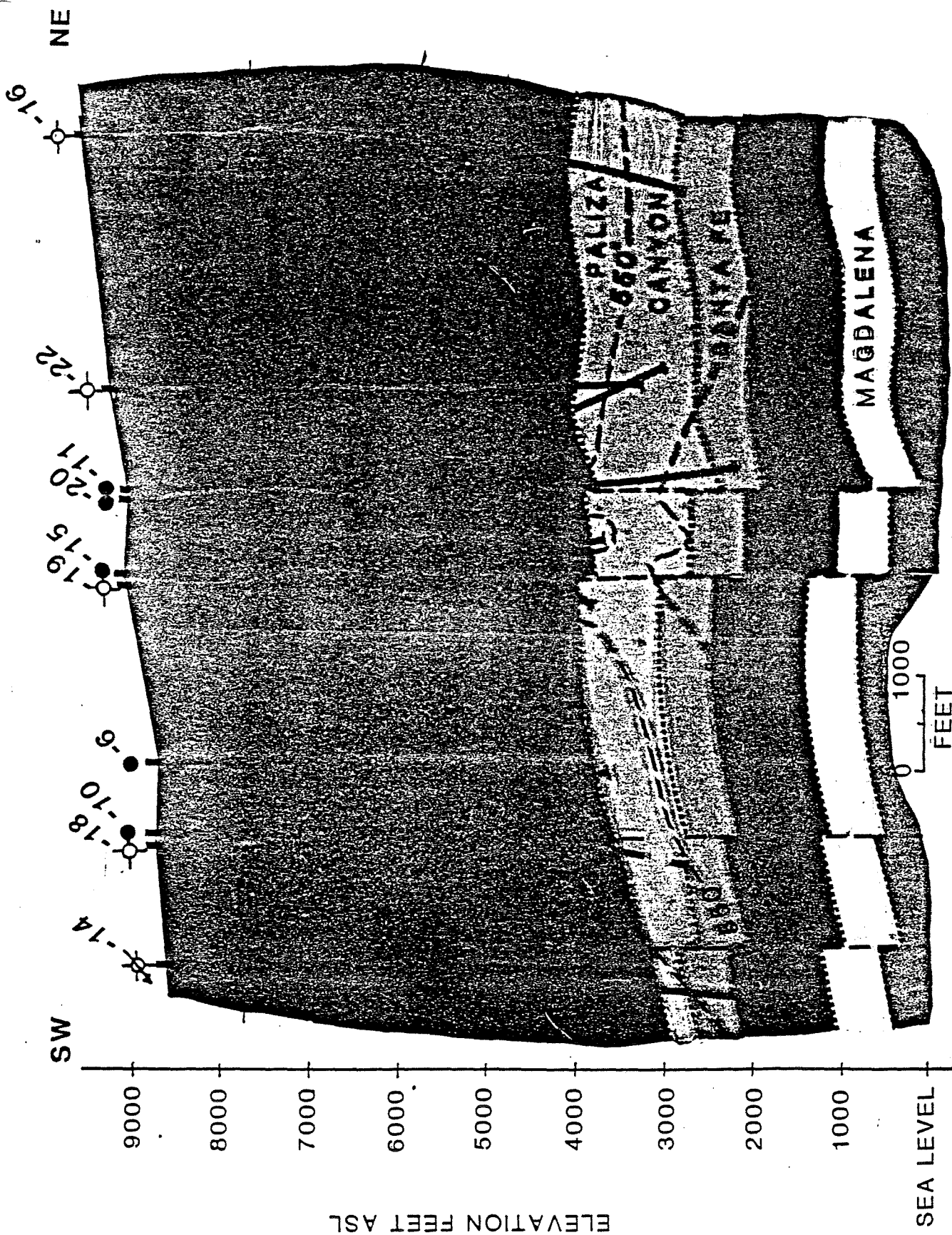
— NON-PRODUCER



— FAULT

ISOTHERM AT 4000' A S L





**GEOLOGIC & ISOTHERMAL CROSS SECTION OF
REDONDO CREEK BACA, NEW MEXICO**

UNION

**GEOHERMAL DIVISION
BACA PROSPECT**

WELL LOCATIONS

● OPEN WELL

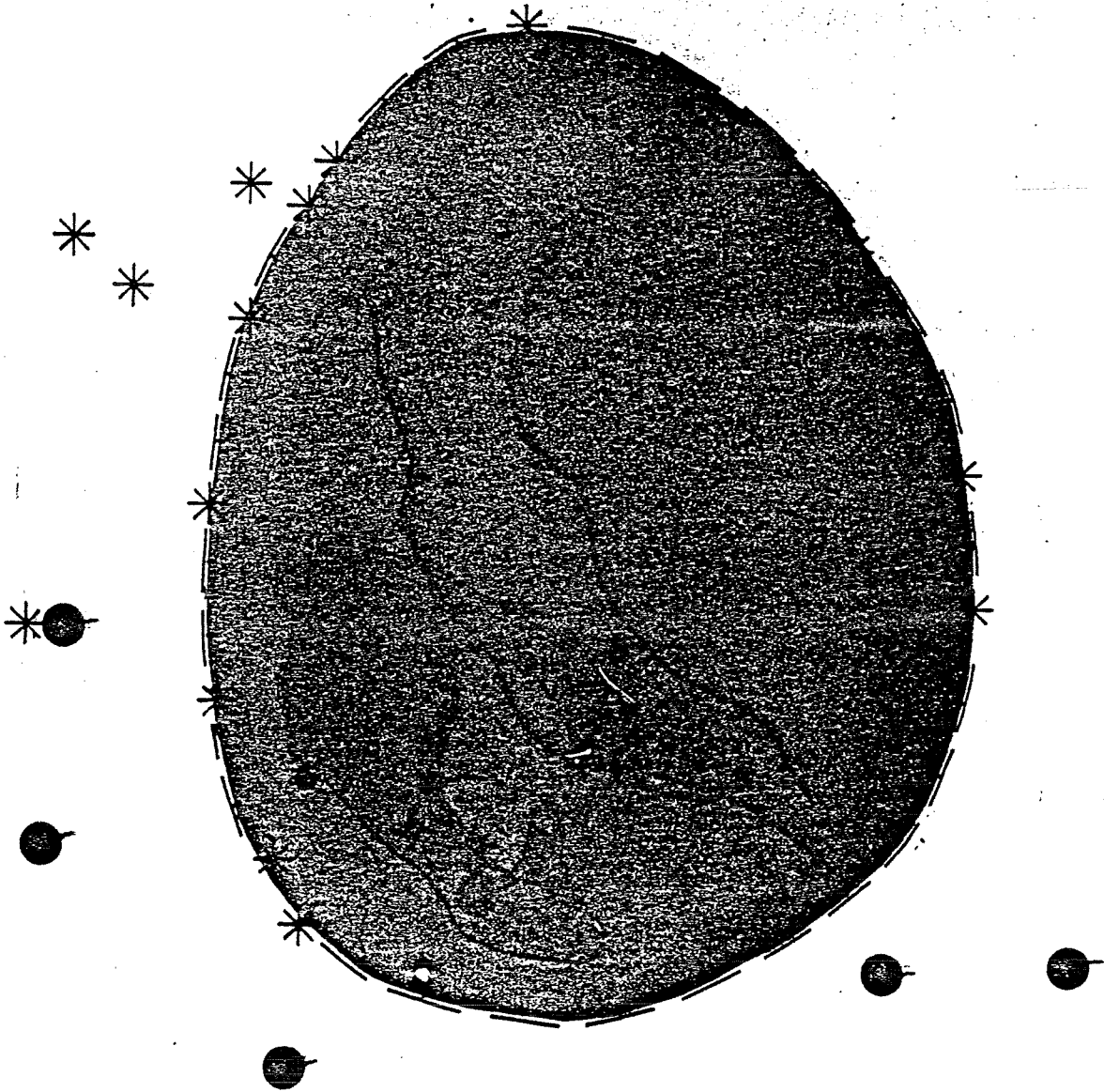
◆ ABANDONED WELL

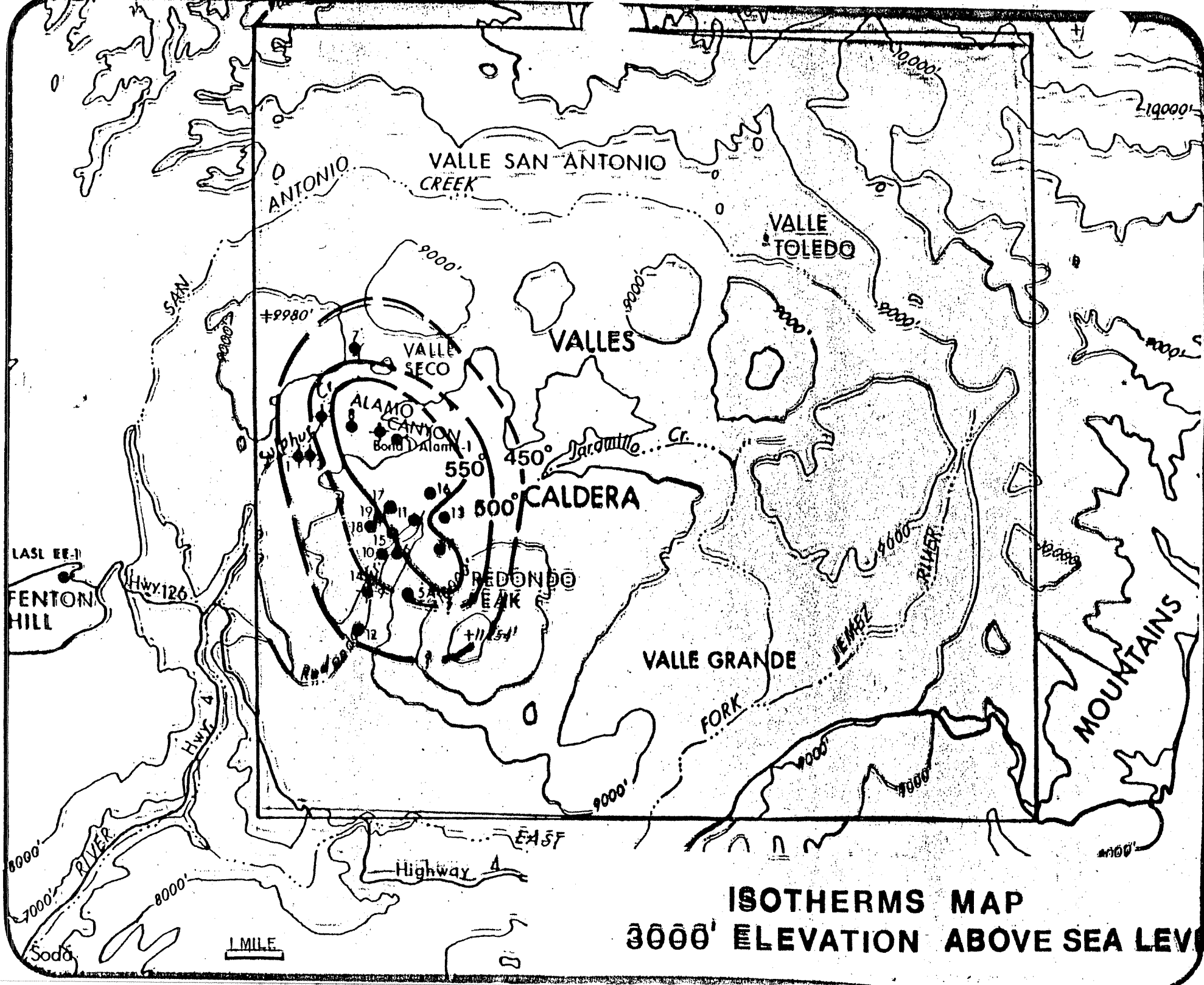
■ ACTIVE ALTERATION

● HOT SPRING

* RHYOLITE DOME

LONGITUDINAL GRABEN








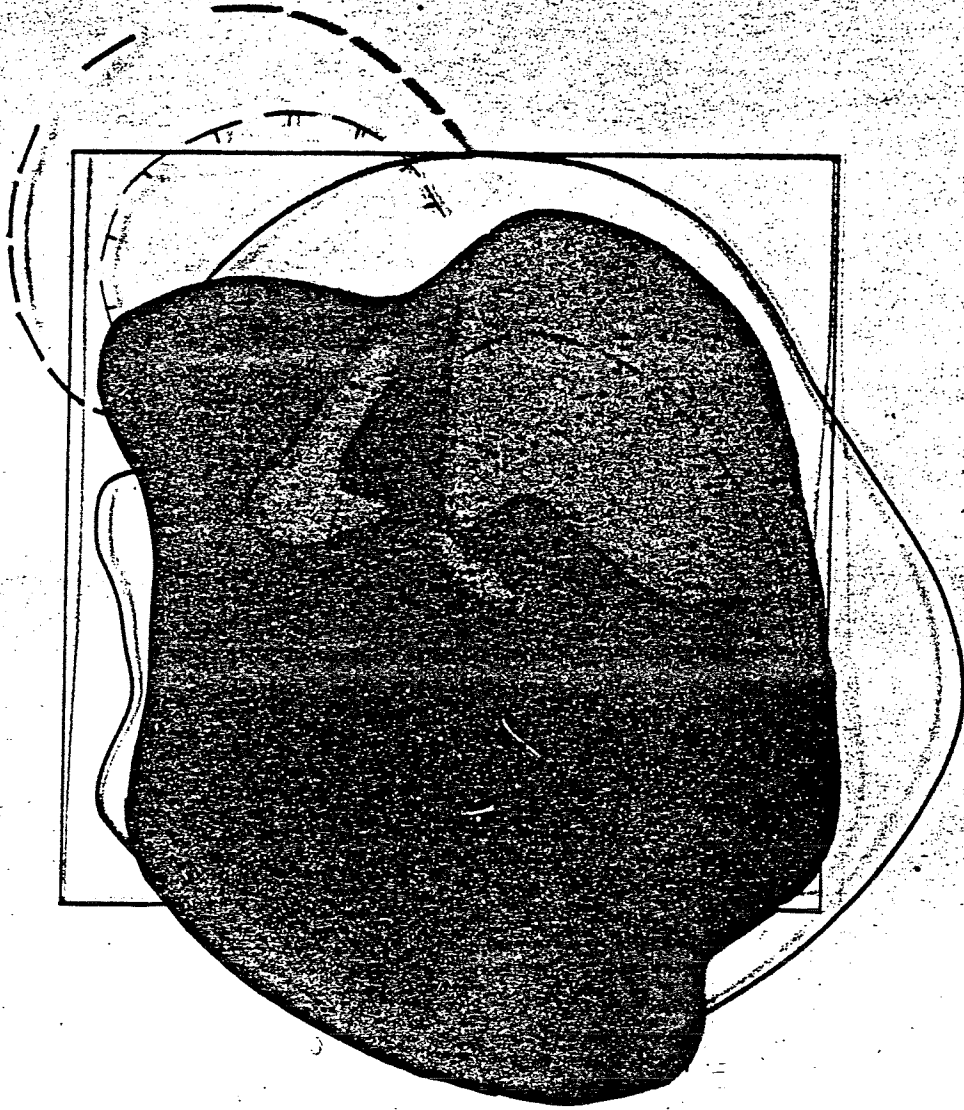


UNION

GEOHERMAL DIVISION BACA PROSPECT

CONDUCTANCE

-  < 25 MHOS
-  25-50 MHOS
-  50-100 MHOS
-  100-200 MHOS
-  > 200 MHOS

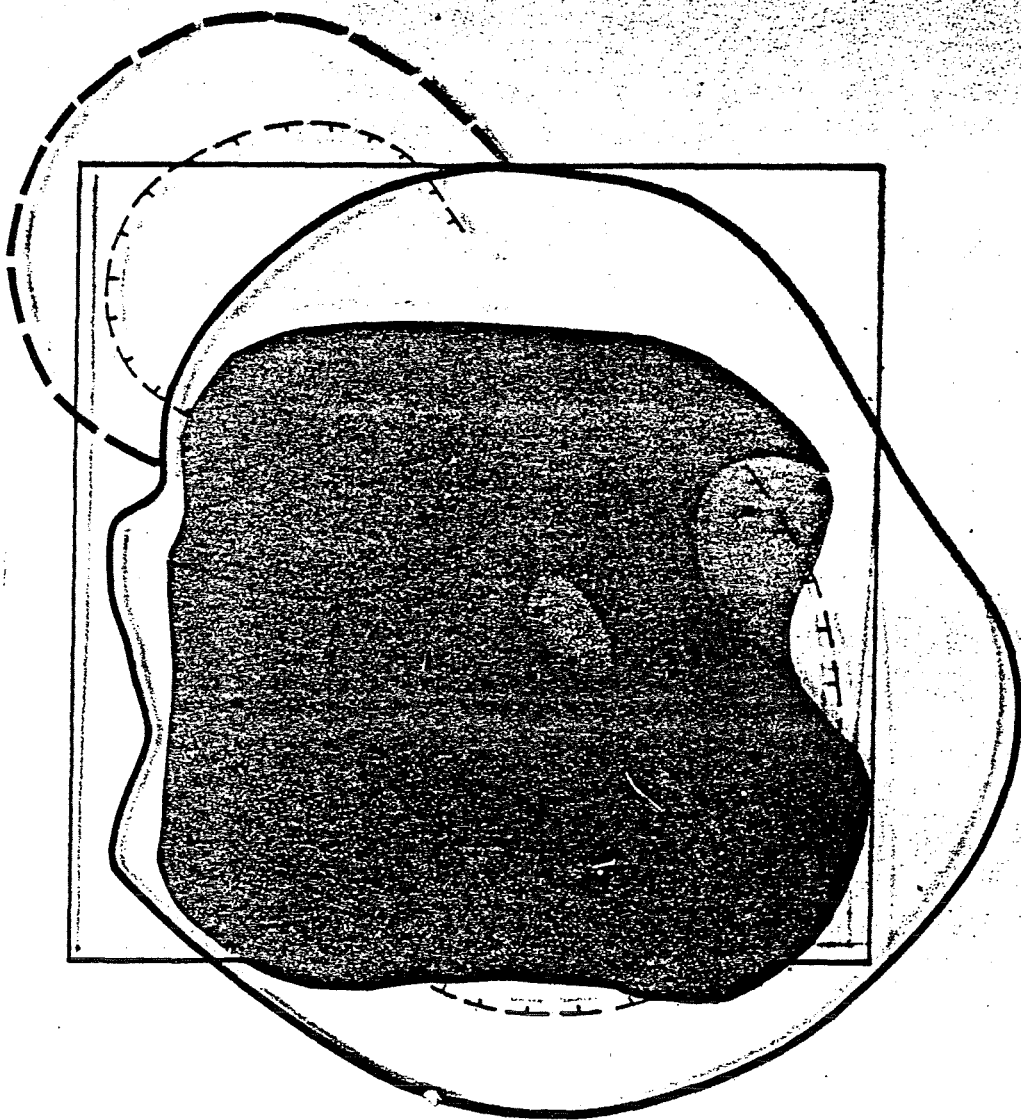
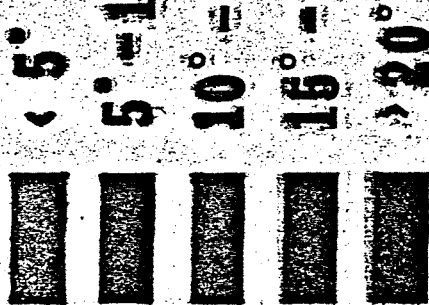


UNION

GEOHERMAL DIVISION BACA PROSPECT

TEMPERATURE GRADIENT FROM 150' - 250' IN F' / 100'

• Data Point

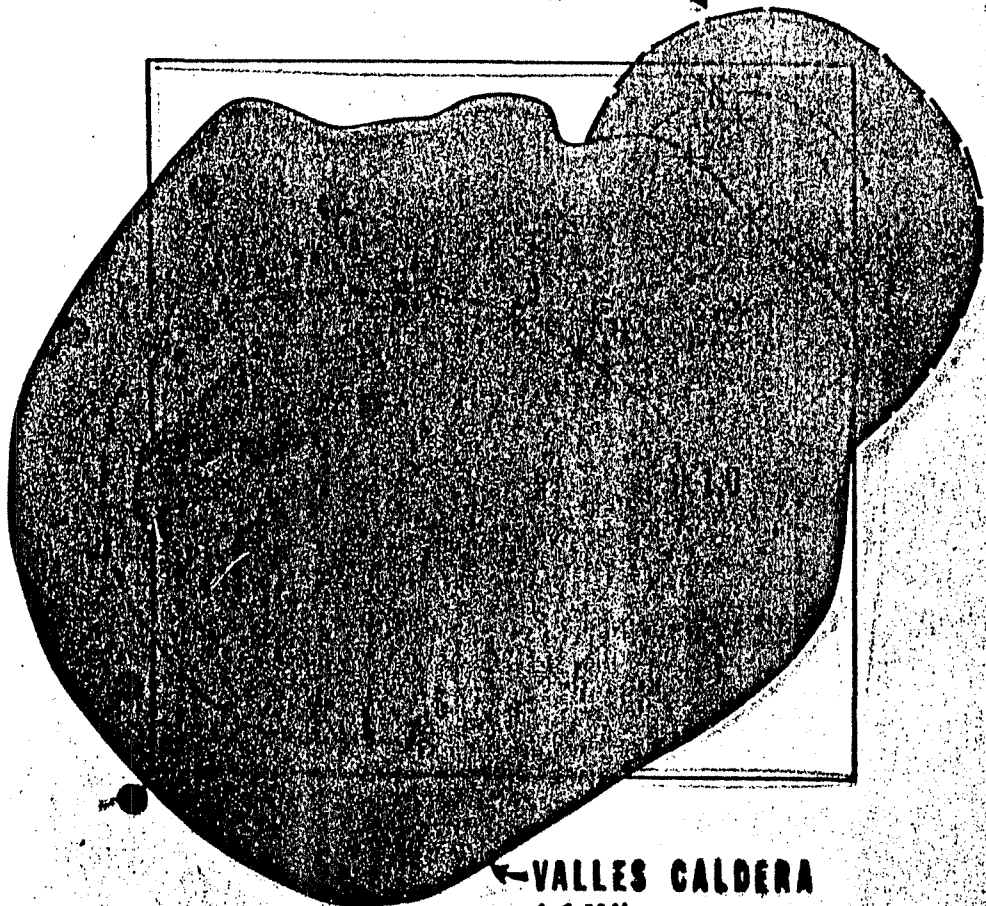


GEMINI



DIVISION

TOLEDO CALDERA
1.4 MY



← VALLES CALDERA
1.1 MY

UNION
GEOHERMAL DIVISION
BACA PROSPECT

**GEOHERMAL
FEATURES**

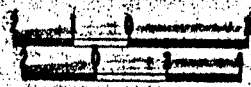
 **ACTIVE ALTERATION**

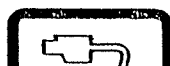
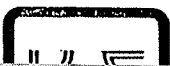
 **RHYOLITE DOME,
AGE (Million Years)**

 **HOT SPRING**

 **GAS SEEP**

 **RING FAULT**

 **MILES
KILOMETERS**



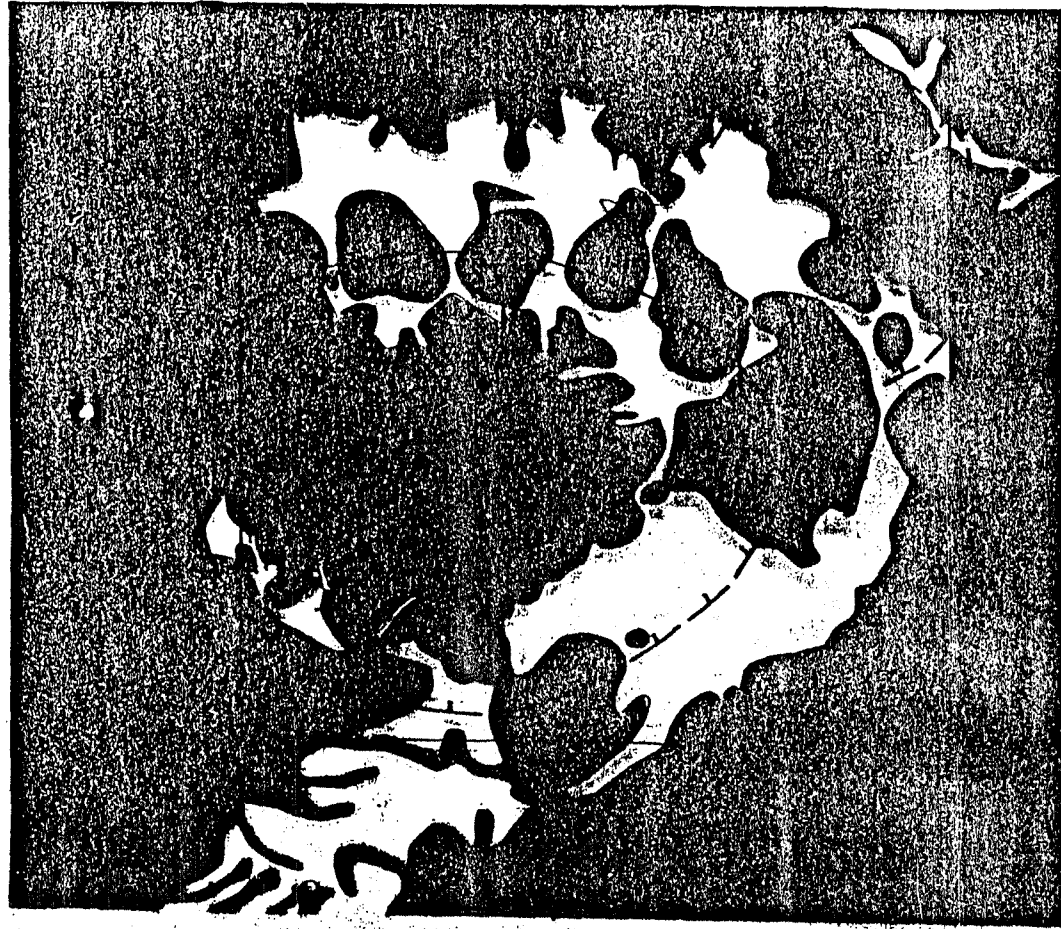
VISUAL







GEMINI

UNION 

**GEOHERMAL DIVISION
BACA PROSPECT**

**VALLES CALDERA
GEOLOGIC MAP**



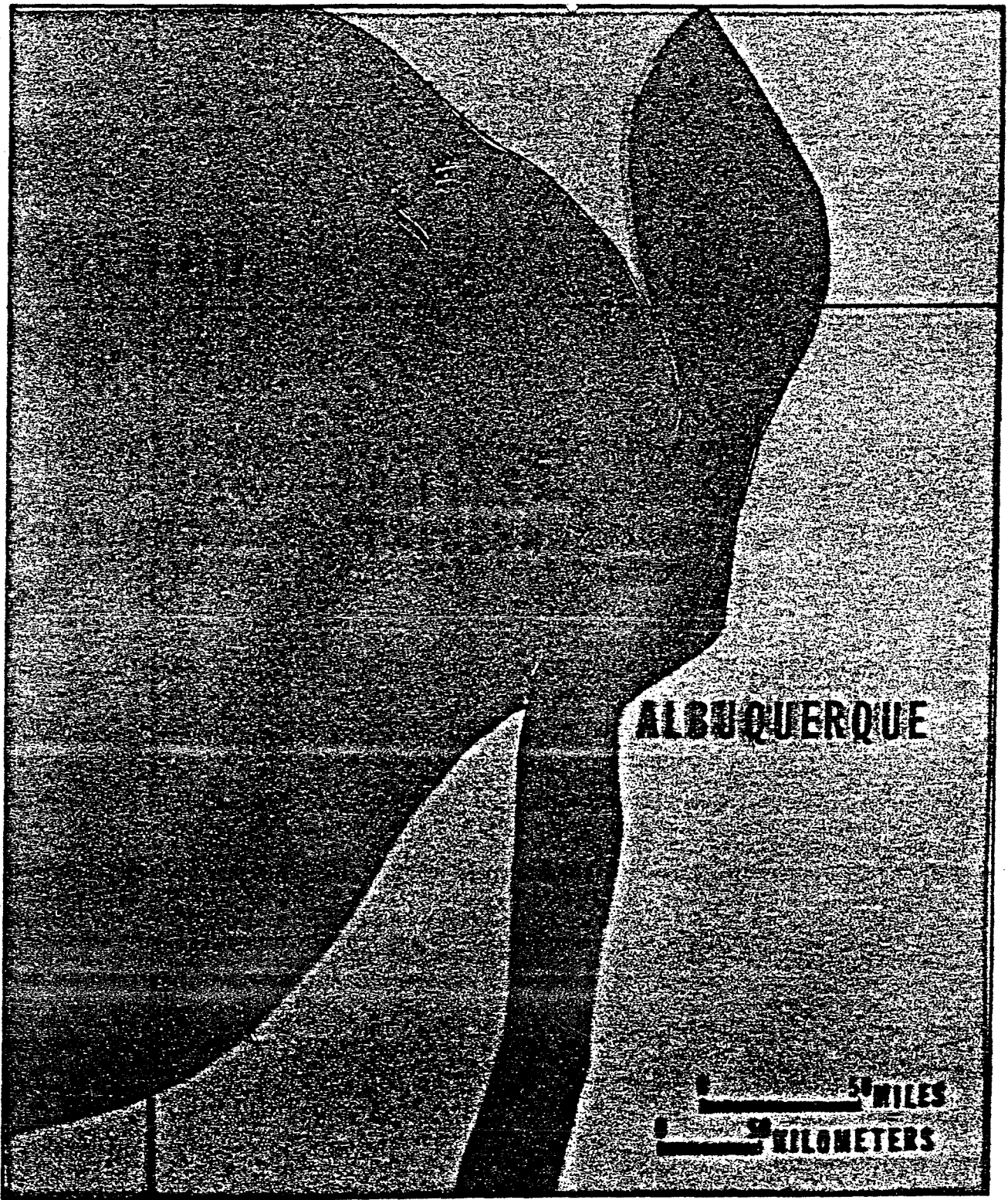
-  **UNDIVIDED RECENT SEDIMENTS**
-  **LATE STAGE RHYOLITE**
-  **CALDERA FILL**
-  **BANDELIER TUFF**
-  **TOLEDO VOLCANICS**
-  **UNDIVIDED PRE-CALDERA ROCKS**

 **FAULT**



GEMINI

UNION 76



UNION 76
GEOHERMAL DIVISION

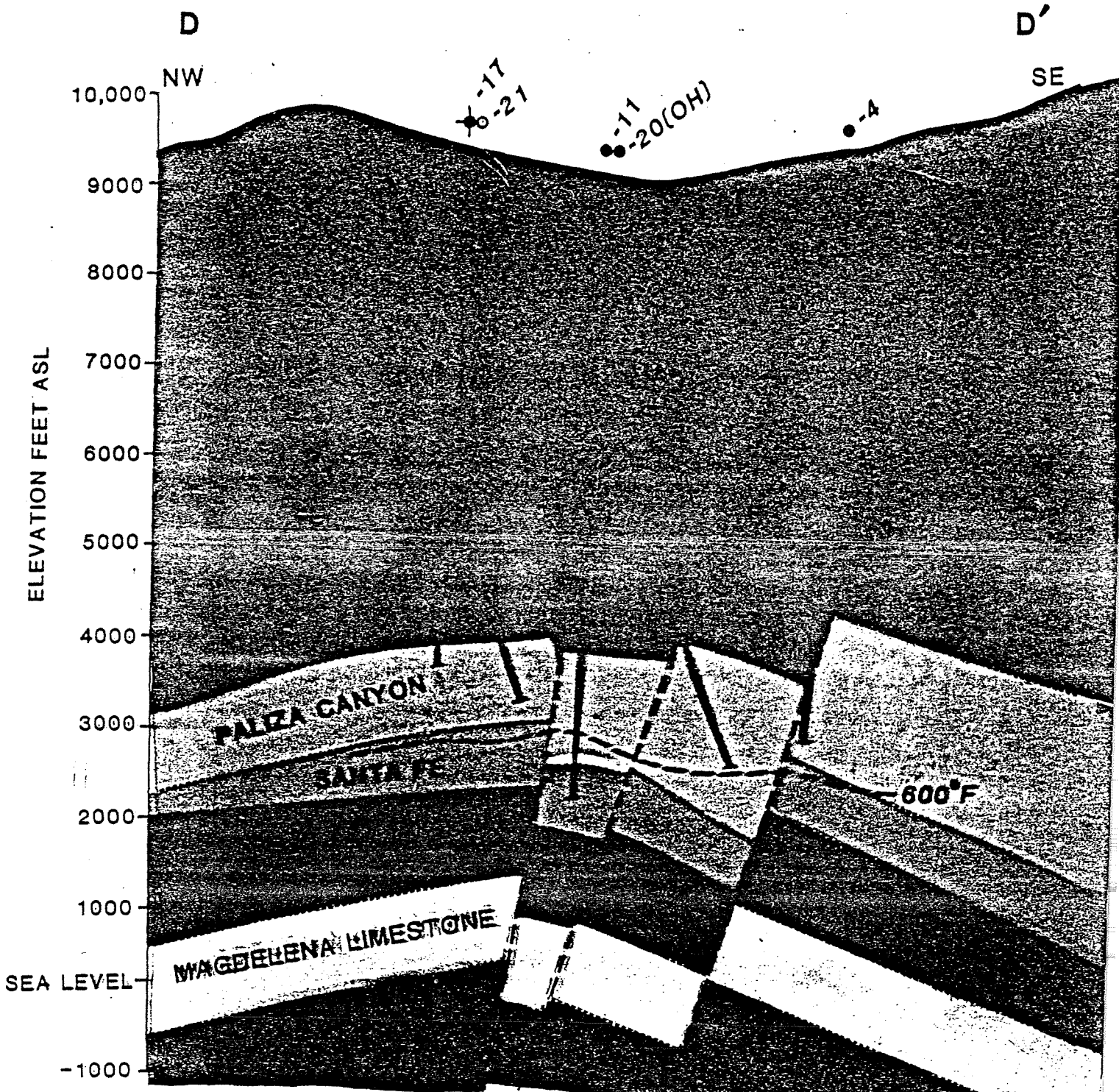
SUMMARY OF REDONDO CREEK

TOTAL WELLS 18

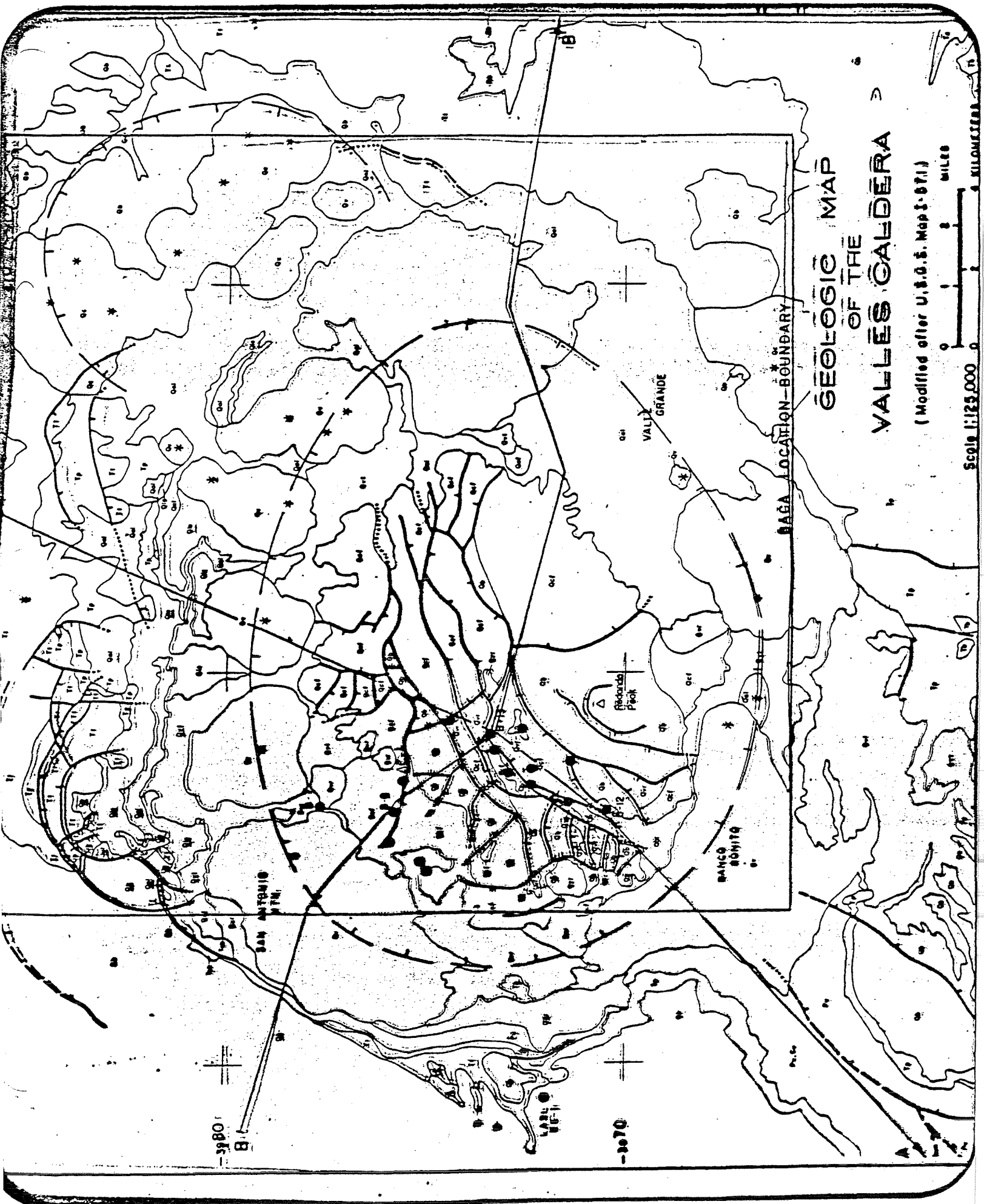
TOTAL HOLES 24

WELL STATUS

5	COMMERCIAL PRODUCERS	(350,000 LBS/HR STEAM)
1	ON TEST	
3	INJECTORS	
8	SUSPENDED	
1	ABANDONED	
<u>18</u>		



**GEOLOGIC & ISOTHERMAL CROSS SECTION of
REDONDO CREEK BACA, NEW MEXICO**



**GEOLOGIC MAP
OF THE
VALLES CALDERA**

(Modified after U.S.G.S. Map 5-5711)



BAGA LOCATION-BOUNDARY

-3980

-3070

BACA #16

R.C.



F(0)

F(13)

F(19)

F(3)

F(0)

A'

1000'

1000'

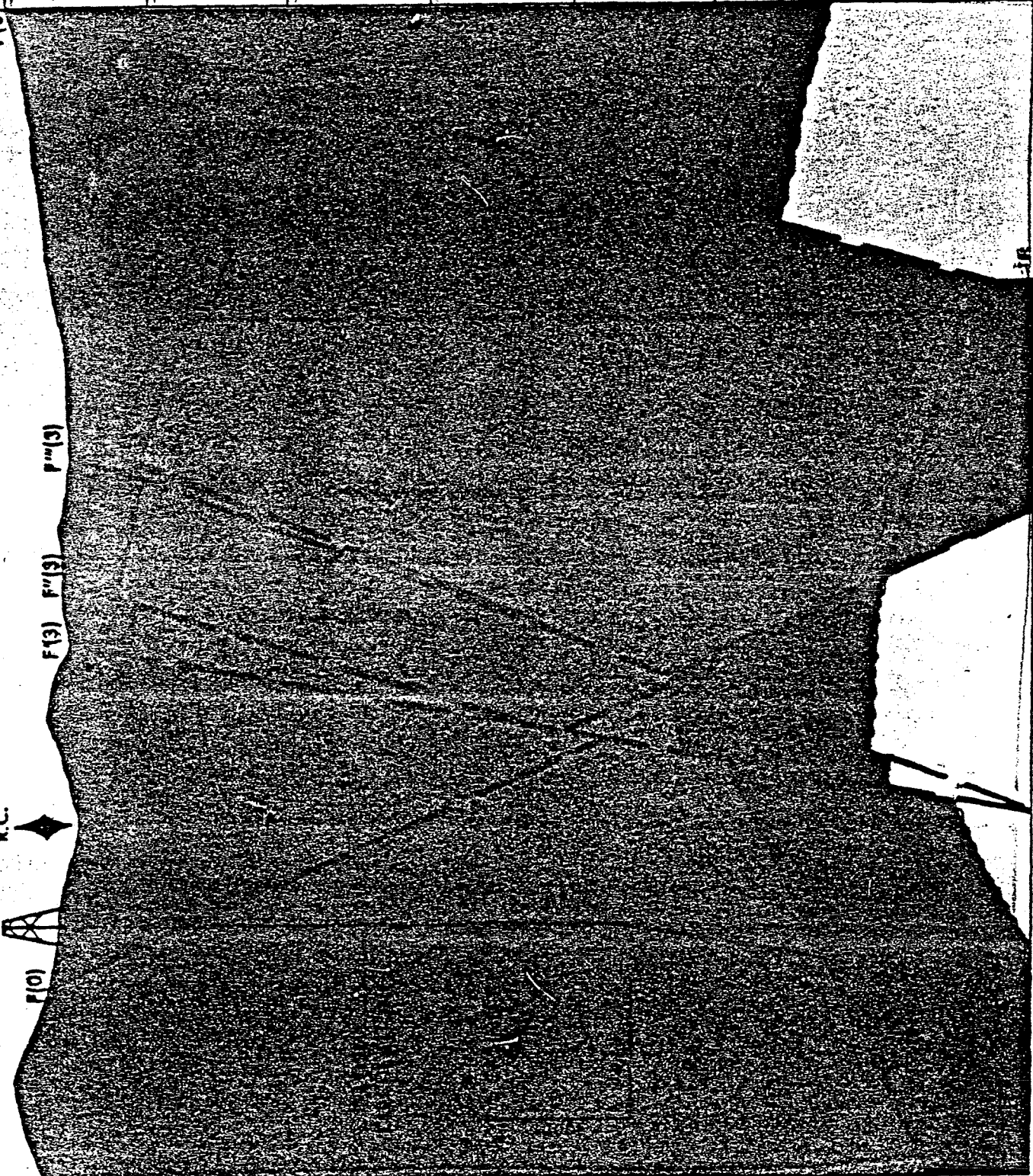
7000'

1000'

3000'

1000'

1000'



A

10,000' 8,000' 6,000' 4,000' 2,000' 2000'

BACA #4



F(16)

BACA #11

R.C.

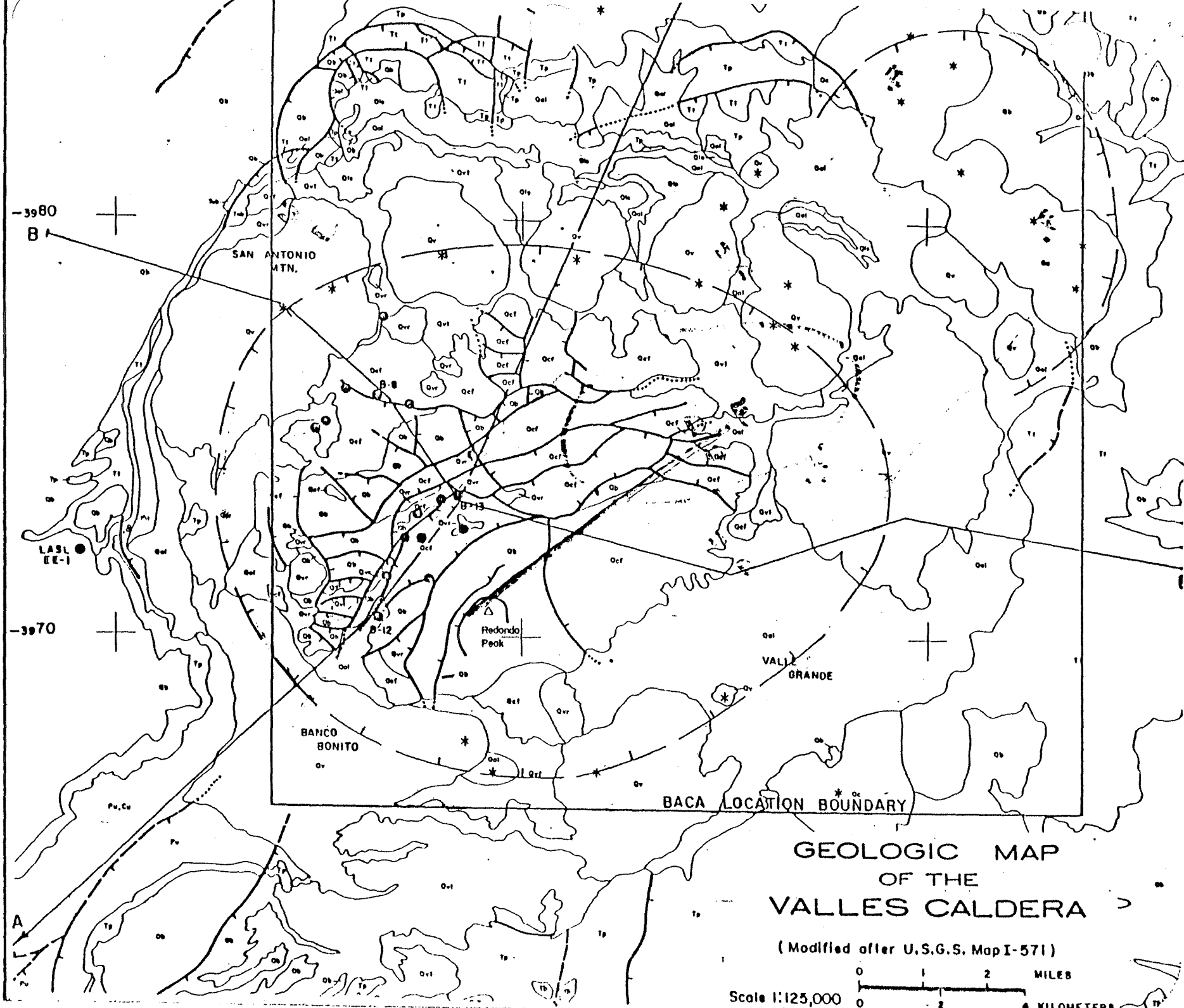


F(15) F(16)

C 572, 0-m

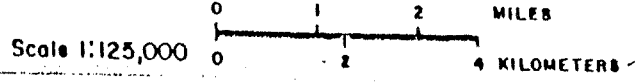
F(0)

D

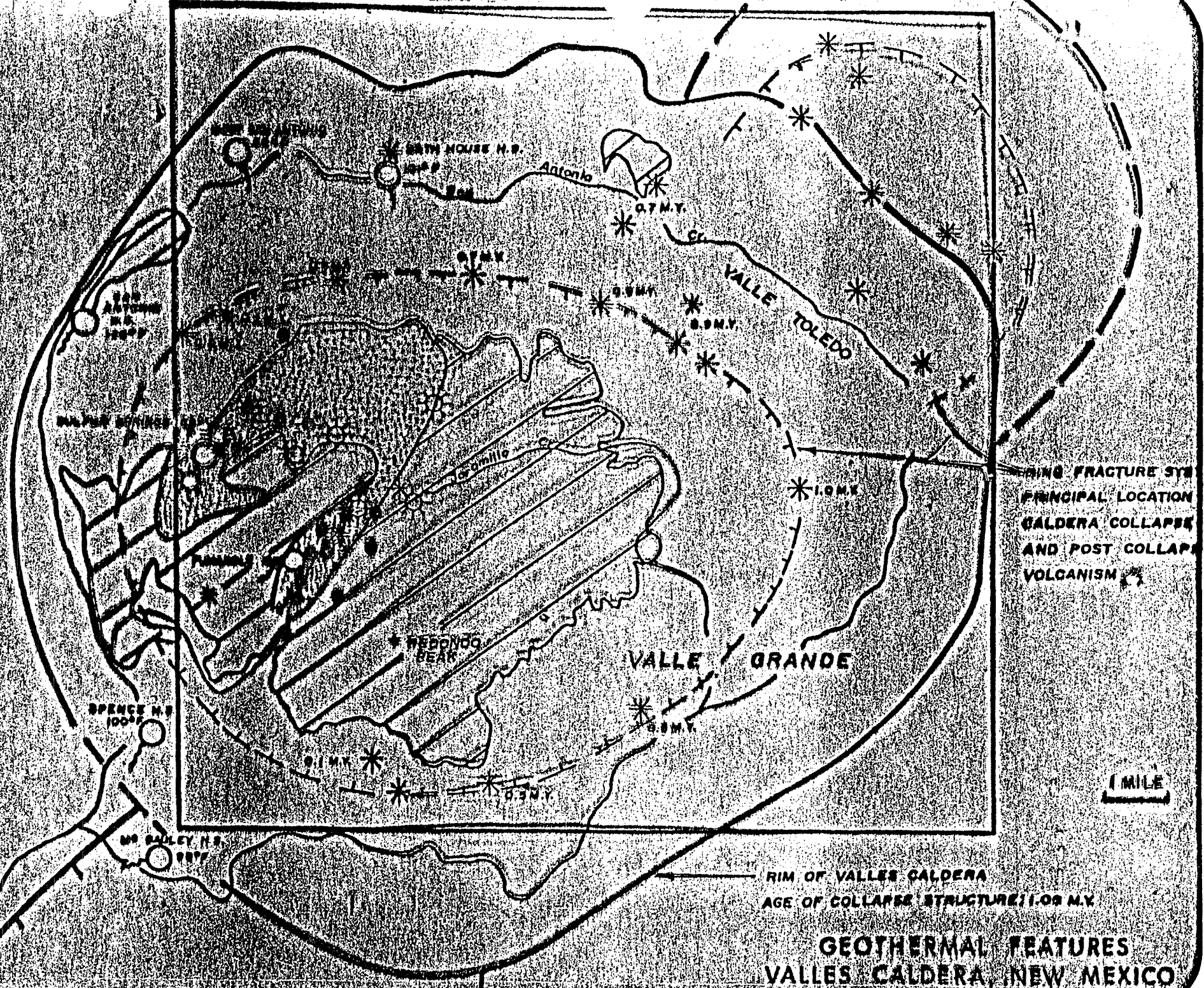


**GEOLOGIC MAP
OF THE
VALLES CALDERA**

(Modified after U.S.G.S. Map I-571)



BAGA LOCATION BOUNDARY



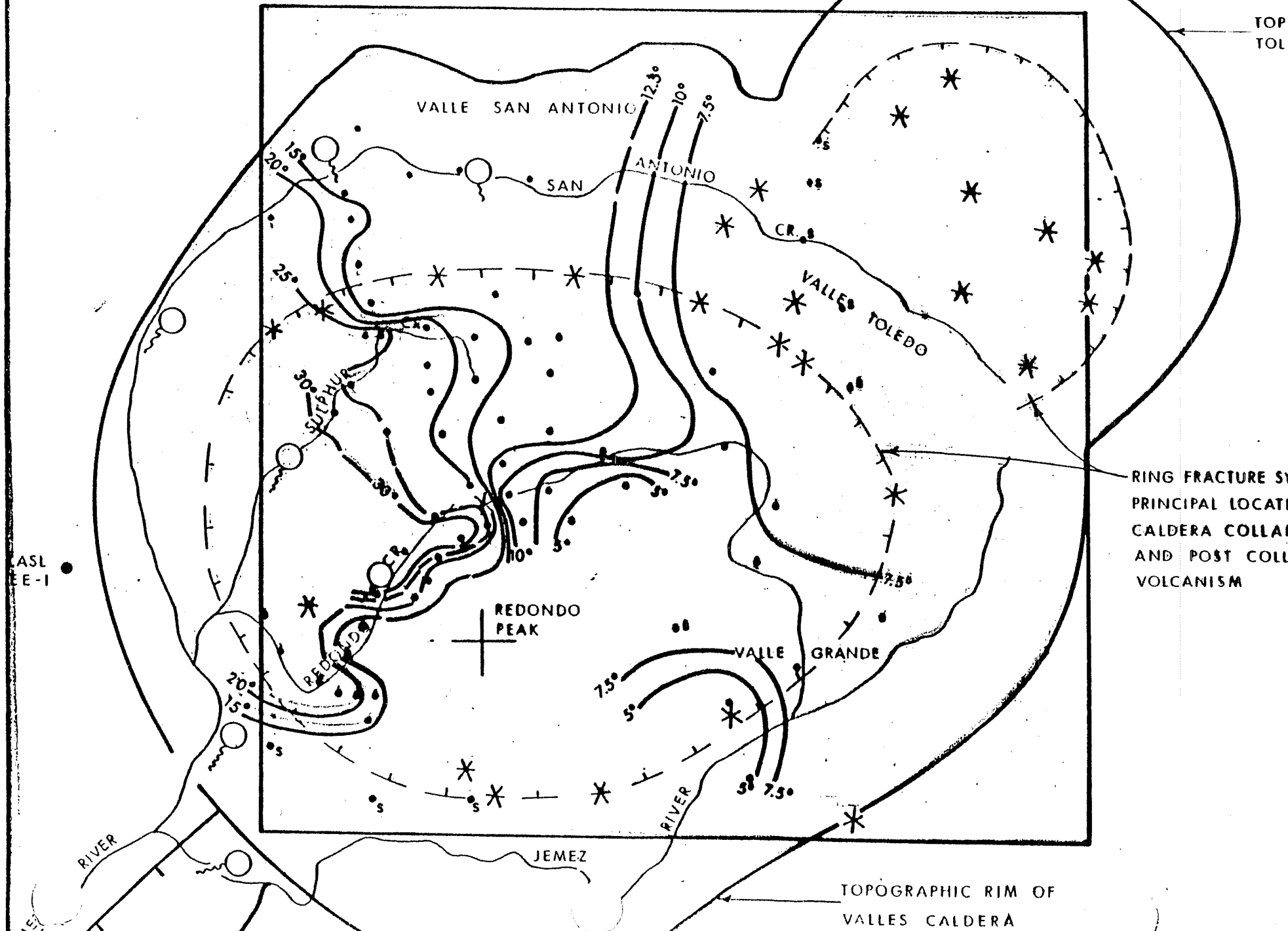
PRINCIPAL FRACTURE SYSTEM
 PRINCIPAL LOCATION
 CALDERA COLLAPSE
 AND POST COLLAPSE
 VOLCANISM

1 MILE

RIM OF VALLES CALDERA
 AGE OF COLLAPSE STRUCTURE 11.08 M.Y.

GEOTHERMAL FEATURES
 VALLES CALDERA, NEW MEXICO

BACA LOCATION BOUNDARY



TOP
TOL

RING FRACTURE SYSTEM
PRINCIPAL LOCATIONS
CALDERA COLLAPSE
AND POST COLLAPSE
VOLCANISM

TOPOGRAPHIC RIM OF
VALLES CALDERA

AVERAGE PRODUCED FLUID CHEMISTRY

	BRINE	CONDENSATE
pH	7.2	4.5
TDS mg/l	6093	29
SiO ₂	599	29
CO ₃ ⁼	19	0
HCO ₃ ⁻	127	6.6
S ⁻	2	8.6
SO ₄ ⁼	64	1.8
Cl ⁻	3061	17
Na	1749	9
K	370	1.4
Ca	15	0.4
Mg	0.3	0.2
Ba	0.05	0.04
B	23	0.8
F	6	<0.2

FLUID CHEMISTRY SUMMARY

Well BACA NO. 4

BRINE

	<u>Avg. Conc.</u>	<u>Range</u>	<u>No. of Samples</u>
pH	<u>6.7</u>	<u>6.5-7.2</u>	<u>3</u>
Suspended Solids, mg/l	<u> </u>	<u> </u>	<u>0</u>
Total Dissolved Solids, mg/l	<u>5100</u>	<u> </u>	<u>1</u>
SiO ₂ mg/l	<u>302</u>	<u>167-701</u>	<u>15</u>
CO ₃ ⁼ "	<u>0</u>	<u> </u>	<u>2</u>
HCO ₃ ⁻ "	<u>182</u>	<u>175-188</u>	<u>2</u>
S ⁻ "	<u> </u>	<u> </u>	<u>0</u>
SO ₄ ⁼ "	<u>42</u>	<u>30-53</u>	<u>2</u>
Cl ⁻ "	<u>2495</u>	<u>1560-2660</u>	<u>15</u>
Na "	<u>1473</u>	<u>950-1580</u>	<u>16</u>
K "	<u>300</u>	<u>198-311</u>	<u>16</u>
Ca "	<u>6.3</u>	<u>4.1-7.0</u>	<u>16</u>
Mg "	<u>0.3</u>	<u> </u>	<u>1</u>
Ba "	<u> </u>	<u> </u>	<u>0</u>
B "	<u>20</u>	<u>19-21</u>	<u>2</u>
F "	<u><0.02</u>	<u> </u>	<u>1</u>
Total Mass Flow, #/hr	<u>171,400</u>	<u>160,300-176,100</u>	
Steam Fraction, %	<u>26.8</u>	<u>24.4-29.4</u>	
Pressure, psig	<u>119.7</u>	<u>111-173.5</u>	

NONCONDENSIBLE GASES

% by wt.	<u>3.16</u> Avg.	<u> </u> Range	<u>1</u> No. of Samples
% by Vol.	<u> </u> Avg.	<u> </u> Range	<u>0</u> No. of Samples

	<u>ppm by weight</u>		<u>ppm by volume</u>		<u>No. of Samples</u>
	<u>Avg.</u>	<u>Range</u>	<u>Avg.</u>	<u>Range</u>	
CO ₂	<u>30,390</u>	<u> </u>	<u>12,430</u>	<u> </u>	<u>1</u>
H ₂ S	<u>165</u>	<u>117-213</u>	<u>87</u>	<u>62-112</u>	<u>2</u>
N ₂	<u>0</u>	<u> </u>	<u>0</u>	<u> </u>	<u>2</u>
H ₂	<u>1.4</u>	<u> </u>	<u>12.5</u>	<u> </u>	<u>2</u>
CH ₄	<u>2.8</u>	<u>2.2-3.4</u>	<u>3.2</u>	<u>2.5-3.8</u>	<u>2</u>

NOTE: Left out values obtained from diluted samples. CO₂ and H₂S concentrations are from total steam samples.

FLUID CHEMISTRY SUMMARY

Well BACA NO. 6

	BRINE		
	<u>Avg. Conc.</u>	<u>Range</u>	<u>No. of Samples</u>
pH	<u>7.4</u>	<u> </u>	<u>1</u>
Suspended Solids, mg/l	<u>26</u>	<u> </u>	<u>1</u>
Total Dissolved Solids, mg/l	<u>6018</u>	<u>5800-6230</u>	<u>5</u>
SiO ₂ mg/l	<u>453</u>	<u>160-600</u>	<u>3</u>
CO ₃ ⁼ "	<u>58</u>	<u>0 -93</u>	<u>3</u>
HCO ₃ ⁻ "	<u>84</u>	<u>68.8-99</u>	<u>2</u>
S ⁻ "	<u>1</u>	<u> </u>	<u>1</u>
SO ₄ ⁼ "	<u>30</u>	<u>29-32</u>	<u>4</u>
Cl ⁻ "	<u>3082</u>	<u>2860-3400</u>	<u>6</u>
Na "	<u>1721</u>	<u>1640-1780</u>	<u>5</u>
K "	<u>322</u>	<u>290-370</u>	<u>5</u>
Ca "	<u>8.5</u>	<u>0.1-12</u>	<u>4</u>
Mg "	<u>0.08</u>	<u> </u>	<u>1</u>
Ba "	<u> </u>	<u> </u>	<u>0</u>
B "	<u>20</u>	<u>17-21</u>	<u>3</u>
F "	<u>6.7</u>	<u> </u>	<u>1</u>
Total Mass Flow, #/hr	<u>163,700</u>	<u>148,500-181,600</u>	
Steam Fraction, %	<u>27.8</u>	<u>23.7-31.5</u>	
Pressure, psig	<u>60.4</u>	<u>38 - 96</u>	

NONCONDENSIBLE GASES

% by wt.	<u>1.33</u> Avg.	<u>1.27-1.38</u> Range	<u>2</u> No. of Samples
% by Vol.	<u>0.78</u> Avg.	<u>0.52-1.06</u> Range	<u>5</u> No. of Samples

	ppm by weight		ppm by volume		<u>No. of Samples</u>
	<u>Avg.</u>	<u>Range</u>	<u>Avg.</u>	<u>Range</u>	
CO ₂	<u>11,140</u>	<u>9,000-15,775</u>	<u>6450</u>	<u>(1 sample)</u>	<u>7</u>
H ₂ S	<u>99</u>	<u>69-257</u>	<u>136</u>	<u>(1 sample)</u>	<u>7</u>
N ₂	<u>2.5</u>	<u>0-5</u>	<u>1.5</u>	<u>0 - 3</u>	<u>2</u>
H ₂	<u>0.5</u>	<u>0.4-0.6</u>	<u>4.5</u>	<u>3.7-5.2</u>	<u>2</u>
CH ₄	<u>0</u>	<u> </u>	<u>0</u>	<u> </u>	<u>2</u>

NOTE: CO₂ and H₂S concentrations are from total steam samples.

FLUID CHEMISTRY SUMMARY

Well BACA NO. 11

BRINE

	<u>Avg. Conc.</u>	<u>Range</u>	<u>No. of Samples</u>
pH	<u>7.2</u>	<u>6.6-8.4</u>	<u>8</u>
Suspended Solids, mg/l	<u>616</u>	<u>522-688</u>	<u>3</u>
Total Dissolved Solids, mg/l	<u>6895</u>	<u>6056-7593</u>	<u>4</u>
SiO ₂ mg/l	<u>740</u>	<u>640-835</u>	<u>7</u>
CO ₃ ⁼ "	<u>11</u>	<u>0 - 48</u>	<u>8</u>
HCO ₃ ⁻ "	<u>99</u>	<u>24-150</u>	<u>8</u>
S ⁻ "	<u>4.1</u>	<u>1.5-6.5</u>	<u>4</u>
SO ₄ ⁼ "	<u>68</u>	<u>50-84</u>	<u>6</u>
Cl ⁻ "	<u>3453</u>	<u>2590-4400</u>	<u>8</u>
Na "	<u>1959</u>	<u>1810-2200</u>	<u>8</u>
K "	<u>456</u>	<u>340-550</u>	<u>8</u>
Ca "	<u>30</u>	<u>17-46</u>	<u>8</u>
Mg "	<u>0.14</u>	<u>0.07-0.2</u>	<u>7</u>
Ba "			<u>0</u>
B "	<u>28</u>	<u>24-35</u>	<u>7</u>
F "	<u>6.6</u>	<u>5-7.6</u>	<u>3</u>
Total Mass Flow, #/hr	<u>227,100</u>	<u>122,700-347,400</u>	
Steam Fraction, %	<u>39.7</u>	<u>24.2-50.3</u>	
Pressure, psig	<u>123.7</u>	<u>96-171</u>	

NONCONDENSIBLE GASES

% by wt.	<u>3.76</u> Avg.	<u>2.30-5.94</u> Range	<u>8</u> No. of Samples
% by Vol.	<u>1.60</u> Avg.	<u>0.96-2.54</u> Range	<u>7</u> No. of Samples

	<u>ppm by weight</u>		<u>ppm by volume</u>		<u>No. of Samples</u>
	<u>Avg.</u>	<u>Range</u>	<u>Avg.</u>	<u>Range</u>	
CO ₂	<u>49,250</u>	<u>33,700-89,100</u>	<u>20,220</u>	<u>13,775-36,450</u>	<u>6</u>
H ₂ S	<u>477</u>	<u>290-867</u>	<u>255</u>	<u>153-474</u>	<u>7</u>
N ₂	<u>132</u>	<u>0-381</u>	<u>86</u>	<u>0-245</u>	<u>8</u>
H ₂	<u>3.8</u>	<u>1.4-7.4</u>	<u>34.5</u>	<u>13-69</u>	<u>8</u>
CH ₄	<u>1.2</u>	<u>0-5.8</u>	<u>1.4</u>	<u>0-6.6</u>	<u>8</u>

NOTE: CO₂ and H₂S concentrations are from total steam samples.

FLUID CHEMISTRY SUMMARY

Well BACA NO. 13

	BRINE		
	<u>Avg. Conc.</u>	<u>Range</u>	<u>No. of Samples</u>
pH	<u>7.6</u>	<u>6.9-8.5</u>	<u>8</u>
Suspended Solids, mg/l	<u>360</u>	<u>5.5-734</u>	<u>3</u>
Total Dissolved Solids, mg/l	<u>6477</u>	<u>5500-8684</u>	<u>8</u>
SiO ₂ mg/l	<u>786</u>	<u>556-963</u>	<u>10</u>
CO ₃ ⁼ "	<u>28</u>	<u>0-97</u>	<u>8</u>
HCO ₃ ⁻ "	<u>214</u>	<u>163-281</u>	<u>8</u>
S ⁻ "	<u>2.2</u>	<u>1-4</u>	<u>5</u>
SO ₄ ⁼ "	<u>164</u>	<u>50-344</u>	<u>7</u>
Cl ⁻ "	<u>2783</u>	<u>2320-3300</u>	<u>8</u>
Na "	<u>1733</u>	<u>1500-2030</u>	<u>8</u>
K "	<u>329</u>	<u>278-394</u>	<u>8</u>
Ca "	<u>6.8</u>	<u>5-11</u>	<u>8</u>
Mg "	<u>0.49</u>	<u>0.04-1.5</u>	<u>6</u>
Ba "			<u>0</u>
B "	<u>22</u>	<u>19-24</u>	<u>8</u>
F "	<u>10.2</u>	<u>8-11.6</u>	<u>7</u>
Total Mass Flow, #/hr	<u>284,600</u>	<u>195,500-507,000</u>	
Steam Fraction, %	<u>28.4</u>	<u>26.8-30.2</u>	
Pressure, psig	<u>89.4</u>	<u>64-118</u>	

NONCONDENSIBLE GASES

% by wt.	<u>2.93</u> Avg.	<u>1.93-3.94</u> Range	<u>12</u> No. of Samples
% by Vol.	<u>1.23</u> Avg.	<u>0.80-1.64</u> Range	<u>12</u> No. of Samples

	ppm by weight		ppm by volume		<u>No. of Samples</u>
	<u>Avg.</u>	<u>Range</u>	<u>Avg.</u>	<u>Range</u>	
CO ₂	<u>38,520</u>	<u>30,040-45,200</u>	<u>15,830</u>	<u>12,300-18,900</u>	<u>5</u>
H ₂ S	<u>149</u>	<u>863-205</u>	<u>79</u>	<u>45.6-108</u>	<u>6</u>
N ₂	<u>33</u>	<u>0-122</u>	<u>24</u>	<u>0-114</u>	<u>14</u>
H ₂	<u>0.22</u>	<u>0-0.9</u>	<u>2.1</u>	<u>0-8.4</u>	<u>10</u>
CH ₄	<u>1.7</u>	<u>0-10</u>	<u>1.9</u>	<u>0-11</u>	<u>9</u>

NOTE: CO₂ and H₂S concentrations are from total steam samples.
Left out values obtained from low rate of two-rate test.

FLUID CHEMISTRY SUMMARY

Well BACA #15

BRINE

	<u>Avg. Conc.</u>	<u>Range</u>	<u>No. of Samples</u>
pH	6.9	6.5-7.3	6
Suspended Solids, mg/l	274	3-566	6
Total Dissolved Solids, mg/l	5,974	5390-6670	6
SiO ₂ mg/l	715	600-792	5
CO ₃ ⁼ "	0	0	6
HCO ₃ ⁻ "	54	37-67	6
S ⁻ "	.9	.1-1.6	5
SO ₄ ⁼ "	18	12-28	4
Cl ⁻ "	3,493	3220-3700	6
Na "	1,860	1730-1970	6
K "	445	407-481	6
Ca "	22	18-27	6
Mg "	.5	.07-.9	
Ba "	.05	.02-.09	6
B "	26	24-27	6
F "	6.7	5.9-7.9	9
Total Mass Flow, #/hr (Avg.)	150,000		
Steam Fraction, % (Avg.)	61		
Pressure, psig	73-202'		

NONCONDENSIBLE GASES

% by wt. of 1.35 Avg. 1.15-1.53 Range 6 No. of Samples
 steam phase
 % by Vol. .56 Avg. .48-.64 Range 6 No. of Samples

	<u>ppm by weight of N.C.</u>		<u>ppm by volume</u>		<u>No. of Samples</u>
	<u>Avg.</u>	<u>Range gases</u>	<u>Avg.</u>	<u>Range</u>	
CO ₂	11,971	9030-15,150	4,933	3650-6250	9
H ₂ S	131	107-162	70	57-86	9
N ₂	0		0		
H ₂	1.9	1.4-2.6	17	13-22	9
CH ₄	0		0		

TABLE 5

Baca #20 10/23/80

Composition of Condensate, Brine and Two Phase System

	<u>Condensate</u>	<u>Brine</u>	<u>2-Phase</u>
<u>Physical Properties</u>			
Specific Gravity @60°F	1.000	1.00050	1.0027
Conductivity, μ mhos/cm	-	7500	3700
Turbidity, NTU	-	0.6	-
<u>Solids</u>			
Settleable, ml/l	-	0.1	-
Suspended, mg/l	<2.0	8	<2.0
Total, mg/l	-	7487	-
Total Dissolved, mg/l	37	7068	3208
<u>Metals and Silicon</u>			
Arsenic, mg/l	nd<1.0	4.0	-
Aluminum, mg/l	-	0.1	-
Barium, mg/l	0.03	0.6	<.02
Beryllium, mg/l	-	<.01	-
Boron, mg/l	<1	33	15
Cadmium, mg/l	-	<.01	-
Calcium, mg/l	0.4	46	10
Chromium (Total), mg/l	-	<.002	-
Chromium VI, mg/l	-	nd<.002	-
Cobalt, mg/l	-	<.02	-
Copper, mg/l	-	0.04	-
Iron, mg/l	0.4	0.4	1.9
Lithium, mg/l	-	3.2	-
Lead, mg/l	-	0.7	-
Magnesium, mg/l	<0.5	<0.5	<0.5
Manganese, mg/l	-	0.5	-
Mercury, mg/l	-	<.0005	-
Molybdenum, mg/l	-	0.1	-
Nickel, mg/l	-	0.22	-
Potassium, mg/l	4.5	455	192
Selenium, mg/l	-	33	-
Silicon, mg/l	1.6	220	180
Silver, mg/l	-	0.03	-
Sodium, mg/l	11	2300	930
Vanadium, mg/l	-	<.03	-
Zinc, mg/l	-	0.7	-

TABLE 5 (cont.)

	<u>Condensate</u>	<u>Brine</u>	<u>2-Phase</u>
<u>Anions and pH</u>			
pH	3.9	6.0	4.9
Bicarbonate, mg/l	3	49	-
Carbonate, mg/l	0	0	0
Chloride, mg/l	12.3	3820	1650
Cyanide, mg/l	-	.01	-
Fluoride, mg/l	0.2	7.2	3.1
Nitrite (as N), mg/l	-	1	-
Phosphate, mg/l	-	0.03	-
Sulfide, mg/l	-	0.1	-
Sulfate, mg/l	1	89	27
<u>Ammonia, mg/l</u>	-	2	-
<u>Demand</u>			
BOD ₅ , mg/l	-	4.7	-
COD, mg/l	-	12	-
TOC, mg/l	-	7.3	-

TABLE 5

Composition of Condensate, Brine & Two-Phase System
 Baca #22, 2/9/81

	<u>Condensate</u>	<u>Brine</u>	<u>2-Phase</u>
<u>Physical Properties</u>			
Specific Gravity @60°F	1.000	1.0125	1.0020
Conductivity, μ mhos/cm	-	22,000	-
Turbidity, NTU	-	110	-
<u>Solids</u>			
Suspended, mg/l	<0.1	34	<0.1
Total, mg/l	-	14,690	-
Total Dissolved, mg/l	37	14,300	2.1
<u>Metals & Silicon</u>			
Arsenic, mg/l	0.13	4.54	-
Aluminum, "	-	0.3	-
Barium, "	0.01	0.04	0.05
Beryllium, "	-	0.01	-
Boron, "	0.2	68	0.1
Cadmium, "	-	nd<.01	-
Calcium, "	0.3	29	0.5
Chromium (Total), "	-	nd<.02	-
Chromium VI, "	-	nd<.002	-
Cobalt, "	-	nd<.03	-
Copper, "	-	0.03	-
Iron, "	0.30	0.25	0.4
Lithium, "	-	50	-
Lead, "	-	nd<.05	-
Magnesium, "	nd<.05	0.4	nd<.05
Manganese, "	-	0.03	-
Mercury, "	-	0.0005	-
Molybdenum, "	-	<0.1	-
Nickel, "	-	<.01	-
Potassium, "	1.3	770	1.7
Selenium, "	-	0.5	-
Silicon, "	<1	314	<10
Silver, "	-	<.02	-
Sodium, "	1.0	4,810	0.9
Vanadium, "	-	0.06	-
Zinc, "	-	1.3	-

TABLE 5 (cont.)

	<u>Condensate</u>	<u>Brine</u>	<u>2-Phase</u>
<u>Anions and pH</u>			
pH	5.2	8.2	5.2
Bicarbonate, mg/l	83	418	82
Carbonate, "	0	77	0
Chloride, "	2.1	7,880	5.1
Cyanide, "	-	<.01	-
Fluoride, "	<0.2	22	<0.2
Nitrite (as N), "	-	<.001	-
Phosphate (as P), "	-	0.22	-
Sulfide, "	-	12.6	28
Sulfate, "	56	170	2
<u>Ammonia, mg/l</u>	-	2.0	-
<u>Demand</u>			
BOD ₅ , mg/l	-	>324	-
COD, "	-	1,570	-
TOC, "	-	61	-

IUM AND POTASSIUM CONCENTRATIONS IN WA.

<u>WELL</u>	<u>TD AT TIME OF SAMPLING</u>	<u>SAMPLE TYPE</u>	<u>DATE REPORTED</u>	<u>Na PPM</u>	<u>K PPM</u>	<u>Na/K ATOMIC RATIO</u>	<u>AVG Na/K MULTIPLE SAMPLES</u>	<u>STD. DEV</u>
Baca 1	2560'	Flashed H ₂ O	06-24-63	400	37	18.39	4.89 (2)	0.48
	2560'	Stm. Condensate	06-13-63	83	27	5.23*		
	2560'	Stm. Condensate	06-18-63	83	31	4.55*		
Baca 2	No data available							
Baca 3	2200'	Flashed H ₂ O	07-24-64	1959	300	11.11		
Baca 4	1892'	Flashed H ₂ O	10-21-70	633	50	21.53*	24.21 (2)	3.79
	2408'	Flashed H ₂ O	10-21-70	917	58	26.89*		
	5048'	Flashed H ₂ O	11-16-70	2100	777	4.60*	8.40 (15)	0.19
	6376'	Flashed H ₂ O	08-22-73	1500	300	8.50		
	6376'	Flashed H ₂ O	Sept., Oct. 1973	1515**	309**	8.34**		
	6376'	Flashed H ₂ O	09-18-73	1580	300	8.96		
Baca 5A	2705'	Flashed H ₂ O	11-08-71	1832	210	14.84	16.71 (5)	2.83
	5684'	Flashed H ₂ O	11-08-71	1020	80	21.69		
	6022'	Flashed H ₂ O	11-08-71	1100	115	16.27		
	6107'	Flashed H ₂ O	11-08-71	1000	110	15.46		
	6793'	Flashed H ₂ O	11-08-71	1080	120	15.31		
Baca 6	2100'	Flashed H ₂ O	10-20-72	1680	280	10.21	9.41 (5)	0.93
	2431'	Flashed H ₂ O	10-20-72	1890	325	9.89		
	3225'	Flashed H ₂ O	10-20-72	2220	395	9.56		
	3715'	Flashed H ₂ O	10-20-72	1630	355	7.81		
	3715'	Flashed H ₂ O	02-13-73	535	95	9.58		

* Data not used in this study

** Average of 13 analyses taken during this period

LIUM AND POTASSIUM CONCENTRATIONS IN WA

<u>WELL</u>	<u>TD AT TIME OF SAMPLING</u>	<u>SAMPLE TYPE</u>	<u>DATE REPORTED</u>	<u>Na PPM</u>	<u>K PPM</u>	<u>Na/K ATOMIC RATIO</u>	<u>AVG Na/K MULTIPLE SAMPLES</u>	<u>STD. DEV</u>
Baca 7	No data available							
Baca 8	2995'	2-Phase Flow	10-20-72	2170	565	6.53	6.33(2)	0.29
	4380'	Flashed H ₂ O	10-20-72	2160	600	6.12		
Baca 9, 10	No data available							
Baca 11	6924'	Flashed H ₂ O	Jan. 1976	2000	463	7.35	6.95(6)	0.41
	6924'	2-Phase Flow	Jan. 1976	1950	455	7.29		
	6924'	Flashed H ₂ O	Feb. 1976	1810	430	7.16		
	6924'	2-Phase Flow	Feb. 1976	1240	302	6.98		
	6924'	Flashed H ₂ O	Apr. 1976	2010	541	6.32		
	6924'	2-Phase Flow	Apr. 1976	2080	535	6.61		
Baca 12, 14, 16	No data available							
Baca 13	8228'	Flashed H ₂ O	Jan. 1976	1700	338	8.55	8.77(6)	0.30
	8228'	2-Phase Flow	Jan. 1976	1575	300	8.93		
	8228'	Flashed H ₂ O	Feb. 1976	1620	328	8.40		
	8228'	2-Phase Flow	Feb. 1976	1550	306	8.62		
	8228'	Flashed H ₂ O	Apr. 1976	1550	296	8.91		
	8228'	2-Phase Flow	Apr. 1976	1600	295	9.22		
Baca 15	5505'	Flashed H ₂ O	10-24-76	1950	470	7.06	7.10(2)	0.05
	5505'	2-Phase Flow	10-24-76	1900	453	7.13		

	<u>Na (PPM)</u>	<u>K (PPM)</u>	<u>Na/K</u> <u>ATOMIC RATIO</u>
BACA 20			
BRINE	2300	455	8.60
CONDENSATE	2300	4.5	4.16

BACA 22			
BRINE	4800	770	10.62
CONDENSATE	1.0	1.3	1.31

Na-K-Ca Geothermometer Indicated Temperatures

Well	Date	Concentrations (ppm)			Indicated Temperature (°F)
		Na	K	Ca	
Baca 4	9/18/73	1580	300	7.0	615
	9/21/73	1500	305	6.8	626
	9/24/73	1500	307	6.7	627
	9/28/73	1500	307	6.6	628
	10/01/73	1525	310	6.4	628
	10/05/73	1525	310	7.0	626
	10/08/73	1500	307	6.4	629
	10/12/73	950	198	4.1	632
	10/15/73	1525	311	6.4	629
	10/19/73	1450	307	6.2	635
	10/22/73	1525	310	6.3	629
	10/26/73	1525	305	6.2	626
	10/29/73	1525	311	6.4	629
	11/02/73	1550	310	6.4	626
	11/05/73	1550	311	6.4	626
	11/09/73	1330	292	5.4	643
	Baca 5	8/24/71	1832	210	19.2
Baca 6	10/11/72	1640	370	0.1	789
	11/09/72	259	25	1.0	515
	10/27/72	1770	319	11	597
	11/07/72	1780	331	11	602
	6/13/75	1900	363	17	596
	11/09/75	1700	300	12	590
Baca 11	12/22/73	1920	360	32	577
	12/22/73	1930	340	32	567
	9/16/74	1900	483	23	636
	9/20/74	1900	483	25	634
	11/08/75	2200	550	46	618
	1/12/76	2000	463	27	617
	2/24/76	1810	430	17	632
	4/08/76	2010	541	36	635
Baca 13	12/07/74	2000	278	5	579
	12/07/74	2030	394	11	613
	12/07/74	1890	377	11	616
	10/15/75	1570	317	5	635
	11/07/75	1500	305	5	635
	1/11/76	1700	338	6	629
	2/26/76	1620	328	6	631
	4/07/76	1550	296	5	625

% wt in total
mass flow

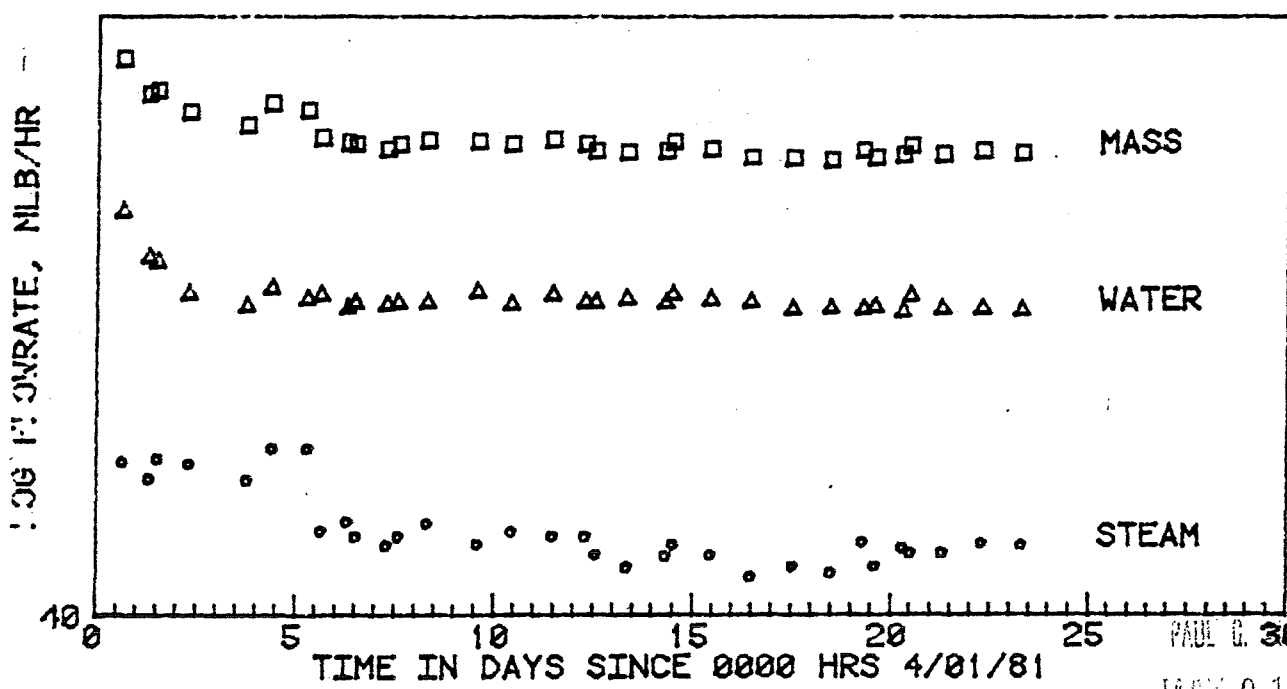
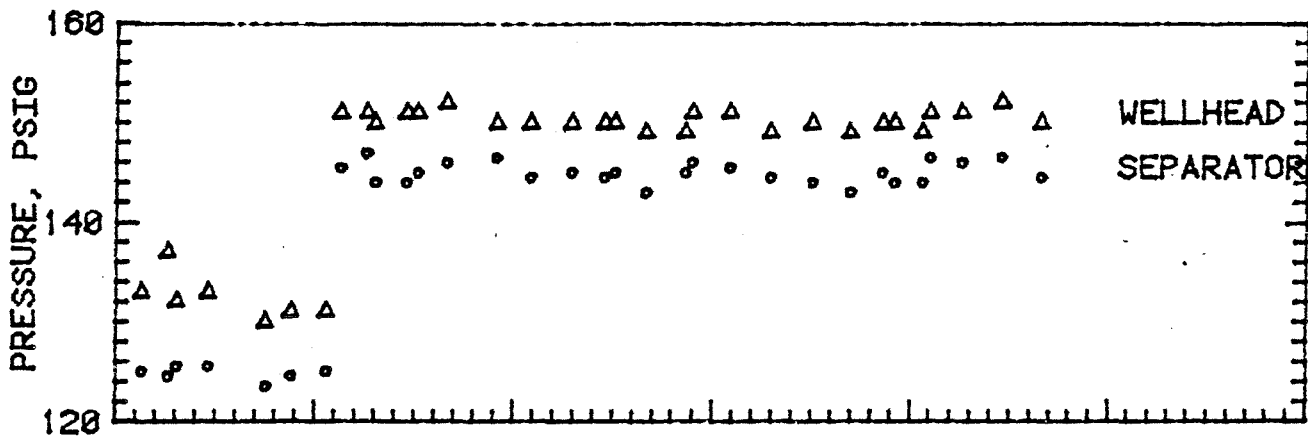
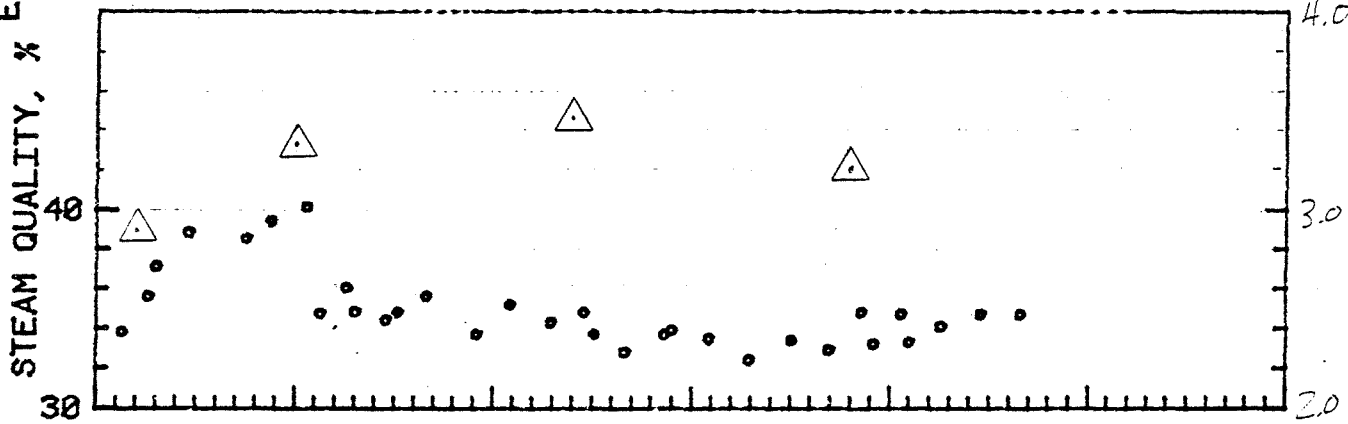
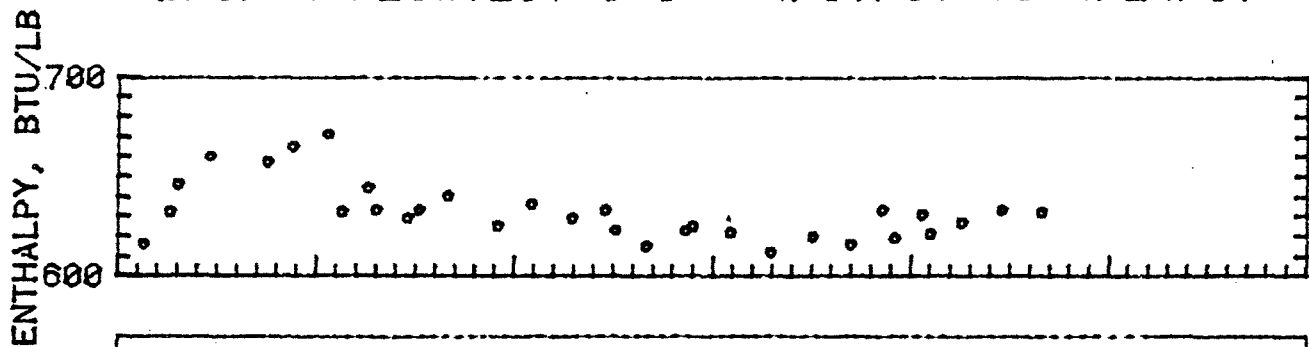
TABLE 7
Average Concentrations of Various Chemical Constituents in Well Effluents

Well	Avg. TDS In Brine	Avg. TDS In Condensate	Silica (ppm) In Brine	Noncondensable Gas % by Wt. of Steam Phase		H ₂ S Concentration (ppm)		Average	
						Noncondensable	Total Steam	Flash %	Flowrate lbs/hr Total
Baca 4	5100	28	302 (167-701)	3.16 3.22	.85 1.10	165 (150-180)	165 (117-213)	26.8 34.0	171,400
Baca 6	6018 (5800-6230)	23 (3-65)	453 (160-600)	1.33 (1.27-1.38)	.37	61 (60-61)	99 (69-257)	27.8	163,700
Baca 11	6895 (6056-7593)	59 (7-105)	740 (640-835)	3.76 (2.30-5.94)	1.5	365 (222-564)	477 (290-867)	39.7	227,100
Baca 13	6477 (5500-8684)	13 (7-25)	786 (556-963)	2.93 (1.93-3.94)	.83 3.9	81 (57-96)	149 (86.3-205)	28.4 27.5	284,600
Baca 20				2.54	1.47		135	58.0	

NOTE: 1. Some samples from Baca 4 were diluted prior to analysis. The results from these analyses are not included in the above.

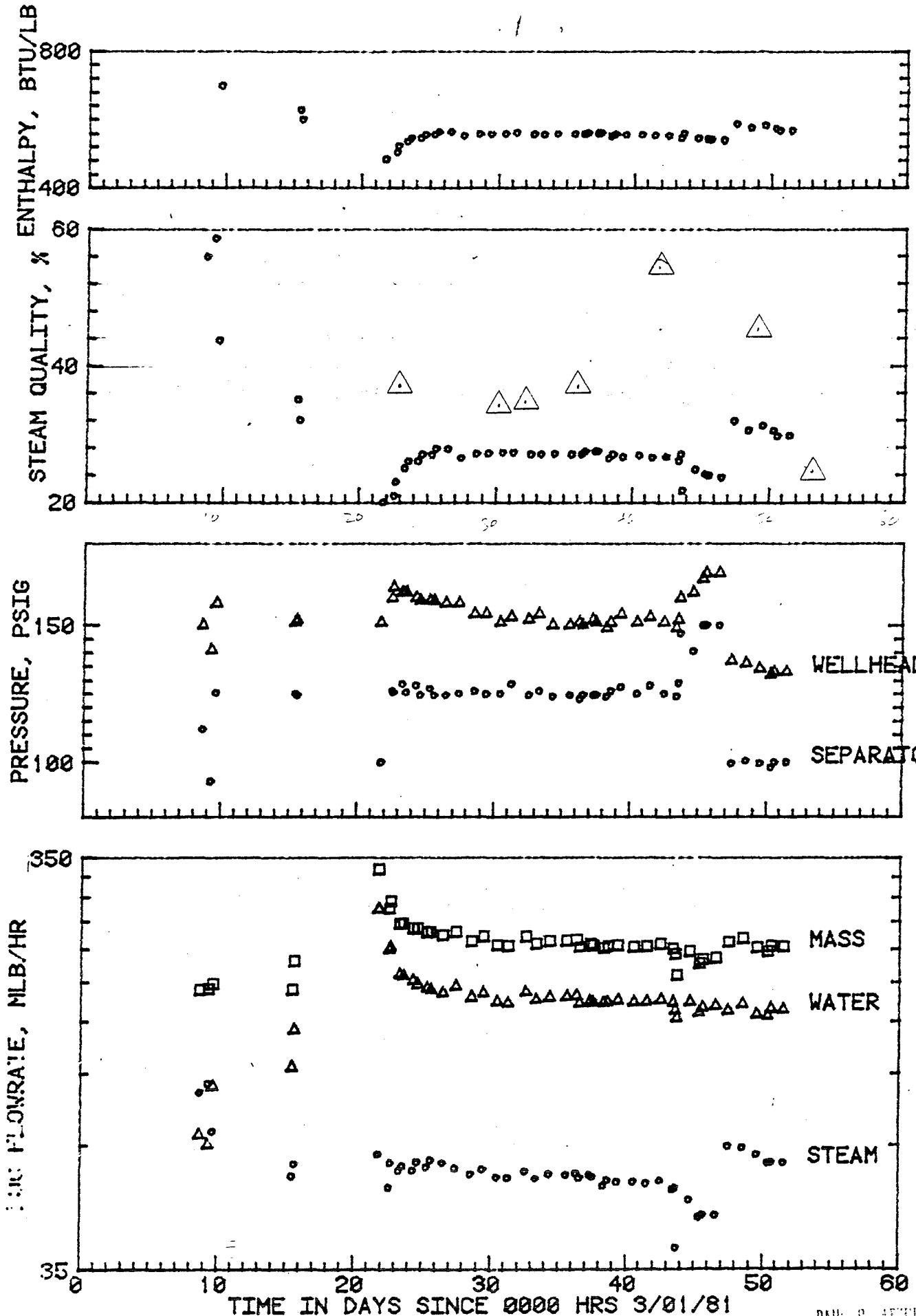
2. Left out values obtained from low rate of two-rate test on Baca 13.

BACA 4 FLOWTEST # 3 - 4/01/81 TO 4/24/81



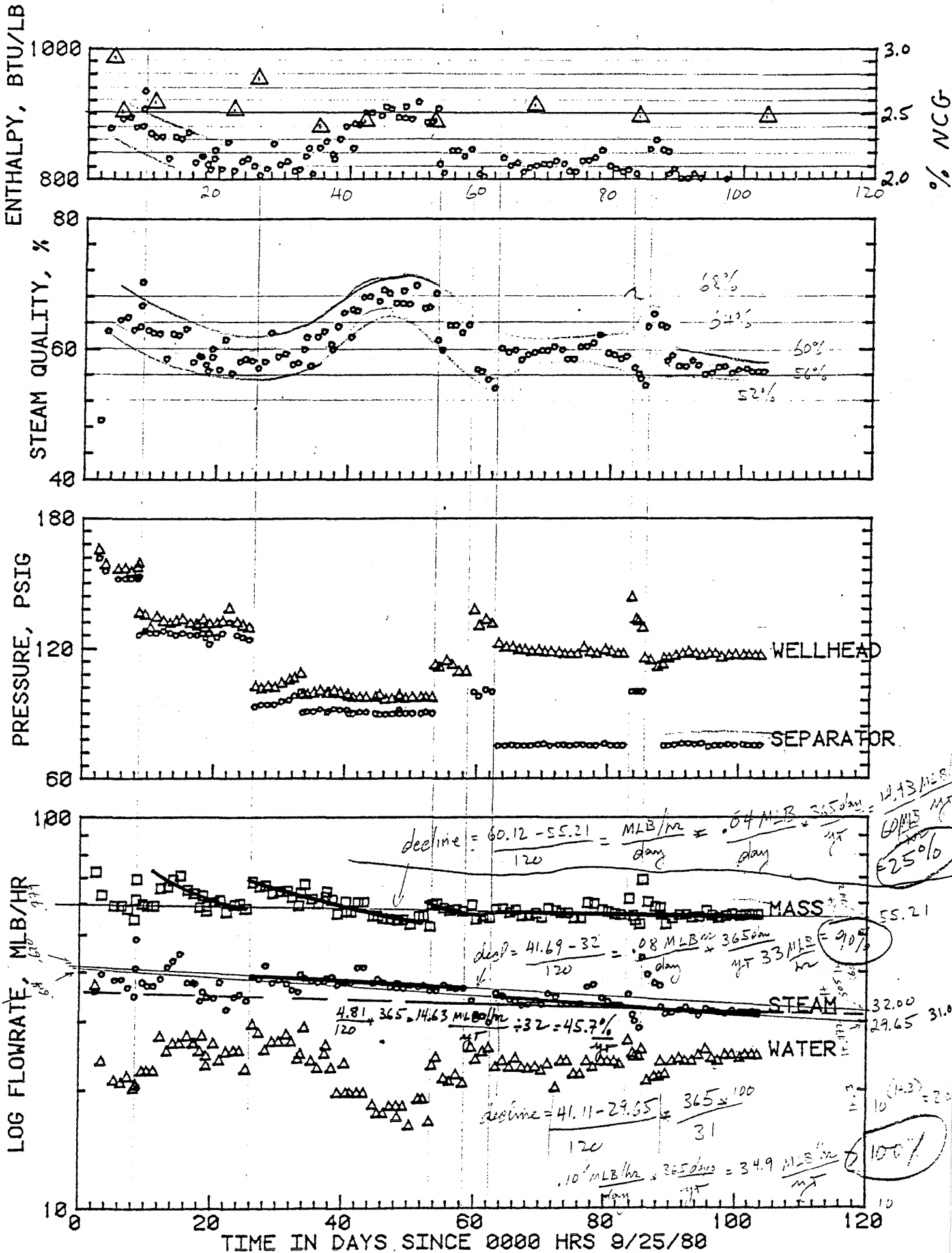
16 wt Noncondensable Gas in Steam

BACA 13 FLOWTEST # 5 - 3/05/81 TO 4/21/81



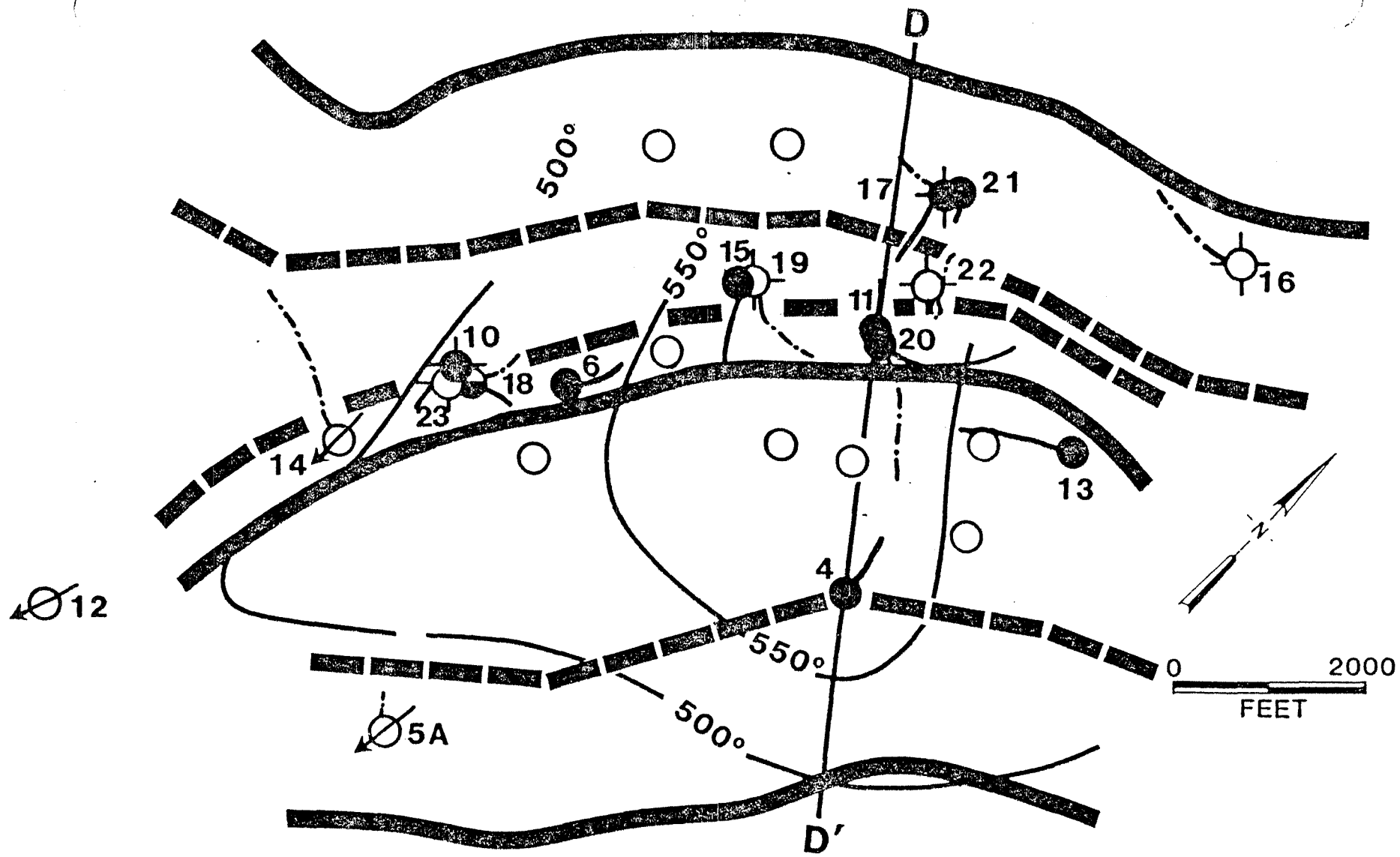
5%
4%
3%
Noncondensable Gas in Steam, wt.

BACA 20 FLOWTEST #4: 9/26/80 - 1/06/81



35.89
41.11 41.69 60.12

14.43 MLB/yr
29.65 MLB/yr
34.9 MLB/yr
25%
90%
100%
n = 10 (4.3) = 20



REDONDO CREEK AREA

MAJOR FAULT

Trace at Surface

Trace at 3750' ASL

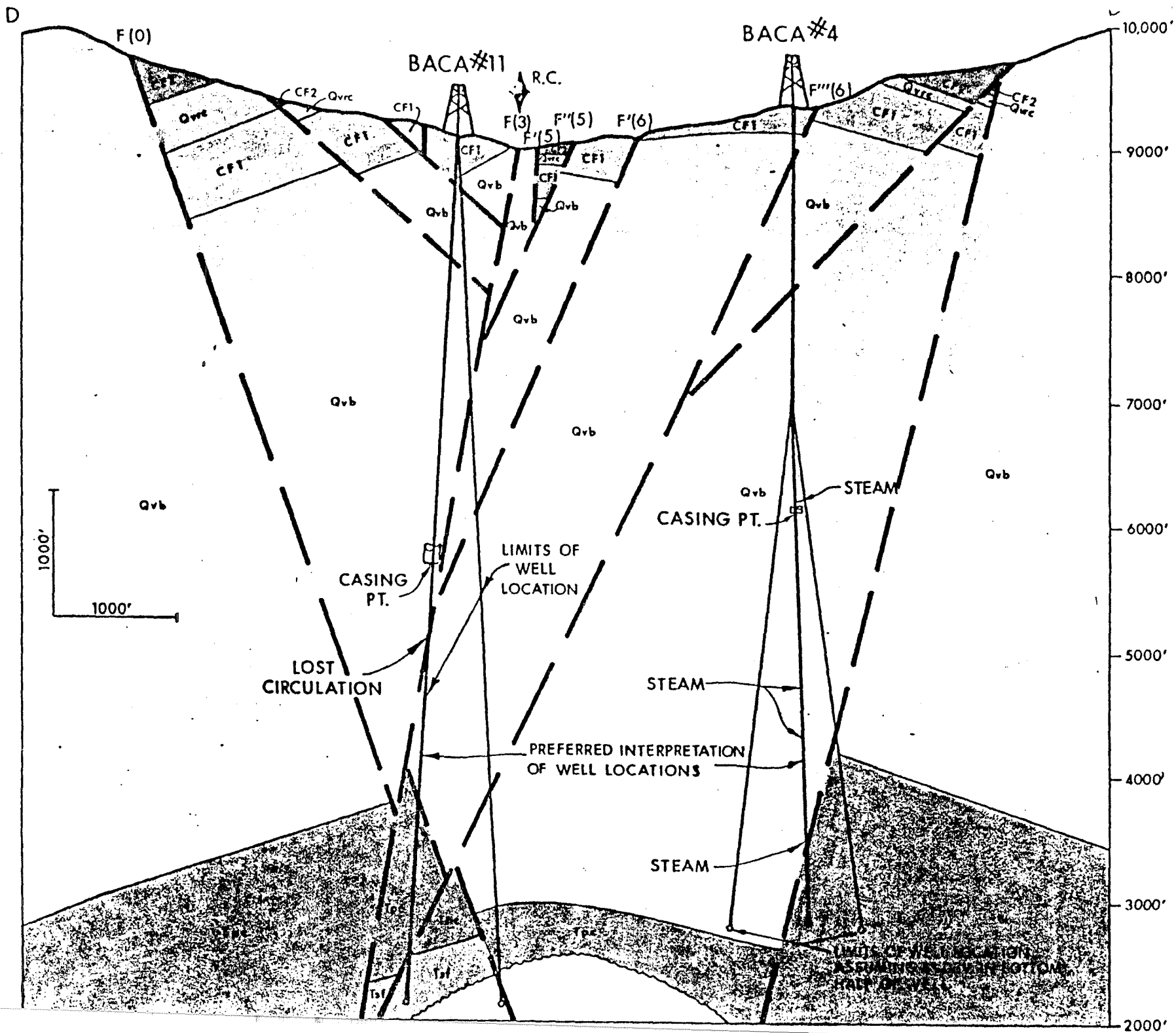


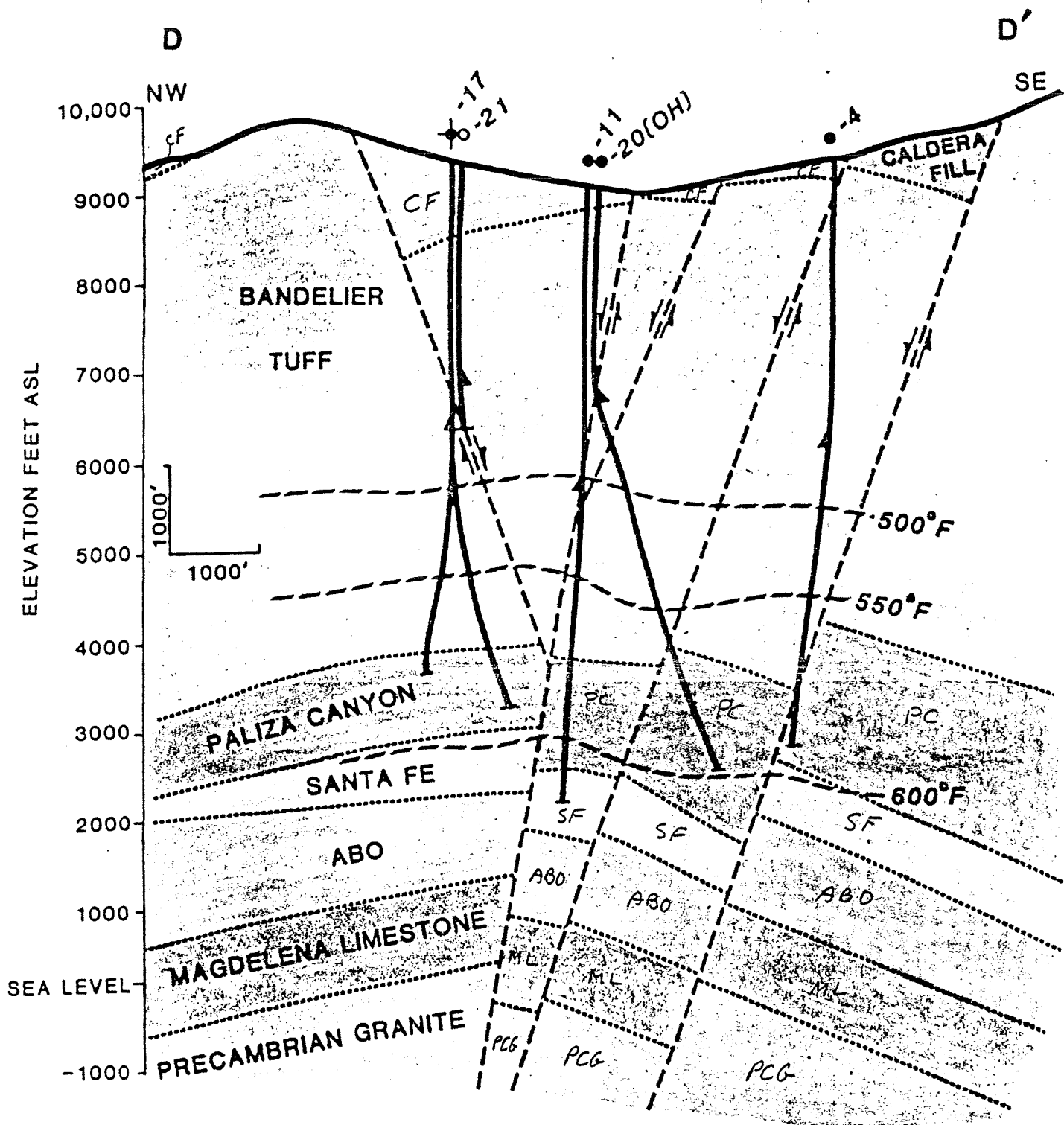
Producing Well Course

Dry Well Course

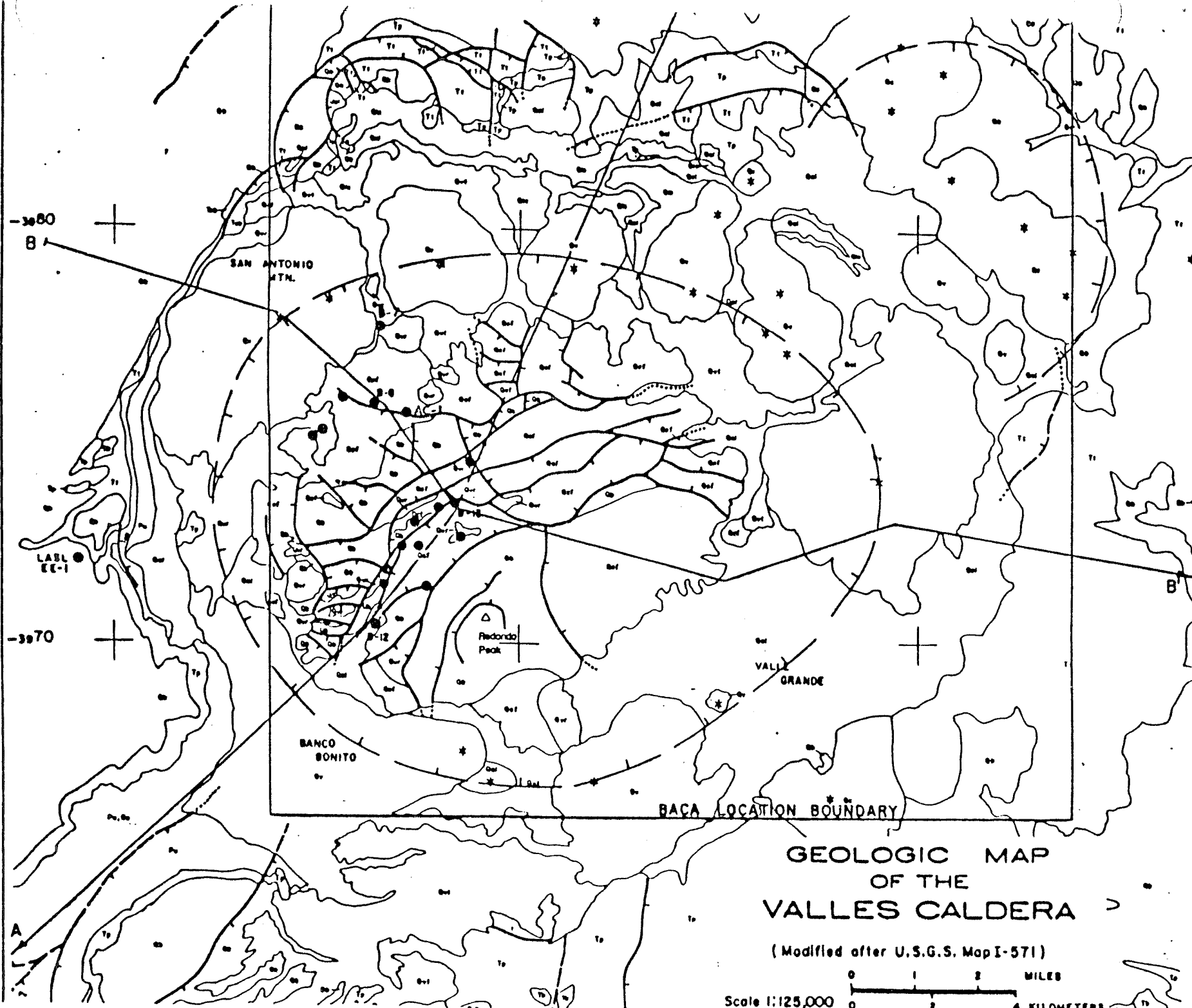
Temperature Contours at 3750' ASL





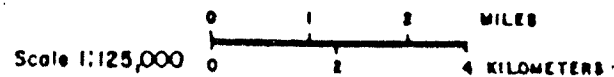


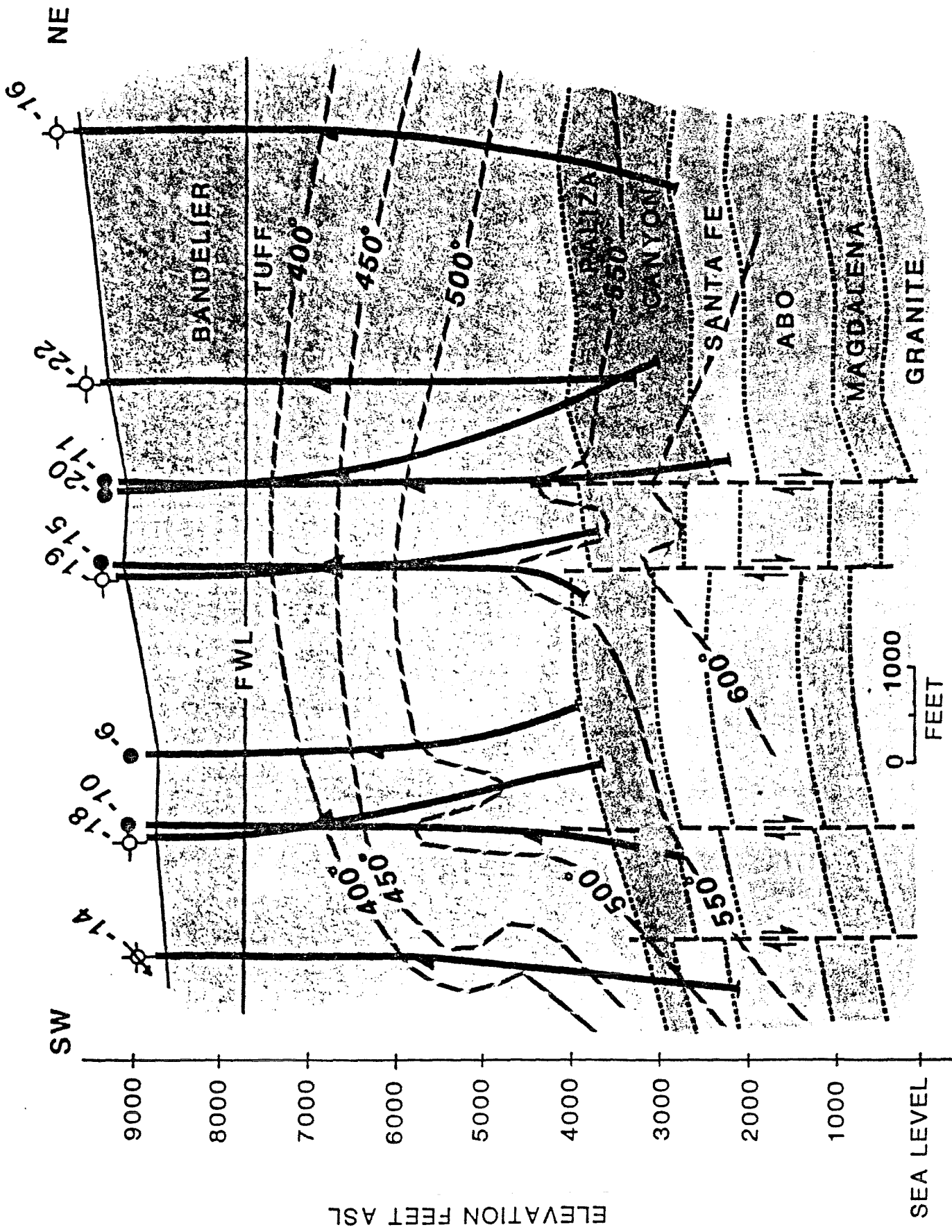
**GEOLOGIC & ISOTHERMAL CROSS SECTION of
REDONDO CREEK BACA, NEW MEXICO**



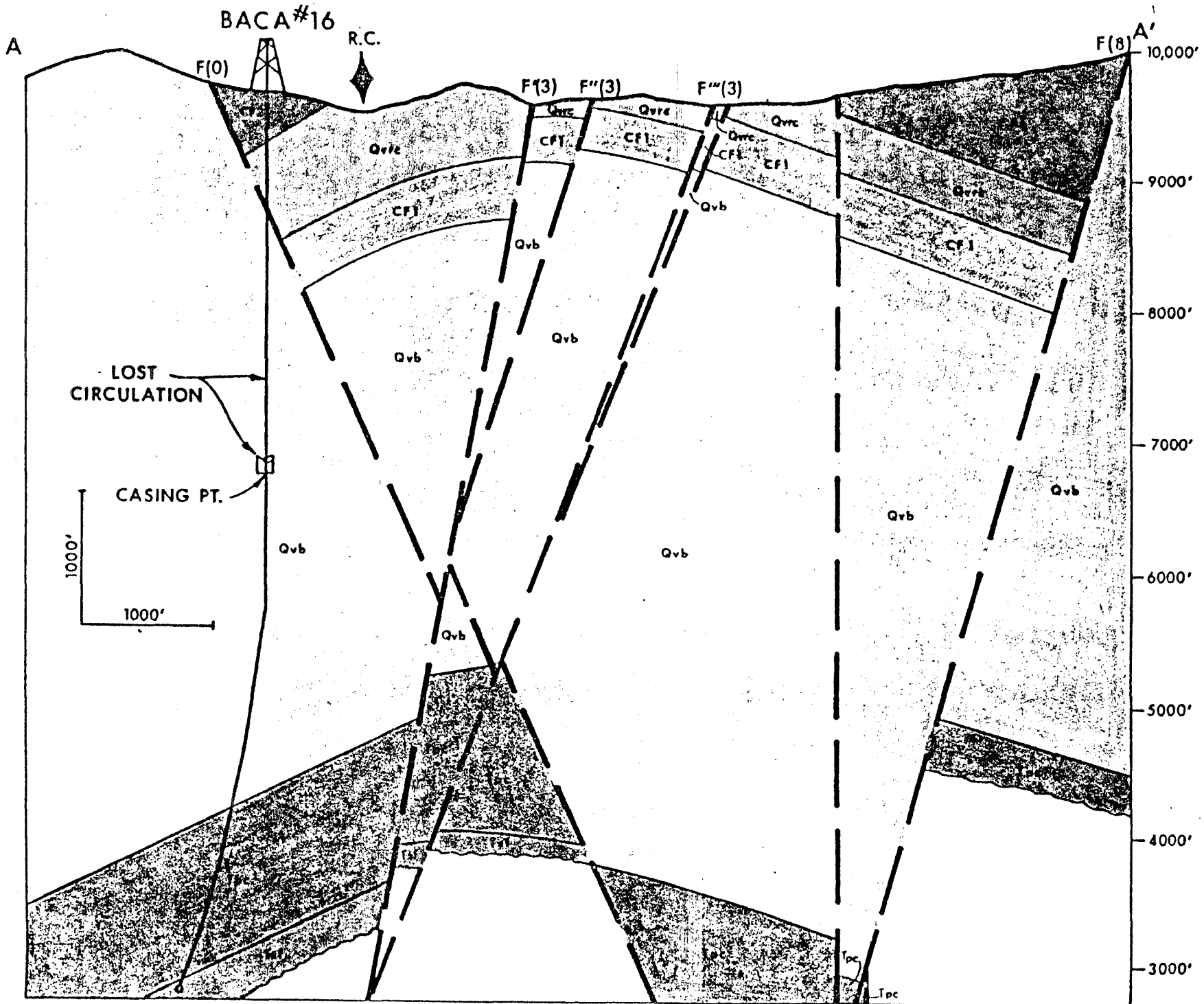
**GEOLOGIC MAP
OF THE
VALLES CALDERA**

(Modified after U.S.G.S. Map I-571)





**GEOLOGIC & ISOTHERMAL CROSS SECTION of
REDONDO CREEK BASIN, NEW MEXICO**








union 76

**GEO THERMAL DIVISION
BACA PROSPECT**

**TEMPERATURE
GRADIENT
FROM 150'-250'
IN F°/100'**

• **Data Point**

I		< 5°
II		5°-10°
III		10°-15°
IV		15°-20°
V		> 20°

