

8/30/78 - Errata - "Documentation of a Finite Element Program for Solution of Geophysical Problems Governed by the Inhomogeneous 2-D Scalar Helmholtz Equation" by John A. Stoltz

Page 2 - Table I
Problem

TM-MT $p = \hat{y}$ should read $p = \hat{z}$

Line Source $S = I\sigma(x)\delta(z)$ should read $S = I\delta(x)\delta(z)$

Page 3 - The second sentence should be replaced by "Any or all of σ , μ , and ϵ , may be considered piecewise constant functions of position, with suitable modifications to the input. The program is currently set up for conductivity variation."

Page 4 - Paragraph 2

The statement "The Greenfield algorithm (see e.g. Swift, 1967 - Appendix 3) is then used to solve the linear system of equations," should be replaced by "A modification of Gaussian elimination applicable to the solution of symmetric banded systems (see Cook, 1974, p. 47) is then used to solve the linear system of equations.". The actual method implemented in this program does not make use of Greenfield's factorization scheme.

Reference: Cook, Robert D., 1974. Concepts and Applications of Finite Element Analysis. John Wiley and Sons, Inc., New York, 402 p.

Page 18 - Figure 4

The node numbering for the quadrilateral element is inconsistent with the global numbering scheme described in figure 2. Note this correction and the correction to the form of the coefficient matrix in the revised figure 4.

Page 20 - Figure 5

Rows 3 and 4 and Columns 3 and 4 of the 5×5 matrix must be interchanged to make it compatible with the corrected node numbering scheme of figure 4. Note also the modification to the reduced 4×4 matrix.

Page 25 - After re-examining the auxiliary field calculations for the TM mode problem, I see no reason to include the one or two node air layer for this problem as long as the derivatives are calculated one node below the air earth-interface. One can experiment with this by setting $M1=0$ for no air layer.

Program Listing - I have discovered an error in the program listing in the section where the element matrices are loaded into the global matrix. The programming error will not affect results from the program unless different conductivities are specified in triangles 1 and 3 of the quadrilateral element of figure 4. This would occur, for example, if one were trying to model a sloping interface. Corrections to the code are required on

pages 37 and 41 of the listing. These corrected pages are provided, with the corrected lines of code highlighted. Sample runs for a sloping contact for both the TE and TM magnetotelluric problems are included from both the uncorrected and corrected versions of the program.

WE WISH TO MINIMIZE IN SOME
SENSE THE ERROR ϵ .

LET'S
TAKE

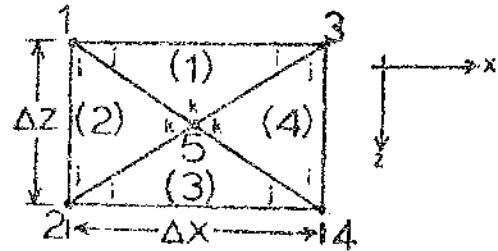
$$\langle N_n^e \epsilon \rangle = \iint_e N_n^e \epsilon dx dz = 0$$

$n = i, j, k$

CARRYING OUT THE INTEGRATIONS:

$$\left\{ \frac{-1}{4K\Delta} \begin{bmatrix} B_i^2 + C_i^2 & B_i B_j + C_i C_j & B_i B_k + C_i C_k \\ B_j^2 + C_j^2 & B_j B_k + C_j C_k & \\ B_k^2 + C_k^2 & & \end{bmatrix} + \frac{P\Delta}{12} \begin{bmatrix} 2 & 1 & 1 \\ 1 & 2 & 1 \\ 1 & 1 & 2 \end{bmatrix} \right\} \begin{bmatrix} \tilde{F}_i \\ \tilde{F}_j \\ \tilde{F}_k \end{bmatrix} = \begin{bmatrix} S_i \\ S_j \\ S_k \end{bmatrix}$$

IT'S MORE EFFICIENT
TO DEAL WITH
QUADRILATERAL ELEMENTS



THE COEFFICIENT
MATRIX FOR THIS
ELEMENT
HAS THE FORM

$$\begin{bmatrix} A & B & C & 0 & | & D \\ E & 0 & F & | & G \\ H & I & J & | & K \\ K & L & M & | & \end{bmatrix} = \begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix}$$

Figure 4. Matrix equations associated with a triangular element;
formation of quadrilateral element and associated matrix
equation from combination of four triangular elements.

$$\begin{array}{c}
 \left[\begin{array}{cccc}
 \frac{1}{4} \left(\frac{\Delta Z}{\Delta X} + \frac{\Delta X}{\Delta Z} \right) \frac{(K_1 + K_2)}{K_1 K_2} + \frac{\Delta X \Delta Z}{24} (P_1 + P_2) & -\frac{1}{4} \left(\frac{\Delta Z}{\Delta X} - \frac{\Delta X}{\Delta Z} \right) \frac{1}{K_2} + \frac{\Delta X \Delta Z}{48} P_2 & \frac{1}{4} \left(\frac{\Delta Z}{\Delta X} - \frac{\Delta X}{\Delta Z} \right) \frac{1}{K_1} + \frac{\Delta X \Delta Z}{48} P_1 & \frac{1}{2} \left(\frac{\Delta X}{\Delta Z} + \frac{\Delta Z}{\Delta X} \right) \frac{1}{K_1 K_2} + \frac{\Delta X \Delta Z}{48} (P_1 + P_2) \\
 \\
 \frac{1}{2} \left(\frac{\Delta Z}{\Delta X} + \frac{\Delta X}{\Delta Z} \right) \frac{(K_1 + K_2)}{K_1 K_2} + \frac{\Delta X \Delta Z}{24} (P_2 + P_3) & 0 & \frac{1}{4} \left(\frac{\Delta Z}{\Delta X} - \frac{\Delta X}{\Delta Z} \right) \frac{1}{K_3} + \frac{\Delta X \Delta Z}{48} P_3 & \frac{1}{2} \left(\frac{\Delta X}{\Delta Z} + \frac{\Delta Z}{\Delta X} \right) \frac{1}{K_2 K_3} + \frac{\Delta X \Delta Z}{48} (P_2 + P_3) \\
 \\
 -\frac{1}{4} \left(\frac{\Delta Z}{\Delta X} + \frac{\Delta X}{\Delta Z} \right) \frac{(K_1 + K_2)}{K_1 K_2} + \frac{\Delta X \Delta Z}{24} (P_1 + P_2) & -\frac{1}{4} \left(\frac{\Delta Z}{\Delta X} - \frac{\Delta X}{\Delta Z} \right) \frac{1}{K_4} + \frac{\Delta X \Delta Z}{48} P_4 & \frac{1}{2} \left(\frac{\Delta X}{\Delta Z} + \frac{\Delta Z}{\Delta X} \right) \frac{1}{K_3 K_4} + \frac{\Delta X \Delta Z}{48} (P_3 + P_4) \\
 \\
 -\frac{1}{4} \left(\frac{\Delta Z}{\Delta X} + \frac{\Delta X}{\Delta Z} \right) \frac{(K_1 + K_2)}{K_1 K_2} + \frac{\Delta X \Delta Z}{24} (P_1 + P_2) & -\frac{1}{4} \left(\frac{\Delta Z}{\Delta X} - \frac{\Delta X}{\Delta Z} \right) \frac{1}{K_3} + \frac{\Delta X \Delta Z}{48} P_3 & \frac{1}{2} \left(\frac{\Delta X}{\Delta Z} + \frac{\Delta Z}{\Delta X} \right) \frac{1}{K_4 K_3} + \frac{\Delta X \Delta Z}{48} (P_3 + P_4) \\
 \\
 -\frac{1}{4} \left(\frac{\Delta Z}{\Delta X} + \frac{\Delta X}{\Delta Z} \right) \frac{(K_1 + K_2)}{K_1 K_2} + \frac{\Delta X \Delta Z}{24} (P_1 + P_2) & -\frac{\Delta X}{\Delta Z} \left(\frac{K_1 + K_2}{K_1 K_2} \right) - \frac{\Delta Z}{\Delta X} \left(\frac{K_2 + K_1}{K_2 K_1} \right) & \frac{1}{2} \left(\frac{\Delta X}{\Delta Z} + \frac{\Delta Z}{\Delta X} \right) \frac{1}{K_4 K_3} + \frac{\Delta X \Delta Z}{48} (P_3 + P_4) \\
 \\
 \end{array} \right] \\
 \downarrow \\
 \text{SYMMETRIC} \\
 \frac{1}{4} \left(\frac{\Delta Z}{\Delta X} + \frac{\Delta X}{\Delta Z} \right) \frac{(K_1 + K_2)}{K_1 K_2} + \frac{\Delta X \Delta Z}{24} (P_1 + P_2)
 \end{array}$$

STATIC CONDENSATION:

$$\begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = \begin{bmatrix} R_1 \\ R_2 \end{bmatrix}$$

ELIMINATE X_2 :

$$[K_{11} \ K_{12} \ K_{21}^{-1} \ K_{22}] [X] = [R_1 \ -K_{12} K_{22}^{-1} R_2]$$

OR:

$$[\tilde{K}] [\tilde{X}] = [\tilde{R}]$$

WHERE

$$\begin{bmatrix} \tilde{K} \end{bmatrix} = \begin{bmatrix} A - \frac{D^2}{M} & B - \frac{GD}{M} & C - \frac{JD}{M} & - \frac{LD}{M} \\ E - \frac{G^2}{M} & F - \frac{LG}{M} & G - \frac{JG}{M} & H - \frac{J^2}{M} \\ H - \frac{J^2}{M} & I - \frac{LJ}{M} & F - \frac{LG}{M} & K - \frac{L^2}{M} \end{bmatrix}$$

Figure 5. Explicit form of the 5×5 coefficient matrix associated with the quadrilateral element of figure 4. Process of static condensation to reduce this matrix to a 4×4 .

Appendix III - Program Listing

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STUDT>PNLS1(1).MAIN1
1      C THIS PROGRAM SOLVES THE TWO DIMENSIONAL LINE SOURCE AND TE AN
2      C MAGNETOTELLURIC PROBLEM ACCORDING TO WHETHER THE INPUT PARAMETER
3      C IDX=1,2, OR 3. THE FINITE ELEMENT METHOD IS USED WITH LINEAR
4      C BASIS FUNCTIONS, MKS UNITS AND EXP(+JWt) TIME DEPENDENCE IS
5      C ASSUMED. THE + COORDINATE DIRECTIONS FOR THE L.S. AND TE PROBLEMS
6      C ARE X=NORTH, Y=EAST, Z=DOWN. FOR THE TM PROBLEM THEY ARE X=EAST,
7      C Y=SOUTH, Z=DOWN. THE STRIKE DIRECTION IS ASSUMED N-S, THE ORIGIN
8      C IS AT THE LEFT EDGE OF THE MESH AT THE AIR-EARTH INTERFACE.
9      C
10     PARAMETER IP1=31,IP4=50,IP6=30
11     S,IP2=IP1*IP4,IP3=IP1+2,IP5=2*IP3
12     PARAMETER NLAYR=3
13     PARAMETER NLYR=NLAYR-1,NK=NLAYR+1,MDIM=2*NLAYR
14     COMPLEX CK(4),CP14,CK12,CK13,CK14,CK23,CK24,CK34,CP12,CP23,C
15     => SCP14,CP1234,A11,A12,A13,A15,A22,A24,A25,A33,A34,A35,A44,A45,A
16     S11,G11,C11,H11,E24,H22,C22,E33,G33,E44,SC(IP4),
17     SBC1(IP4),S1(IP2+5),S2(IP5,IP3),S(IP3,IP3),R(IP2),R1(IP5),ZERO
18     COMPLEX XE(MDIM),XK(NK),DUM(MDIM,MDIM),EFLD,HFLD
19     DIMENSION H(NLYR),P(NLAYR)
20     COMMON/BLK2/DUM,XE,XK
21     COMMON/BLK3/H,W
22     COMMON/BLK1/S,S2,R,R1,NT1,NF1,NCOL1,NS1,NEG1
23     COMMON/BLK4/WU,WE,RHO,CK,CP
24     COMMON/BLK5/XX,ZZ,BC,BC1,NTART,NODEX,NODEX1,NODEZ
25     COMMON/BLK6/IOX,L,M
26     INTEGER NPT(IP1+4,IP4),NX(IP6),NZ(IP6)
27     REAL DELTAX(IP4),DELTAZ(IP1),DELX(IP6),DELZ(IP6),RHO(IP1+4,IP4
28     $,Y(10),XX(IP4),ZZ(IP4),RE(IP4),AIE(IP4)
29     C
30     ****
31     C
32     ZERO=(0.,0.)
33     ELARGE=10E+15
34     READ 1 IDX,NODEX,NODEZ,NXX,NZZ,NRES,M1,NPRINT,LINE1,LINE2
35     READ 4 (T(I),I=1,NRES),F          QINPUT MESH CONDUCTIVITIES
36     READ 1 (NX(I),I=1,NXX)
37     READ 4 (DELX(I),I=1,NXX)
38     READ 1 (NZ(I),I=1,NZZ)
39     READ 4 (DELTZ(I),I=1,NZZ)
40     NODEX1=NODEX-1
41     NODEZ1=NODEZ-1
42     DO 29 I=1,NODEZ1
43     DO 29 L=1,4
44     READ 4B (NPT(I,L,J),J=1,NODEX1)
45     CONTINUE
46     PRINT 20 IDX
47     PRINT 410 NODEX,NODEZ,NXX,NZZ,NRES,M1,NPRINT,LINE1,LINE2
48     PRINT 420
49     PRINT 300 (Y(I),I=1,NRES),F
50     PRINT 430
51     PRINT 1 (NX(I),I=1,NXX)
52     PRINT 440
53     PRINT 300 (DELX(I),I=1,NXX)
54     PRINT 450
55     PRINT 1 (NZ(I),I=1,NZZ)
56     PRINT 460

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228      CK14=(CK(1)+CK(4))/(CK(1)*CK(4))
229      CK25=(CK(2)+CK(3))/(CK(2)*CK(3))
230      CK24=(CK(2)+CK(4))/(CK(2)*CK(4))
231      CK34=(CK(3)+CK(4))/(CK(3)*CK(4))
232      CP12=CP(1)+CP(2)
233      CP23=CP(2)+CP(3)
234      CP34=CP(3)+CP(4)
235      CP14=CP(1)+CP(4)
236      CP1234=CP12+CP34

237      C      THESE ARE THE ELEMENTS OF THE 5 X 5 MATRIX.
238      C
239      C
240          A11=A*CK12+2,*C*CP12
241          A12=-B/CK(2)+C*CP(2)
242          A13=BD/CK(1)+C*CP(1)
243          A15=DELXZ/CK(1)+DELZX/CK(2)+C*CP12
244          A22=A*CK23+2,*C*CP23
245          A24=BD/CK(3)+C*CP(3)
246          A25=DELXZ/CK(3)+DELZX/CK(2)+C*CP23
247          A33=A*CK14+2,*C*CP14
248          A34=-B/CK(4)+C*CP(4)
249          A35=DELXZ/CK(1)+DEL2X/CK(4)+C*CP34
250          A44=A*CK34+2,*C*CP34
251          A45=DELXZ/CK(3)+DELZX/CK(4)+C*CP34
252          A55=2,*C*CP1234-DELXZ*CK13-DEL2X*CK24)

253      C      THESE ARE THE ELEMENTS OF THE 4 X 4 CONDENSED MATRIX.
254      C
255      C
256          E11=A11-A15*A15/A55
257          E12=A12-A15*A25/A55
258          E13=A13-A15*A35/A55
259          E15=-A15*A45/A55
260          E22=A22-A25*A25/A55
261          E25=A25*A35/A55
262          E22=A24-A25*A45/A55
263          E33=A33-A35*A35/A55
264          E35=A34-A35*A45/A55
265          E44=A44-A45*A45/A55

266      C      THIS SECTION LOADS THE ELEMENT MATRICES INTO THE GLOBAL MATRIX
267      C
268      C
269          S1(L1,1)=S1(L1+1)+E11
270          S1(L1,2)=S1(L1+2)+G11
271          S1(L1,4)=S1(L1+4)+C11
272          S1(L1,5)=S1(L1+5)+H11
273          L2=L1+1
274          S1(L2,1)=S1(L2+1)+E22
275          S1(L2,3)=S1(L2+3)+G22
276          S1(L2,4)=S1(L2+4)+C22
277          L3=L1+NODEZ
278          S1(L3,1)=S1(L3+1)+E33
279          S1(L3,2)=S1(L3+2)+G33
280          L4=L3+1
281          S1(L4,1)=S1(L4+1)+E44
282
283      I3 L1=L1+1
284      IF (IUX,NE.,3) GO TO 14

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LEET LANE, EASTVILLE, DEPARTMENT AND REGISTRARIES

corrected results - TE mode

uncorrected results - TE mode

LLFT ELEC INTERFACE DEPTHS(M) AND RESISTIVITIES	
.1000+03	.1000+03
.1000+03	.1000+03
RIGHT ELEC INTERFACE DEPTHS(M) AND RESISTIVITIES	
.1000+03	.1000+03
.1000+02	.1000+03

corrected results - TM mode

NPX	N-12	NPX22	NPX21	NPX2	NPX18	NPX17	NPX16	NPX15	NPX14	NPX13	NPX12	NPX11	NPX10	NPX9	NPX8	NPX7	
-46.4767	-173-12	-303-13	-975-12	-176+03	-106-03	-105-03	-140-03	-449+02	-531-02-	-280-06	-531-02-	-302-02	-90,805	94,915			
-53.4767	-204-11	-972-14	-242-11	-145+02	-155-03	-145-03	-140-03	-449+02	-531-02-	-280-06	-531-02-	-302-02	-90,627	44,918			
-53.4767	-173-12	-971-13	-171-12	-147-02	-150-02	-155-03	-107-03	-149+02	-449+02	-531-02-	-280-06	-531-02-	-302-02	-90,618	44,918		
-17.4767	-271-11	-130-15	-271-11	-110+03	-105-03	-105-03	-140-03	-449+02	-531-02-	-280-06	-531-02-	-302-02	-90,720	64,034			
-14.4767	-470-11	-770-15	-970-11	-180+03	-105-03	-105-03	-140-03	-449+02	-531-02-	-280-06	-531-02-	-302-12	-90,578	44,950			
-14.4767	-571-12	-571-12	-571-12	-147-02	-150-02	-155-03	-149+02	-449+02	-531-02-	-280-06	-531-02-	-302-02	-90,515	44,910			
-53.4767	-352-14	-582-14	-582-14	-160+02	-105-03	-104-03	-142+03	-447+02	-531-02-	-280-06	-531-02-	-302-02	-90,308	64,678			
-53.4767	-134-14	-437-14	-437-14	-143+02	-287-02	-107-03	-140-03	-437+02	-531-02-	-280-06	-531-02-	-302-02	-90,157	63,659			
-3.4767	-204-11	-170-15	-214-12	-150+03	-110-03	-900-04	-150-03	-417+02	-531-02-	-280-06	-531-02-	-302-02	101,245	41,735			
-7.4767	-261-10	-175-14	-261-10	-375-02	-110-03	-900-04	-150-03	-418+02	-531-02-	-280-06	-531-02-	-302-02	107,004	40,019			
-1.4767	-140-10	-213-11	-140-10	-384-02	-112-03	-100-03	-165-03	-374+02	-531-02-	-280-06	-531-02-	-302-02	122,904	57,404			
-4.4767	-115-10	-120-12	-416-11	-100+03	-178-03	-110-03	-213-03	-337+02	-531-02-	-280-06	-531-02-	-302-02	204,515	35,677			
-1.4767	-114-10	-114-10	-410-07	-320-01	-250-03	-160-03	-306-03	-320+02	-531-02-	-280-06	-531-02-	-302-02	420,416	32,249			
-1.4767	-114-10	-114-10	-410-07	-320-01	-250-03	-160-03	-306-03	-320+02	-531-02-	-280-06	-531-02-	-302-02	420,416	32,249			
-1.461-1367-03	-876-10	-367-09	-178+03	-563-03	-350-03	-463-03	-318+02	-531-02-	-280-06	-531-02-	-302-02	21975,855	71,842				
-4.4767	-371-08	-142-07	-274-03	-177+03	-770-03	-476-03	-930-03	-318+02	-531-02-	-280-06	-531-02-	-302-02	323952,826	31,829			
-1.4767	-172-10	-221-10	-181-07	-316-07	-772-04	-177-03	-818+02	-531-02-	-280-06	-531-02-	-302-02	94,791	31,824				
-1.44-143-03	-143-03	-244-09	-466+02	-971-04	-600-04	-115-03	-318+02	-531-02-	-280-06	-531-02-	-302-02	58,717	31,850				
-1.44-137-07	-826-09	-772-10	-124+03	-851-04	-530-04	-100-03	-310+02	-531-02-	-280-06	-531-02-	-303-02	45,197	31,913				
-1.4767	-114-10	-114-10	-410-07	-320-01	-250-03	-160-03	-306-03	-320+02	-531-02-	-280-06	-531-02-	-302-02	79,124	31,970			
-1.4767	-284-12	-216-07	-364-17	-447+02	-614-08	-407-04	-762-04	-323+02	-531-02-	-280-06	-531-02-	-286-02	26,070	32,263			
-1.45-130-07	-351-12	-510-07	-316+02	-577-04	-360-04	-605-04	-326+02	-531-02-	-470-07	-531-02-	-105-02	21,103	32,504				
-1.4767	-140-09	-171-09	-419-02	-677-04	-318-04	-574-04	-337+02	-531-02-	-966-07	-531-02-	-455-03	14,705	33,894				
-1.4767	-152-11	-152-11	-415-10	-171+03	-627-04	-209-04	-521-04	-349+02	-531-02-	-963-07	-531-02-	-453-03	12,193	34,877			
-1.46-111-11	-174-12	-675-15	-129+02	-305-14	-288-04	-438-04	-371+02	-531-02-	-961-07	-531-02-	-450-03	10,715	36,150				
-1.4767	-114-12	-114-12	-414-09	-247-04	-290-04	-440-04	-326+02	-531-02-	-984-07	-531-02-	-450-03	8,775	36,467				
-1.4767	-243-12	-720-14	-370-12	-153+01	-227-04	-313-04	-431-04	-464+02	-531-02-	-280-07	-531-02-	-950-03	8,362	46,459			
-2.4767	-270-12	-127-14	-370-12	-971-01	-320-04	-530-04	-453-04	-492+02	-531-02-	-280-07	-531-02-	-950-03	8,234	48,158			
-3.4767	-220-11	-164-13	-230-11	-123-02	-618-04	-357-04	-469-04	-576+02	-531-02-	-286-07	-531-02-	-960-03	8,982	47,797			
-1.4767	-214-10	-115-15	-120-10	-173-02	-718-04	-342-04	-472+04	-475+02	-531-02-	-980-07	-531-02-	-1050-03	10,014	47,409			
-2.4767	-188-10	-135-10	-145-10	-131-02	-327-04	-345-04	-475-04	-456+02	-531-02-	-280-07	-531-02-	-950-03	12,159	46,598			
-3.4767	-222-12	-125-14	-222-12	-125-02	-329-04	-345-04	-474-04	-450+02	-531-02-	-280-07	-531-02-	-950-03	14,046	46,454			
-5.4767	-110-11	-95-17	-110-11	-427-03	-329-04	-337-04	-471-04	-457+02	-531-02-	-286-07	-531-02-	-950-03	2,956	45,659			
-7.4767	-111-11	-111-15	-611-11	-110+03	-328-04	-374-04	-468-04	-455+02	-531-02-	-286-07	-531-02-	-950-03	6,937	45,591			
-2.4767	-101-11	-127-12	-110-11	-110-02	-327-04	-374-04	-468-04	-455+02	-531-02-	-286-07	-531-02-	-950-03	4,768	45,517			
-11.4767	-670-12	-110-16	-110-12	-777-03	-582-04	-351-04	-465-04	-456+02	-531-02-	-280-07	-531-02-	-950-03	9,415	46,459			
-11.4767	-121-12	-100-17	-101-12	-100+03	-322-04	-371-04	-462-04	-455+02	-531-02-	-280-07	-531-02-	-950-03	9,553	45,510			
-17.4767	-173-12	-102-17	-102-17	-102-02	-323-04	-372-04	-463-04	-456+02	-531-02-	-280-07	-531-02-	-950-03	2,602	45,445			
-21.4767	-370-13	-187-15	-370-13	-527-01	-322-04	-372-04	-465-04	-456+02	-531-02-	-280-07	-531-02-	-950-03	9,613	45,498			
-23.4767	-273-12	-180-15	-273-12	-102+03	-322-04	-372-04	-465-04	-456+02	-531-02-	-280-07	-531-02-	-950-03	9,617	45,496			
-33.4767	-103-12	-107-14	-107-12	-107-02	-322-04	-372-04	-465-04	-456+02	-531-02-	-280-07	-531-02-	-950-03	2,610	45,460			
-43.4767	-873-13	-635-14	-675-13	-417+21	-322-04	-372-04	-463-04	-455+02	-531-02-	-280-07	-531-02-	-950-03	9,621	45,915			

uncorrected results - TM mode