GL04380

Subject: two PPs for THE ms..... Date: Wed, 29 Mar 2000 10:39:21 -0700 From: "denis l norton" <denis@ruralnetwork.net> To: "Jeff Hulen" <jhulen@egi.utah.edu>

Jeff:

Hope yous folks had a great trip back to Z: We really enjoyed you being here. Please post me Brians phone number. Edits follow:::::::::

Page 10 replacment PP::::: Edit as to your desire. ********

>From the previous section it was shown that the total heat added by the felsite to the heat the reservoir, fluid plus rock, to its If the balance, ~91 percent, of the felsite heat was transferred directly to c: 730 km3 of fluid would have been heated to This is more than seven times the current steam-reservoir volume, and using a reserv 2% (Williamson, 1992) this 730 km3 of fluid would be equivalent 1 pore space 365 times.

(Jeff: well this seemed intuitively large to me but I redid the calc about 5 times, EACH of these 5 times I misused a conversion from kcal to cal...duahshudaaaaa!) But, the preceding values are correct I managed to edit out some critical words. First we use nine percent of the heat to get the reservoir up to its current state....then we say how many times can we fill that reservoir with fluid at 235C from the heat left(91percent) in the pluton. three hundred and sixty five times, eg 365. still quite interesting AND reasonable. Cant understand why the reviewers didnt catch the error.)

Page 12 PP that begins with.....These results conflict with....

Add to PP

Although extreme choices of transport parameters used in the calculations could increase the thermal life of the numerical felsite body by 75,000 yr, the values chosen are consistent with laboratory and field values. Alternatively, a more complex intrusive sequence with continuing magma supply into portions of the crust below 5.4 km subsequent to

1.2my ago might prolong the numerical systems life in ways that would be consistent with the extent and style of alteration. Recall that the shift in oxygen isotopic values, Brikowski, this volume, is explained reasonably well with a 305km3 felsite, as does the apparently single pulse vein patterns.

We strongly suggest that the geochronological data sets be reevalutated in the

context of the type of events dated and intrinsic errors in those methods. Our guess is that the numerical and chronological and alteration data sets are actually in quite good agreement if all errors are explicitly included. yaty tyayyatyayya unhyui.

Denis

SALTAS

Dk a

to the gesthing

a dog pluid

60le zt begand.

Bending the roof not really lifting it











1512 kg 0. 98

15/2 kg X 1kg/cm² cm² X 1kg/cm²

1512 × 1 0.9804

1482 4 barra × 1MP2 -

148 MPa lith load









• -- • .

· · .



P.02



P.08

The general hydrothermal system evolution during early stages is rich in complex behavior because of the intricate coupling among transport processes and the non-linearity of the fluid equation of state. A progressive thermal field early in the magmas cooling history generates fluid pressures sufficient for the formation of extensive networks of hydraulic fractures. The percolation paths through these fracture networks are probably most extensive near steep pluton-lithocap contacts where the mechanical energy dispersed early in the cooling history is less likely to be mitigated by fracture filling, and where the contact geometry focuses stress, Lantz, 1984, Marder, 1998, Norton, Taylor, and Bird, 1985. These prograde thermal conditions develop within the first few thousand years it takes the magma to reach its apogee in the crust, then evolve upward into the lithocap through a mechanism of complex process interaction that features alternating chemical and mechanical events. This stage of hydrothermal activity is confined to within crystalline portions of the pluton and contiguous rocks in its lithocap. Consequently, the geometric form of the chamber, rate of emplacement, and state-of-stress strongly control the style of evolution.

Geometric Form of Chamber

The geometric form of the magma chamber and extent of stress interaction with regional stresses can be reconstructed by considering the combined processes of magma infiltration into a middle to upper crust regime where strike-slip tectonics was actively forming extension openings between the Coll and Mercuryville faults. If we presume that the lateral margins of steam extend laterally beyond the present margins of the felsite by a couple of kilometers, then the girth of the felsite is roughly elliptical in plan with a (major axis) = 16km and the b(minor axis) = 6 km; the a axis is oriented N?W. This asymetry in plam view implies that during emplacement of the main mass of magma the horizontal stresses were unequal as magma inflated its chamber and deflected its roof. Given this extent of magma in plan, and modest magma pressures, but weak overburden strengths one can account for a 5-10 km maximum thickness of the magma, Pollard and Johnson , 1973, and Norton, Taylor, and Bird, 1984. However, the regional state of stress in the magma hosts during intrusion is demonstrably one of strike-slip tectonics. We suggest an interaction among deflection of the magmas lithocap and extensional opening along fracture sets associated with the coupling of stress between the Mercuryville and Colliomyi faults attended the flow of magma. The sharp keel and apparent offset of the southern end of the intrusion into geometric patterns similar to the nearby strike-slip basins we attribute to the ongoing regional tectonics but the overall form and aggregate thickness of the felsite

appears to be explicable by simple deformation of the lithocap by magma pressure followed by sill like emplacemnet of the main granitic mass.

As magma was intruded fractional crystallization produced a volatile-rich phase as evident from the presence of mirialotic cavities??, biotite and hornblende, and tourmaline rich regions of the carapace. This phase of the magma on cooling would augment the emplacement magma pressure with locally enormous overpressures that were relieved in part by eruption, augmented motion on local strands of the strike slip fault arrary, and or dike emplacement??.

Concommitant transfer of thermal energy to the lithocap during intrusion caused further deformation of the lithocap as a consequence of increased fluid pressures in the wet Franciscan series sediments. These fluid pressure increases tend to be localized around isolated porous zones in matrix blocks or otherwise sealed fault segments, consequently, they may either augment additional opening of extension zones and/or intiate the generation of fracture networks along which embryonic hydrothermal convective flow occurs.

References

Pollard, David, D. and Arvid M. Johnson, 1973. Mechanics of Growth of some Laccolithis intrusions in the Henry Mountains, Utah, II. Tectonophysics, 18, p 311-354.

Norton, Denis, H.P. Taylor Jr., Dennis K. Bird, 1984. The geometry and high-temperature brittle deformation of the Skaergaard Intrusion, Journal of Geophysical Research. v 89. p 10178-10192.

Comments

- Not sure I like making the edge of steam the delineation of the edge of magma. This edge also coincides with the Hg-ville and Collyami structures, particularly the former. I can envision good convective upflow along these structures driven by the margin of lateral heat dispersed from the magma, if edge of magma is within a couple of kms of the structure....so lets shrink the magma margin by about 4km in length and width.
- 2) the emphasis of Pollards work relates to "laccoliths" but I see it as a general quantitative description of the deformation processes that occur in ALL magma lithocaps where magma is emplaced in regionally quiescent tectonics.
 - the Pollard lithocap deflection analysis

actually pertains to all magmas emplaced into the mid-upper crust. A combination of deflection of the roof, mass wasting of rocks from overstepened surfaces, apropos normal and strike slip deformation to provide additional room, and some degree of wall and roof block stoping accompany all such mass transfer of melts into the crust. I suggest that the Pollard roof deflection principles definitely pertain to the Geysers felsite,,, but it is clearly modified by concurrent strike-slip/extensional mechanics.

The overall elliptical plan view and roof profile of the felsite from 5-6000ft below sea level to depth X to the Pollard lithocap deflection process, as this occurs fractionation of the magma to a volatile rich phase about the same volume that we would get for the keel from the top to -5or6000 ft or about 5 percent of the total mass as drawn in your color figs. this volume is the filler of extensional strike slip features. (NB: this fraction is in the general range of volatile rich fractions I have noted in high-level plutonic bodies.

-as the lithocap is deflected, eg domed up, the rocks are subject to tensional stress, this helps a pre-existing extensional feature in the already deforming lithocap, AND also sets up a very convenient stress situation for the dissipation of magma fluid pressures in the chamber and isolated pore pressures in the lithocap.

The rate of chamber filling for granitic family magma is more problematic. The mechanism of aggradation of a granitic affinity batholith/pluton is through a sequence of magma dikes ranging in thickness from a few meters to 50 meters and upto several hundred meters in width. Each magma dike flows along the prior body in relatively rapid sequence utilizing the exsolving fluids to augment magma pressure and decrease viscose resistance. In effect a continuous dike swarm(one can see these in outcrops of all granitic affinity plutons.

The rate of this process seems fast because the plutons retain their thermal mass as if they were emplaced during a time interval that is but a small fraction(<1 percent) of their total thermal lives. A slower emplacement time would result in a thermal lag such as we note along the spreading ridge environment where each dike event degrades prior to the next dike.

Notes on deviations from the ideal Pollard sill-laccolith.

Geologists have proposed that plug like shapes of plutons arise because of heat loss from the extreme tips of the initial sill, viscosity increases and pressure is directed toward the roof over a smaller area. HOWEVER, the roof is raised by a force, Fz, that relates to magma pressure, P, through the area over which it is distributed, A. Consequently, any decrease in area over which the magma pressure acts Acutally decreases the force. Therefore the more plug like shape requires an increase in magma pressure during the intrusion process, something that is indeed possible IF a volatile rich phase is fractionated from the magma batch and causes increase in magma pressure !!!!!!!



present-day total heat content of Geysers reservoir 10° cal



steam reservoir 9.5 × 109 ft³ in Graywack 3.5 × 10¹⁰ ft⁹ km³

2.71 × 10⁻¹ km³ 27.1 × 10° km³

Total steam-reservoir volume (Williamson, 1992) 660 km³

:. vol. of steam reservoir in fe site = 390 km³

Certer 250

Aug. depth to steam = 1.74 km 10° ambient to 230° Top of res 120°C mid-point

Assume 40°C/Km pre-pluton

Geometry and state of stress for Geysers Plutons May 26, 2000

Jeff:

Follows a simple diagram of about the proportions for the Entire Geysers pluton. It can be viewed as a time series, starting with a very thin sill of 2.2 km half-width then increasing in length and thickness proportionate to equation 3 in Skaergaard paper number 2.. Note: A 25 percent increase in sill major axis from approx 8-10km produces a factor of 3 increase in maximum thickness. So as one trims the ellipitical plan view dimensions pluton thickness is less. Deflection of Lithocap for a/b=2.5



distance along major axis, km

Now if one increases the magma pressure by a factor of 1.5 in the central 1.5 km region of the sill; this would be like having the outer margins mostly crystalline and resistant to further flow, perhaps with synchronous extensional tectonics in this same region, we get a $\frac{1}{1000}$ do-keel form.

Okay want to get this to you so will quit here. denis





distance along major axis, km

Geometry and state of stress for Geysers Plutons May 26, 2000

Jeff:

Follows a simple diagram of about the proportions for the Entire Geysers pluton. It can be viewed as a time series, starting with a very thin sill of 2.2 km half-width then increasing in length and thickness proportionate to equation 3 in Skaergaard paper number 2.. Note: A 25 percent increase in sill major axis from approx 8-10km produces a factor of 3 increase in maximum thickness. So as one trims the ellipitical plan view dimensions pluton thickness is less.

Deflection by a = 7.5 km Intrusion; a/b = 2.5



distance along major axis km

Now if one increases the magma pressure by a factor of 1.5 in the central 1.5 km region of the sill; this would be like having the outer margins mostly crystalline and resistant to further flow, perhaps with synchronous extensional tectonics in this same region, we get a pseudo-keel form.

Margin xllzation Pmagma inc. by x 1.5



distance along major axis, km

Big Sulphur Creek fault zone strikes of major (>1 km long) high-angle faults & fault segments



* 67% of total strike length

Big Sulphur Creek fault zone strikes of major faults & fault segments

NS - NSW NS-N5E N5-10E N5-10W -N 10-15W N10-15E NI5-20W 0.7, N15-20E (2.7) N20-25W 2.0, 0.7 N20-25E 1.5, N25-30E N25-30W 0.7 (3.5) N30-35E 1.1 N 30 - 35W 2.8, 1.0 (4.0) N 35 - 40W 0.1, 1.6, 1.7, N35-40E 1.6 NAO - 45W 1.7, 1.0, 0.7, 1.0, (4.4) N40-45E (3.8) N45-50E N45-50W 1.7, 1.3, 0.8 (3.7) N50 - 55E N50-55W 1.7, 1.4, 0.6, (5.7)~ N55-60E 0.8 N55-60W 3.9, 1.1, 0.7 1.2, 1.9, 1.5, 1.3 (5,9) N60-65E N60-65W (3.1) N65-70E 0.3,2.8 N65-70W N70-75E N70-75W 1.7, N75-80E N 75 - 80W N80-85E (2.0) N80-85W 1.2, 0.8 N85-90E N85-90W

25.7 = 1km

3.8 km @ N52°W 6.6 Km @ N43°W 7.5 Km @ N53 W 3.7 Km @ N60° W

465

65

NOTES ON EVOLUTION OF THE GEYSERS FIELD.

Rick Allis, 30 September, 1998

In natural state, there was evidence for:

- Vapor-dominated, largely between cap rock and underlying felsite intrusive; vaporstatic pressure gradient implies considerable under-pressures at depth (~ 1kbar/km relative to hydrostatic gradient) and low permeability around reservoir boundaries (White et al., 1971)
- Productive reservoir area is about 50 km², elongate to the NW (~10 km x 5 km)
- Productive thickness greater in SE than NW, but assume here 2 km average
- Matrix and fracture porosities are low; (0.01 0.05 Williamson, 1992; Gunderson, 1992). Matrix porosity decreases downwards. Assume average fracture porosity in reservoir is 0.02
- Heat flow through cap rock is conductive in most places, and averages 0.4 W/m² (10 HFU) over 50 km² reservoir. The cap rock is thinnest (and heat flow highest) over the high point of the felsite in the SE Geysers
- Lateral gradient in oxygen isotopes (heavier to northwest) implies some natural recharge of meteoric water in SE perhaps down through Cobb Mtn rhyolite (Truesdell et al., 1993)
- High temperatures (350 °C) and the presence of chloride (as HCl) in steam exist in the NW Geysers at depth (Walters et al., 1988). Fluid inclusions here record a fossil cooling gradient from magmatic fluids (> 400 °C; 44wt% NaCl equivalent; lithostatic pressure) near the pluton to modified connate waters (325°C, 5 wt% NaCl equivalent, hydrostatic pressure) 1500 m from the pluton (Moore and Gunderson, 1995)
- There is no evidence for an earlier high temperature history in the SE Geysers (Moore and Gunderson, 1995)
- Magmatic intrusion, volcanism and hydrothermal alteration evidence suggest that the system could be at least 1 m.y. old, with it being liquid dominated for much of this time. (adularia dates 600 300 k.y.; perhaps vapor-dominated for last few hundred thousand years; Hulen and Moore, in prep...check dates)
- All models for evolution of system invoke "boil-down" of liquid system, at some critical moment. Large-scale venting of excess fluids, perhaps hydrothermal eruptions; the bottom line is net discharge exceeds recharge. Numerical models simulate this by having a well drawdown the reservoir during short period of time until a small liquid mass fraction remains in fractures. The system is then assumed to be sealed (Pruess, 1985; Shook, 1995). The vapor-dominated system is then stable.

Comments

The transition from a liquid-dominated to a vapor-dominated system is poorly constrained. What circumstances caused the discharge event and the "boil-down"? If it was some tectonic event like a major earthquake causing rupturing of the reservoir, why

should this be unique? Why shouldn't it recur and cause later flooding of the reservoir? Could there be alternative explanations for the "boil-down"? Isotopic evidence indicates that the vapor-dominated system was not totally sealed – any model should allow for this.

The model proposed here is that the fracture volume of the reservoir has been enhanced by extension resulting from ongoing tectonism and magmatic intrusions into the upper crust beneath the reservoir. There is no need for a major discharge event, although it is not precluded. Increased fracture volume in a reservoir with low permeability boundaries will cause and sustain a vapor-dominated system.

Constraints from the natural heat flow

The average heat flow of 0.4 W/m^2 over a 50 km² reservoir area implies a conductive heat loss of 20 MW_{th}. This is sustained by the upward flux of steam condensing near the top of the reservoir, and condensate draining back down into the reservoir. Some steam leaks to the surface as steaming ground and fumaroles. This has apparently increased with time. Early descriptions and photographs (Koenig, 1992; Hodgson, 1992) suggest that the steaming ground was largely limited to the Big Sulfur Creek area. It is likely to have been more than 10 MW_{th} but less than 100 MW_{th}. Here we conservatively assume it was about 30 MW_{th}. The sum of the conductive and convective heat losses from the reservoir is therefore inferred to be about 50 MW_{th}.

The natural convective heat loss has implications for both the rate of mass discharge from the vapor-dominated reservoir and the magmatic heat input beneath the reservoir necessary to sustain the reservoir. A natural steam discharge of about 30 MW_{th} implies a mass loss of 10 kg/s. This could have been the same order of magnitude as the natural meteoric recharge to the reservoir if the Geysers reservoir was close to steady state prior to development. If the natural mass recharge was as high as 100 kg/s, for example, the fracture volume of the reservoir (0.02 x 50 km² x 2 km) of 2 km³, would become liquid-dominated within 700 years (unless steam discharge rate was also significantly higher). Since the time-scale for the vapor-dominated reservoir is apparently the order of 10^5 years, an approximate mass balance may be implied.

If the heat output has been at least 50 MW_{th} for most of the reservoir's existence, some minimum order of magnitude estimates of magmatic heat and mass input to the crust beneath the Geysers can be derived. (refer to ?? papers by Cathles, Norton, etc for more elaborate models of the heat lost from cooling intrusions). If the heat originates from cooling magma, and the amount of cooling is 500°C (750 to 250°C), then 50 MW_{th} requires $1 \times 10^6 \text{ m}^3/\text{y}$ of continuously cooling magma. Considering the latent heat of fusion may decrease this by a small fraction (20 - 30% ref.?). If sustained for 10^5 years, this amounts to 100 km³ of total intrusion. It could be viewed as the equivalent of a 2 km slab (dike) 5 km wide by 10 km deep beneath the reservoir, or a 2 km thick slab (sill) in the upper crust beneath the entire reservoir. Irrespective of whether this is new crustal material (basaltic) or largely remobilised lower crustal material, its intrusion into the upper crust is likely to be associated with doming and extension. Movement on low angle faults and ductile deformation may have accommodated much of the extension, but

some enhanced fracture volume is also likely. It is argued here that this could have been the main factor causing a substantial pressure decline in the fractures (and hence the "boil-down").

Other evidence for reservoir extension

Stanley et al. (1998) review the evidence for a NE-SW extension zone extending between the Geysers reservoir and Clear Lake, where Quaternary north-northeast and northeast trending faults, fractures, lineaments and mineralised veins are common. These are consistent with fault plane solutions from seismicity in the Geysers region which indicate uniaxial extension in a 105° azimuth below 1 km depth (Openheimer, 1986). Although evidence from steam-bearing fractures suggests an effectively randomly oriented fracture network within the reservoir, the results of tracer studies indicate preferential permeability in a north-northeast direction (Beall and Box, 1992). Thompson and Gunderson (1992) suggest that low angle fractures may be important in the greywacke, whereas in the felsite, fractures are more commonly encountered in north-northwest and southwest-northeast wellbore directions. The overall domed shape of the reservoir coinciding with and over-lying the felsite suggests a close structural relationship (Thompson, 1992).

The rate of extension is poorly constrained. The present day west-northwest extension derived from geodetic measurements in the Geysers-Clear lake area is 0.2 µstrain/y (Prescott and Yu, 1986). However there was no significant dilatation. This does not preclude dilatation in the Geysers reservoir area because it is a small part of the geodetic network. More rapid extension is likely to occur at the time of magmatic intrusions. This is likely to be periodic over geologic time, but as discussed above, must be able to accommodate of the order of $1 \times 10^6 \text{ m}^3/\text{y}$ intruded beneath the reservoir area in order to sustain the heat output. Depending on how the intrusion occurs, the extensional strain could range up to $2 \ge 10^{-6}$ /y. The actual extension history could be several orders of magnitude higher than this during intrusion events, which are separated by long periods of quiescence, or even slight contraction due to the effects of cooling of the newly intruded material. If the reservoir fracture porosity at the Geysers is only 2% on average, and there is little evidence for healed fractures, much of the reservoir deformation at the time of intrusion could be on low angle faults. Alternatively, a large component of the intrusion could be contributing to increased upper crustal thickness (and uplift) rather than extension. Increased uplift increases average ground elevation, and has probably also increased erosion of the area. Although the overall component of extension that has created new fracture volume at the Geysers may be small, it could still be important if original fracture volume was low.

Proposed mechanism for the formation of the vapor-dominated reservoir

Most high temperature geothermal systems are situated in extensional tectonic regimes. This is often a consequence of the coincidence between active volcanism providing an upper crustal heat source, and arc or rift tectonism. Most geothermal systems are liquiddominated. The small percentage of developed fields that have vapor-dominated reservoirs are The Geysers, Lardarello, Matsukawa, Kamojang and Darajat. This list excludes shallow vapor-dominated zones in structural highs overlying liquid reservoirs. The latter are have limited vertical extent and are readily explained by natural drainage above the hot liquid reservoir. Often liquid pressures are controlled by the nature and elevation of the main outflow zone of the reservoir, and the permeability regime connecting with the main liquid recharge zone.

In the case of vapor dominated reservoirs, low permeability boundaries and little recharge are essential for their survival. The under-pressuring means that any potential flow is inwards to the reservoir, with the exception of steam loss to the surface. In most fields the extensional tectonism probably ensures that both reservoir permeability is sustained (new fractures replace healed fractures) and liquid recharge keeps the reservoir liquiddominated. The question is therefore why the few reservoirs that have, or develop, low permeability boundaries also develop an under-pressured, vapor dominated state.

Once the mass flux through a liquid dominated reservoir is reduced to low levels due to low permeability boundaries, the reservoir becomes sensitive to fracture volume changes. If the initial fracture volume is low (e.g. 1% if the 'reservoir" is hosted in basement rocks), then even small amounts of new fracturing due to extension could cause large pressure changes. If the enhanced fracturing occurs at the time of an intrusive event, or is coseismic, then it is less likely that mass inflows can compensate for the fracture volume increase. The relatively sudden pressure decline causes increased boiling, and further pressure declines are possible if the steam is able to leak to the surface.

Extension at the time of upper crustal intrusion(s) is more appealing than coseismic extension for the Geysers reservoir because of the close relationship between the fracture permeability and the felsite. The Geysers-Clear Lake tectonic extension zone is much larger in area, and relatively high temperatures (albeit with lower conductive heat flows) have been observed in exploration wells (Stanley et al., 1998). Both magmatic intrusions and volcanism have also occurred across much of this extension zone, but the coincidence of high temperatures and high permeability have yet to found outside The Geysers reservoir. The difference may that the geothermal system at the Geysers appears to have been sustained for most of the last 1 m.y. implying sustained magmatic intrusion into the upper crust in that area, and arguably, enhanced fracture permeability in and overlying the intrusion zone. Relatively ductile capping rocks at The Geysers may have restricted the enhanced permeability vertically, and minimized downflows of meteoric water into the reservoir.

Comments on other vapo-dominated reservoirs....

Modeling evidence supporting mechanism?





Fig. 3. Sketch map of granite plutons along the South Armorican shear zone. (R-B et al., 1997)

Collayomi fault zone major (>1 km long) high-angle fault segments.



ALL THE

What is <u>deviatoric</u> stress? " " a stress trajectory = 2×105 CHAL × 10 m 2 cm/yr for * 10 yr | cm = 10 m2 X 10 m Avg. San Andreas 7 cm/year k km opening in 100,000 yr Dw km opening in 200,000 yr. - MM-4/10 10 = 10 km opening Dal Stanley likely - multiple intrusive mechanisms in the crust Material Transfer Processes - Those involving the movement of mass of mass, without changing its volume Lathe crust's Near-field MTP is those operating within the structural aureole of a pluton and which provide a means of moving material away from the immediate path of the magna. Far-field MTPs-those which provide space for an invading pluton but operate keyond the pluton's structural aureole, Good Example: lowering Moho; raising Earth's surface

- felsite and extent - 100 km² within steam reservoir - & ang. elevation increased by 0.2 km (656) within this area by felsite doming - 20 km³ extra space. (not much) - need area of little sulphur Ck. basin & volume of sedimentary fill = space avail, for pluton fill - moving serpentine asider (cf Roman-Berdiel compaction in cort-met aureole? (suspect transfersion opening (rhomboe(h) 25m)



N.

JBH00039





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JBH00036

Subject: manuscript more stuff

Date: Fri, 7 Apr 2000 09:45:56 -0600 From: "denis l norton" <denis@ruralnetwork.net> To: "Jeff Hulen" <jhulen@egi.utah.edu>

Jeff:

1)On the Tvstime plot that shows temperature for 2 locations in the lithocap, lets smooth the tit on the high temperature one, when i replay that curve there may be some instability in the numerics contributing to part of the tit. Rather than explain at lenght what is going on numerically here lets smooooth it.

2)Tom also encouraged me to add some prose on "salt water", as per your and his request please include the following disclaimer:

In this study, the natural fluid has been represented by the EOS for the H20-system. Samples of the fluids in many hydrothermal system trapped by fluid inclusions imply that fluid compositions ranged from several to zero molal NaCl equivalents during the quartz deposition. Departure of fluid compositions from the single component H2O-system would alter the nature of convective fluid transport in several ways. With increased concentrations of other components in the fluid, the critical point will shift to higher temperatures and pressures then at large concentrations will evolve to a critical line. The influence of the nonlinear transport properties associated with the critical region will however still exert a strong control on the hydrothermal processes. These effects need to be explored but await the generation of a robust EOS for multicomponent fluids, and better geologic definition of how these fluids are initially distributed in the system.

Variations in fluid densities caused by variable concentrations of aqueous components would alter buoyancy forces, heat capacities, shift state conditions at which critical phenomena are encountered, and introduce local heats of mixing among fluids of differing composition. Generally the uncertainties in depths below the ancient ground surface, emplacement times of the magma, permeabilities, how fluid percolates through a hierarchy of fractures, and the relationship between observed fluid inclusion data and flowing fluid compositions appear to be partially self-compensating errors intrinsic in the application of the theory of magma-hydrothermal systems to reality. Over all errors in the timing of events caused by all of these items are probably on the order of plus or minus 50to70 K years. There remains considerable opportunity for refinement of estimates made about the felsites history as well as for discovery of new concepts.

d

Mercuryville Fault Fore stlikes of major high-angle faults

NS-N5E NS - NSW N5-10W 0.6, 0.7, 1.1 (2.4) N5-10E N10-15E N 10-15W NI5-20W N15-20E N20-25E N20-25W 0.4 (2.9)N25-30W 1.6, 1.3, N25-30E (2,2)N30-35E 1.4 (ACFZ) N 30 - 35W 1.3, 0.9 N35-40W 2.0, 1.5, 1.4, 1.2, 0.5 (6.6) N35-40E NAO - 45W 0.8, 3.5, 1.3, 0.7, 0.5 (6.8) N40-45E N45-50W 0.6, 2.6, 1.2, 1.6, 1.3, 0,8, 0.7 (8.8) N45-50E N50-55E N50-55W 0.9,0.8 (2.7) N55-60W 1.2, 0.9, 0.5, (2.6) N55 - 60E N60-65W 2.4, 0.7, 1.0 (4.1) N60-65E N65-70E N65 - TOW 0.8 N70-75E N70-75W 1.0 N75-80E N75-80W 0.5 N80-85E 1.7 (ACFZ) N80-85W 1.0, N85-90E N85-90W

POZ Trend 11.3 km @ N42°W 5 km @ N52°W 5.3 km @ N52°W Maacama fault zone strikes of major high-angle faults & fault segments

NS - NSW	N5-N5E
N5-10W	N5-10E
N10-15W 1.0, 1.2	N10-15E
N15-20W 1.7	N15-20E
N20-25W 0.7, 0.8,	N20-25E
N25-30W 1.5, 1,7	N25-30E
N 30 - 35W	N30-35E
N35-40W 2.7, 7.3, 1.5, 3.5, 3.5	N35-40E
N40-45W 6.2, 1.6, 0.9, 1.3, 3.2	N40-45E
N45-50W 1.9, 4.1, 1.4, 2.9	N45-50E
N50 - 55W 1.2, 1.5, 1.3, 0.8, 0.4, 1.0, 3.8	N50-55E
N55-60W 0.8	N55-60E 1.4
NGO-65W 0.8, 1.3,	N60-65E
NG5 - 70W	N65-TOE
N70-75W 1.4	N70-75E
N75-BOW 0.4	N75-80E
NRO-85W 1.0, 1.2, 1.2	N80-85E
N85-90W 1.1, 1.7	N85-90E 0.9,

20,1 Km@ N42°W 7,4 Km@ N48°W







Feet/Meter = 3.280839895/1 Meters/foot = 0.304614307 9687.52 ft²/pixel

Albers Equal Area Projection:

 1^{st} Standard Parallel = 38.83 N 2^{nd} Standard Parallel = 38.77 N Central Meridian = 122.77 W Central Parallel = 38.80 N

Volumes: ToF and paleosurface = $14,522,480,928,000 \text{ ft}^3$ ToSR and paleosurface = $7,399,159,776,000 \text{ ft}^3$ ToF to - 5km = $10,755,263,289,600 \text{ ft}^3$

VOLUMETRIC ANALYSIS

To facilitate the analysis the data we first projected to an Albers equal area projection. A standard footprint of the maps was then generated using a combination (merge) of both the top of the felsite and top of the steam reservoir maps.

Top of the Steam Reservoir to + 1 km

A three dimensional Riemann sum was used to estimate the volume of the rock between the top of the steam reservoir and the paleosurface. The paleosurface was assumed to be 3280.80 ft. (1 km) above sea level.

To facilitate this process a combination both vector and raster GIS domains were used to prepare the data. Top-of-the-steam reservoir contours (reference), relative to sea level in feet, were digitized into a vector GIS database and attributed with depth values ranging from -7500.00 to +1500.00 feet (Fig. If needed?). This data set was then rasterized into a grid format with each pixel, or grid cell, representing 3600 ft² ft (60.00 ft² x 60.00 ft²) (Fig. If needed?). A formula was then set up to determine the difference between the elevation values of the top-ofthe-steam reservoir and the paleosurface. The calculation was simplified by adding 7500.00 to all elevations, thus clearing negative values. This gave a new range of +0.00 to +9000.00 feet. The complete formula is shown below:

$$T_{v}=\left[P_{a}*\left(\sum\left(\left(S+A\right)-\left(P_{v1\ldots n}+A\right)\right)\right)\right]$$

where T_v is the total volume, P_a is the area of one pixel, S is the paleosurface elevation in feet, A is the constant used to eliminate negative numbers, P_v is pixel elevation values, and n is the total number grid cells.

In practice the above operation had to be done in two steps. The first was to generate a new raster image containing the difference values produced from:

$$P_{d1...n} = \left(\left(S + A \right) - \left(P_{v1...n} + A \right) \right)$$

where $P_{dl...n}$ is the difference value for each pixel in the output grid.

The next step was to export the difference values as an ASCII data set which, in essence, represented a single column, with an area P_a , containing all of the difference values. The ASCII data were further processed with a script to give the sum of the difference data and to multiply the sum by P_a to give the total estimated volume of rock. The results:

$$T_v = 7,399,159,776,000 \text{ ft}^3$$

١

Top of Felsite to + 1 km

A similar procedure as described above was used with the exception that the maximum depth was 8500 ft. below sea level and the minimum depth as 500 ft. above sea level.

 $T_{\rm v}=14,522,480,928,000~{\rm ft}^3$

Felsite Volume to 5 km depth (- 16,414.2 feet)

Volume below the known mapped felsite :

16404 (5 km) was added to each of the felsite depth values. The highest point is 500 ft. above, and the lowest point 8500 ft. below sea level. The maximum difference is 16904 ft. and the minimum difference is 7914 ft.

 $T_{\rm v} = 10,755,263,289,600 \ {\rm ft}^3$

-levate item to beginning item to beginning to beginning to beginning Energy & Geoscience Institute December 20, 1 Denis L. Norton Geologist-Geochemist The School of Thought P.O. Box 310 Stanley, ID 83278 Dear Denis:

Below is the outline we discussed for the Geysers thermal-history paper when last I was in Stanley, or rather, at the Rico River Rancho. It was good to see you guys, for sure, and I half expected you might stop down this way. You're always welcome, of course. I mean it.

A good name for those two fine Great Pyrenees - the whitebarks.

tourmaline Did you get the pendant and mineral specimen?

Anyway, here goes:

IGNEOUS AND HYDROTHERMAL HISTORY OF THE GEYSERS STEAM FIELD. CALIFORNIA

- 1. Abstract (JH and DN)
- 2. Introduction (JH and DN)
 - A. Purpose and scope (attorneys at law)
 - Mathematical modeling constrained by multiple geothermometers (fluid-inclusion; Β. vitrinite and pyrobitumen-reflectance; thermally sensitive secondary minerals, etc.)
 - C. Another constraint – system still vigorously active
 - D. Apply unique insights gained during similar modeling of (tens?, hundreds?) of magmatically-hydrothermal systems around the world, including porphyry copper systems.



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Big Sulphur Creek

- Is it feasible that The 1.1-1.1 Ma Geysers felsite, >100 km³ in known volume, could still be the heat source for the modern vapor-dominated geothermal system? If not, what is the likely nature and timing of post-felsite magmatism. Did emplacement of these younger igneous bodies have anything to do with the changeover from liquid- to vapor-dominated conditions?
- Is the only analysis of the absolute timing of this transition (Hulen et al., 1997) a reasonable one; and if not what are its flaws? What alternative timing scenario?) would be mor appropriate?
- Can we explain the prominent northwest-southeast elongation of the felsite and The Geysers. Do we want to for this paper? Or would another be appropriate.

Denis – I've enclosed Dalrymple's rough draft FYI. I wrote a very cursory geologic setting for the felsite for this paper as 88th author, but have held back all the maps, geologic cross sections, alteration/mineralization sections for our paper. Told those guys I wanted to place all that material in a separate forum since I'd been working on it for years (and didn't want to just hand the stuff over to 'em, much as they'd have appreciated it)

H. How does the "high-temperature" reservoir fit into the model?

You may want to reserve your analysis of this for your paper(s) with Brickowski and Blackwell, and that'd be fine with me, but I would like us to be able to include one or two models which incorporate the effects of convection on heat transfer out of the felsite. OK?

Geologic Setting (JH and DN)

- A. Relationship to the Clear Lake volcanic field (lithospheric slab windows, asthenospheric upwelling, crustal melting, etc. We can be very brief on this since several authors have covered it pretty well.
 - Structural preparation for emplacement of the felsite (San Andreas system, pullaparts, strike-slip faulting, "sigmoidal bends" (DN)). How was such a huge body accomodated; how was the necessary space created?
 - Correlation of felsite with Cobb Mountain volcanic center. Why did a magma chamber large as the felsite only erupt a few km³ of volcanic material? Is this paucity of volcanics tied in with creation of vapor-dominated conditions?
- D. Summary of age, petrogenesis, mineralogy, texture, likely emplacement temperatures of the felsite's three main igneous rock types. Mention abundant vesicles in the high-level microgranite porphyry, which looks pretty much identical

E.

F.

G.



3.

invent state

Β.

C.

to some of the late felsic dikes in the Sawtooth batholith (see accompanying photographs.

E. Summary of The Geysers hydrothermal system as it's presently known. Very brief, again, since Joe Moore has covered a lot of it, and we don't want to be redundant. I can, however, add a lot of secondary-mineral maps which haven't appeared previously, and which might help constrain the system's evolution somewhat).

Geothermometric Constraints for the Models (JH)

- A. Fluid inclusion summary from Moore and Gunderson, 1995
- B. Secondary-mineral geothermometry from same and other publications, augmented by felsite secondary-mineral level maps and cross sections (?)
- C. Organic-matter geothermometers Here's where a lot of new material can be added. Should perhaps prepare a <u>schematic cross section</u> showing paleo-isotherms relative to the felsite as indicated by these and the other two types of geothermometers.

Physical and Thermal Properties of The Geysers Felsite (DN, JH)

- A. Shape, known volume, extrapolated or geophysically constrained volume, density, etc.
- B. C_p , H, "rho", etc.

Denis, I believe we talked about putting this into a table for convenience of reference.

6. Tabulated and discussed variables and constraints utilized for numerical approximation of hydrothermal history.

- 7. Models (DN)
- 8. Discussion and Conclusions (DN, JH)
 - A. Need or lack thereof for additional magmatic input after initial emplacement of the felsite at 1.2
 - B. Type and timing of additional magmatic input required (deep beneath initial felsic pluton or into the body of the pluton once it was partially crystallized, etc.). Any physical evidence which might bear upon this (dikes with certain compositions and ages, etc. pretty slim pickin's for this latter).

4.

- C. Conductive heat transfer sufficient to explain paleoisotherms? No, I know, but we should explain from your model why it couldn't be so.
- D. Porosity and permeability required in convective system(s) to explain secondarymineral distribution and paleo-isotherms.
- E. Nature and timing of transition from liquid- to vapor-dominated conditions.
- F. Correlations with porphyry copper or other magmatic-hydrothermal systems you've analyzed?
- G. Implications for exploration and development?
- H. Recommendations for additional research.

8. Acknowledgements

9. References

FIGURES

Location map

Regional geologic map

Geologic level maps and cross sections of The Geysers felsite – maybe 3-D (yes) Know ages of igneous intrusion and secondary mineralization – paragenetic diagram Multiple models of hydrothermal circulation and heat transfer around the felsite Some sort of summary diagram ?)

TABLES

Chemical, thermal, and other physical properties of the felsite Ditto for the Franciscan metagraywacke/metavolcanic host rocks Ditto for the fluids involved ("connate", meteoric, magmatic, etc.)

Denis -

Also enclosed FYI are three photomicrographs of the felsic dike we sampled near Redfish Lake. It's a microgranite porphyry, vesicular, much like the one forming the cupola of The Geysers felsite. Also contains a microcrystalline, early-crystallized, acicular opaque mineral resembling sea-urchin spines, which I've seen nowhere else but The Geysers. Have sent Geysers and Sawtooth samples off for polished-section preparation, and when they get back will get some "probe" data to satisfy my curiosity.

One photo is at 50X (field of view 5.6 X 3.7 mm) crossed nicols; another is a 100X version of a portion of the first. Letter abbreviations are as follows (see accompanying photomicrographs): G – granophyric groundmass; m – myrmekitic texture; Q – quartz, late-stage, probably micropegmatitic; K – potassium feldspar, probably also late-stage; A- albite, definitely late-stage, crystal projecting into vesicle (V); FI – fluid inclusions in quartz. M – coarse mica, either muscovite, or, more likely, bleached biotite.

The other photo is at 200X and shows a few trains of secondary fluid inclusions in the late-stage quartz. From their liquid to vapor ratios, I'd say they'll have a T_h of about 180°C.





FIGLIRE. LEVEL MAPS OF THE GEYSERS PLLITONIC COMPLEX, SHOWING DISTRIBUTION OF BORDSILICATE MINERALIZATION.





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FIGURE . LITHOLOGIC LEVEL MAPS OF THE GEYSERS PLUTONIC COMPLEX (THE FELSITE). AREALLY RESTRICTED UPPER FOUR LEVELS COMBINED FOR CLARITY.

PRAFT JBH 03/09/99













(A) ELEVATION CONTOUR, FT × 10³ <u>BELOW</u> MEAN SEA LEVEL (MSL)
* VENT LOCATIONS, COBB MTN. VOLCANIC CENTER., PROJECTED
* VENTICALLY POWNWARP TO TOP OF FELSITE
* B) Rhyolite of Alder Creek (1.2 Ma), elev. 1390 m
* D'acite of Cobb Mtn. (1.1 Ma), elev. 1430 m
* D'acite of Cobb Valley (1.1 Ma), elev. 1100 m

FIGURE 1 PERSPECTIVE 3-D BLOCK DIAGRAM OF THE UPPER SURFACE OF THE GEYSERS FELSITE. SECTION A-A', WHICH PASSES THROUGH COREHOLE SB-15-D, WAS CHOSEN FOR NUMERICAL THERWAL HISTORY MODELING TO APPROXIMATE PEAK PALEOTEMPERATURES OBTAINED FROM FLUID INCLUSIONS AND VITRINITE REFLECTANCE.