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ASSESSMENT OF THE GEOTHERMAL RESOURCES OF CARSON-EAGLE VALLEYS AND BIG SMOKY VALLEY, NEVADA

FIRST ANNUAL REPORT MAY 1, 1979 • MAY 1980

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D. T. TREXLER, B. A. KOENIG, T. FLYNN, AND J. L. BRUCE

WORK PERFORMED UNDER U.S. DEPARTMENT OF ENERGY CONTRACT NO. DE-AC08-79NV10039

NEVADA BUREAU OF MINES AND GEOLOGY UNIVERSITY OF NEVADA, RENO RENO, NV 89557

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First Annual Report May 1, 1979 • May 30, 1980

DENNIS T. TREXLER, BRIAN A. KOENIG, THOMAS FLYNN, AND JAMES L. BRUCE

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ABSTRACT

During the period 1 May 1979 through 31 May 1980 members of the Nevada Bureau of Mines and Geology under contract to the U. S. DOE as the statecoupled geothermal resource assessment team completed two geothermal investigations in three Nevada locations. The regions studied were selected from areas outlined as having direct utilization potential (Trexler and others, 1979) and included the Carson-Eagle Valley, Big Smoky Valley and Caliente. The Caliente investigations are discussed in a previously issued report dated March, 1980. Studies were organized around the completion of all or a selected group of tasks in each area. These tasks included:

Geologic Reconnaissance Gravity Surveys Aerial Photography Fluid Sampling and Analysis Shallow Depth Temperature Probe Surveys Soil Mercury Surveys Shallow Electrical Resistivity Measurements Temperature Gradient Hole Drilling

Goals of the project were to provide regional information about the nature and extent of the resources and to offer a critical evaluation of the techniques employed.

Results from our work in the Carson-Eagle Valley demonstrate that geothermal fluids are meteoric waters heated by relatively deep circulation in the earth's crust. The dominant structural controls are high angle, large displacement, normal faults which provide conduits for fluid migration and dictate resource localization. Identification of these faults was accomplished by examining gravity data and abrupt changes in lithology and topography. The association of faults with thermal waters is substantiated by data obtained from two meter temperature probe studies and water well records which reveal linear isotherm patterns in the vicinity of geothermal manifestations. Distinctions between thermal and non-thermal fluids can be made on the basis of major and minor dissolved constituents while trace

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elements are of limited utility. Thermal waters were not encountered in two temperature gradient wells drilled to depths of 240 ft. and 500 ft. in the area.

In the Big Smoky Valley a similar picture of fault-related, deep circulation of meteoric waters emerges. Gravity transects, low sun-angle photography, linear patterns in two meter probe isotherm configurations and soil mercury anomalies all aided in determining the location and orientation of important structural controls. Chemical composition, in terms of major and minor dissolved constituents details the similarities and distinctions between hot and cold waters throughout the study area while isotopic data demonstrate the probable high temperature (>150°C) history of fluids at the Darrough site. Integration of the results obtained from several techniques applied in the Darrough vicinity led to the siting and drilling of a 500 ft. well which encountered thermal fluid and extended the known resource limits.

Techniques used to accomplish the outlined exploration tasks are evaluated on a scale of 1-10. During evaluation consideration was given to parameters such as cost, time and manpower requirements, inter-regional applicability and the quality and quantity of data obtained. Methods receiving generally higher ratings include geologic reconnaissance, gravity, low sun-angle photography, 1-2 m temperature probes, fluid sampling and analysis and temperature gradient drilling. Intermediate rating is assigned to water well data and soil mercury surveys, and low rating is assigned to shallow resistivity.

Analysis of major, minor and trace constituents in fluids from Caliente, Nevada showed the compositions of hot and cold waters to be essentially indistinguishable. However, stable light isotopic data indicate that thermal fluids are derived from a distinct and homogeneous source.

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ACKNOWLEDGEMENTS

We wish to express our sincere thanks to the many people whose cooperation and kindness played an important part in helping us complete our studies in the Big Smoky Valley and the Carson-Eagle Valley. In particular, we extend thanks to the Darrough familty - Luther, Lillian and Larry - of the Big Smoky Valley for providing us with useful information we might not have learned otherwise, for their permission to conduct surveys and drill test sites on their property and especially for their warm hospitality.

We also wish to thank another special group of people at the Frontier Tavern Motel near Austin, Nevada who, over several months, consistently provided us with delicious meals and comfortable lodging.

And finally, in the Big Smoky Valley, a special thanks go to Frenchy and Bill who were instrumental in helping us drill a well under trying circumstances, and Carl Haas who supplied us with necessary water for drilling.

In the Carson-Eagle Valley, much of the data were obtained thanks to the cooperation, assistance and encouragement of many more Nevadans including Harold Wilson along with friends at the Dangberg Farms, Mr. Richard Langson and and Mr. Craig Cedar at the Carson Hot Spring, Mr. Mike Filing of Walley's Hot Spring, Mr. Andy Hofer of Saratoga Hot Spring, Mr. John Asquaga and Mr. Noble Murray. Fluid composition data were obtained thanks to Mr. Lewis Nagy, superintendent of the Carson City Wastewater Treatment Plant and Mr. James Hadden of the Carson City Works. Special thanks also go to Mr. Harvey Whitecome of the Nevada Highway Department for providing aerial photographs and Mr. Cameron Covington who produced excellent graphics for this report.

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INTRODUCTION

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In 1977 the U.S. Department of Energy Division of Geothermal Energy began to formulate a mission-oriented program for the development of geothermal resources. The program began with the western states which contain most of the geothermal resources in this country. The program consisted of integrating the cooperative efforts of participating "state teams", the U.S. D.O.E. Division of Geothermal Energy (DOE/DGE), the U.S. Geological Survey (USGS), the National Oceanic and Atmospheric Administration (NOAA) and several other contractors which the DOE/DGE used in an administrative and technical consulting capacity.

The main objectives of the geothermal program were to (1) broaden the field of technical knowledge of geothermal resources by performing preliminary resources assessments, and (2) plan for the commercialization of the resources by creating area development scenarios using the most recent information supplied by the resource assessment teams. In Nevada the Nevada Bureau of Mines and Geology (NBMG) is responsible for resource assessment and the Nevada Department of Energy (NDOE) is responsible for commercialization.

The first objective of the resource assessment team was to define the geothermal resource potential on a regional scale by producing a 1:500,000 scale map of the state that showed the location of thermal springs and wells and ranked areas of highest potential for direct utilization.

In June, 1979, the NBMG completed a one-year regional assessment for the low- to moderate-temperature geothermal resources in Nevada. The 1:500,000 scale map entitled "Geothermal Resources of Nevada and their Potential for Direct Utilization " depicts both technical resource information for more than 300 springs and wells throughout the state and evaluates nearly 40 large areas with potential for geothermal development on the basis of a numerical scheme developed at NBMG.

A second objective of the resource team was to stimulate geothermal development by performing various geological, geophysical and geochemical surveys in favorably-assessed areas. These "Area Specific" studies were designed to:

- 1. expand the data base of the preliminary assessment
- remove some of the risk in exploration by examining areas in more detail, and
- develop and test scientific exploration methods for low- to moderate-temperature geothermal resources.

The area specific studies began in May, 1979, in two study areas: the Big Smoky Valley in central Nevada and the Carson-Eagle Valley in the western part of the state (fig. Al). These two areas were selected on the basis of their high potential for the development of industrial process heat and residential space heating, respectively. In November, 1979, a third study area, Caliente, was added to the program.

Baseline Data

The investigations began with a search and review of all pertinent literature including topographic maps, geologic reports, geologic maps, Bouguer gravity maps, theses, lithologic well logs and water resources reports. The compilation provided both a general understanding of the areas as well as an initial direction for the area specific study.

The following 7.5-minute topographic maps were used in the Carson-Eagle Valley study area: Carson City, New Empire, Genoa, McTarnahan Hill, Minden and Gardnerville. The Reno and Walker Lake 1:250,000 scale topographic sheets were also used.

In the Big Smoky Valley a combination of 7.5-minute series, 15 minute series and 2 degree maps was used. The 15 minute series maps included Austin, Spencer's Hot Springs, Millet Ranch, Wildcat Peak, Pete Summit Road, Hickson Summit and Diana's Punch Bowl. The 7.5-minute series maps consisted of Carvers, Carvers NE,



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Carvers SE, Carvers SW, Mt. Jefferson and Jet Spring. The Tonopah and Millet 2-degree sheets were also used.

Geologic maps were available in the Carson-Eagle Valley area at two scales. A 1:250,000 scale geologic map (Moore, 1969) provided a regional framework for the study. More detailed stratigraphic and structural information was obtained from the available 7.5-minute series geologic maps including Carson City (Trexler, 1977), New Empire (Bingler, 1977) and Genoa (Pease, 1979).

Most of the major geologic structures in the Big Smoky Valley could be identified on the 1:500,000 scale Geologic Map of Nevada (Stewart and Carlson, 1978). This map, however, was not particularly useful in the vicinity of thermal waters where smaller structures which are not mappable units at such large scales are generally the features of interest. Somewhat more detailed data were obtained from other geologic maps of the area including Kleinhampl and Ziony (1967), Means (1962) and McKee (1968). But an extensive portion of the Big Smoky Valley remains unmapped at a scale suitable for area specific studies.

Regional Bouguer and gravity data from the Reno (Erwin and Berg, 1977) and Walker Lake (Oliver and Robbins, 1973) 2-degree sheets were projected onto the 7.5-minute series base maps for the Carson-Eagle Valley study area. Since the contour interval for these data is 5 milligals, the technique helped to delineate some of the major geologic structures in the subsurface but failed to resolve the minor structural details.

In the Big Smoky Valley Bouguer gravity data were also available but the area included was limited to the region north of latitude 39° (Erwin and Bittleston, 1977). This map also failed to provide the information needed for the area specific study, and a full scale gravity program was planned to gather. the necessary information.

Chemical analyses of both thermal and non-thermal waters were collected from several sources from both study areas. Garside and Schilling (1979) provided

major and minor element chemical analyses for thermal springs and wells in both study areas. Additional water quality data were collected from the files of the Consumer Health Protection Services, a Division of the Nevada Department of Health, in Carson City. These data pertain mainly to non-thermal waters and included only the major dissolved constituents.

Lithologic logs for residential and agricultural water wells are available for public inspection in the Office of the State Engineer, Carson City. Although the quality of most of the logs is poor, they have been helpful in determining the distribution and depth of warm water aquifers. This is especially true in the Pinyon Hills area in Carson City. Oil and natural gas exploration has been focused on Railroad Valley in southeastern Nevada and data from that area are, unfortunately, of little value in this study. Also, the data from mineral and geothermal exploration holes remain largely proprietary.

Geologic Reconnaissance

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The geologic reconnaissance consisted of identification of the important rock stratigraphic units and structures in the field. No large-scale geologic mapping was involved because of the need to complete the other items within the allotted time-frame.

Much of the reconnaissance was incorporated into other phases of the program such as the gravity and low sun-angle photo surveys. In the Big Smoky Valley several previously unmapped faults, which were identified on low sun-angle photographs, were verified during the geologic reconnaissance. Measurements of strike, dip and fracture and fault plane orientations were made in areas where a limited amount of geologic data were available. In addition, hydrothermally altered areas were examined for evidence of recent thermal spring deposits and cemented sediments.

Several representative samples of the major rock units were collected for petrographic examination, and the mineral assemblages were compared to thin

sections of chips from the geothermal test holes. X-ray diffraction techniques were also used to identify several microcrystalline and water-soluble mineral phases.

Gravity

Gravity measurements were selected as a means of obtaining useful subsurface structural information. This choice was based in part on the results obtained by other investigators working the Basin and Range region.

One of the earliest studies was carried out in the Virginia City and Mt. Rose quadrangle areas, Nevada, by Thompson and Sandberg (1958). Their study combined gravity data with density measurements of the surrounding sedimentary, volcanic and metamorphic rocks. From their data the authors were able to calculate the thickness of the sedimentary rocks in several of the basins. A more regional survey was completed by Thompson (1959) in the area between Hazen and Austin, Nevada. These measurements depicted a series of north-south trending horsts and grabens bordered by normal faults along which several thousand feet of vertical displacement had occurred. Stewart (1971) also used regional gravity data to characterize the Basin and Range, horst and graben structures for several areas in north-central Nevada. He interpreted the steep gravity gradients which occur near the basin-range interface as an indication of normal faulting. Goldstein and Paulsson (1979) integrated gravity data with seismic and deep electrical resistivity survey data in Grass Valley and Buena Vista Valley, Nevada. They were also able to estimate a basement configuration, fault patterns and depth to the Paleozoic basement.

Additional reasons for using gravity measurements were the ready availability of the necessary equipment and the relatively high rating assigned to the technique by Goldstein (1977) for area-specific studies.

Approximately 400 stations were occupied in the two areas examined during our study. Readings were taken using a Worden gravimeter having a scale constant

of 0.4656 milligals per division and a working range of 80 milligals. The instrument was allowed to thermally equilibrate (as judged by an unchanging reading over a five minute interval) for 15-20 minutes before making an initial measurement at the first station of a loop. A second reading was taken at the initial station as the termination measurement of the loop to establish instrument drift. Loop duration ranged from two to six hours with the smaller interval being used as frequently as conditions permitted.

Required elevation data were collected using a digital readout 30-power theodolite capable of measuring angles to the nearest three seconds of arc, combined with a 12-foot stadia rod. Control was established by tying in all measurements to U.S. Coast and Geodetic Survey and U.S. Geological Survey benchmarks. In general, the use of this equipment resulted in elevation measurement accuracy of approximately one foot over the horizontal distance covered.

Appropriate latitude and longitude data were computed for each station and combined with elevation data, raw measurements and instrument drift figures entered into a computer program for reduction to a simple Bouguer anomaly according to the formula adopted by the International Geodetic Commission in 1930. Reduction density was 2.67 grams per cubic centimeter. Terrain corrections were computed manually using the method of Hammer (1939) and applied to the "simple" data to obtain a "complete" Bouguer value.

The gravity data for all traverses conducted during this study are presented in Appendix II.

Aerial Photography

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Three approaches were employed in the application of aerial photographic techniques to our study areas: a) examination of moderate to high altitude imagery, b) low altitude photography along selected flight lines and c) low sun-angle photography. Efforts under the first category were limited to scrutiny of LANDSAT RBV imagery at 1:250,000 scale and 1:78,000 scale black and white

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U.S.G.S. aerial mapping photography. This imagery was used to check for the presence of regional trends which might be related to the location of geothermal occurrences within the area. Work within the second category involved the examination of black and white photographs flown at a scale of 1:12,000 along the same lines that were used in the gravity traverses. This was done to provide a means of searching for possible surface features related to subsurface changes as indicated by the gravity data. Low sun-angle photography was available at a scale of 1:12,000 for one of the study areas and was flown at a scale of 1:24,000 in the second area. An appropriate time of year was chosen to maximize sun-angle illumination and the photos were taken with 60% forelap and 20% sidelap to allow for stereoscope examination. Trexler and others (1978) demonstrated the usefulness of the low sun-angle photographic technique in studying geothermal occurrences in Nevada. The major use of the technique during our study was in delineating near-surface structural features associated with known geothermal manifestations.

Fluid Sampling

Thermal and non-thermal fluids were collected in each study area for analysis of major dissolved constituents, minor and trace dissolved species and oxygen and hydrogen stable light isotopic composition. The major goal of this segment of the study was to gather information on the nature and possible flow paths of fluids recharging the geothermal systems. This approach has been used with good results by several previous investigators as documented by White (1968), Ellis and Mahon (1977) and Cusicanqui and others (1975). Additional goals included providing a chemical data base compiled with uniform sampling and analysis procedures, and establishing a means of comparing the merits and drawbacks of each type of analysis on an area to area basis.

Sampling consisted of collection of a 250 ml raw unfiltered aliquot in screw-capped polyethylene containers for bulk and trace element analysis and 125 ml in a glass bottle for isotopic studies. In each case an attempt was made to

"top off" the container with liquid to reduce interaction with trapped air. Additionally, isotopic sample caps were dipped in hot paraffin prior to application and the top portion of the vessel was immersed in the wax to form an airtight seal. Samples of selected thermal fluids were also taken for sulfide analysis. Preservation of the sulfide was accomplished by the addition of 2N zinc acetate to the fluid at the time of collection.

Subsequent to collection, the raw and isotopic samples were promptly shipped to outside laboratories for analysis. The results of these analyses are listed in tabular form in Appendix B. Values for SiO₂ are derived from an undiluted sample using an atomic absorption analysis technique. Reported sulfide figures represent total recoverable sulfide, i.e., all sulfur species capable of reacting with zinc acetate.

Temperature Probe Surveys

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Temperature anomalies located near the surface of the ground can be mapped by using thermistor probes buried to a depth of 1 to 2 meters. These surveys have been most effective when probes are buried to depths at which diurnal effects are insignificant, approximately 1.5 m (Birman, 1969). However, temperature probes to a depth of 1 m have effectively delineated high temperature gradients in areas of known geothermal activity (Kintzinger, 1956; Olmsted, 1977). Seasonal temperature variations have been shown to be insignificant below a depth of approximately 6 m, but some temperature variations can still be measured at a depth of nearly 25 m.

Subsurface temperature surveys have been used to locate groundwater (Birman, 1969; Cartwright, 1966) to estimate thermal stresses on the walls of underground buildings (Singer and Brown, 1956) and to locate subsurface leaks in barge canals (Kappelmeyer, 1957).

In this study, temperature probes buried to depths of 1, 1.5 and 2 m were used to delineate areas of anomalous heat flow. Temperature measurements were

made with a DIGITEC model 5800 series portable thermometer. General purpose, vinyI-tipped thermistor probes were used in conjunction with the thermometer. The probes are 3 m in length and are equipped with a standard phone-jack. The thermometer is battery operated with rechargeable batteries, and the entire unit can be operated in the field for up to 16 hours without the use of an external power source.

Small diameter holes (8 to 9 cm) were drilled to the various depths with a gasoline-engine powered auger and a thermistor probe encased in a 2 m section of pvc pipe was emplanted. The holes were then backfilled and the entire unit including the phone-jack was covered with soil. The phone-jack was wrapped in a small plastic bag prior to burial to protect it from moisture condensation. Spacing between probes varied from 100 to 400 m depending on the size of the area under investigation.

Field tests indicate that reliable temperature measurements may be taken within 24 hours of the installation. This short reading interval is applicable only to those areas where relatively unconsolidated materials permit drilling times of ten to fifteen minutes per hole or less. In general, the holes were allowed 2 to 4 days to equilibrate. After reading the temperatures the probes were removed for further use in other areas.

For large areas, and working with a limited number of probes, the survey consisted of a series of sub-surveys. The area of interest was subdivided into smaller areas which could then be probed as a single unit. Probes were emplanted into one subdivision, allowed to equilibrate, measured and removed for use in the adjoining subdivision. For internal consistency one probe from the initial survey was left in the ground as a standard for the duration of the survey. The new temperature measurements could then be related directly to the previous measurements.

The 2 m temperature probe survey was employed in the Carson-Eagle Valley study area at Saratoga Hot Springs in the Big Smoky Valley at Spencers's

McLeod Ranch and Darrough's Hot Springs and in the Caliente Study area. A 1 m temperature probe survey was employed in the Carson-Eagle Valley at the site of the geothermal test hole number one.

Soil Mercury Geochemistry Surveys

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Soil mercury geochemistry is one of many types of soil surveys used in general geologic exploration. Soil mercury geochemistry has proved relatively reliable in geothermal energy exploration (Matlick and Buseck, 1975) and is a relatively simple exploration tool to use. The basic principle behind the method is that mercury is generally volatile above 80°C and since many geothermal systems are higher than 80°C at depth, mercury is released from the rock. The vaporized mercury then migrates upward until encountering absorbent clays, which capture the mercury. Many of these absorbent clays are found in the "B" or clayey horizon of soils.

Sampling this clayey soil layer provides the sample base for the analysis. After collection the samples are oven-dried at about 40-60°C to remove excess moisture. Then the samples are sieved to a minus 80 mesh (180 micron) fraction. These samples are then geochemically analyzed usually by an atomic absorption method or a Jerome gold film mercury detection machine (McNerney and others, 1972).

This data base is then analyzed and background values are determined. Anomalous regions are then studied to determine what relationship the soil mercury values have to the proposed geothermal system (i.e., structure controls, areal extent, etc.).

Resistivity Surveys

Electrical resistivity drilling surveys were carried out in several areas using a Geo-Western X-1 type prospecting instrument. This unit is designed primarily for traversing, and the self-contained 200-Watt converter supplies

sufficient current output to achieve a 500-foot depth penetration under nominal conditions.

The transmitter and receiver are housed in a single unit with a 12-Volt D.C. external, sealed, rechargeable power supply. The instrument is used in conjunction with solid transmitter electrodes and porous plastic potential electrodes which are designed for use with a saturated copper sulfate solution.

A Werner array was employed in both study areas and the electrode spacings used were 10, 25, 50, 100 and 200 feet. An attempt was made to use a constant electrode spacing of 25 feet for an electrical mapping survey near the McLeod Ranch Hot Springs.

The apparent resistivity (ρ_a) was calculated using the formula:

$\rho_a = \frac{2\pi "A" \text{ Delta V}}{I}$

where,

"A" is the electrode spacing in feet Delta V is the Impressed Potential in millivolts

I is the current in milliamperes

π is 3.14

The data were reduced by comparing the curves of electrode spacing vs. apparent resistivity plotted on 2 X 1 cycle logarithmic paper with two-layer model curves. The reduced data yielded a horizontal boundary layer between the surface and a second conducting layer located some distance below the surface.

Drill Site Selection Criteria

Locations for the slim temperature gradient holes were selected on the basis of numerous parameters. The sites were generally located within an area which showed anomalous values based on one or more of the field exploration techniques.

The primary parameters used in siting the holes were structural, proximity to known thermal anomalies, soil mercury anomalies, shallow temperature probe

surveys and land availability. Land availability was a key factor in the Carson-Eagle Valley area because much of that area is fee simple land. Thus, drilling was conducted on fee land which would have the greatest benefit to the maximum number of people. The sites were located on Carson City School District property, hole CC-1, and the University of Nevada property, CC-2. It was felt that if a resource had been found at either location it would have benefited more people than if the holes had been drilled on land owned by an individual or group of individuals.

Temperature Gradient Drilling

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Gradient drilling was implemented during the final quarter of the project as a technique to analyze selected areas for low- to moderate-temperature resources. The drill sites were selected from the data base which was developed from the field and analytical techniques described above, and on the availability of land and its potential use.

Five holes ranging in depth from 90 to 500 ft. were drilled. Cumulative footage was 1520 ft. which was 170 ft. more than originally planned. This additional footage was required because one of the original four holes, BSD-1, had to be abandoned due to drilling problems resulting from restrictions imposed on the drilling program by the BLM. All five holes were drilled according to the guidelines and regulations of the Geothermal Resource Operational Orders (GROO's) of the USGS.

General specifications for the holes were 6 1/2" surface casing to about 20 ft. with a 3" production casing string installed to total depth. Only three of the holes were completed to meet the general specifications due to problems or logistics which prevented the completion of the other two holes.

All five holes were drilled by the Rotary Division of Longyear, Inc. of Sedalia, Colorado. The drill rig was a Schramm Rotadrill Model CF 15

(fig. A2) with a 2565 Gardner Denver compressor and a 5"x6" two stage Gardner Denver mud pump. The bits used were a 7 1/2" tricone bit for the 6 1/2" surface casing and a 6" Ingersoll Rand downhole hammer or a 6" or 5 7/8" tricone bit for the remainder of the hole.

Of the five holes, four were drilled with air or partially with air and mud, and one hole was drilled with only mud. Drilling muds were primarily bentonite materials. Air drilling was augmented by the use of foam.

Generally, the data collected from the drilling and gradient tests made after the hole was completed were not encouraging. Only one significant temperature gradient was measured. This gradient was found in BSD-2 which was the third hole drilled in the Big Smoky Valley. Its gradient was 16.6° C per 100 meters. One of the holes in Eagle Valley was vandalized before gradient tests could be made. Thus, the end results of five holes were that only four could be tested and of these four only one provided enough positive data to predict the existence of a thermal anomaly.

The daily on-site drilling logs for each gradient hole are presented in Appendix III and completion diagrams are presented in Appendix IV.



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CARSON-EAGLE VALLEYS

Geographic Setting

The study area is located in west-central Nevada and occupies portions of Carson City and Douglas Counties (fig. Al). The 650-square-kilometer area is contained within two distinct valleys, Carson Valley and Eagle Valley.

Carson Valley, the larger of the two, trends north-south. It is approximately 32 km long and as much as 32 km wide. The elevation of the valley floor varies from 4600 to 5000 feet above sea level. Topographically it is bounded on the south by portions of the Sierra Nevada and the Pine Nut Range, on the west by the Carson Range, on the east by the Pine Nut Range and on the north by a low alluvial divide that separates it from Eagle Valley (fig. Bl).

Eagle Valley is much smaller. It attains a maximum north-south dimension of 13 km and a maximum east-west dimension of only 10 km. The elevation of the valley floor varies from 4600 to 4800 feet. Eagle Valley is bounded by the Carson Range (Sierra Nevada) on the west, the Virginia Range to the north and by the northern extension of the Pine Nut Range to the east (fig. B1).

The north-flowing Carson River is the principal drainage for both valleys entering the southeast end of Carson Valley and exiting at the east end of Eagle Valley.

The major population centers in this area are Carson City, the state capital (pop. 36,712) located in Eagle Valley and Gardnerville-Minden (pop. 3045) located at the southern end of Carson Valley.

Geology

Historically the area has been indirectly involved in many geologic studies because of its proximity to the famous Comstock Mining District at Virginia City, Nevada. More recently, however, it has become the focus of attention for environmental geology and earthquake hazard studies. The principal cause of



this is the large-scale urban development which is currently underway in Eagle Valley. The result is a rather substantial data base for this study.

The entire area is underlain by rocks associated with the Mesozoic granodiorite batholith. There are no Precambrian or Paleozoic rocks exposed. The oldest exposures are Jurassic-Triassic metamorphic rocks, which appear as roof pendants in the granodiorite. Post Mesozoic deposits include a series of Tertiary volcanics that range in composition from andesite to rhyolite. Most of the Quaternary formations consist of fluvial and alluvial deposits but a very recent basaltic-andesite volcanic vent and its associated flows is exposed in the Virginia Range just north of Carson City.

Moore (1969) has compiled the most comprehensive report on the area. The report contains a 1:250,000 scale geologic map which was completed on the basis of reconnaissance geologic field work in the mountain ranges where the rocks are best exposed as well as some more detailed work in and near important mining districts. A structural interpretation based partly on aerial photograph interpretation is also included.

In addition to the 1:250,000 scale map, geologic maps at a scale of 1:24,000 have been completed for the New Empire (Bingler, 1977), Carson City (Trexler, 1977), and Genoa (Pease, 1979) 7.5-minute quadrangles.

The geology of the area can be roughly divided into 3 sections (fig. B2). The western section is the north-trending Carson Range, the central section is the alluviated Carson-Eagle Valley and the eastern section consists of the Pine Nut Range and the southern portion of the Virginia Range. Although the rock units in each of these sections are distinct the areas are also separated from one another by north-trending range-bounding faults.

The Carson Range consists of a relatively homogeneous mass of granodiorite although extensive exposures of early Mesozoic volcanic rocks do appear as roof pendants in the batholith. The granitic rocks in this area are mapped as



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Figure B2. Generalized Geologic Map of Carson-Eagle Valley Study Area. (modified after Moore, 1969)

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undivided, non-porphyritic quartz monzonite and granodiorite (Moore, 1969). Similar rocks are exposed in the Pine Nut Range. The Carson Range is a horstlike structure and is bounded on the east by the Genoa fault. The displacement on this normal fault is greater than 1200 meters and a recent scarp is visible along the base of the range. This scarp is known to have existed since 1854 when the town of Genoa was first settled.

The Genoa fault extends from Walley's Hot Springs north and south along the range. To the north near Hobo Hot Springs the fault changes from a simple normal fault to a complex pattern of distributive faulting (fig. B3) (Moore, 1969). This pattern of distributive faulting may be the result of regional deformation that occurred during the Quaternary at the intersection of the northeast-trending Carson lineament (Shawe, 1965) and the north-trending Genoa fault. This abrupt change from north-trending to northeast-trending structures has been described as a "knee"-bend structure (Gilbert and others, 1968). In the area of the knee-bend the dominant style of deformation is block faulting although warping is also common.

The Pine Nut Range is a broad mountain block which is sharply upfaulted on the east and tilted westward (Moore, 1969). Metamorphic rocks of Triassic and Jurassic age and granodioritic rocks related to the Sierran Batholith are widespread in the eastern portion of the range. On the western side of the range extensive sections of Tertiary sedimentary and volcanic rocks as well as some Quaternary sediments overlie pre-Tertiary rocks.

The Pine Nut Range is separated from the Virginia Range directly to the north by a structural and topographic low (Moore, 1969). A complex sequence of interbedded Triassic and Jurassic sedimentary rocks including shale, limestone and gypsum crops out near the southern end of the Virginia Range. These rocks are also exposed in portions of the Pine Nut Range, and the limestones are the

host rock for the skarn-type mineral deposits. Gypsum is presently being mined at a quarry near Mound House, 12 km east of Carson City.

Unlike the Carson Range the interface between the Pine Nut Range and the valley consists of an intricate series of north-trending horsts and grabens which are also tilted to the west. The Carson Valley itself has been interpreted as the alluviated backslope of the Pine Nut Range (Moore, 1969). The sediments consist of unconsolidated to slightly consolidated Quaternary deposits and include gravels, sands, silts and clays. The maximum thickness of these sediments has been estimated to be at least 1200 meters. Further north in Eagle Valley basement rocks are within 200 to 400 m of where the surface Quaternary deposits are considerably thinner.

In the Carson-Eagle Valley area thermal springs are located near or at the periphery of the alluviated basin, and surficial evidence of faulting can be recognized at most of the sites. In addition to thermal springs, faults are recognized by scarps, abrupt changes in lithology and topography, the occurrence of sag ponds and the alignment of cold springs.

Walley's Hot Springs occur over an area of several acres with an estimated discharge of 600 gpm and a temperature range of 60° to 70°C (Garside and Schilling, 1979). The springs are located at a salient in the Carson Range (fig. B2) and discharge from portions of the Genoa fault. In 1962 and 1963, 26 shallow holes were drilled to determine the area of maximum water temperature (Garside and Schilling, 1979). Temperature profiles obtained for several holes indicate that the hot water is confined to a narrow fault zone. The fault zone was penetrated several times. In each case, the water temperature increased in the vicinity of the fault and then rapidly decreased away from the fault. The highest temperature recorded in a drill hole was 83°C at 20 m.

Hobo Hot Springs consists of 6 to 8 small springs with a combined flow rate of 10 to 20 gpm that range in temperature from 30° to 50° C. They also

occur over an area of several acres and their discharge appears to be directly related to several small faults (fig. B4) which have been mapped in that area (Moore, 1969; Pease, 1979).

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At the Saratoga site a single spring issues from the base of Hot Springs Mountain (fig. B2) and flows at a rate of 100 to 200 gpm. The temperature of this spring is 50°C and several warm and hot wells have been reported to the south and east of the spring. The surrounding area is covered by a thick layer of eolian sand of Quaternary age, and many of the surface manifestations of faults have been obscured. Several faults terminate near the southern end of Hot Springs Mountain and have been mapped by Moore (1969).

There is no surface discharge of geothermal fluids in the Pinyon Hills area located 8 km southeast of Carson City (fig. B2). Nearly 50 shallow residential wells in this area have measured water temperatures that range from 25° to 40°C. The wells in this area which range in depth from 60 to 150 m were not drilled for their geothermal benefit. The water was intended to be used for drinking and bathing but its temperature and hardness all but precluded that possibility. Some residents are now considering using the geothermal fluids for space heating. Approximately 1 km north of the thermal area, Bingler (1977) has mapped a normal fault in the Mesozoic sedimentary rocks. If extended southward the fault trend would pass through the center of the thermal area.

Carson Hot Spring located north of Carson City (fig. B2) flows from the contact between an outcrop of Jurassic metavolcanic rocks and the Quaternary alluvium. Rogers (1975) has mapped several small faults in the area of the springs but none seems to be aligned with the point of discharge. A group of normal faults that trend northeast parallel to the Carson Lineament (Shawe, 1965) occur approximately 1.5 km southwest of the spring. Directly to the south several north-trending normal faults have also been mapped. Displacements on these faults have been reported to be as much as 2 m.



Figure B4. Spatial relationship between Hobo Hot Springs and nearby mapped faults (after Pease, 1979)

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A small thermal spring flows near the site of the Nevada State Maximum Security Prison which is located at the north end of Prison Hill (fig. B2). The temperature of the water is 24°C and the discharge is very small. At the nearby Carson Sewage Plant a 60 m deep well produces water at a temperature of 32°C. Both of these thermal occurrences are associated with the normal fault that occurs at the northwest side of Prison Hill.

Gravity

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Much of the study area is included in a regional gravity map of the Reno, Nevada 1° by 2° quadrangle (Erwin and Berg, 1977). This 1:250,000 scale map is a compilation of data from several sources including extensive work by the authors. The data are adjusted to U.S. Air Force base stations and the terraincorrected results are presented in 5 milligal contour intervals.

In the southern part of the study area below latitude 39°N Oliver and Robbins (1973) have compiled a complete Bouguer gravity map of a portion of the Walker Lake, Nevada 1° by 2° quadrangle.

Taken together the maps indicate a large, deep depression in Carson Valley that narrows to the north in the vicinity of Hot Springs Mountain (fig. B5). A smaller and more shallow depression occurs in Eagle Valley just south of Carson City. A portion of the Carson Range, a prominent north-trending topographic high, extends to the northeast. The gravity contours indicate that it is joined with Hot Springs Mountain in the subsurface and forms a barrier between Carson Valley and Eagle Valley.

Although useful for examining regional geologic structures, maps at a scale of 1:250,000 cannot be successfully used to delineate those structures that are directly responsible for the control of geothermal fluid migration.

In order to further elucidate these structures and to supplement the existing gravity data base, gravity stations were established along three cross-valley traverses (fig. B6).





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An attempt was made to locate as many bench marks as possible in order to supplement the leveled stations and to check the accuracy of the leveling technique. However, many of the monuments could not be located and were presumably removed during highway expansion or maintenance. The calculated elevations agree with the existing data which appears on the U.S. Geological Survey topographic maps for the area.

A total of 129 gravity stations were occupied in the Carson-Eagle Valley Study Area. All of the pertinent station data including latitude and longitude, elevation and gravity results are presented in tabular form in Appendix II.

Topographic profiles and gravity profiles, including both simple Bouguer and complete Bouguer data are illustrated for the three traverses in Figures B7, B8 and B9. The gravity profile roughly approximate the basement configuration and each figure depicts one-half of the length of a particular traverse.

The gravity profile for the Carson Hot Springs area, traverse CS - figures B7A, B7B - is the least diagnostic of the three. The gravity profile does show a slight gradient in the vicinity of the spring which corresponds to a northeasttrending normal fault mapped nearby (Rogers, 1975). The bedrock in this area consists of a series of metamorphosed Mesozoic volcanic and sedimentary rocks which dip 30° to the south and strike east-west. Based on the lithologic logs from several water wells in the area the vertical displacement on this fault is approximately 10 to 15 m. In the vicinity of the traverse directional change, figure B7A, the gravity data also correspond with Rogers' (1975) interpretation of a thickening of the Quaternary deposits. Further to the southeast along traverse CS (Figures B7A, B7B) gravity values decrease and peak near the Carson River. This gravity high is interpreted to be the buried northern extension of Prison Hill. Continuing to the southeast the basement structure is obscured by a thick section of Tertiary volcanic rocks, but some displacements can be identified in the gravity profile. These displacements correlate well with

north- and northeast-trending normal faults which are exposed at the surface to the south in Jurassic and Triassic sedimentary rocks.

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The HS traverse, figure B8, was designed to pass through two geothermal areas, Hobo Hot Springs and Saratoga Hot Springs. The gravity profile for this traverse shows two prominent gravity highs coincident with two topographic highs separated by a gravity low. The topographic expression for the gravity low is the flat alluviated surface of the north end of Carson Valley.

At Hobo Hot Springs faults mapped on both sides of the topographic high (fig. B2) correlate well with the steep gradients in the gravity contours (fig. B8A). Similarly, at Saratoga Hot Springs the steep gravity gradient on the west side of the topographic high and the gravity low on the east side (fig. B8B) correspond to the faults which are exposed just to the south (fig. B2). At both geothermal sites the springs are directly associated with both the surface manifestations of faulting as well as the basement offset which was identified by the gravity profile.

The final traverse, DF, trends west-east from Walley's Hot Springs (fig. B6). The configuration of the gravity profile, figures B9A, B9B, seems to confirm the hypothesis for the basement structure proposed by Moore (1969) as a west-tilted fault block. The thesis further states that the west side of the valley has been filled with a thick section of alluvial deposits of Quaternary age.

The gravity profile near the hot springs shows an extremely steep contour gradient and indicates substantial offset along the fault (fig. B9A). The eastern section of the traverse delineates a gravity high which contains several irregularities. These irregularities are modest gravity gradients and are roughly coincident with the location of several north-trending normal faults (fig. B2); the irregularities in the profile probably represent offset along these faults in the subsurface. This configuration supports a second hypothesis for the basement structure in the Carson Valley, a slightly west-tilted asymmetrical



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Figure B7a . CS gravity traverse, northwest section.



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Figure BBa . HS gravity traverse, western section.



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graben. This graben is bounded on the west by the steeply dipping (60°-70°) Genoa Fault and on the east by a series of nearly vertical normal faults (fig. B2).

Similar gravity surveys have concluded that steep gravity gradients associated with range-bounding faults support the horst and graben hypothesis for Basin and Range structure (Thompson and Sandberg, 1958; Thompson, 1959; Goldstein and Paulsson, 1979).

An estimation of the thickness of the Quaternary alluvial sediments can be made using the formula T = A/0.013S (Thompson and Sandberg, 1959) where T is the thickness of the sediments in feet, A is the difference between the regional gravity gradient and the local gravity anomaly and S is the difference in specific gravity between the sediments and the bedrock. The number 0.013 represents the attraction of an infinite slab in milligals per foot of thickness, and a value of 0.5 grams per cubic centimeter has been assigned to the contrast in specific gravity between bedrock and alluvium.

Figures BlOA, BlOB show the approximate configuration of the basement along traverses DF and CS, respectively. The figures indicate that the alluvial fill along both traverses may reach depths of 1.2 km (5000 ft) which is comparable to the topographic relief. In both figures the vertical scale has been greatly exaggerated so that minor irregularities in the basement surface which probably represent small displacements along faults can be more easily identified.

Aerial Photograph Interpretation

Aerial photographs were used to trace fault patterns at Walley's Hot Springs, Hobo Hot Springs and Saratoga Hot Spring. The imagery for this task included the use of black and white vertical photos (scale, 1:12,000), low-sun angle photos (scale, 1:12,000) and various scale oblique photos.



Vertical and oblique air photos were flown along the lines of traverse used in the gravity survey (fig. B6). An attempt was made to correlate observable surface features with gravity anomalies.

The trace of the Genoa fault can be easily identified in the oblique air photo (fig. B11) as well as in the vertical photo (fig. B12). This is a recent scarp possibly less than 300 years old and can be traced for more than 20 km along the east side of the Carson Range. The displacement along this fault scarp varies from 2 to 5 meters and total displacement along the entire fault plane may be as much as 1200 meters. The springs at Walley's appear to emanate directly from the fault zone.

Further north at Hobo Hot Springs a series of less extensive faults branch out from the larger Genoa fault. In figure B13 as many as 4 hot springs can be identified flowing from the fault zone which trends to the northeast. Even though the fault can be traced at least 2 km to the northeast the hot springs flow only from the small area shown on the photo.

Although somewhat obscured by eolian sand deposits of Quaternary age the trace of a normal fault can be seen just to the south of Saratoga Hot Springs (fig. B14). The spring flows from a point along the fault zone.

Gravity survey data also correlate well with the surface manifestations previously discussed. Gravity profiles in the vicinity of the fault scarps shown near Saratoga, Hobo and particularly Walley's Hot Springs all show steep gravity gradients near the spring orifices.

Air photo interpretation is useful in areas that have not experienced extensive urban or agricultural development which may obscure fault scarps. In figure B15 which is a vertical airphoto of Carson Hot Spring, fault scarps cannot be clearly identified. The photo indicates that the housing developments surrounding the spring may have already obliterated the subtle topographic features which are used to identify recent faulting.





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Figure B 15. Aerial photograph of the Carson Hot Springs area. (Scale 1:12,000).

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The final oblique air photo (fig. Bl6) depicts the spatial and areal distribution of hot springs in the north end of the study area. Other important features such as the drill site CC-1, the Mound House gypsum mine and the Carson River are also shown.

Fluid Geochemistry

Chemical analyses of water samples from the Carson-Eagle Valley study area were obtained from several sources. Analyses from the files of the Nevada Department of Health Division of Consumer Protection included Ca^{+2} , Mg^{+2} , K^+ , Na^+ , $S0_4^{-2}$, $C1^-$, $HC0_3^-$ and $C0_3^{-2}$. The chemical analyses from this source pertained mostly to residential and commercial shallow-depth water wells. Many analyses of thermal waters were found during the initial literature search including Garside and Schilling (1979) who provide major, minor and trace element analyses for most of the thermal waters in the study area. In addition to published data 13 water samples from thermal and non-thermal sources were collected and analyzed for major, minor and trace elements plus stable isotopes of hydrogen and oxygen. Table B1 lists the source and location as well as all of the pertinent physical and chemical data for each sample collected. Data collected from the other sources are listed in Appendix I.

In general, the waters from the Carson-Eagle Valley study area can be divided into three groups based on the analyses of the major dissolved constituents which were listed above. The classification is illustrated in the trilinear diagram (fig. B17) which shows the anion, cation and average "total" compositions of the fluids (Piper, 1944).

In the trilinear diagram the anion $(HCO_3^{+} + CO_3^{+2}, SO_4^{+2})$ and C1) and cation $(Ca^{+2}, Mg^{+2}, and Na^{+} + K^{+})$ compositions are represented on the small triangles. Fluid composition for a particular sample is represented by either open circles (non-thermal fluids) or closed circles (thermal fluids). The



Sample Name	Sample Number	Location	T ^o C	pĤ	SC µmhos	B ppm	Ca ppm	Mg ppm	K ppm	Na ppm	Li. ppb
Hobo Hot		SE4,SE4,Sec.23,	· · · · · ·	· · · · · · · · · · · · · · · · · · ·	• .		••••				
Spring	CW1	T14N,R19E.	46	7.93	778	2.07	4.34	<0.05	1.64	142	350
Walley's	Hot	NW4, NE4, Sec. 22,			-						
Spring	CW2	T13N,R19E.	58	9.08	778	1.55	9.81	<0.05	3.98	130	215
Job's Car	iyon .	SW1, SW1, Sec. 14,	ŕ., ,	;		· ·		·			
stream	CW3	T12N,R19E.	3	7.58.	62	0.077	7.57	0.994	0.456	4.18	10.8
Carson R:	lver.	NW%, SW%, Sec. 31,			· .'						
south	CW4	T13N,R20E.	3.5	7.98	224	0.429	20	5.07	2.43	15.7	35.1
City of 1	finden	SWR. SWR. Sec. 29.	•			·				•	
well	CW5	T13N,R20E.	12	8.08	216	0.291	-22	5.64	2.43	12.9	20.1
Unruh's		SEX.NWX.Sec.33.				199	•				
well	CW6	T14N,R20E.	12	8.25	329	0.186	28.1	~7.43	5.41	27.6	20.5
Saratoga		SH4.NW Sec.28.				•	2		2	. *	
well	CW7	T14N,R20E.	26	7.32	1847	0.125	168	<0.05	5.17	159	100
Saratorà	Hot	SFk. SWk. Sec. 21	,		· .	•	•			¢	
Spring	CW8	T14N,R20E	50	8.55	1857	1.37	166	0.10	5.03	161	95.5
Carson Se	wage	NWX.SWX.Sec.15.				•					•
Plant	CW9	T15N,R20E.	32	7.83	501	1.19	11.6	<0.05	0.632	89.5	84.8
Noble Mu	rrav	NEL SWA. Sec. 23.				· · · ·	•			:	
well	CW10	T15N,R20E.	41	7.26	2470	1.39	270	0.14	5.90	173	120
Carson H	ot	SE4, NE2, Sec. 5,									
Spring	CW11	T15N,R20E.	50	8.84	-515	1.48	2.16	<0.05	1.64	98.5	216
Carson R	iver,	SEL, SWL, Sec.23,				· · ·			,		•
north	CW12	T15N,R20E.	5	8.09	299	0.418	25.3	6.43	3.68	22.4	31.2
	÷.	•					·			· · ·	•
Dodd wel	1 CW13	NE ¹ 2, SW ¹ 2, Sec. 31,	16	0 1 -	207	0.0614		e en		10 2	5 0
	•	T,1/N,KZUE.	10	8.15	297	0.051	51.9	0.02	2.13	18.3	5.0

Table B1 . Chemical analyses of water from sampled sites:

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Sample Number	C1- ppm	NO3/NO2 ppm	510 ₂ ppm	SO ₄ /S ^{≖*} ppm	СО3/НСО3 ррт	F- Ppm	As ⁺⁴ ppb	Ba ppm	Fe+2 ppm	Rb ppb	Cs ppb	Sr ppb
CW1		<0.01	38.3	133/ .707	72.8	7.83	19.8	<0.1	0.04	13.2	<3	<200
CW2	45.5	0.06	72.3	205	42.6/ 1.90	4.66	167	<0.1	0.03	57	17.2	210
сиз	0.31	6 <0.01	21.8	6.15	28.4	0.208	< 5	<0.1	0.167	<1	<3	<200
CW4	8.18	<0.01	24.6	25.4	82.4	0.185	14.9	0.08	0.192	109	4.2	298
CWS	4.94	1.34	33.8	16.3	100.1	0.110	<5	0.08	0.243	2.2	< 3	298
CW6	7.46	2.55	77.9	34.6	140	0.364	20	0.16	0.03	<1	4.8	210
CW7	39.6	0.869	25.5	617/ .264	23.4	3.26	<5	<0.1	0.066	40.8	4.8	2520
CW8	39	<0.01	33	617/ .215	11.2/ 4.51	3.26	<s< td=""><td><0.1</td><td>0.04</td><td>41.2</td><td><3</td><td>2380</td></s<>	<0.1	0.04	41.2	<3	2380
CW9	19.7	<0.01	35.5	132	47.4	6.42	50.3	0.08	0.447	2.2	4.2	<200
CW10	34.3	<0.01	43.9	843	26.4	4.14	<5	0.1	0.116	63.9	15.9	2950
CWII	27.4	<0.01	59.5	89.4	13.3/ 56.7	7.53	75.5	<0.1	0.03	32	24	<200
CW12	11.3	0.75	23.8	37.7	111	0.336	5.5	<0.1	0.192	8.4	5.5	350
CW13	3.19	13.4	34.7	18.3	137	0.217	< 5	0.08	0.550) ~1	4.2	350

*Measured and reported as total recoverable sulfide.

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apexes of the triangles represent 100 percent of the indicated dissolved species. The center of each triangle represents a fluid composed of essentially equal amounts of the species designated at the apexes. A 'total' chemical analysis for a particular fluid is represented by a point in the center quadrilateral which can be derived by projecting the association anion and cation compositions from the triangles into the quadrilateral. Total analysis for Steamboat Hot Springs fluids (open square) is obtained by projecting the cation value (in the left triangle) and the anion value (in the right triangle) into the quadrilateral along lines parallel to the quadrilateral coordinates.

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Non-thermal waters (T<20°C) account for the majority of the plotted points, and these also show the largest variation in chemcial compositions. Most of the non-thermal waters show CO_3^{-2} + HCO₃ enrichment relative to Cl and SO_4^{-2} . Some fluids show SO_4^{-2} enrichment which is probably the result of mixing with sulfate rich thermal waters. None of the samples have Cl⁻ compositions higher than 25 percent. The cation compositions of the non-thermal waters is also widely distributed but most of the waters consist of approximately 40 percent Ca^{+2} , 40 percent Na⁺ + K⁺ and 10 percent Mg⁺².

The 'total' analysis shows two categories of thermal waters both of which are chemically different from the non-thermal waters. The Na⁺-SO₄⁻² waters include Walley's, Hobo and Carson Hot Springs, and plot near the open square that represents waters from Steamboat Hot Springs. The Ca⁺²-SO₄⁻² waters include samples from the Saratoga Hot Springs area and the Pinyon Hills area. These waters plot near the upper apex of the quadrilateral. Chemical variation between these two water types is small compared to the non-thermal waters.

Figure B18 shows the geographic distribution of both thermal and non-thermal waters throughout the study area. The name, location and chemical data for each of the symbols is listed in Table B2. The chemical similarity of the two types





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TABLE B2. Chemical Data (in milliequivalents per liter) for Symbols in Figure B18.

Sample Name	Sample Number	Ca meq/l	Mg meq/1	K meq/l	Na meq/1	SO4 meq/1	Cl meq/l	F meq/1	HCO ₃ meq71	CO3 meq71	Data Source
Hobo Hot Springs	1	.217	0	.042	6.18	2.77	2.58	.412	1.19	0	A
Walley's Hot Springs	2	.490	0	.102	5.66	4.27	1.28	.245	0	1.42	A
Saratoga Hot Springs	3	8.28	.008	.129	7.00	12.9	1.10	.172	.074	.373	A
Carson Hot Springs	4	.108	0	.042	4.28	1.86	.773	.396	.929	1.372	А
Job's Canyon Stream	5	.378	.082	.012	.182	.128	.008	.010	.465	O	А
Carson River South	7	.998	.417	.062	.683	.529	.231	.009	1.35	0	A
City of Minden Well	8	1.10	.464	.062	.561	.340	.139	.005	1.64	0	A
Unruh's Well	9	1.40	.611	.138	1.20	.721	.210	.019	2.29	0	A
Bennett Well	14	13.98	.093	.139	9.60	22.0	1.01	.205	.360	0	С
Dickerson Well	32	.999	.576	.076	.869	.041	.197	.011	2.16	0	с
Maximum Security Prison Well	41	.674	.027	.051	3.56	3.08	. 593	0	.785	0	в
Medium Security Prison Well	48	1.59	.576	.025	.652	.145	.254	.013	2.38	0	с
Bowland Well	56	16.98	2.30	.357	13.04	25.37	1.69	.097	2.88	0	С
Sullivan Well	57	1.04	.411	.051	.869	.020	.141	.007	1.91	0	с

Sources of Data: A. AMTECH LABS, this study

B. Trexler and others, 1979

C. Nevada Division of Health, public files

of thermal waters is preserved even for hot springs separated by as much as 25 km. The figure also indicates the chemical variations in the non-thermal waters especially near the Mound House gypsum mine in the northeast corner of the study area.

Trexler and others (1979) have shown that $Na^+-SO_4^{-2}$ rich fluids are the dominant thermal fluids in a region that extends north from the study area to Reno and southeast as far as Tonopah. Adjacent to this large region is an equally large area in which Na^+-Cl^- type geothermal fluids are the dominant type. This area extends from the Steamboat Hot Springs area north approximately 120 miles to Winnemucca and as far east as Fallon. $Ca^{+2}-SO_4^{-2}$ type waters occur in both of these regions and include waters from Virginia City, Mound House, the Pinyon Hills area and the Saratoga Hot Springs area. The chemical similarities of these water types suggest that Triassic and Jurassic age deposits of gypsum and anhydrite which are presently being mined at Mound House extend from the mine site to the southwest along the west side of the Pine Nut Range. Geothermal fluids compositionally similar to the Steamboat Hot Springs fluids probably interact with the sulfate deposits in the subsurface and produce the characteristic $Ca^{+2}-SO_4^{-2}$ type fluids.

The investigation also included analyses of the following minor and trace elements: F^- , As^{+4} , Ba^{+2} , Fe^{+2} , Rb^+ , Cs^+ , and Sr^{+2} . Regrettably, these data were of comparatively little value for the investigation.

Fluoride (F⁻) was the only minor element that showed any correlation to water temperature. The data are not conclusive but Figure B19 illustrates that thermal fluids contain significantly more F⁻ than non-thermal fluids.

Strontium values for most fluids analyzed (table B1) were 350 ppb or less with the exception of the two samples from the Saratoga Hot Springs area and the one from the Pinyon Hills. The strontium values for these fluids range from 2380 ppb to 2950 ppb. The characteristic strontium values for these moderately separated geothermal fluids (10 km at the surface) are probably due to the chemical





similarities between calcium and strontium. Calcium has an ionic radius of $0.99\overset{\circ}{A}$ which is very close to that of strontium, $1.12\overset{\circ}{A}$. Strontium is also found in greatest amounts in calcium-rich minerals such as calcite (CaCO₃) or anhydrite (CaSO₄). Strontianite (SrCO₃) and celestite (SrSO₄) are usually associated with the respective calcium-rich minerals. The characteristic strontium values also indicate that thermal fluids are interacting with gypsum and anhydrite deposits in the subsurface.

The sampled fluids were also analyzed for deuterium (D) and ¹⁸0 which are the stable isotopes of hydrogen and oxygen, respectively. The results of these analyses are presented in Table B3. Figure B20 shows the isotopic compositions of the sampled fluids relative to the Worldwide Meteoric Line and some of the Steamboat Hot Springs fluids. The samples are essentially isotopically identical with respect to ¹⁸0 because the magnitude of the difference between the heaviest and lightest waters (1 and 2) is not significantly greater than the magnitude of the error bar (2 °/00). A small distinction does exist however in the samples with respect to D composition. Most of the thermal waters with the exception of sample number 1, have $\delta D^{\circ}/oo$ values of -119 or less. High negative values for D are generally attributed to fluids derived from snow which contains the isotopically lightest water. Nehring (1979) has shown waters sampled from the Virginia and Carson Ranges are isotopically lighter than surface and ground waters in the adjacent valleys. For these relatively dilute and neutral thermal waters it appears that a likely source or recharge fluids is the snow pack in the Sierras and, to a lesser extent, the Pine Nut and Virginia Ranges.

Chemical geothermometers can be useful for semiquantitative estimates of geothermal reservoir temperatures when certain assumptions regarding the chemical behavior of thermal fluids have been satisfactorily met. The common chemical geothermometers include the use of dissolved SiO_2 , Ca^{+2} , Mg^{+2} , K^2 and

Hydrogen and Oxygen stable light isotope Analysis results - Carson-Eagle Valleys

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Sample Name	Sample Number	δD ⁰ /00	\$ ¹⁸ 0°/00	T°C
Hobo Hot Spring	1	-115	-13.7	46
Walley's Hot Spring	2	-132	-16.3	58
Job's Canyon Stream	3	-117	-15.4	3
Carson River, South	4	-116	-14.6	3.5
City of Minden Well	5	-120	-14.3	12
Unruh's Nell	6	-118	-15.4/-15.0	12
Saratoga Vell*	7	-133	-16.0	26
Saratoga Hot Spring	8	-130	-16.2	50
Carson Sewage Plant	9	-123	-15.4	32
Noble Murray Well	10	-130	-16.2	41
Carson Hot Springs	11	-127/-128	-14.9	50
Carson River North	12	-121	-14.0	5
Dodd Well	13	-120	-14.2	16
Saratoga Well*	16	-133	-16.1	26

Values separated by a slash indicate duplicate runs on a single sample.

* Two samples collected simultaneously and submitted under different designations.



Carson-Eagle Valley

Figure 820. Stable light-isotopes of thermal and non-thermal fluids. Worldwide meteoric water line (after Craig, 1963). Numbers refer to samples in Table 83.

Na⁺. The temperature estimate is based on the variations in the solubilities of the dissolved constituents as the fluid temperature is increased. One of the critical assumptions states that mixing of thermal and non-thermal fluids does not occur. The trilinear diagram (fig. B17) illustrates that some mixing of thermal and non-thermal fluids does occur in the study area and essentially rules out any serious consideration of chemical geothermometers for use in this portion of the study.

Silica geothermometers yield accurate results for neutral to slightly acid pH fluids (USGS, 1978). Fluids with pH greater than 8 such as some of those listed in table Bl may contain anomalously high concentrations of dissolved silica especially in granitic terrains. Table B4 illustrates the use of the chalcedony geothermometer assuming conductive cooling of the fluid.

Fournier (1979) has re-evaluated the Na/K geothermometer and the results of the use of the revised equation for thermal waters from the Carson-Eagle Valley study area are also presented in table B4. These temperature estimates ranging from 75° C to 134° C are presented only to demonstrate that there is considerable scatter in the data.

The data indicate that the range of temperature estimates from chemical geothermometers at Carson and Walley's Hot Springs is negligible compared with the other thermal fluids. These consistent data may accurately reflect maximum temperatures that can be expected at economical depths. The estimates at Walley's also concur with the maximum temperature measured in a 20 m deep well.

Shallow Depth Temperature Probe Surveys

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Temperature probe surveys to depths of 2 m and 1 m were conducted at Saratoga Hot Springs and drill site CC-1, respectively. At the Saratoga site 23 2 m and 2 1 m holes were drilled. The thermistor probes were allowed to equilibrate for 24 to 72 hours. Eighteen thermistor probes were used at drill site CC-1 and they were allowed to equilibrate for 5 days.

Drilling at the Saratoga site was easy because most of the material consisted

Table B4.

Location	т ^о с	Depth (m)	Chemical geothe Chalcedony ¹	ermometers* Na/K ² •
Hobo Hot Springs	46	surface	57	90
Saratoga Hot Springs	50	surface	50	134
Saratoga Hot Wells	55	61	39	110
Carson Hot Springs	50	surface	79	75
Walley's Hot Springs	58	surface	89	90
U.S. Steel Wells	83	30-365	(maximum te 20 m inter front faul	emperature at sected range

Temperature estimate of thermal waters in Carson and Eagle Valleys

* Equations for geothermometers

1. Chalcedony, conductive cooling

$$t^{o}c = \frac{1015.1}{4.655 - \log 100} - 273.15$$

2. Na/K

$$t^{\circ}c = \frac{1217}{\log(Na/k)t1.483} - 273.15$$

of coarse- to medium-grained unconsolidated sand with some minor lenses of clay. These deposits belong to a Quaternary age sedimentary unit of eolian sand and are very common along the east side of Carson Valley. The material at drill site CC-1 consisted of a thin soil horizon (.5 m) which was underlain by a thick regolith that mantled the Mesozoic volcanic rocks. This material could not be penetrated to any significant depth with the hand-operated power auger; a jeepmounted auger was used instead for drilling the 1 m holes in this area.

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At the Saratoga site the measured temperatures range from 18°C to 35°C and the survey covered an area of approximately 25 square km. The highest recorded temperature was measured at a probe located nearly .8 km south of the hot spring. The spring itself discharges from a point 60 m northwest of its original orifice. It was moved several years ago during construction of a road.

The configuration of the isotherms (fig. B21) delineates a linear zone of high heat flow which is parallel to the nearby range-bounding fault. The data also show that the area of highest heat flow extends for only .8 to 1.2 km in a north-douth direction. Temperatures drop off even more rapidly west of the thermal high. The isotherms also reveal that the zone of highest heat flow is not coincident with the orifice of the hot spring.

These data suggest that geothermal fluids are rising along a selected portion of the fault and produce a linear isotherm configuration as they spread out near the surface. Although no fault scarp is exposed or mapped the abrupt topographic and lithologic change at the southern end of Hot Springs Mountain (fig. B21) suggest the presence of an east-west trending normal fault possibly related to a similar fault near Hobo Hot Springs four miles to the west. The intersection of such a fault with the existing north-trending fault correlates well with the location of the highest recorded temperatures in the 2 m probe temperature survey.

A shallow depth temperature probe survey was initiated at Carson Hot Springs but was not completed because of drilling difficulties. The area is also highly developed and many of the existing structures including several buildings, a



Figure 821. Spatial relationship between Saratoga 2 m. temperature probe isotherms and nearby fault (modified after Moore, 1979). Isotherm contour interval is 2°C; ball on downthrown side of fault.
swimming pool and a paved parking lot precluded the deployment of temperature probes in the vicinity of the hot springs.

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The surface material at Hobo Hot Springs consists almost entirely of coarse gravel and alluvial fan conglomerates which cannot be drilled with gasolinepowered auger. The area is also a prime grazing pasture for cattle owned by the Stewart Indian School, and access was limited to reconnaissance activities.

A shallow depth temperature probe survey was also completed at the primary site for the 150 m temperature gradient hole, CC-1. At this site the temperatures ranged from 6.5° to 8.5° C (fig. B22) over an area that measured .4 km wide and .5 km long. There are no thermal springs associated with this site but the Pinyon Hills thermal area (fig. B2) is located across the valley 2 miles to the east.

The configuration of isotherms (fig. B22) outlines a small area of somewhat higher heat flow near the south end of the property. This thermal high is bounded on both the east and west by normal faults. The thermal area located on the horst was thought to be the result of thermal fluids percolating up one of the adjacent faults. Subsequent drilling, however, failed to locate thermal fluids; the highest temperature recorded in the well was 20°C. The temperature difference shown on the isotherm map may be the result of solar radiation warming the ground surface on the south end of the property.

No temperature probe survey was attempted at Walley's Hot Springs because the area surrounding the springs is a swamp. In 1962 and 1963 the Columbia Mining Co., a subsidiary of U.S. Steel, drilled 26 shallow holes in the area around Walley's Hot Springs (Garside and Schilling, 1979). The maximum temperature encountered was 83°C at 21 m depth.

Figure B23 is a shallow temperature gradient map of the Walley's Hot Springs area based on temperature logs of the 26 holes. The isothermal contours were derived using the formula:



Figure B22. Shallow depth isotherms and mapped faults at drill site CC-1. Ball on downthrown side of fault. (after Bingler, 1978)



Figure B23. Spatial relationship between shallow temperature gradients and nearby mapped faults. See text for explanation. Ball on downthrown side of fault. (after Garside and Schilling, 1979)

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 $T_{iso} = \frac{T_{max} - T_{amb}}{Depth_m}$

where, T iso is the isotherm temperature

T_{max} is the maximum recorded temperature

Tamb is the mean annual ambient temperature

Depthm is the depth of maximum temperature

It should be noted that all of the temperature profiles show reversals at various depths and the isothermal contours should not be extrapolated.

The data show that the highest water temperatures are limited to the fault zone not only in an east - west direction but also north and south. This observation supports the hypothesis that only a selected portion of the fault zone is being used to conduct rising geothermal fluids.

Figure B24 illustrates the shallow temperature gradients in the Pinyon Hills area and was constructed on the basis of existing water well data. A formula similar to that described for the Walley's Hot Springs area was used to derive the isotherms but the gradient is expressed in units of °C/100 m.

The data show that the isotherms form a linear configuration that is parallel to the range-bounding fault which is exposed just north of the area. The hightemperature isotherms show closure and are of limited areal extent suggesting that only a portion of the fault is currently conducting geothermal fluids.

Soil Mercury

Three soil survey traverses were established concurrently with the gravity traverses in the Carson-Eagle Valley area. Time and budget restrictions limited the extent of the soil geochemistry studies to the existing traverses although the northern traverse, CS, was expanded to cover a larger area.

In general, the data show anomalous mercury values adjacent to known thermal anomalies and the Sierran front indicating a possible thermal source at depth



Figure B24. Spatial relationship between Pinyon Hills Wells shallow temperature gradient and nearby mapped faults. Contour interval is 20°C; ball is on downthrown side of fault (after Bingler, 1978)

along the Sierran front. The highest anomalous values greater than 6000 parts per billion are located on the CS traverse along the northern Pinyon Hills. The closest geothermal anomaly is the Pinyon Hills area which is 2-3 km south of this mercury anomaly.

Further research of this anomalous area revealed that nearby is a site for several gold and silver mills operated during the mining of the Comstock Lode from approximately 1850 to 1900. These mills used mercury amalgamation to process the ore. Therefore, the anomalous mercury values for these soils is certainly artificial. Thus, this particular mercury soil geochemistry anomaly can not be directly related to a geothermal anomaly. Figure B25 shows the anomalous soil mercury areas in the Carson-Eagle Valley area.

A detailed soil mercury survey was conducted on the property selected for the location of one of the gradient holes, CC-1. Figure B26 shows the results of the survey. The northeast trending zone is subparallel to a fault trending north-northeast in the east central portion of the study area.

Electrical Resistivity Surveys

Using a Werner array for the electrode spacing which ranged from 3-60 m (10-200 ft), electrical resistivity drilling surveys were attempted at Carson Hot Springs and Hobo Hot Springs. The results were not very diagnostic. The data for the Carson area show a conducting layer at 13 m (42 ft) below the surface but this may simply be the top of the water table. Unfortunately, no large scale electrical mapping could be attempted due to the presence of many buildings and recreational vehicles on the property.

A similar experiment was attempted at the Hobo Hot Springs and a conducting layer was found at 15 ft. below the surface. Here, too, electrical mapping was not attempted.

This task was originally intended to aid in the location of unexposed faults. Unfortunately, the benefits of using electrical methods are not matched by the



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Figure B26. Contour map of mercury (concentrations in ppb) in soil sample at drill site CC-1.

cost of implementation. The method is time consuming and the results are ambiguous. Three other methods, air photo interpretation, soil analysis for mercury and shallow depth temperature probe surveys can be implemented more quickly and more economically over a wider range of conditions and produce results that are more unequivocal.

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Drill Site Selection Criteria in Carson-Eagle Valley

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The two gradient holes in the Carson-Eagle Valley area, CC-1, and CC-2 were located on the basis of land availability as well as geologic structure criteria. Much of the property in the area is fee simple land is owned by individuals. The holes were located on public land to avoid a possible conflict of interest. The possibilities for selection included properties owned by the Carson City School District, the Carson City municipalities and the State of Nevada.

The final site selections were based on several parameters. CC-1 was sited east of Carson City on property owned by the Carson City School District (fig. B27). This site is located between two known thermal anomalies, Pinyon Hills to the east and the Carson City Sewer Plant to the west and is also the location of a proposed new school building. The actual drill site was located on the basis of temperature survey combined with the presence of a soft, muddy zone surrounded by frozen ground.

CC-2 was selected on the basis of land availability and was located on property owned by the University of Nevada System near the Western Nevada Community College. This area also showed evidence of snow melt patterns indicating a possible high heat flow area and was situated in an area of recent faulting (fig. B3).

Other sites had been considered but they did not meet the requirements needed for a gradient hole site.



Figure 827 . Locations of temperature gradient holes CC-1 and CC-2 in the Carson-Eagle Valley.

Carson-Eagle Valley Gradient Drilling

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The first two gradient holes of the project were drilled in Eagle Valley during the month of February, 1980. The holes were located on opposite sides of Eagle Valley (fig. B27) and were designated CC-1 and CC-2.

CC-1 was located between two thermal anomalies within Eagle Valley, Pinyon Hills to the east and the Carson City Sewer Plant to the west. Drilling began on 12 February at approximately 4:30 p.m. using a 7 1/2" tricone bit to drill a large enough hole for the 6" surface casing. Drilling was carried out by a single crew on a 12-hour shift with project personnel on hand to monitor the return temperatures and log the cuttings during the entire shift.

A single joint (22 ft) of 6" casing was installed in the hole on the morning of the 13th. The 7 1/2" tricone bit was replaced with a 6" Ingersoll Rand downhole hammer which was used to drill the remainder of the hole. Drilling continued at a moderate rate until the 15th when the drill string became stuck in the hole due to caving.

Only minor rotation, one to two turns, and a few inches of vertical movement were obtainable. This movement continued all day but resulted in an overheated hydraulic system which had to be shut down to cool.

At approximately 6:00 p.m. the drill string began to work free and by 10:30 p.m. the entire string was out of the hole. Unfortunately, the hammer had twisted off at an internal joint leaving the hammer box sub still attached to the string. A decision was made to try fishing the tool out the next day.

The first attempts to recover the hammer were made on the morning of the 16th using the string to try to fish the tool out and by washing out the hole with air. These methods were unsuccessful, and a decision was made to switch to mud to clean out the hole and then attempt to recover the tool. Additional parts were needed to convert the rig to mud drilling. A decision was made to

take the next day off while the parts were shipped via air freight from Denver, Colorado.

Drilling began again on the 18th using a tricone bit and washing the hole out with mud. Some circulation was lost but was regained by adding lost circulation material, LCM, to the mud. The operation was stopped near mid-shift because of inclement weather. Very low temperatures, high wind and rain mixed with snow produced unsafe working conditions.

With improved weather conditions washing of the hole continued on the 19th. By 9:45 a.m. the drilling string had reached the top of the hammer and the hole appeared stable. The string was tripped out and the bit was replaced with the hammer sub. An attempt to spear the hammer with its own sub was made and the hammer was recovered on the first effort and slowly removed from the hole. The bit was put back on the string and drilling continued.

The target depth of 500 ft. was reached at 2:00 p.m. on the 20th, and casing was prepared for installation on the 21st.

Prior to installing casing on the 21st the hole was flushed with Barafos to break down the drilling mud. The casing operation was started and was nearly complete when logistic problems caused a 24 hour delay in the casing operation. Following the correction of the problems, the casing operation was routinely completed on the 22nd at about 1:00 p.m.

CC-2 was located in the western Part of Eagle Valley (fig. B27) on property owned by the University of Nevada. The drill site is situated in an area of recent faulting. There are reports of rapid snowmelt in that area as well.

CC-2 was spudded in at 7:30 p.m. on February 22 after improvements on the road leading to the site were made. These improvements allowed the drill rig to reach the site. Drilling rates with the 7 1/2" tricone bit were rapid because the material consisted of decomposed granitic rock. At the end of

the first day of drilling the depth of the well was 95 feet. Drilling was stopped because the surface casing had not arrived on site.

Drilling resumed at 12:00 p.m. on the 23rd after 97 feet of 6" surface casing had been installed. A 5 7/8" tricone bit and an air-foam medium were used in this drilling operation. A total depth of 240 feet was reached at about 2:00 p.m. and the gradient casing string was installed by 4:30 p.m. Drilling progress charts for both CC-1 and CC-2 are shown in figure B28.

Results of Temperature Gradient Drilling

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Soon after completion of CC-1 a temperature profile was completed using a DIGETEC temperature sensor attached to a 1000 foot cable for down-hole measurements. The results of the temperature log are illustrated in figure B29. The diagram on the left shows the actual measured temperature as a function of depth. The gradient is positive but the maximum temperature recorded was only 20°C at 500 feet. The diagram on the right illustrates the change in the geothermal gradient with increasing depth. This diagram indicates that normal geothermal gradient for this area was perterbated between the 300 and 400 foot interval. This was the result of large volumes of cold ground water which were encountered at all intervals during drilling.

No warm water intervals were encountered during or after the drilling of CC-1. There appeared to be some indication that warm or hot water was encountered during the final phases of drilling. Unfortunately, a wet thermistor probe connection was found to be the cause of the anomalously high temperatures.

The lithologic log for CC-1 is illustrated in figure B30. Most of the drilled material consisted of slightly metamorphosed (greenschist facies) volcanic breccias and mudflows of Triassic and Jurassic age. These rocks are among the oldest exposed in this study area and have been described as roof pendants in the granodioritic batholith which underlies the entire area.









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Figure 8 30.

Samples of the drill chips from several intervals were examined with a polarizing microscope and X-ray diffraction equipment. The petrographic analyses revealed a fine- to medium-grained highly altered and highly variable mineral assemblage. The original rock appears to have been of volcanic origin containing micro-phenocrysts of plagioclase and pyroxene in various stages of alteration and obliteration. Many of the samples showed a vuggy texture, and these voids were often filled with calcite and quartz. Sericite, chlorite and epidote are widespread in all the samples and probably reflect the alteration episode prior to and during emplacement of the granite batholith. Minor minerals included magnetite, biotite and potassium feldspar. The mineralogic composition was consistent throughout the 500 foot interval and there is no indication that the contact between the lower Mesozoic metamorphic rocks and the upper Mesozoic intrusive rocks was reached.

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No temperature gradient profiles could be measured in CC-2 because the hole was vandalized shortly after it was completed. The locked cap on the well bore was destroyed and the well bore was filled with debris. An attempt was made to remove the clog with a small cable tool but the hammer could not dislodge the obstruction. Apparently the hole had been filled with sand to a level 60 feet below the surface.

During the drilling a small amount of cold water was encountered but the level of static water was not measured.

The lithologic log for hole CC-2 is presented in figure B31. This diagram shows granite bedrock overlain by almost 200 feet of alluvial material, primarily a decomposed granite. The alluvial material is mineralogically identical to the basement material. Both units contain abundant plagioclase, quartz and perthitic potassium feldspar. Accessory minerals include biotite, hornblende, magnetite and sphene. Small volumes of more mafic mineral assemblages were





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present in the drill chips and these were probably parts of xenoliths which are widespread in the batholith.

Summary and Conclusions

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Normal faults associated with Basin and Range style deformation are the major structural controls for geothermal fluids in the Carson-Eagle Valley study area. These faults can be identified on the surface by abrupt changes in topography and lithology and can also be seen in gravity profiles along traverses normal to the strike of the fault. Total displacement along these faults appears to be at least 1.5 km and may be as much as 3 km. Portions of these fault zones are presently conducting rising geothermal fluids to the surface. Lineament analysis supports previous interpretations which suggest that the orthogonal intersections of faults along major range fronts in the Basin and Range and the Sierra Nevada Front provide major zones of weakness in the upper crust (Trexler and others, 1978; Trexler, 1979). In many cases only one of the orthogonal fault patterns reaches the surface. This fault plane intersection may be a zone of enhanced permeability which provides the initial conduits for rising thermal fluids. A model of this hypothesis is illustrated in Figure B32.

Near-surface temperature measurements from 2 m probes and shallow depth water wells reveal a linear isotherm configuration in the area surrounding the rising geothermal fluids. The lineation is probably the result of thermal fluids that spread out along the zone of most recent faulting.

Chemical analyses of fluids from the study area indicate significant compositional differences in major dissolved constituents between thermal and nonthermal fluids. Non-thermal fluids show greater chemical variation and appear to be mixing with the two varieties of thermal fluids in this area. Chemical geothermometers are of little value for these fluids, and maximum reservoir temperatures based on direct measurements in shallow wells probably range from 90° C to 100° C. Stable isotopes of hydrogen and oxygen indicate that the thermal



Figure B32. Graphic model showing the inferred structural controls on the upwards migra-tion of geothermal fluids in the Carson-Eagle Valley study area.

fluids are compositionally similar to the non-thermal fluids and are ultimately derived from meteoric waters. Some of the thermal fluids are, however, slightly isotopically lighter than the non-thermal fluids and these are probably derived from the snow-pack in the nearby Carson, Virginia and Pine Nut Ranges.

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No thermal fluids were encountered in the two temperature gradient holes. Based on shallow, warm water wells and a 2 m depth temperature probe survey the geothermal reservoirs in this area appear to be narrow zones of limited areal extent.

Although the geothermal resources in this area are low- and moderatetemperature and are of limited extent commercial development is currently underway at Walley's Hot Springs. Plans have also been made to use the thermal waters at Saratoga Hot Spring for space-heating in a new residential subdivision. The Carson Hot Spring is currently being used as a spa but may be tapped to heat a new commercial office complex. The Pinyon Hills area geothermal resource is now being used to heat some residences. There are no planned uses for Hobo Hot Springs at the present time.



BIG SMOKY VALLEY

INTRODUCTION

The Big Smoky Valley is situated in central Nevada. It begins at a point 12 miles east of the town of Austin and extends approximately 100 miles in a southwesterly direction to reach a southern terminus near Coaldale Junction some 40 miles to the west of Tonopah. Hydrologically and topographically the valley is divided into northern and southern sections by a physiographic high near the mining community of Round Mountain. Our study area was limited to the northern section (fig. Al) and contains three geothermal resources located at the points labeled Darrough's, McLeod and Spencer's in figure Cl. The area was chosen for study based on its "high" potential rating for industrial process heat direct utilization (Trexler and others, 1979).

Geologically the region is complex with a lithologic history extending from the pre-Cambrian to the Holocene. Rocks comprising the Toiyabe Range which forms the valley's western boundary within the study area include Pre-Cambrian and Paleozoic siliceous, argillaceous and calcareous sediments and metasediments, Paleozoic lavas, Mesozoic intermediate to acidic intrusives, Tertiary lavas, tuffs and sediments. The Toquima Range forms the valley's eastern limit and contains Paleozoic siliceous, argillaceous and calcareous sediments and metamorphic rocks, Mesozoic intermediate intrusives and Tertiary intermediate flows and silicic ash flow tuffs. Quaternary to recent alluvial, fluvial, lacustrine and playa deposits form the valley floor.

Structural features of the region are also indicative of a long and complex history. Evidence can be found for regional metamorphism folding from a scale of near invisibility to several tens of feet in amplitude, large scale low angle faulting related to the Robert's Mountain Thrust, large displacement high angle faulting largely associated with the Basin and Range tectonics, small to moderate scale faulting in alluvial materials and numerous intrusive events.





Generalized geologic maps (figs. C2, C3) outline the distribution of some of the lithologies and structural features of the study area. More detailed information is available in Ferguson and Cathcart (1954), Kleinhampl and Ziony (1967), Means (1962), Meinzer (1917), McKee (1968), McKee (1972), McKee (1976), Speed and McKee (1976) and Stewart and Carlson (1978).

GEOTHERMAL RESOURCE INVESTIGATION

The techniques and equipment used to conduct the investigation of the geothermal resources within the Big Smoky have been described in the introduction of this report. This section reviews the data gathered, discusses the specifics of and problems associated with the application of the techniques in this study area and presents possible interpretations of the results.

Geological Reconnaissance

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Because of limited accessibility and time considerations our study was devoted to field stratigraphic and structural examination in this area. Samples of some of the major rock types were collected in the range near the geothermal occurrences and were made into thin sections for study. This was completed as a preliminary step in choosing appropriate samples for whole rock chemical analyses for use in determining possible fluid recharge paths (by comparing whole rock chemistry to that of the thermal fluids). Unfortunately, because of problems associated with the fluid analyses which will be discussed under a separate heading no whole rock analyses were performed.

An area of altered rocks along the range front of the Toiyabe Range and in the vicinity of the McLeod Ranch hot springs was also visited. Examination of the rocks revealed no currently active or recent geothermal phenomena, that the rocks were highly altered tuffs which have been placed in the present position by block faulting and that the alteration is probably the result of pre-Quaternary hydrothermal processes.







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Alluvial processes along the range fronts bounding the valley have remained active over a considerable period of recent geologic time. This activity has essentially eliminated any clear definition of fault plane dips in the area. Thus, no attempt was made to measure these angles. The orientation of faults and their relationship to the present geothermal occurrences are more easily studied using aerial photographic techniques and will be discussed under that topic.

Gravity

Prior to our study only a limited amount of gravity data was available for the area in the form of a 1:250,000 scale Bouguer gravity map by Erwin and Bittleston (1977). This map provides regional trends for the section of the study area from the McLeod Ranch northward. In general, their data indicate a basin with the western side dipping more steeply than its eastern counterpart and the deepest segment occurring along the valley's central axis. The five milligal contour interval used on the map does not provide sufficient detail to accurately define the location of range bounding faults. For this reason and the complete lack of data for the study area's southern portion, a series of traverses were completed with emphasis on the data-deficient area.

Approximately 250 stations were occupied along six traverses. Four of the traverses were oriented approximately normal to the valley's central axis while the remaining two maintain a nearly north-south direction (fig. C4). Station spacing varied from 0.4 to 0.54 kilometers which provided both a practical working distance for theodolite measurements and a sufficient data density for our purposes. A short description of the individual traverses follows. Traverse S (Spencer's) the "simple" and "complete" Bouguer anomaly curves are plotted with the corresponding topography in Figures C5a and C5b. Evidence of the western range bounding fault system is seen as a group of inflections in the curve at and to the left (northwest) of the point labeled BM6034 in Figure C5a. From BM6034



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Figure C4 . Locations of gravity traverses in Big Smoky Valley.



Figure C5a . Simple and complete Bouguer anomaly, and topography of the western segment of the S (Spencer's) gravity traverse.



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Figure C5b. Simple and complete Bouguer anomaly, and topography of eastern segment of the S (Spencer's) gravity traverse.

moving to the right (southeast) the subsurface slopes downward in two gentle approximately linear segments to a point about 35,000 feet from the beginning of the traverse. This point appears to be the location of the greatest thickness of valley fill encountered on the traverse. For comparison purposes the thickness of the alluvial materials can be roughly estimated using the formula of Thompson and Sandberg (1958) with a density contrast of 0.5g/cm³ (2.7 bedrock, 2.2-alluvium). Applying the formula to that density contrast and the 15 milligal difference in gravity between the regional value and this locality yields a thickness of approximately 2300 feet. Proceeding southeastward the subsurface configuration takes a rapid rise towards the surface to a local high in the vicinity of Spencer's Hot Springs (fig. C5b). At this point the valley fill thickness estimated using the same formula, is only 460 feet. It should be noted that the traverse line does not pass directly through the surface geothermal expression at Spencer's. It is displaced approximately one half mile to the southwest. However, this same trend is apparent on the regional map and it does substantiate the presence of a subsurface structural feature which is likely related to the localization of the hot springs. Continuing southeastward the gravity data indicate a graben structure which rises into an undulating segment of bedrock.

Traverse MR - The line of this traverse passes within 100 meters of the geothermal springs and therefore provides an on site picture of the subsurface configuration (figs. C6a, C6b). Gravity data indicate a very well defined, large displacement fault on the valley's western edge. Moving eastward (to the right) three approximately linear segments are present in the curve from 6,000-14,000 feet, 14,000-18,000 feet and 18,000-23,000 feet. It is likely that these segments represent a series of step-faulted blocks whose long axes parallel the current range front trends. At approximately 23,000 feet the curve takes a steeply inclined dip that correlates with the location of the thermal springs.

From this point eastward the curve becomes nearly linear and level reaching its lowest point at approximately 41,000 feet after a slight change in slope. Applying the previously used formula the depth of valley fill is computed to be approximately 5100 feet. Following the curve to the east (fig. C6b) a series of slope changes are apparent and probably related to a series of blocks formed by tectonic activity acting on rocks of the Northumberland caldera complex. The origin of the feature at 81,000 feet is not clear but it may result from a tilted block or buried body of higher density. It is apparent that along this traverse the valley's western boundary dips notably more steeply than does that of its eastern edge.

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Traverse OMC - Traverse OMC does not pass in the vicinity of any known surface or subsurface geothermal activity and was conducted to determine the nature of the subsurface configuration between the Darrough's and McLeod Ranch resources. As was the case along MR, the western side of the valley is defined by rather steep changes in slope. However, at this location these changes occur in only three approximately linear segments (0-4,000, 4,000-12,000 and 12,000-22,000 feet) (fig. C7a). The direction changes shown are the result of available road configurations. Maximum computed depth of valley fill along this traverse is approximately 4,100 feet and occurs in the vicinity of 37,000 feet horizontal distance (fig. C7b). The subsurface configuration resembles that of MR in its more gentle slope and step faulted nature as the Toquima Range front is approached.

Traverse D - In the vicinity of Darrough's Hot Springs the closure of the northern segment of the Big Smoky Valley is evidenced by the nearly six mile shorter transect distance compared to traverses MR and OMC (figs. C8a, C8b). This traverse passes through the area of known surface and subsurface geothermal expressions at this location and its subsurface configuration closely resembles those of MR and OMC. Like MR the location of the hot springs correlates well with a steeply dipping slope change on the gravity curve which is most likely the



Figure C6a. Simple and complete Bouguer anomaly, and topography of the western segment of the MR (McLeod Ranch) gravity traverse.

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Figure C6b. Simple and complete Bouguer anomaly, and topography of the eastern segment of the MR (McLeod Ranch) gravity traverse.

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Figure C7a. Simple and complete Bouguer anomaly, and topography of the western segment of the OMC . (Ophir-Moores Creek) gravity traverse.



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Figure C8b. Simple and complete Bouguer anomaly, and topography of the eastern segment of the D (Darrough) gravity traverse.

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result of large displacement on a fault at this point. Computed maximum valley fill thickness occurs in the vicinity of 27,000 feet horizontal distance and has a value of approximately 3,800 feet. This figure also tends to indicate subsurface closure of the valley.

Traverses 8A and 8B - The purpose of these lines was to test for the presence of a subsurface structure which might be related to the Pritchards Station Lineament described by Ekren and others (1976). North-south orientations were used to accomplish this objective. Traverse 8A (fig. C9) possesses a single well defined inflection point while 8B (fig. C10) has two and possibly three slope changes. Consideration of the overall pattern produced by contouring at a five milligal interval using data from OMC, 8A, 8B and D does not show any relation between the inflections on 8A and 8B. The slope changes on 8B appear to be a function of the step faulted nature of the valley's eastern boundary while the single inflection along 8A seems to be a local anomaly.

Summary

Gravity data indicate the presence of subsurface structural features associated with all three of the known geothermal resources in the study area. In the north (Spencer's) this feature occurs along the valley's eastern boundary while in the central (McLeod Ranch) and south (Darrough's) the structures are located along the steeply dipping frontal faults of the Toiyabe Range. Additional information includes the assymetrical nature of the subsurface in the central and southern portions of the area and the subsurface closure of the valley as it approaches Round Mountain.

Aerial Photography

Imagery used to examine the Big Smoky study area included: 1:250,000 RBV LANDSAT, 1:78,000 9"x9" B&W, 1:24,000 low sun-angle 9"x9" B&W and 1:12,000 9"x9" B&W along gravity traverse lines. The LANDSAT and 1:78,000 scale photos were available through the EROS DATA CENTER while the remaining work was flown



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Figure C9. Simple and complete Bouguer anomaly, and topography of gravity traverse 8A.



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Figure C10. Simple and complete Bouguer anomaly, and topography of gravity traverse 88.

during the course of our investigations. RBV LANDSAT images proved to be of no use in determining hot spring localization. This was in large part due to poor image quality and the presence of snow during the mid-May flyover. Photography at 1:78,000 helped to a limted degree by providing a base for regional trend investigation and allowing the possible relationship between large scale (longer than 5 km) linear and curve-linear features and geothermal occurrences to be examined. However, the most useful aerial imagery technique applied during our work was low sun-angle photography (LSAP). Regions flown using LSAP are labeled "A" and "B" in figure Cll. The missions were conducted late in the year (December) to increase available flight time, and between 5 and 18 degrees solar elevation to maximize light-shadow contrast as indicated in Walker and Trexler (1977). Forelap and sidelap were incorporated to aid stereoscopic study. These restrictions combined with the selected scale of 1:24,000 which permitted detection of small displacement alluvial fault scarps resulted in the successful application of this technique to the study area.

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Examination of the low sun-angle imagery revealed information on both the physiographic expression of the geothermal occurrences and the presence of local structural features which appear to be related to resource localization. For example, figure Cl2 is a frame taken over the Spencer's Hot Springs area. Ground study has shown the springs and wells to be located in a region of undulating topography which is related to the deposition of calcareous sinter. The areal extent of this sinter is clearly defined in the photograph and stereoscopic study points out the generally raised nature of this feature. No fault traces are seen which can be related to the geothermal phenomena. Fault traces and lineations which appear to be related to hot spring localization as well as a distinctive physiographic expression are revealed in LSAP taken in the vicinity of the McLeod Ranch occurrence. The bounding faults in the Toiyabe Range approximately one mile south and four miles west of the hot springs possess a



Figure C11. Low sun-angle photography areas in Big Smoky Valley.

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Figure C12 . Low sunrangle photography over Spencer's Hot Springs area, scale 1:24,000.

notable sawtooth appearance (fig. Cl3) and this pattern is repeated though somewhat distorted in nearby alluvial materials. The approximately orthogonal nature and spatial orientation of these faults is duplicated in the shallow probe isotherm configuration and will be referenced in the discussion of that technique. Moving northward along the range front a strong N45°W lineation is observed in the orientation of canyons and rock fracture patterns. The extension of this lineation from one of its major expressions as depicted in figure Cl4 passes directly through the surface geothermal manifestations. This linear also parallels one of the faults depicted in figure Cl3 and thus appears to represent a definite local structural trend. Topographically the McLeod Ranch occurrence possesses a readily distinguishable roughly circular expression as shown in figure Cl5. Surface examination has shown this feature to be a large diameter low profile tuffa mound.

The geothermal manifestations at the Darrough site are developed in alluvial fan materials and do not exhibit a distinctive physiographic expression. LSAP flown over the resource does demonstrate the presence of a structural feature which is likely related to the localization of the thermal fluids. If the trend of the range bounding fault visible in the left portion of figure Cl6 is extended northward a colinear fault scarp is encountered in alluvial fan materials. Further extension of this line in the same direction, as depicted in figure Cl7 shows that it passes through the zone of known surface and subsurface geothermal occurrences. This same line correlates well with the distinct inflection in the gravity curve discussed earlier and defines a trend which parallels that found in the two meter probe isotherm configuration (discussed in a later section).

Black and white 9"x9" format photography was flown along gravity traverse lines to check for surface features which could be associated with subsurface changes in gravity profiles or areas of anomalous high mercury as determined during soil sampling. This effort did not prove useful. Scale of the imagery





Figure C14 . Lineaments described by canyons and fracture patterns immediately northwest of McLeod Ranch resource. Extension of upper dashed line to lower right (southeast) passes directly through geothermal springs.



Figure C15 . Low sun-angle photograph over McLeod Ranch Hot Springs, scale 1:24,000. Note roughly circular pattern which reflects extent of the broad low tufa mound.



Figure C16 . Low sun-angle photography of range bounding and alluvial fault traces southwest of Dar-rough's Hot Springs, scale 1:24,000. Note colinear trend as shown by dashed line.

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Figure C17 . Low sun-angle photograph over Darrough's resource area, scale 1:24,000. Alluvial fault of Figure C16 is visible in lower left.

was 1:12,000 but it did not provide additional information when compared to that flown at 1:24,000.

Summary

Photo imagery used to examine the Big Smoky Valley consisted of black and white prints ranging in scale from 1:250,000 (LANDSAT) to 1:12,000. LANDSAT imagery was of poor quality and lacked necessary detail. Large scale linear and curvelinear and other regional features were examined using available 1:78,000 scale photos. The greatest amount of useable data was derived from 1:24,000 scale low sum-angle photography. It provided pertinent information on local structural features which show likely relationships to thermal spring locations as well as physiographic distinctions associated with the occurrences. Photography at 1:12,000 scale did not prove useful.

Fluid Sampling and Analysis

Sixteen fluid samples were collected in the Big Smoky Valley area during the study. Two thermal wells and six thermal springs were sampled. In addition, six non-thermal springs and two non-thermal wells were sampled. Results of chemical analyses for major, minor and trace constituents are listed in Table Cl along with a sample designation and temperature measured at collection. Values for pH represent measurements made in the laboratory during analysis. Figure Cl8 depicts the generalized chemical composition of the sampled fluids using modified Stiff diagrams. The data depicted in the figure demonstrate a marked compositional difference between thermal and non-thermal fluids in the Darrough's and McLeod Ranch regions while sampled hot and cold waters in the Spencer's Hot Springs area possess notable similarities. A more detailed discussion of these relationships follows.



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Table Cl. Chemical analyses of fluids from Big Smoky Valley.

Sample Name	Sample Number	Location	ToC	рЩ	SC umhos	B ppm	Ca	Mg	K ppm	Na ppm	L1 ppb
Darrough's	s well	SWISELSELSec.	7							•)	
(800 ft)	DB1	T11N,R43E	90.5	8.77	432	0.700	1.12	<0.05	3.30	98.8	349
Darrough	orth	SWISWISSINGSec.	8								
spring	DB2	TLLN, R43E	71.2	8.72	444	0.575	1.35	<0.05	2.72	94.2	324
Darrough :	south	SEKSEKNEKSec.	18								
spring	DB3	T11N,R43E	68	8.68	440	0.590	1.44	<0.05	2.20	91.1	309
Darrough's		SWISHISHISEC.	8								
pool	DB4	T11N, R43E	95.5	8.85	465	0.630	1.24	<0.05	3.00	98.2	328
Aqueduct		NESSELNWISSec	13								
stream	DBS	T11N,R42E	1.8	7.75	125	0.060	20.1	1.42	0.683	5.29	5.5
Barker		SWASE SWASec.	15								
Creek	DB6	TIIN, R44E	3.9	7.69	102	0.077	11.8	1.98	0.646	8.08	2.94
Jake's	2	NELSWASEASec	24			100	à .				
well	DB7	T11N,R43E	10	7.83	175	0.113	20.5	1.81	1.40	15.4	13.2
Spencer		NEWNEWNEWSec	24								
73	SBL	T17N, R45E +	72.5	8.14	1021	3.33	14.9	9.06	36.6	181	1810
Spencer-3	9 Dead	NEWNEWNEWSec.	24								
Burro	SB2	T17N, R45E +	38.8	7.89	848	1.46	25.2	16.5	22.4	100	594
well north	a of	Ne Sec. 18									
Linka Mine	a SB3	T17N,R46E +	-	8.22	808	1.39	30.4	17.5	18.0	95.4	464
linner Onb	1.	NUKSUNSec. 33									
Creek	OBL	T13N, R42E	5.8	8.05	249	0.136	34.3	8.84	1.20	4.31	2.83
Lower Onh:	ir	SUKSUKSEKSec	34				•				
Creek	OB2	T13N, R42E	3.7	8.21	289	0.077	40.4	9.15	1.38	5.37	4.13
McLeod 88		SEKNEKSWKSec	34								
Spring	MBL	T13N,R43E +	87.9	8.59	2318	3.47	10.4	2.49	38.3	525	1670
Mcl.eod 63		SERNERSWISSE	34								
Spring	MB2	T13N,R43E +	62.7	8.17	2466	3.61	18.4	9.02	40.2	537	1780
Peult		SUMMISSING	16								
Spring	MB3	T14N, R43E	13.6	7.97	177	0.204	28.5	2.45	0.796	6.80	2.08
Decker Rol	6	SUKSUKNEKSer	18								
Creek	MB4	T14N, R43E +	6.7	3.11	187	0.082	36.8	3.00	0.796	4.84	3.9

"Measured and reported as total recoverable sulfide.

*Measured and reported as total location estimated.

Sample Number	C1 ppm	NO3/NO2 ppm	S10 ₂ ppa	SO ₄ /S ^{mak} ppma	CO3/HCO3	ppm	As ⁺⁴ ppb	Ba ppa	Fa ⁺² ppm	Rb ppb	Ca ppb	Sr ppb
D81	12.2	0.13	122	47/ 0.439	21.1/ 119	14.2	86.4	<0.1	0.03	25.3	58.8	<200
DB2	11.8	0.07	112	52.9/ 1.37	16.7/ 125.9	13.7	78.8	<0.1	0.04	19.8	44.7	<200
DB3	11.6	0.07	108	49.4/ 0.464	11.2/ 125.7	13.1	41.5	<0.1	0.04	16.5	41.7	<200
DB4	13.5	0.04	114	50.7/ 0.910	22.3/ 108	14.2	58.6	<0.1	0.091	21.5	49.8	<200
DB5	1.10	0.36	9.91	3.56	71.9	0.106	<5	<0.1	0.066	2.1	4.2	298
DB6	2.02	<0.01	25.5	2.71	57.3	0.129	<5	<0.1	0.04	2.0	3.6	<200
DB7	3.82	0.85	35.5	7.44	86.1	0.264	-	0.08	0.04	2.7	3.6	210
SB1	22.9	<0.01	93.5	35.8/ 0.249	525	0.466	28.7	0.344	0.167	250	209	848
5 B 2	13.3	0.06	46.7	35.0/ 0.273	444	2.10	38.7	0.21	1.78	100	50.8	1500
SB3	15.2	1.03	58.6	48.8	390	1.94	26.5	0.16	0.04	83.3	5 7.31	866
081	1.71	0.03	11.7	7.53	143	0.119	5.3	0.21	0.03	<1	3.6	298
082	2.38	0.06	11.7	17.9	155	0.145	6.0	<0.1	0.04	<1	4.8	316
mb1	48.2	<0.01	107	64.7/ 0.345	40.1/ 1380	11.7	149	0.344	0.14	449	216	419
MB2	48.2	0.25	162 .	64.5/ 0.361	1420	13.1	163	0.252	0.04	374	171	333
MB3	3.05	1.20	17.2	9.27	93.6	0.192	<5	0.08	0.066	<1	<3	316
MB4	1.39	0.71	20.9	3.71	143	0.264	<5	<0.1	0.066	<1	<3	-402

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Sample Name	Sample Number	Location	TOC	pH	SC µmhos	B ppm	Ca	Mg	K ppm	Na. ppa	Li ppb
Darrough	s well	SWISELSELSec.7	•								
(800 ft)	DB1	Tlln,R43E	90.5	8.77	432	0.700	1.12	<0.05	3.30	98.8	349
Darrough	north	SWCSWCSWCSec.8									
spring	DB2	TLLN, R43E	71.2	8.72	444	0.575	1.35	<0.05	2.72	94.2	324
Darrough	south	SEKSEKNEKSec.1	8								
spring	DB3	TLLN, R43E	68	8.68	440	0.590	1.44	<0.05	2.20	91.1	309
Darrough	s	SWISSINSWISSec. 8									
pool	DB4	TLLN, R43E	95.5	8.85	465	0.630	1.24	<0.05	3.00	98.2	328
Aqueduct		NEWSERNWASec. 1	3								
stream	DBS	T11N,R42E	1.8	7.75	125	0.060	20.1	1.42	0.683	5.29	5.5
Barker		SWISELSWISEC. 1	5								
Creek	DB6	TIIN, R44E	3.9	7.69	102	0.077	11.8	1.98	0.646	8.08	2.94
Iske's		NELSULSELSec . 2	4				5				
well	DB7	TLLN, R43E	10	7.83	175	0.113	20.5	1.81	1.40	15.4	13.2
Spencer		NEWNERNERSec. 2	4								
73	SBL	T17N,R45E +	72.5	8.14	1021	3.33	14.9	9.06	36.6	181	1810
Spencer-3	9 Dead	NEWNERNERSec. 2	4								
Burro	SB2	T17N, R45E +	38.8	7.89	848	1.46	25.2	16.5	22.4	100	594
well nort	h of	Nile Sec. 18									
Linka Mir	e SB3	T17N,R46E +	-	8.22	808	1.39	30.4	17.5	18.0	95.4	464
linner Onk	1.	NURSUPISAC . 33									
Creek	OBL	T13N, R42E	5.8	8.05	249	0.136	34.3	8.84	1.20	4.31	2.83
Louer Onk	4.0	SubsubsRisses 3	4								
Creek	OB2	T13N, R42E	3.7	8.21	289	0.077	40.4	9.15	1.38	5.37	4.13
McLeod 8		SELNELSULSec. 3	4								
Spring	MBL	T13N,R43E +	87.9	8.59	2318	3.47	10.4	2.49	38.3	525	1670
Not and 63		STUNFISTING 3	4								
Spring	MB2	T13N,R43E +	62.7	8.17	2466	3.61	18.4	9.02	40.2	537	1780
Paule		SUL-NULSULSee 1	6								
Spring	MB3	T14N, R43E	13.6	7.97	177	0.204	28.5	2.45	0.796	6.80	2.08
Decker Pr	h	SULSULNELS	8								
Creek	MB4	T14N,R43E +	6.7	3.11	187	0.082	36.8	3.00	0.796	4.84	3.9

Table Cl. Chemical analyses of fluids from Big Smoky Valley.

"Measured and reported as total recoverable sulfide.

*Unsurveyed area - township and range location estimated.

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Major and Minor Dissolved Components

The composition of Big Smoky fluids plotted as percent equivalent per million of major cations and anions is shown in figures C19, C20 and C21. Sample designations in these figures correspond to those used in Table C1 in figure C18. In some instances compositions of several fluids from a given area are so similar that plotting them as individual points is not practical. Where this occurs a larger symbol with a compound designation such as "ME1,2" or "DB-1 - DB-4" is used. Points with designations such as "Sec. 12" represent results obtained from records of the Nevada State Department of Health. The number represents the section in which the water source is located. "Sec. 12" is a well from T11N,R34E and "Sec. 30" is also a well in the same township.

Similarities and contrasts in fluid cation characteristics for the system Ca⁺²-Mg⁺²-Na⁺ can be studied in figure C19. The hottest Spencer's thermal fluid sampled (72.5°C) is labeled SB-1 in the figure. A second sample of thermal water collected at the same site (SB-2, 38.8°C) along with a non-thermal fluid from that area (SB-2, approximately 17°C) lie along a straight line extending from SB-1 to the midpoint of the Ca⁺⁺-Mg⁺⁺ join. This straight-line relationship suggests that the composition of SB-2 may result from mixing SB-1 and SB-3 type fluids. Disregarding SB-3, the remainder of the non-thermal liquids sampled and those analyzed by the Department of Health are grouped in the upper half of the diagram and are relatively calcium rich. A distinction between cold waters from the vicinity of the Toquima Range and those near the Toiyabe Range can also be made. The former (DB-7, DB-6, Sec. 12) are notably more sodium rich while the latter (DB-5, MB-3, MB-4, Sec. 30, OB-1,)B-2) are relatively more calcium and magnesium (Sec. 30, OB-1, OB-2) rich. Shifting to the system Ca⁺²-K⁺-Na⁺ (fig. C20) similar distributions are observed. However, the range in variation with respect to potassium content is distinctly more limited. Once again OB-1 and OB-2 are part of a distinct grouping. The anomalous Mg⁺² values of OB-1 and OB-2 are likely related to dolomite and greenstone rocks through which this creek



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Figure C 19. Distribution of thermal and non-thermal fluids with respect to Mg-Ca-Na cations in the Big Smoky Valley. Points are plotted as percent equivalents per million of the sum for the species.

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Figure C 21. Distribution of thermal and non-thermal fluids with respect to CO₃ + HCO₃-SO₄-CI anions in the Big Smoky Valley. Points are plotted as percent equivalents per million of the sum for the species. passes. No ready explanation is apparent for the relatively high potassium content of these samples.

Geothermal fluids when plotted in terms of the anions $SO_4^{-2}-CO_3^{-2}+HCO_3^{+}-C1^{-}$ do not possess the uniform distribution apparent in the cation plots (fig. C21). Hot waters from McLeod Ranch and Spencer's are found mixed within a grouping of cold waters near the $CO_3^{+2}+HCO_3^{+}$ apex. Thermal fluids from the Darrough site, however, display a distinct displacement from other waters and are in relative terms decidedly more sulfate and somewhat more chloride rich. This unique character of the Darrough hot waters will also be apparent in their isotopic characteristic.

Silica is an important nonionic constituent of geothermal fluids. Frequently it is used to estimate reservoir temperatures using a chemical geothermometer developed by Fournier and Rowe (1966). No attempt will be made to apply this technique to fluids sampled during our study because we feel that the assumptions necessary to obtain meaningful results cannot be adequately demonstrated to hold in our systems. However, it is interesting to study the silica content in terms of the solubility of various polymorphs. This can be accomplished by plotting the values obtained from analysis on agraph whose axes are log molality SiO_2 and temperature. The assumption is made that the activity coefficient for this species is unity and therefore that activity equals molality. For convenience the solubility curves are also plotted (fig. C22). These curves are drawn from the data given by Walther and Helgeson (1977).

All of the fluids sampled plot above the curve for alpha-quartz and are thus saturated with respect to this phase. The majority of the points fall between the curves for alpha-cristobalite and beta-cristobalite. Exceptions to this are MB-2 and SB-3 which fall between beta-cristobalite and amophous silica. Silica content does not appear to be simply a function of temperature. In certain cases it may be possible to explain the silica levels of various fluids from a given



area as heating or cooling of solutions with little or no change in SiO₂ content (e.g. SB-1, SB-2, SB-3, or DB-1, DB-2, DB-3, DB-4). However, this explanation does not hold for MB-1, MB-2 where the higher silica is associated with the lower temperature. More detailed study would be required to determine the possible source or sources which contribute to the distribution of silica in the fluids sampled.

Trace Constituents

Nine elements are grouped into the trace category although their levels may equal or exceed those of some of the components discussed under the major and minor heading. Included in this subdivision are B^{+3} , Li^+ , F^- , As^{+3} , Ba^{+2} , Fe^{+2} , Cs^+ , Rb^+ and Sr^{+2} . Analytical results for these elements are given in Table Cl.

Some relationships associated with the distribution of these elements are reasonably straight-forward while others are not clear from the data available from this study. A comparison of the levels of these elements in thermal versus non-thermal fluids is presented in Table C2. The information presented in the

Table C2. Relative change when comparing thermal to non-thermal fluids (E=enrichment, B=both enrichment and depletion occur, N=approximately equal level in both.)

Element	As ⁺³	B+3	Ba ⁺²	Cs ⁺	F .	Fe ⁺²	Li ⁺	rb ⁺	Sr ⁺²
Relative Change	E	E	B	E	E	В	E	E	B

table does indicate that concentrations of certain trace constituents could be used to distinguish hot from cold water on a local basis e.g., Darrough's or Spencer's. Care should be exercised in applying this approach because levels of these constituents in thermal fluids vary considerably from one location to another while their concentrations in cold waters throughout the study area are similar. The nature of trace element concentration with respect to temperature

varies both with location and the element being considered. For example, Rb⁺ levels at Spencer's and Darrough's both increase with increasing fluid temperature. However, Spencer's concentrations of this element are as much as an order of magnitude greater than those at Darrough's even though the latter has measured temperatures nearly 23°C greater than those recorded at the former. Consideration of the information in Table 1 demonstrates that in the thermal fluids sampled, arsenic levels are generally higher in lower temperature fluids. The above relationships indicate that fluid trace element chemistry is significantly variable throughout the study area. It should be noted that the geothermal sites are located within (McLeod), or near (Darrough's, Spencer's) playa deposits which may explain some of this complexity.

Stable Light Isotopes

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Fourteen of the sixteen fluids sampled within the Big Smoky were submitted for analysis of hydrogen and oxygen stable light isotopic composition with the aim of using the results to aid in understanding the nature and possible paths of recharge within the geothermal systems. Analysis results are listed in Table C3 and plotted along with a worldwide meteoric water line in Figure C23. A cross present in the lower center of the figure depicts error bars constructed from data supplied by the analysts. The data plotted in Figure C23 indicate within analytical error limits that thermal fluids at Spencer's and McLeod Ranch are heated meteoric waters with a possible slight oxygen shift resulting from interaction with carbonate rocks which are present in the respective areas. Calcium carbonate (tuffa and calcareous sinter) are being deposited at both of these sites from thermal fluids further substantiating this hypothesis. Clayton and others (1968) have presented data demonstrating oxygen shifts in fluids in equilibrium with carbonates in the Salton Sea system at temperatures as low as 100°C. Fluids from Spencer's also lie along an approximately straight line indicating the possibility of mixing discussed earlier. It is also

Sample Name	Sample Number	δ D 0/00	^{81800/00}	T°C
Darrough's well	DB-1	-131	-8.4	90.5
Darrough's north spring	DB-2	-130	-6.7	71.2·
Darrough's south spring	DB-3	-128	-15.1/-15.0	68
Darrough's pool.	DB-4	-129	-8.1	95.5
Aqueduct stream	DB-5	-123/-122	-10.8	1.8
Barker Creek	D B-6	-125	-15.9/-15.2	3.9
Spencer 73	SB-1	-141	-15.4	72.5
Spencer 39 Dead Burrow	SB-2	-143	-15.9	38.8
Well north of Linka Mine	SB-3	-141/-141	-17.8	-
Upper Ophir Creek	0B1	-132	-16.0	5.8
Lower Ophir Creek	0B-2	-126	-11.2	3.7
McLeod 88 Spring	MB-1	-132	-17.7	87.9
McLeod 63 Spring	MB-2	-125	-16.3	62.7
Fault Spring	MB-3	-132	-15.1	13.6

Table C3. Hydrogen and oxygen stable light isotope Analysis results - Big Smoky Valley

Values separated by a slash indicate duplicate runs on a single sample.



interesting that Spencer waters possess distinctly lower deuterium concentrations than fluids sampled farther south in the valley. This may result from higher recharge elevations or a greater component of snow melt but no data is available upon which definite conclusions can be drawn.

Data from the Darrough's Hot Spring area appear to represent a more complex scenario. Three of the four thermal fluids sampled at Darrough's exhibit an oxygen shift of seven to nine per mil. Although a minor amount of carbonate rocks are present in the Toiyabe Range near the Darrough's surface geothermal site, chemical analysis has shown the fluids to be deficient in calcium by more than an order of magnitude compared to non-thermal fluids in the area. In addition, these springs are not depositing tufa. Based on these facts and the magnitude of the oxygen shift it seems reasonable to postulate that these fluid isotopic compositons are the result of a relatively high temperature thermal history. Comparable isotopic shifts are present in the Salton Sea system (Ellis and Mahon, 1977, Figure 3.1) where Clayton and others (1968) determined isotopic equilibrium with fine-grained silicates to have occurred at fluid temperatures in excess of 150°C). Such temperatures at the Darrough's location are not improbable as one of the fluid samples (DB-1) comes from a well with a recorded temperature of 129°C at a depth of 800 feet. One of Darrough's thermal fluids exhibits an isotopic composition falling within the meteoric range. This is thought to be the result of recharge which occurs along a relatively shallow path possibly in alluvial materials where it is heated by conduction.

Two non-thermal fluids exhibit oxygen isotopic shifts with a magnitude of about one half or two thirds that was found in the Darrough's thermal waters (fig. C23). Chemically these cold fluids are similar to other non-thermal waters sampled (the two points labeled Ophir Creek were collected from different elevations along the same stream). Both of the samples displaying the shift were taken at points along the bounding faults of the Toiyabe Range approximately six

miles apart. In consideration of the above it is suggested that the isotopic composition of these fluids results from the mixing of a fluid similar to the shifted thermal fluids at Darrough's, with those of a type resulting from precipitation in the range. Thermal fluids migrating upward along the range bounding fault could dissipate heat via conduction with minimal chemical alteration because their recharge path keeps them in contact with the same rock types encountered in their downward migration.

Summary

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Analyses of major and minor dissolved constituents demonstrate the distinctive nature of the Darrough's resource compared to other Big Smoky geothermal locations. It is also noted that all thermal fluids sampled exhibit relative calcium depletion when compared to local cold waters. Silica content of all fluids indicates saturation with respect to quartz and most values lie between the solubility of alpha- and beta-cristobalite. No simple relationship between SiO₂ content and temperature is readily apparent.

Trace element chemistry shows certain elements to exhibit increasing levels as temperatures increase for all thermal fluids at a given site while others appear to have random temperature associations. Levels of these trace constituents vary widely from one location to another but are generally enriched in the thermal fluids when compared to local meteoric and groundwater values.

Isotopic analysis of thermal and non-thermal fluids indicate that waters which recharge the geothermal systems are of meteoric origin. Darrough's fluid isotopic compositions show large oxygen shifts which are likely related to a relatively high temperature recharge history. And finally, samples collected along the bounding faults of the Toiyabe Range suggest mixing of meteoric and thermal fluids where meteoric waters cross the faults.

Shallow Depth Temperature Probe Surveys

The distribution of temperatures at a depth of two meters was determined for all three of the resource areas in the Big Smoky Valley. Initially a series of two meter holes was attempted at the Spencer's location, but this endeavor met with limited success due to the presence of a layer of calcareous sinter at approximately 1.3 meters depth and a poor design of cutting bit for use in such material. Only five holes were completed in the vicinity of surface geothermal manifestations and they seemed to indicate a rapid drop in temperature as one proceeds laterally away from a surface thermal expression. In addition to the five holes in the vicinity of the thermal springs and wells at Spencer's, three other holes were drilled at distances of approximately 1 and 2 1/2 miles (1.6 and 4 km) from the area of known geothermal occurrences. These holes exhibited temperatures comparable to those recorded in holes drilled as close as 300 ft. (91.5 m) from thermal springs and wells at the Spencer's site. This limited work was completed during mid-October.

A second two meter depth temperature study was undertaken in the Spencer's Hot Springs area in mid-November. Use of a more effective bit design permitted the completion of 15 holes. The location of the majority of the holes and the isotherm constructed from the data obtained are depicted in figure C24. Background temperatures determined during this investigation were $6-8^{\circ}C$ lower than those recorded in mid-October. This difference likely reflects seasonal ambient changes. Daily highs for the first study period averaged $15^{\circ}C$ while those of mid-November fell to $-1^{\circ}C$. Information from this study generally supports the earlier observation of rapid decrease in temperature with short lateral movement from the location of a thermal spring or well. This phenomenon combined with the sample point spacing resulted in the limited nature of the isotherm configuration shown in figure C24. Based on the available data it can be concluded that the



Figure C 24. Two meter probe isotherm configuration at Spencer's Hot Springs.

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near surface thermal manifestations at Spencer's occur as relatively localized phenomena which appear to be separated from one another and not related to any (as yet discernible) trend.

The sample point labeled 31.5°C in figure C24 is approximately twice the magnitude of the next highest temperature recorded during the study but is not associated with a spring or well. Probe hole location is within a few feet (3 meters) of a topographic high, covered with an anomalous amount of foliage which could be suspected of being a former spring in a tufa mound. The temperature recorded seems to substantiate this hypothesis and indicates a potential usefulness of the shallow depth probe in delineating buried near surface thermal phenomena within a local study area.

A total of 16 holes of two meter depth were drilled on a rectangular grid pattern with 800 foot (244 m) spacing between points at the McLeod Ranch Hot Springs. All of the holes were drilled and the probes implanted within a single day. Temperatures were measured shortly after sensor implantation and at times approximately 16, 24 and 36 hours after implacement. It was found that temperatures became stable to within 0.1°C (as detected by our sensors) after a period of 24 hours. This agrees with stabilization times determined during the limited work done at the Spencer's location during mid-October.

A diagram of the interpreted isotherm configuration based on the two meter study at McLeod Range is presented in figure C25. The material drilled was largely playa silt with varying amounts of clay. Mud was frequently encountered at a depth of 1-1.5 m and standing water was encountered in one hole at a depth of 1.3 m. Based on these observations it can be concluded that the isotherm patterns are derived from measurements taken in water rich to saturated materials and are not representative of a strictly conductive temperature distribution. Examination of the isotherm configuration reveals two interesting phenomena: the two meter depth thermal highs are not coincident with surface geothermal


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Figure C 25. Two meter probe isotherm configuration at McLeod Ranch Hot Springs. Line R-R' represents the path used during shallow resistivity study (see text under shallow resistivity heading for discussion).

manifestations (shown by solid circles in fig. C25) and the presence of two linear trends. No explanation of the displaced highs is readily apparent from our study. However, the linear features do correlate with other data previously discussed. The two linears alluded to are described by (1) the colinear arrangement of the subsurface thermal highs and surface hot springs-orientation approximately N45[°]E, and(2) the distortion of the isotherm pattern along an approximately N45[°]W direction. These features parallel the directions noted in the section describing low sun-angle photography over this location. On-site examination indicates the presence of a 25[°]C spring within 10 feet (3 m) of the hot spring labeled "63" in figure C25. This information combined with the nature of the distorted pattern indicates the possibility of a fault allowing non-thermal fluids to enter the hot spring site along a N45[°]W trend.

A relatively detailed shallow-depth temperature probe study involving 29 two-meter holes was completed at the Darrough's Hot Springs site. The isotherm configuration prepared from the accumulated data is shown in figure C26. Study of the patterns in the figure indicates that the thermal fluids migrate in the near-surface along distinct paths which extend eastward from the approximate locations of the springs labeled "71" and "68". These paths may be former channels in the alluvial materials through which the hot springs surface. The pattern extending from the 68°C source is rather well defined while that from the 71°C spring is noticeably more irregular. This is interpreted to be the result of the influx and mixing of non-thermal fluids in the near surface environment. Non-thermal fluids were present as a standing body of water in a region surrounding the 8°C isotherm during the study. Temperatures within this region were the lowest recorded.

In addition to the eastward pattern caused by fluid migration, a second linear feature is described by closure of the isotherm pattern about an axial high. The presence of alluvial materials containing cobble- and boulder-size



Figure C 26. Two meter probe isotherm configuration at Darrough's Hot Springs. Scale of the figure prohibits probe locations from being depicted.

rubble prohibited drilling in the area to the west of the road (indicated by the dashed line) which in turn results in the abrupt termination of the isotherms. However, a sufficient amount of data are available to assign a general orientation to the axial high of between N15°E and N20°E. A marked inflection in the slope of the gravity curve derived for this location is coincident with the lineation axis. Furthermore, if this axial trend is extended to the southwest it is seen to be the same trend described by the range-bounding fault and alluvial faults discussed under the section devoted to low sun-angle photography.

Summary

Two-meter depth temperature probe studies at the location of the three known geothermal resource sites in the Big Smoky Valley have indicated the usefulness of the technique in defining the distribution of the resource in the near surface environment. Isotherm configurations at the Darrough and McLeod ranch sites can be related to structural features present in the Toiyabe Range and nearby alluvial materials. At the Spencer's location no structural correlation could be determined but the isolated nature of the individual springs is demonstrated and a subsurface thermal high is located in a mound which may have been developed by a formerly active thermal spring. It was found that alluvial materials and calcareous sinter can present formidable obstacles to drilling when using a handheld power auger.

Soil Mercury

Six soil survey traverses were established concurrently with the gravity traverses in the Big Smoky Valley area. Due to time and budget restrictions sampling was limited to the gravity traverses and short extensions beyond the traverse limits. Lithologic variations along the traverses and poor sampling control due to the lack of developed soil horizons caused widespread variations in the mercury values. Several samples show mercury concentrations

less than 1 ppb, which is probably related to insufficient sampling depth. In addition, several point anomalies had to be disregarded because samples collected on either side of these anomalies did not exhibit sufficient mercury levels to establish the area surrounding the points as an anomalous region.

In general, areas of high Hg concentrations did correlate with known thermal anomalies. Many of these areas are in close proximity to slope changes along gravity profiles substantiating the postulated structural control of the thermal anomalies. A definable northwest trending linear anomaly is outlined in the eastern portion of the OMC traverse. However, correlation with gravity profile inflection in the vicinity is uncertain. The interesting fact about this northwest trend is its parallel and subparallel relationship to several surface lineations in the mountain ranges on either side of the valley. A similarly oriented linear pattern defines a structural direction which appears to play a major role in the localization of the McLeod Ranch Hot Springs. Figure C27 shows the anomalous regions found in the Big Smoky Valley.

Shallow Electrical Resistivity

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Shallow resistivity measurements were conducted only at the McLeod Ranch site in the Big Smoky. The survey consisted of a Wenner array with an electrode spacing of 25 feet (7.6 m) used for mapping and 10, 25 and 50 feet (3.05, 7.6 and 15.2 m) for vertical electrical sounding (VES). Because the survey was undertaken after the two meter temperature study some knowledge of near surface material, composition and distribution was available. R-R' on figure C28 shows the location of the mapping line. A VES at point R with electrode spacings of 10, 25 and 50 feet (3.05, 7.6, 15.2 m) indicates a highly conductive layer between depths of penetration of the 25 and 50 (7.6 and 15.2 m) spacings. The layer was so conductive that our equipment could not supply a sufficient amount of current to register a potential. Assuming this conductive layer to



Figure C 27 . Areas of anomalously high soil mercury values in the Big Smoky Valley.



Figure C 28. Line (R-R') used during shallow resistivity study. Station spacing 100 feet. See figure 25 and accompanying text for temperature study.

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-137 represent a water saturated zone, mapping was conducted with a 25 foot (7.6 m) electrode spacing in a northerly direction towards R'. It was hoped that the resistivity would drop significantly in the vicinity of R' which is known from drilling to be nearly saturated at a depth of 1.5 m. No notable decrease was noted. An electrode spacing of 50 feet (15.2 m) near R' failed to penetrate the conductive layer encountered at R and the survey was discontinued.

Results of the study were at best indeterminate and the time expended in gathering the information excessive in view of the results. To use this method to locate near surface but buried faults would require 6-8 mapping-lines each requiring two man-days. The information obtained would be from a distinctly limited area, and if similar highly conductive materials were encountered the effort would likely be wasted.

Summary

A shallow resistivity study was conducted at only one geothermal resource site in the Big Smoky-McLeod. The survey produced ambiguous results and required too much time to be considered an effective exploration method when bounding in highly conductive layers found at this location.

Temperature Gradient Drilling

One primary and two alternative sites were selected prior to the commencement of drilling in the Big Smoky. Primary status was assigned to the Darrough's area while second and third choices were Spencer's and the Ophir-Moores Creek region respectively. Several criteria were used to make the selection as described below. Highest priority was assigned to the location we felt had the greatest potential of extending the limits of a known resource.

The decision to site the hole in the primary (Darrough's) area was made after consideration of the numerous complimentary lines of evidence discussed previously. To review, these include 1) a distinct inflection in the gravity

profile below the known surface and subsurface manifestations,(2) an area of anomalously high soil-mercury levels in the same position,(3) the linear pattern of shallow temperature isotherms and its colinear orientation with(4) the lineation described by the range-bounding fault trace and alluvial fault trace to the southwest of the geothermal expression. Also considered was the relatively high $(129^{\circ}C)$ temperature recorded from the 800+ foot well situated within the area defined by the hot springs.

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Fewer positive and supportive criteria were available to aid in choosing secondary sites. The Spencer's site was selected on the basis of the coincidence in location of a soil-mercury high and a relatively high shallow temperature probe measurement. Additionally, a slight inflection in the gravity profile was noted in the vicinity. A northwest trend of soil mercury anomalies combined with steep changes in the slope of the gravity profile led to the choice of the Ophir-Moores Creek alternate.

Drilling activities in the Big Smoky Valley study area were carried out during the last week of March and first week of April, 1980. A decision was made to apportion the remaining footage on the contract (610 ft.) between the Darrough's (BSD) and Spencer's (BSS) sites (fig. G30). In keeping with the restrictions discussed above, drilling at BSD-1 began with air although a limited capacity portable sump was available. A chronological description of drilling operations and their associated problems follows.

A significant problem with drilling was encountered at location BSD-1 which resulted in the drilling of a second and successful hole at nearby BSD-2 (fig. C29). The problem revolved around restrictions imposed by the Bureau of Land Management (BLM) because chipping fragments were found during site examination by a BLM geologist. These restrictions included a prohibition against the digging of a mud sump. In accordance with their request, BSD-1 was drilled using air and foam in thick alluvial fill. This endeavor ended in failure



Figure C29. Location of drill sites BSD-1, BSD-2, and thermal springs and well in the vicinity of Darrough's Hot Springs.

and was abandoned after the five day effort produced a caving hole less than 200 feet in depth. Seeking to avoid future BLM limitations, permission to drill on private land was acquired from a landowner, and approval of this approach was obtained from DOE. Using mud, a successful 500-foot hole was completed in similar materials in three days.

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29 March - BSD -1 spudded in at 1300 with a 7 7/8" tricone bit. Very coarse alluvial cover: difficult drilling. Operations terminated at 16:30 - water truck requires filling.

30 March - Owner of a local ranch agrees to supply water to the drilling contractor. Drilling is resumed at 11:30 and progresses slowly. All circulation is lost between 50 and 75 feet and only partial fluid recovery occurs above this interval. At the 75 foot level the drill string is tripped out and preparations made to install a 6" surface casing. A blockage is encountered at 50 feet which prevents further movement of the casing. It is decided to cease operations and drill ahead of the casing the following day.

31 March - Activity begins with the installation of a 5 7/8" bit which is run down the hole inside the casing. It is hoped that drilling ahead of the casing with the smaller diameter bit will permit the casing to be driven with the top head drive unit (kelley). The casing is finally set to 75 feet at 16:30 and drilling continues with the 5 7/8" bit. Attempts to maintain a heavy foam consistency are hampered by significant groundwater influx. Drilling stopped at 100 feet because of excessive caving. Mud and portable tank will be used the following day.

1 April - The morning is used to rig up for mud drilling. Over 400 gallons of mud are pumped downhole without returns. Lost circulation material is pumped downhole but returns are not gained. Drilling with an air-foam-mud mixture begins at 12:50 and continues until 18:00 at which time a 200 foot depth is attained. The drill string is tripped up into the cased section of the hole and operations terminated for this day.



Figure C 30. Locations of temperature gradient holes BSD-1, BSD-2, and BSS, in the Big Smoky Valley.

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DRILLING PROGRESS

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2 April - Rig requires recentering and string must be tripped out for replacement of a bit with a defective bearing. Drilling resumes at 14:00. Caving occurs and progress is severely hindered. At 15:30 a decision is made to abandon the effort before the string becomes jammed in the hole. During string removal continued caving of coarse material occurs. The string is out at 16:30 and mobilization to BSS site is ordered.

3 April - BSS is spudded in at 14:00 using a 7 7/8" tricone bit. Drilling proceeds rapidly in the fine alluvium and playa silts reaching a depth of 78 feet by 16:00. Casing of 6" diameter is run to total depth by 17:40 and the string is tripped into the hole and daily activity terminated.

4 April - Activities at BSS are halted while discussions are carried out with DOE Nevada Operations and the owner of the private land immediately north of BSD-1 regarding the prospect of drilling a second hole in the primary target area. The dialogue results in a decision to return to the Darrough area and drill on private land using mud.

5 April - BSS is abandoned and the drill crew leaves the area to obtain additional supplies required for the new hole. Drilling is scheduled to be resumed on 7 April. A rider is added to the original footage allowed in the contract to permit a total depth of 500 feet at the new location.

7 April - Operations at site BSD-2 with the digging of a mud pit and erection of the rig.

8-11 April - Drilling begins at 09:00 on 8 April. A single length of 6" surface casing is set to a depth of 22.5 feet and drilling continued using a 5 7/8" tricone bit. Progress is rapid and problems minimal. A comparison of drilling rates for BSD-1 and BSD-2 (fig. C31) demonstrates the marked increase in efficiency of the mud method in the alluvial materials. Total depth - 500 feet is attained at 19:30 on 10 April and the hole cased the following day using 3" steel pipe.

Results of Temperature Gradient Drilling

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Of the three gradient holes drilled in the Big Smoky Valley study area only one, BSD-2, had a good gradient and bottom hole temperature. Figure C32 is a plot of the gradient for BSD-2. As can be seen from the diagram, this hole has an excellent gradient, 14.3°C/100 m, and a maximum bottom hole temperature of 28.8°C was recorded at 471 feet approximately one month after the hole was completed. Additional gradient measurements after this showed no major changes in the gradient.

The results of this gradient hole helps expand the known extent of the Darrough's resource as no subsurface evidence had indicated that the resource extended west of the highway (see figure C29).

Figures C33, C34 and C35 are the general lithologic logs for gradient holes BSD-1, BSS and BSD-2, respectively. Holes BSD-1 and 2 were drilled along the alluvial boundaries of the valley, whereas BSS was drilled in the north central portion of the valley in the playa silts and fine sands. Drilling rates with air were best in the finer playa silts and sands (BSS) whereas drilling rates with mud were much better than drilling rates with air in the alluvial material of BSD-1 and 2.





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Figure C34.



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SUMMARY

Evaluation of Exploration Strategy

In addition to the geothermal resource assessment of three areas in Nevada, the techniques employed in each area were evaluated on the basis of useful data derived from the methods. The evaluation (table D1) considers the applicability of the contractual tasks to only low- and moderate-temperature geothermal resource exploration. Exploration programs for potential high-temperature electricity producing resources may employ some of these techniques but generally rely heavily on extensive drilling.

The tasks for this study are rated on a scale of 1 to 10 for each area studied. The rating system is somewhat subjective and is strictly related to the areas studied. Appropriate comments for each task are included.

In general, tasks that provided abundant information for little time, effort or money expended have the highest ratings. Those tasks that could be integrated with other parts of the program to facilitate data interpretation are also favorably evaluated. The lowest ratings are awarded to time-consuming tasks that provide little or dubious data.

Review of geologic literature includes published reports, maps and thesis studies and constitutes one of the most essential tasks in any exploration program. The moderate to high ratings for this task reflect the quality and availability of geologic data. The scale of the available data should, however, be closely matched to the scale of the project. Regional geologic maps at a scale of 1:250,000 are adequate for regional geothermal assessments but should be supplemented by more detailed work in a site-specific program.

Properly conducted gravity surveys can furnish abundant data at low cost. The surveys conducted during this study did provide abundant data but required

nearly 6 man-months to complete the field work alone. An additional 5 manmonths were consumed during data reduction and interpretation. Although the cross-valley traverses were useful for a regional interpretation, a grid-like pattern would be much more effective especially for a site-specific effort. Also, data extrapolation between distant traverses may lead to erroneous interpretations. The resultant data from gravity surveys are easily integrated with existing gravity data and can be very valuable if depth to bedrock is known from either well-log data or seismic surveys.

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Low sun-angle photographic surveys represent a component of imagery analysis that is particularly well suited to geothermal exploration programs. Economically attractive geothermal resources in the Basin and Range are generally associated with recent faulting. Subtle topographic features such as fault scarps are easily identified on air photos and greatly facilitate mapping and structural interpretation. However, ground verification of any linear feature is essential. Ground-disturbing activities such as agriculture, surface mining and urban activities may destroy parts or all of the target fault scarps. Natural erosion and deposition may also conceal the faulted topography.

Direct measurements of geothermal resources provide the most valuable data in any assessment program. Drilling is the most reliable method of obtaining subsurface temperatures but high drilling costs can limit the number and depth of planned holes. Drill-hole siting becomes a critical factor when funds are limited.

Shallow depth temperature probes have been used in this study to outline near-surface temperature anomalies. Temperatures measured 2 m below the ground surface are usually not affected by diurnal temperature variation. The effects of the annual temperature variation can be minimized if the reading interval for the temperature survey is small. Temperature corrections may be necessary, however, in areas where extreme inhomogeneous conditions occur in the soil,

shade-cover, moisture content or topography. Holes may be hand-augered or drilled with a truck-mounted rig in clay-rich or cobbly soils. The technique is applicable to regional studies but may be most helpful for locating wells in site-specific program.

Collecting existing water well data broadens the data base and helps to reduce the costs of fluid analysis programs. This is true only in areas for which reliable data are available. Although very little useful data was available for the Big Smoky Valley area principally due to the small population, there was a tremendous amount of useful data for the Carson-Eagle Valley area. The available data include water chemical analyses, temperature measurements and lithologic logs. These data should be thoroughly evaluated prior to use in the assessment.

Shallow resistivity surveys received the lowest rating because the time required to implement the task was high and the resultant data was dubious. The technique is especially useless in the vicinity of hot springs where conductive saline brines saturate near-surface layers and show no resistance at all. This technique was eliminated from the program and was replaced by the soil-mercury sampling task.

Soil samples collected along the gravity traverse lines generally showed high concentrations of mercury in the vicinity of faults. These faults were identified by geologic mapping and air photo interpretation and generally corresponded to the location of steep gravity contour gradients. This technique also requires considerable evaluation; mercury anomalies can also be caused by analyzing soils with an above average clay fraction and may lead to erroneous interpretations. Low mercury values may also arise from a remobilization of soils.

The fluid sampling task was used to distinguish the chemical characteristics

of thermal and non-thermal waters. In general, the major dissolved constituents provided the required data but trace and minor dissolved constituents were also used in the final interpretation. Isotopic analyses revealed a meteoric source for most of the sampled fluids, but fluids from Darrough's Hot Springs in the Big Smoky Valley appear to be chemically and isotopically different from local meteoric waters and probably represent a more complex heating history. Chemical geothermometers have been reliable indicators of subsurface temperatures in fluids that demonstrate little or no mixing with non-thermal fluids. Most of the fluids sampled here, however, have probably been mixed with shallow, cool, ground water. It should also be noted that commercial analytical laboratories may not provide reliable results for all samples and care must be exercised in laboratory selection.

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Temperature gradient holes were drilled in the study areas to obtain reliable subsurface temperature information, to possibly identify new sources of thermal fluids and to obtain reliable lithologic data. The data from the drill holes support the hypothesis that the geothermal fluids are limited in areal extent. The thermal fluids apparently rise along portions of faults and fault plane intersections.

Problems associated with drilling included the site-selection process and drilling fluids used. Although drilling permits for test holes can be easily obtained, primary drill sites in urban areas can raise conflict-of-interest problems and may result in law suits. Drilling on public land requires bonding and permitting procedures. Drilling with air is advantageous for eventual downhole fluid sampling, but mud is often needed to support the wellbore walls in unconsolidated material. Mud-drilled wells should be thoroughly flushed prior to sampling and fluid disposal may become problematic on both private and public land. Despite the logistical and technical problems, drilling represents the ultimate test of the assessment program.

Site-Specific Studioe Caliante Reting	vailable 7 Ugaful for gructural and strati- The acudy graphic interpretations. For a swall xemine in area, 1:230,000 acale maps are or reliable not approprista.	on indicates N/A N/A th location a. Study on than transact valuable to	vicinity of M/A W/A for defining of Tange- luvial fault occurrence.	ting mear- 3 2-m. probe aurvay results ware tes and nearly identical to data obtained to then. from down-hole temperature measure- epecific means of warm water wells in the ta).
hig Smoky,Yalley Commanie	Geologic information a on a large scale only. area is too large to a tha detail necessary f structural and strarig interpretations.	Subauface configurati faulting associated vi of getchermel resource a grid pattern, rather pattern, would be more study.	Particularly useful in Durrough's Not Springs co-linest arrangement bounding faults and al traces with geothermal Recommend scale of 1:2 Tagional studies.	Very useful in deliase surface thermal anomal pattern associated ut Applied only on a site besis (lass than 1 ag.
Ret ing	•	а.	æ	0 9
Regional Studies Lon-Regie Valley Comments	Regional data used in com- junction with gravity and air photos. Saail scale data used to aid in atructural and strati- graphic interpretations near thermal anomaly sites.	Yields Information on basement configuration, total displacement along faults, and depth of alluvial fill.	Delineated subtle copographic features of older fault scarps. Not especially useful in ground- disturbed areas-urban and agri- cultural.	Outlined areas in which the absolute measured temperature is high, relative to background. Configuration of isotherms configuration of isotherms fand-suggering holes becomes pholematic in clay-rich and cobble-rich areas. No tempera- ture corrections were applied
Care Bating	a	3 9	•	~
Taak	Geology	Gravicy	Lou Sua-Angle	1-2 m dapth Cemperature probe survey

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Table Di. Evaluation of Exploration Techniques.

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	Car	Regional Studies		Rie Smoky Vallay	Site Specific Studies				
Task	Ratin	Comments	Rating	Comments	Rating	Comments			
Water w ali data	8	Where available and reliable, may be used to identify both thermally and chemically anomalous areas.	3	Vary limited availability com- bined with selectively useful chemistry in the Big Smoky Valley study area.	N/A	¥/A			
Shallow Resistivity	1	Time-consuming technique that yields dubious results	2	Requires excessive time and yields indeterminate results. Especially useless in saline brine-saturated materials in the vicinity of hot springs.	N/A	. ¥/A			
Soll mercury	6	Best when sampled on a grid system and in an area of un- disturbed ground. The technique is quick and simple.	5	Requires consistent sampling tech- niques to produce meaningful re- suits.	7	Data obtained should be evaluated on the basis of original deposition favor- ability and probability of remobilization.			
fluid sampling	8 5 8	Major ion concentrations can be used to distinguish thermal waters from non-thermal waters. Minor and trace ion concentrations may not always be diagnostic. Iosotopes are very useful for identification of sources of fluids.	9 4 9	Nost meaningful approach obtained through consideration of combined isotopic and major ionic data. Trace elements useful only on a site specific basis.	8 4 3	Although thermal and non- thermal fluids were chemi- cally indistinguishable, their isotopic composition was different.			
Temperature gradient drilling	6	Identified geothernal gradient but failed to locate thernal fluids. Confirmed structural interpretation in drilled areas.	9	Particularly useful in delimiting the areal extent of the resources.	N/A	N/A			

Caliente Study Area

In addition to the major efforts conducted in the Carson-Eagle and Big Smoky areas, a smaller scale investigation was completed in the city of Caliente, Nevada and its immediate surroundings. The results from the majority of the techniques applied are detailed in a report published earlier this year (Trexler and others, 1980). However, data from isotopic analysis of fluids were not available at publication time. These data and their interpretation are discussed below.

Although major, minor and trace chemical constituents of thermal and non-thermal fluids do not show any clear distinctions, the hydrogen and oxygen-stable, light, isotopic data presented in Table D2 and plotted in Figure D1 indicate a prominent contrast. Thermal fluids are clearly grouped separately and within analytical error, present identical signatures. From their position in relation to the meteoric water line (Fig. D1) it seems reasonable to assume they are derived from meteoric water precipitated at a higher elevation than local non-thermal fluids and probably recharge from a single source. It is interesting to note that cold waters 9 and 6 form a distinct set. These fluids were collected in the southern portion of the area and display a similar distinct grouping in terms of major and minor dissolved constituents. Sample 7 which lies isotopically between the 9, 6 and thermal groups is chemically similar and may represent a mixing of these two types of waters. Because no isotopic data are available from fluids surrounding the Caliente area, no conclusions as to the source of the recharge can be drawn at this time.

Sample Name	Sample Number	δD ⁰ /00	δ ¹⁸ 0°/00	T°C
Wallis Well	CW-2A	-109	-14.6	67.0
Hospital rein- jection well	Cw-3A	-109	-14.4	29.2
Hot Springs Motel well	CW-5A	-106	-14.3	45.0
Clover Valley Wash	CW-6A	-88/-84	-11.7	12.0
Meadow Valley Wash	CW-7A	-97	-13.1	5.0
Van Kirk Well	CW-8A	-109	-14.4	42.8
Caliente City Well	CW-9À	-84	-12.1	15.0

Table D2. Hydrogen and oxygen-stable light Isotopic analysis results - Caliente

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Values separated by a slash indicate duplicate runs on a single sample.



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Appendix I

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Chemical Analyses of Water from Thermal and Non-thermal Sources: collected from the files of the Nevada Department of Health, Division of Consumer Protection Services.

Name	Location	T°C	рН	Depth m.	Ca ppm	Mg ppm	Na+K ppm	C1 ppm	F ppm	CO3/HCO3 ppm	SO4 ppm	TDS ppm
Bennett	T15NR20E								12			· ·
well no. 1	Sec. 23	44	8.03	39	280	1.14	214	36	3.9	0/22	1056	1554
Bennett	T15NR20E											-150
well no. 2	Sec. 23	44	8.14	-	277	7	105	34	4.3	0/32	840	1552
Bennett	T15NR20E											
well no. 3	Sec. 23	39	7.81	37	280	0	226	37	4.2	0/29	1090	1529
Bennett	T15NR20E											
well no. 4	Sec. 23	38	7.98	37	264	10	113	34	4.2	0/32	840	1517
	T15NR20E											
Brown well	Sec. 23	43	8.43	49	272	5	150	33	4.4	6/37	913	1614
Everson	- T15NR20E								•			
well	Sec. 23	29	8.33	28	181	26	196	33	4.0	0/37	873	1501
Hackett	T15NR20E											
well	Sec. 23	27	7.95	-	296	5	231	38	3.7	0/51	1120	1662
Hurin	T15NR20E											
well	Sec. 23	43	8.31	48	277	12	90	34	4.3	6/41	820	1606
Lagliamonte	T15NR20E			14								2
well	Sec. 23	45	8.22	46	277	2	147	33	4.3	2/29	913	1563
McKinzie	T15NR20E											
well	Sec. 23	42	8.1	-	269	12	110	32	4.0	0/34	859	1554

Table 1 . Chemical data for water in Pinyon Hills area. Source Nevada Division of Health.

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Name	Location	T°C	pH	Depth m.	Ca ppm	Mg ppm	K pmm	Na ppm	C1 ppm	F PPm	CO3/HCO3 ppm	SO4 ppm	TDS ppm
Merrimac well #1	T15NR2OE Sec. 2	С	7.97		49	17	8	85	43	.61	0/259	66	453
Merrimac well #2	T15NR2OE Sec. 2	C	7.70	21	65	21	4	50	28	. 52	0/273	. 57	432
Merrimac well #3	T15NR2OE Sec. 2	C	7.95		48	14	4	38	15	. 52	0/220	37	297
Mills well #1	T15NR2OE Sec. 2	С	7.82	21	87	24	10	71	42	. 54	0/154	276	661
Mills well #2	T15NR2OE Sec. 2	С	8.07	59	35	4	6	28	9	.74	0/61	78	255
Bowers well	T15NR2OE Sec. 2	С	7.65	27	33	10	6	27	13	.44	0/117	57	234
Bowland well	T15NR2OE Sec. 2	С	8.00	27	340	29	14	300	60	1.86	0/176	1218	2325
August well	T15NR2OE Sec. 2	С	7.75	30	94 [°]	27	18	242	64	1.15	0/439	425	1101
Schreinert well	T15NR2OE Sec. 2	С	7.52	30	630	60	18	544	195	. 92	0/222	2786	4338
Maximum security prison well	T15NR20E Sec. 16	W	8.8		13.5	.33	2	82	21	-	0/48	148	-
Burgess well	T15NR2OE Sec. 23	W	8.6	61	265	0	5	173	33	4	8/10	889	1587
Matthews well	T15NR2OE Sec. 23	н	7.31	30	262	1	4	176	34	3.2	0/12	1036	1546

Table 1 . Chemical data for water in Pinyon Hills area. Source Nevada Division of Health.

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Name	Location	T°C	рН	Depth m.	Ca ppm	Mg ppm	K ppm	Na ppm	C1 ppm	F Ppm	CO3/HCO3 ppm	SO4 ppm	TDS ppm
Imer well	T14NR2OE Sec. 28	н	8.5	25	170	0	4	182	40	3.42	4/2	707	1175
Hofer well	T14NR2OE Sec. 27	н	7.76	-	177	0	4	177	41	3.2	0/15	600	1193
Seaman well	T14NR2OE Sec. 33	C	8.14	33	19	5	4	41	8	1.5	0/144	36	247
McGowan well	T14NR2OE Sec. 33	C	7.9	-	117	1	5	152	28	3.6	0/24	553	926
Hickman well	T14NR2OE Sec. 33	C	7.75	34	19	4	5	69	28	1.54	0/139	54	284
Quirk well	T14NR2OE Sec. 33	C	7.8	-	18	4	4	53	9	1.75	0/146	38	254
Cave well	T14NR2OE Sec. 33	C	7.8	-	65	1	4	121	25	3.08	0.107	267	602
Ford well	T14NR20E Sec. 33	C	8.1	35	21	6	4	41	8	1.58	0/134	43	245
Kuperus well	T14NR20E Sec. 33	C	7.6	-	20	4	6	52	17	1.3	0/102	70	269
Longstrom well	T14NR20E Sec. 33	W	8.8	60	14	0	1	132	35	4.72	10/17	202	461
Pierce well	T14NR20E Sec. 33	C	7.7	_	19	7	4	45	8	1.4	0/159	35	235
Medium security prison well	T14NR2OE Sec. 4	C	7.73	107	32	7	1	15	9	.26	0/146	7	118

Table	2	•	Chemical	data	for	water	in	Saratoga	Hot	Springs	area.	Source	Nevada	Division of	Health.	:
Table 3 . Chemical data for water in Carson Hot Springs area. Source Nevada Division of Health.

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Name	Location	T°C	ЪН	Depth m.	Ca ppm	Mg ppm	K ppm	Na ppm	С1 ррт	F ppm	CO3/HCO3 ppm	SO4 ppm	TDS ppm
Carson Hot Spring	T15NR20E Sec. 5	50	9.41	_	3	0	1	103	30	8.1	32/7	98	307
Carson well	T15NR2OE Sec. 5	С	8.87	18.3	7	0	1	96	27	8.1	10/67	. 94	307
Odum well	T15NR2OE Sec. 6	С	7.58	27.5	19	8	2	19	4	.22	0/132	1	142
Thoreson well	T15NR2OE Sec. 5	С	7.64	-	27	10	2	19	5	.12	0/144	11	168
Stanley well	T15NR2OE Sec. 5	С	7.46	31.4	26	5	1	27	4	.19	0/137	10	182
Dickerson well	T15NR2OE Sec. 8	С	7.25	-	20	7	3	20	7	.22	0/132	2	148
Pagliaro well	T15NR2OE Sec. 5	С	7.9		17	б	2	15	0	.14	0/95	2	107
Brockuche well	T15NR2OE Sec. 5	С	7.89	-	16	5	1	12	2	.15	0/100	0	105
Frisbee well	T15NR2OE Sec. 5	С	7.72	-	16	4	2	14	1	.13	0/95	0	9 5
Barker well	T15NR2OE Sec. 5	С	7.70	-	18	4	2	16	3	.13	0/105	1	119
Fitts well	T15NR2OE Sec. 5	С	8.13	55	17	6	2	17	2	.2	0/102	1	106
Rudolph well	T15NR2OE Sec. 5	С	8.09	34.7	15	3	2	22	0	.19	0/102	4	144

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Name	Location	T°C	рН	Depth m.	Ca ppm	Mg ppm	K ppm	Na ppm	Cl ppm	F PPm	CO3/HCO3 ppm	SO4 ppm	TDS ppm
Hubert well	T15NR2OE Sec. 5	С	7.81	50	18	5	4	15	2	.14	0/98	6	138
Roulette well	T15NR2OE Sec. 6	C	7.65	45.7	15	6	2	17	0	.21	0/102	2	125
Ruby well	T15NR2OE Sec. 5	C	8.11	-	20	6	2	20	5	.16	0/124	ŝ	122
CCWD No. 7 well	T15NR2OE Sec. 6	С	8.16	170.7	16	2	2	17	1	0.05	0/105	4	98
Schoenfelde well	r T15NR2OE Sec. 5	C	8.03	24	22	5	2	14	3	0	0/110	1	128
Sullivan well	T15NR2OE Sec. 7	С	7.89	42	21	5	2	20	5	.15	0/117	1	125

Table cont.

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Gravity data from traverses in Carson-Eagle Valley and Big Smoky Valley study Areas

	Station	Latitude	Longitude	Elevation (Feet)	Theoretical Gravity (mg)	Observed Gravity (mg)	Simple Bouguer (mg)	Còmplete Bouguer (mg)
, â	BM 6034	39 24.13	116 56.44	6034	9801 27.48	9795 53.22	-212.22	-211.0
	S 1	39 24.31	116 56.52	6073	9801 27.74	9795 52.16	-211.20	-210.0
-2.1	S 2	39 24.35	116 56.73	6114	9801 27.80	9795 50.30	-210.66	-209.4
	S 3	39 24.37	116 56.84	6125	9801 27,83	9795 49.63	-210.70	-209.4
	s 4	39 24.42	116 56.98	6133	9801 27.90	9795 50.16	-209.77	-208.4
	S 5	39 24.54	116 57.11	6159	9801 28.08	9795 50.02	-208.52	-207.2
	S 6	39 24.86	116 57.20	6243	9801 28,55	9795 47.42	-206.55	-205.3
1	S 7	39 25.04	116 57.46	6333	9801 28.82	9795 42.94	-205.90	-204.4
	S 8	39 25.12	116 57.67	6394	9801 28.94	9795 39,60	-205.70	-204.2
	S 9	39 25.27	116 57.89	6480	9801 29,16	9795 35.00	-205.36	-204.0
	S 10	39 25.43	116 58.00	6535	9801 29.39	9795 32.04	-205.25	-203.7
	S 11	39 24.93	116 56.40	5986	9801 28.66	9795 54.41	-215.09	-213.9
	S 12	39 23.78	116 56.26	5937	9801 26.96	9795 56.25	-214.49	-213.4
	S 13	39 23.61	116 56.10	5911	9801 26.71	9795 57.73	-214.32	-213.4
	S 14	39 23.38	116 55.87	5873	9801 26.37	9795 59.01	-214.98	-214.0
	S 15	39 23.18	116 55.69	5846	9801 26.07	9795 59.87	-215.44	-214.5
	S 16	39 22.95	116 55.47	5824	9801 25.74	9795 60.55	-215.74	-215.0
	S 17	39 22.71	116 55.26	5812	9801 25.38	9795 60.76	-215.90	-215.3

GRAVITY DATA OF SPENCER TRAVERSE

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S	18	39 22.46	116 55.03	5793	9801 25.01	9795 61.62	-215.81	-215.1
S	19	39 22.24	116 54.83	5778	9801 24.69	9795 62.26	-215.75	-215.4
s	20	39 22.00	116 54.60	5763	9801 24.33	9795 62.15	-216.41	-215.7
s	21	39 21.79	116 54.42	5752	9801 24.03	9801 61.76	-217.14	-216.7
S	22	39 21.62	116 54.24	5742	9801 23.77	9795 61.24	-218.02	-217.5
S	23	39 21.42	116 54.04	5732	9801 23.48	9795 60.57	-218.99	-218.5
S	24	39 21.23	116 53.88	5724	9801 23.20	9795 60.09	-219.67	-219.3
S	25	39 21.00	116 53.66	5718	9801 22.86	9795 59.56	-220.22	-219.7
S	26	39 20.79	116 53.46	5706	9801 22.55	9795 60.27	-219.92	-219.5
S	27	39 20.61	116 53.28	5700	9801 22.29	9795 60.17	-220.12	-219.9
S	28	39 20.38	116 53.09	5693	9801 21.95	9795 62.11	-218.26	-219.0
S	29	39 20.20	116 52.89	5687	9801 21.68	9795 63.64	-216.83	-217.6
S	30	39 19.98	116 52.71	5686	9801 21.36	9795 65.18	-215.02	-214.8
\$	31	39 19.79	116 52.56	5678	9801 21.08	9795 67.85	-212.55	-212.3
S	32	39 19.61	116 52.36	5673	9801 20.81	9795 70.70	-209.73	-209.5
S	33 ·	39 19.43	116 52.19	5671	9801 20.55	9795 73.23	-207.06	-206.8
S	34	39 19.24	116 52.02	5669	9801 20.27	9795 74.50	-205.63	-205.4
S	35	39 19.06	116.51.85	5669	9801 20.00	9795 73.36	-206.51	-206.3
S	36	39 18.89	116 51.69	5669	9801 19.75	9795 72.76	-206.85	-206.5
S	37	39 18.68	116 51.50	5685	9801 19.44	9795 71.42	-206.92	-206.7

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77	S 38	39 18.50	116 51.33	5708	9801 19.18	9795 68.55	-208.15	-208.0
	S 39	39 18.32	116 51.17	5735	9801 18.91	9795 65.92	-208.90	-208.6
	s 40	39 18.14	116 50.98	5763	9801 18.65	9795 64.25	-208.79	-208.6
	S 41	39 17.94	116 50.80	5792	9801 18.35	9795 63.25	-207.94	-207.6
	S 42	39 17.72	116 50.59	5843	9801 18.03	9795 59.68	-208.12	-207.6
	S 43	39 17.52	116 50.39	5865	9801 17.73	9795 59.01	-207.18	-206.9
	S 44	39 17.31	116 50.22	5913	9801 17.42	9795 57.50	-205.50	-205.1
i.	S 45	39 17.10	116 50.03	5970	9801 17.11	9795 55.57	-203.71	-203.3
	S 46	39 16.90	116 49.84	6027	9801 16.82	9795 52.83	-202.73	-202.2
	S 47	39 16.73	116 49.67	6069	9801 16.57	9795 49.35	-203.44	-202.9
	S 48	39 16.53	116 49.51	6083	9801 16.27	9795 48.91	-202.74	-202.3
3.5	S 49	39 16.31	116 49.28	6117	9801 15.95	9795 46.55	-202.74	-202.3
	S 50	39 16.12	116 49.11	6168	9801 15.67	9795 42.79	-203.16	-202.6
	S 51	39 15.95	116 48.96	6217	9801 15.42	9795 40.09	-202.67	-202.0
	S 52	39 15.76	116 48.79	6253	9801 15.14	9795 37.38	-202.93	-202.3
	S 53.	39 15.57	116 48.61	6301	9801 14.86	9795 34.27	-202.89	-202.0

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GRAVITY DATA OF TRAVERSE OMC

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Station	Latitude	Longitude	Elevation (Feet)	Theoretical Gravity (mg)	Observed Gravity (mg)	Simple Bouguer (mg)	Complete Bouguer (mg)
omc-1	38 52.15	116 59.13	6581	9800 80.41	9794 60.44	-225.10	-222.5
omc-2	38 52.13	116 59.43	6468	9800 80.38	97 9 4 65.30	-227.00	-224.5
OMC-3	38 52.09	117 09.22	6400	9800 80.32	9794 67.75	-228.57	-226.3
omc-4	38 52.18	117 09.51	6310	9800 80.45	9794 73.03	-228.82	-226.5
OMC-5	38 52,33	117 09.85	6223	9800 80.67	9794 78.42	-228.88	-227.5
omc-6	38 52.55	117 09.98	6174	9800 81.00	9794 82.87	-227.68	-226.5
omc-7	38 52.82	117 01.18	6084	9800 81.39	9794 90.71	225.64	-224.5
OMC-8	38 52.99	117 01.37	6022	9800 81.64	9794 94.83	-225.49	-224.4
0MC-9	38 53.08	117 01.59	5966	9800 81.77	9794 97.73	-226.08	-225.3
OMC-10	38 53.19	117 01.87	5906	9800 81.94	9795 01.14	-226.43	-225.3
омс-11	38 53.31	117 02.19	5845	9800 82.11	9795 04.09	227.32	-226.5
0MC-0	38 52.12	116 09.28	6697	9800 80.36	9794 53.42	-225.12	-222.6
OMC-1A	38 52.15	116 09.12	6713	9800 80.41	9794 53.57	-224.06	-221.5
OMC-12	38 53.47	117 02.47	5795	9800 82,35	9795 07.22	-227.43	-226.8
OMC-13	38 53.57	117 02.77	5755	9800 82.49	9795 09.42	-227.77	-227.4
OMC-14	38 53.66	117 02.97	5729	9800 82.63	9795 11.83	-227.06	-226.9
омс-15	38 53.77	117 03.23	5709	9800 82,79	9795 13.25	-226.99	-226.7
OMC-16	38 53.86	117 03.50	5687	9800 82,92	9795 14.31	-227.39	-227.0
OMC-17	38 53.93	117 u3.75	5661	9800 83.02	9795 15.24	-228.12	-227.7
OMC-18	38 54.03	117 04.07	5627	9800 83.17	9795 16.47	-229.08	-228.8

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1	OMC-19	38 54.12	117 04.38	5601	9800 83.30	9795 16.99	-230.25	-230,0
ļ	OMC-20	38 54.18	117 04.58	5578	9800 83.39	9795 17.66	-231.05	-230.8
	OMC-21	38 54.26	117 04.83	5561	9800 83.51	9795 17.86	-231.99	-231.6
	OMC-22	38 54.33	117 05.08	5549	9800 83.61	9795 17.78	-232.89	-232.5
	OMC-23	38 54.40	117 05.37	5537	9800 83.71	9795 17.51	-233.98	-233.6
	OMC-24	38 54.48	117 05.58	5535	9800 83.83	9795 16.88	-234.85	-234.5
	OMC25	38 54.55	117 05.80	5534	9800 83.93	9795 16.34	-235.56	-235.3
	OMC-26	38 54.60	117 06.08	5531	9800 84.01	9795 15.52	-236.63	-236.2
	OMC27	38 54.55	117 06.42	5521	9800 83.93	9795 14.87	-237.80	237.3
	OMC-28	38 54.53	117 06.80	5511	9800 83.90	9795 14.61	-238.63	-238.3
	онс-29	38 54.53	117 07.12	5507	9800 83.90	9795 13.78	-239.71	-239.3
	OMC-30	38 54.55	117 07.43	5506	9800 83.93	9795 13.18	-240.39	-240.0
	омс-31	38 54.41	117 07.77	5510	9800 83.73	9795 12.02	-241.11	-240.6
	OMC-32	38 54.37	117 08.08	5514	9800 83.67	9795 11.65	-241.18	-240.6
	OMC-33	38 54.32	117 08.36	5518	9800 83.60	9795 11.14	-241.37	-240.8
	omc-34	38 54.30	117 08.70	5532	9800 83.57	9795 10.96	-240.68	-240.2
	OMC-35	38 54.28	117 09.05	5558	9800 83.54	9795 09.90	-240.16	-239.5
	онс-36	38 54.43	117 09.10	5557	9800 83.76	9795 10.83	-239.50	-238.7
	OMC37	38 54.63	117 09.10	5552	9800 84.05	9795 11.49	-239.44	-238,7
	omc-38	38 54.88	117 09.12	5544	9800 84.42	9795 11.87	-239.91	-239.3
	OMC-39	38 55.12	117 09.13	5540	9800 84.77	9795 12.24	-240.13	-239.3
	omc-41	38 55.15	117 09.52	5555	9800 84.81	9795 12.58	-238.94	-238.0
	OMC-42	38 55.15	117 09.70	5566	9800 84.81	9795 12.77	-238.09	-237.2

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OMC-43	38 55.38	117 09.73	5561	9800 85.15	9795 13.01	-238.49	-237,5
OMC-44	38 55.58	117 09.73	5560	9800 85,45	9795 13.33	-238.51	-237.5
OMC-45	38 55.82	117 09.73	5554	9800 85,80	9795 14.04	-238.52	-237.5
OMC-46	38 55.92	117 10.10	5570	9800 85,95	9795 14.60	-237.15	-236.0
OMC47	38 56.00	117 10.45	5589	9800 86.06	9795 15.93	-234.79	-233.7
OMC-48	38 56.07	117 10.75	5607	9800 86,17	9795 16.47	-233.28	-233.5
OMC-49	38 56.15	117 11.08	5622	9800 86.28	9795 18.24	-230.72	-228.8
OMC-50	38 56.22	117 11.38	5633	9800 86.39	9795 19.34	-229.07	-226.7
OMC-51	38 56.30	117 11.72	5664	9800 86.50	9795 21.03	-225.63	-223.7
OMC-52	38 56.35	117 11.95	5689	9800 86.58	9795 21.77	-223.47	-222.4
OMC~53	38 56.42	117 12.25	5725	9800 86.68	9795 22.69	-220.49	-217.6
OMC-54	38 56.48	117 12.57	5767	9800 86.77	9795 22.45	-218.30	-215.7
OHC-55	38 56.55	117 12.86	5807	9800 86.87	9795 21.56	-216.89	-214.0
0MC56	38 56.63	117 13.15	5856	9800 86.99	9795 19.75	-215.88	-212,6
OMC-57	38 56.70	117 13.40	5900	9800 87.09	9795 18.01	-215.08	-211.0
OMC-58	38 56.68	117 13.72	5965	9800 87.06	9795 14.84	-214.33	-210.0
0MC-59	38 56.63	117 13.95	6047	9800 86.99	9795 10.55	-213.62	-208.2
OMC-60	38 56.45	117 14.32	6205	9800 86.73	9795 02.07	-212.35	-205.5
OMC-61	38 56.47	117 14.57	6507	9800 86.75	9794 84.99	-211.34	-204.0

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		Station	Latitude	Longitude	Elevation (Feet)	Theoretical Gravity (mg)	Observed Gravity (mg)	Simple Bouguer (mg)	Complete Bouguer (mg)	
	-	MR 7	39 2.56	117 9.95	5564	9800 95.71	9795 35.96	-225.91	-223.8	
		MR 9	39 4.05	117 12.04	6882	9800 97.90	9794 78.24	-206.74	-198.3	
		MR 8	39 4.14	117 12.15	6753	9800 98.03	9794 85.99	-206.86	-200.0	
		MR 10	39 4.00	117 11.87	6419	9800 97.83	9794 98.50	-214.19	-205.9	
		MR 11	39 3.87	117 11.73	6145	9800 97.64	9795 11.77	-217.16	-210.0	
	1	MR 12	39 3.69	117 11.48	6003	9800 97.37	9795 17.35	-219.84	-214.0	
TT	1	MR 13	39 3.54	117 11.29	5934	9800 97.15	9795 19.84	-221.27	-217.0	
Ø	1	MR 14	39 3.40	117 11.10	5867	9800 96.94	9795 22.97	-221.95	-217.9	
		MR 15	39 3.19	117 10.84	5776	9800 96.64	9795 26.87	-223.21	-220.2	
		MR 16	39 3.05	117 10.60	5719	9800 96.43	9795 29.27	-224.02	-220.6	
		MR 17	39 2.94	117 10.36	5660	9800 96.27	9795 31.65	-225.01	-222.1	
		MR 18	39 2.76	117 10.18	5619	9800 96.00	9795 33.38	-225.48	-222.8	
	100	MR 22	39 1.82	117 9.93	5492	9800 94.62	9795 36.19	-228.91	-227.0	1
		MR 23	39 1.72	117 9.66	5471	9800 94.47	9795 35.13	-231.08.	-229.5	
		MR 24	39 1.64	117 9.41	5462	9800 94.36	9795 33.61	-233.02	-231.5	
		MR 25	39 1.54	117 8.96	5465	9800 94.21	9795 31.72	-234.59	-233.4	
		MR 26	39 1.55	117 8.70	5459	9800 94.22	9795 30.83	-235.85	-234.6	
		MR 27	39 1.52	117 8.38	5462	9800 94.18	9795 28.92	-237.54	-236.3	

GRAVITY DATA OF MCLEOD RANCH TRAVERSE

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MR 28 39 1.52 117 8.18 5473 9800 94.18 9795 25.25 -240.55 -239.4 MR 29 39 1.46 117 7.95 5476 9800 94.09 9795 23.63 -241.90 -240.7 MR 30 39 1.44 117 7.74 5463 9800 94.06 9795 23.54 -242.74 -241.8MR 31 39 1.47 117 7.22 5442 9800 94.11 9795 24.07 -243.51 -242.5 MR 32 39 1.50 117 6.70 5438 9800 94.15 -243.2 9795 23.99 -243.88MR 33 39 1.49 117 6.29 5449 9800 94.13 9795 23.08 -244.12 -243.4 **MR 34** 39 1.49 117 5.87 5452 9800 94.13 9795 22.95 -244.06 -243.5 MR 35 39 1.49 117 5.41 5455 9800 94.13 9795 22.64 -244.19 -243.8 MR 36 39 1.50 117 5.01 5459 9800 94.15 9795 22.66 -243.95 -243.6 MR 37 39 1.51 117 4.60 -244.5 5463 9800 94.16 9795 21.56 -244.83 MR 38 39 1.52 117 4.19 5467 9800 94.18 9795 21.75 -244.40 -244.0 MR 39 39 1.53 117 3.81 5466 9800 94.19 9795 22.05 -244.18 -243.9 MR 40 39 1.54 117 3.27 5476 9800 94.21 -243.71 -243.2 9795 21.93 MR 41 39 1.58 117 2.88 5490 -241.0 9800 94.27 9795 23.47 -241.39 MR 42 39 1.58 117 2.54 5499 9800 94.27 9795 23.67 -240.65 -240.3 MR 43 39 1.59 117 2.23 5512 9800 94.28 9795 23.96 -239.60 -239.2 MR 44 39 1.59 117 2.23 5528 9800 94.28 9795 23.69 -238.91 -238.4 MR 45 39 1.69 117 1.57 5554 9800 94.43 9795 22.70 -238.49 -238.0 MR 46 39 1.83 117 1.26 5584 9800 94.63 9795 21.16 -238.43 -237.8 MR 47 39 1.96 -237.4 117 .91 5614 9800 94.83 9795 19.93 -238.06 MR 48 39 2.10 -237.0 117 .67 5642 9800 95.03 9795 18.81 -237.71

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MR	49	39	2.24	117 .37	5674	9800 95.24	9795 17.86	-236.94	-236.3
MR	50	39	2.36	117 .14	5701	9800 95.41	9795 17.36	-235.99	-235.3
MR	51	39	2.51	116 59.80	5733	9800 95.63	9795 16.87	-234.78	-234.0
MR	52	39	. 45	116 56.06	6419	9800 92.61	9794 80.60	-226.86	-225.5
MR	53	39	.57	116 56.28	6387	9800 92.78	9794 81.90	-227.66	-226.4
MR	54	39	.69	116 56.61	6318	9800 92.96	9794 84.90	-228.98	-227.8
MR	55	39	.87	116 56.90	6264	9800 93,22	9794 90.72	-226.67	-225.5
MR	56	39	.98	116 57.10	6224	9800 93.38	9794 91.07	~228.88	-227.7
MR	57	39	1.13	116 57.31	6179	9800 93.61	9794 93.52	-229.34	-228.0
MR	58	39	1.27	116 57.54	6128	9800 93.81	9794 97.22	-228.91	
hr	59	39	1.41	116 57.76	6080	9800 94.02	9795 00.19	-229.03	-227.8
MR	60	39	1.56	116 57.98	6035	9800 94,24	9795 03.26	-228.88	-227.8
MR	61	39	1.69	116 58.19	5996	9800 94.43	9795 05.67	-229.00	-228.0
MR	62	39	1.84	116 58.42	5948	9800 94.65	9795 08.20	-229.57	
MR	63	39	1.99	116 58.69	5902	9800 94.87	9795 10.47	-230.28	-220, 3
MR	64	. 39	2.10	116 58.95	5862	9800 95.03	9795 11.56	-221 76	
MR	65	39	2.19	116 59.20	5821	9800 95 16	9795 13 05		~230.7
MR (66	39	2.29	116 59.41	5780	0000 05 31		-232.60	-232.0
1410	6 7	20			2763	2000 23,31	A1A2 13480	-234.12	-233.7
TIR (77	2.40	116 59,60	5755	9800 95.47	9795 14.96	-235,21	-234.3

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GRAVITY DATA OF TRAVERSE 8A

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Station	Latitude	Longitude	Elevation (Feet)	Theoretical Gravity (mg)	Observed Gravity (mg)	Simple Bouguer (mg)	Complete Bouguer (mg)
8A-2	38 58.38	117 11.57	5747	9800 82.21	9795 08.48	-228.91	-226.6
8A-3	38 53.12	117 11.57	5746	9800 81.83	9795 08.32	-228.75	-226.4
8 A -4	38 52.90	117 11.55	5740	9800 81.51	9795 08.12	-228.99	-226.5
8A-5	38 52.65	117 11.53	5732	9800 81.14	9795 07.98	-229.24	-226.5
8A-6	38 52.40	117 11.52	5722	9800 80.77	9795 08.10	-229.36	-226.5
8A7	38 52.08	117 11.52	5703	9800 80.30	9795 08.24	-229.88	-227.0
8A-8	38 51.80	117 11.52	5682	9800 79.89	9795 07.97	-231.01	-228.0
8A-9	38 51.52	117 11.50	5664	9800 79.48	9795 09.55	-230.09	-226.9
8A-10	38 51.25	117 11.48	5662	9800 79.09	9795 10.07	-229.29	-226.0
8A-11	38 51.00	117 11.48	5678	9800 78.72	9795 09.19	-228.85	-225.0
8A-12	38 50.72	117 11.47	5678	9800 78.31	9795 08.97	-228.66	-224.4
8A-13	38 50.43	117 11.45	5665	9800 77.88	9795 09.30	-228.68	-224.3
8A-14	38 53.62	117 11.58	5745	9800 82.57	9795 09.19	-228.68	-226.5
8A-15	38-53.83	117 11.58	5741	9800 82.88	9795 09.78	-228.63	-226.5
8A-16	38 54 07	117 11.60	5732	9800 83.23	9795 10.80	-228.51	-226.4
8A-17	38 54.28	117 11.62	5724	9800 83.54	9795 12.00	-228.10	-226.0
8A-18	38 54.53	117 11.63	5719	9800 83.90	9795 12.77	-227.99	-225.7
8A-19	38 54.80	117 11.63	5709	9800 84.30	9795 14.07	-227.70	-225.5
8A-20	38.55.07	117 11.65	5698	9800 84.70	9795 15.26	-227.55	-225.4
8A-21	38 55.30	117 11.67	5689	9800 85.04	9795 16.46	-227.23	-225.1
8A-22	38 55.52	117 11.68	5683	9800 85.36	9795 17.47	-226.91	224.8

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STATISTICS AND ADDRESS

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Station	Latitude	Longitude	Elevation (Feet)	Theoretical Gravity (mg)	Observed Gravity (mg)	Simple Bouguer (mg)	Complete Bouguer (mg)
8B-1	38 51.05	117 02.66	6001	9800 78.79	9794 87.28	-231.45	-230.0
8B-2	38 51.30	117 02.64	5973	9800 79.16	9794 89.39	-231.39	-230.1
8B-3	38 51.54	117 02.68	5921	9800 79.51	9794 92.89	-231.36	-230.1
8B-4	38 51.77	117 02.68	5887	9800 79.85	9794 95.56	-231.07	-229.9
88-5	38 52.02	117 02.73	585 9	9800 80.22	9794 97.11	-231.57	-230.3
8B6	38 52.23	117 02.73	5849	9800 80.53	9794 98.20	-231.39	-230.3
8B7	38 52.43	117 02.75	5840	9800 80.82	9794 99.47	-230.95	-229.9
8B-8	38 52.67	117 02.78	5819	9800 81.17	9795 02.00	-230.03	~229.0
88-9	38 52.88	117 02.75	5804	9800 81.48	9795 03.36	-229.88	-228.9
5B-10	38 53.07	117 02.77	5790	9800 81.76	9795 04.50	-229.86	-229.0
8B-11	38 53.32	117 02.78	5768	9800 82.13	9795 07.81	-228.23	-227.4
8B-12	38 53.82	117 02.73	5762	9800 82.86	9795 10.60	-226.54 ·	-225.0
8B-13	38 54.02	117 02.73	5779	9800 83.15	9795 10.07	-226.35	-225.6
8B-14	38 54.27	117 02.73	5792	9800 83.52	9795 10.92	-225.08	-224.4
8B-15	38 54.43	117 02.75	5794	9800 83.76	9795 11.63	-224.48	-223.9
88-16	38 54.62	117 02.68	5767	9800 84.04	9795 14.06	-223.95	-223.3

GRAVITY DATA OF TRAVERSE 8B

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Station	Latitude	Longitude	Elevation (Feet)	Theoretical Gravity (mg)	Observed Gravity (mg)	Simple Bouguer (mg)	Complete Bouguer (mg)
D 2	38 49.17	117 12.83	6728	9800 76.03	9794 50.91	-221.44	-210.0
D 1	38 49.16	117 12.75	6536	9800 76.02	9794 60.82	-223.03	-211.7
D 3	38 49.28	117 12.10	6106	9800 76.19	9794 83.84	-226.00	-219.6
D 4	38 49.25	117 12.34	6253	9800 76.15	9794 76.05	-224.92	-216.4
D 5	38 49.25	117 11.83	5974	9800 76.15	9794 90.19	-227.52	-228.7
D 6	38 49.27	117 11.57	5856	9800 76.18	9794 97.02	-227.80	-223.7
Ð 7	38 49.27	117 11.27	5743	9800 76.18	9795 02.41	-229.19	-225.3
D 9	38 49.32	117 10.61	5559	9800 76.25	9795 08.37	-234.34	-231.3
D 10	38 49.34	117 10.32	5549	9800 76.28	9795 07.45	-235.89	-233.5
Ð 11	38 49.37	117 10.03	5548	9800 76.32	9795 06.57	-236.87	-234.6
D 12	38 49.39	117 9.72	5544	9800 76.35	9795 05.88	-237.83	-235.7
D 13	38 49.42	117 9.41	5543	9800 76.40	9795 05.52	-238.30	-236.5
D 14	38 49.46	117 9.06	5542	9800 76.46	9795 05.01	-238.93	-237.5
D 15	38 49.49	117 8.70	5541	9800 76.50	9795 04.92	-239.12	-237.6
Ð 16	38 49.58	117 8.34	5539	9800 76.63	9795 04.70	-239.59	-238.9
D 17	38 49.82	117 8.22	5536	9800 76.99	9795 04.90	-239.93	-239.3
D 18	38 49.76	117 7.88	5538	9800 76.90	9795 04.05	-240.57	-239.7
D 19	38 49.70	117 7.57	5538	9800 76.81	9795 03.67	-240.86	240.0

GRAVITY DATA OF DARROUGH'S RANCH TRAVERSE

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	D 20	38 49.64	117 7.26	5542	9800 76.12	9795 03.42	-240.78	-240.0	
	D 21	38 49.57	117 6.92	5548	9800 76.62	9795 03.13	-240.61	-239.8	
	D 22	38 49.49	117 6.53	5550	9800 76.50	9795 03.73	-239.77	-239.0	
	D 23	38 49.41	117 6.25	5559	9800 76.38	9795 04.19	-238.65	-237.9	
25	D 24	38 49,33	117 5.96	5572	9800 76.27	9795 04.28	-237.66	-236.9	
	D 25	38 49.28	117 5.62	5591	9800 76.19	9795 04.93	-235.80	-235.0	
	D 26	38 48.32	117 1.48	6769	9800 74.78	9794 39.91	-228.73	-223.6	
	D 27	38 48.40	117 1.81	6636	9800 74.90	9794 48.62	-228.13	-225.4	
	D 28	38 48.47	117 2.18	6494	9800 75.00	9794 56.12	-229.25	-226.6	
H	D 29	38 48.51	117 2.44	6398	9800 75.06	9794 61.50	-229.68	-227.0	
14	D 30	38 48.54	117 2.70	6305	9800 75.11	9794 67.63	-229.18	-226.5	
	D 31	38 48.59	117 2.98	6205	9800 75.18	9794 73.32	-229.56	-227.1	
	D 32	38 48,68	117 3.24	6104	9800 75.31	9794 78.72	-230.35	-228.0	
13. 1	D 33	38 48.79	117 3.48	6007	9800 75.47	9794 83.98	-231.08	-228.9	
	D 34	38 48.91	117 3.71	5908	9800 75.65	9794 89.48	-231.69	-229.8	
We a	D 35	· 38 48.99	117 4.02	5805	9800 75.77	9794 95.40	-232.07	-230+2	*).**
	D 36	38 49.06	117 4.32	5745	9800 75.87	9795 00.36	-230.81	-229.2	
	D 37	38 49.10	117 4.53	5694	9800 75.93	9795 02.74	-231.55	-230.0	
	D 38	38 49.13	117 4.83	5650	9800 75.97	9795 04.65	-232.33	-231.0	
	D 39	38 49.19	117 5.10	5623	9800 76.06	9795 05.25	-233.43	-232.4	
	Ð 40	38 49.24	117 5.38	5601	9800 76.13	9795 05.66	-234.41	-233.5	

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Station	Latitude	Longitude	Elevation (Feet)	Theoretical Gravity (mg)	Observed Gravity (mg)	Simple Bouguer (mg)	Complete Bouguer (mg)
CS-1	39 07.15	119 37,87	5272	9801 02.46	9795 75.63	-183,21	-182.18
CS-2	39 07.37	119 37.87	5667	9801 02.79	9795 80.12	-182.64	
CS-3	39 07.42	119 38.06	5644	9801 02.86	9795 80.99	-183.23	
CS-4	39 07.68	119 38,43	5598	9801 03.24	9795 85.74	-181.62	
CS-5	39 07.87	119 38,63	5487	9801 03.52	9795 89.70	-184.60	
CS-6	39 08.07	119 38.75	5422	9801 03.82	9795 94.56	-183.93	
CS-7	39 08.29	119 38.84	5352	9801 04,14	9795 97.63	-185.39	
CS-8	39 08.58	119 38.91	5215	9801 04.57	9796 06.70	-184.96	
CS-9	39 08.78	119 39,15	5123	9801 04.86	9796 10.54	-186.94	
CS-10	39 09.13	119 39.39	5073	9801 05.38	9796 17.39	-183.61	
CS-11	39 09.23	119 39,72	5008	9801 05.52	9796 21.07	-183.97	-182.76
CS-12	39 09.36	119 39.97	4985	9801 05.71	9796 22.33	-184.28	
CS-13	39 09.48	119 40.13	4922	9801 05.89	9796 26.34	-184.23	
CS-14	39 09.62	119 40.47	4892	9801 06.10	9796 28.91	-183.67	
CS15	39 09.81	119 40.81	4777	9801 06.38	9796 36.55	-183.21	
CS-16	39 09.97	119 40,96	4807	9801 06.61	9796 35.38	-182.81	
CS-17	39 10.18	119 40.95	4712	9801 06.92	9796 42.61	-181.59	
CS~18	39 10.33	119 41.27	4657	9801 07.14	9796 47.97	-179.75	
CS-19	39 10.54	119 41.31	4602	9801 07,45	9796 53.24	-178.09	

9801 07.67

9796 55.43

-176.49

GRAVITY DATA OF TRAVERSE CS

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CS-20

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119 41.09

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	CS-21	39 10.86	119 41.12	4606	9801 07.92	9796 54.37	-177.20		
•	CS-22	39 10.84	119 41.34	4633	9801 07.89	9796 52.73	-177.18	-175.85	
	PUMPHS	-23 39 10.84	119 41.67	4612	9801 07.89	9796 52.06	-179.11		
	CS-24	39 10.99	119 41.73	4614	9801 08,11	9796 51.90	-179.37	-178.56	
	CS25	39 11.13	119 42.01	4646	9801 08.32	9796 47.96	-181.60	-180.89	
	CS-26	39 11.32	119 42.13	4647	9801 08.60	9796 47.79	-181.99	-181,27	
	CS-27	39 11.22	119 42.46	4620	9801 08.45	9796 47.96	-183.29	-182.58	
	CS28	39 11.08	119 42.83	4622	9801 08.25	9796 45.05	-185.88	-185.17	
	CS-29	39 10.94	119 43.2	4632	9801 08.04	9796 42.76	-187.36	-186.59	
	CS-30	39 10.81	119 43.45	4636	9801 07.85	9796 41.25	-188.44	-187.57	
н	CS-31	39 10.69	119 43.73	4640	9801 07.67	9796 39.37	-189.91	-189.16	
л 16	CS-32	39 10.59	119 43.94	4642	9801 07.52	9796 36.43	-192.57	-191.74	
•	CS-33	39 10.86	119 43.93	4657	9801 07.92	9796 40.45	-188.05	-187.22	•
	CS-34	39 11.15	119 43.93	4672	9801 08.35	9796 42.36	-185.67	-184.89	
	CS-36	39 11.43	119 44.18	4687	9801 08.76	9796 41.57	-185.97	-185.05	
	CS-37	39 11.41	119 44.48	4683	9801 08.73	9796 41.19	-186,56	-185.68	
	BM R316	39 11,60	119 44.90	4704	9801 09.01	9796 39.19	-187.58	-186.51	
	BH 4697	39 11.57	119 45.23	4697	9801 08.97	9796 40.17	-186.98	-185.89	
	CS-38	39 11.90	119 45.24	4745	9801 09.45	9796 38.10	-186.65	-185.56	
	CS-39	39 11.91	119 45.57	4729	9801 09.47	9796 37.86	-187.87	-186.69	
	CS-40	39 12.22	119 45.63	4899	9801 09.92	9796 27.82	-188.16	-186.37	
	CS-41	39 12.58	119 45.75	5279	9801 10.45	9796 03.97	-189.75	-188.14	
	CS-42	39 12.89	119 46.08	5970	9801 10.91	9795 61.06	-191.65	-189.57	

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GRAVITY DATA OF TRAVERSE HS

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Station	Latitude	Longitude	Elevation (Feet)	Theoretical Gravity (mg)	Observed Gravity (mg)	Simple Bouguer (mg)	Complete Bouguer (mg)
HS-1	39 03.76	119 50.00	4931	9800 97.47	9796 01.63	-199.98	
HS-2	39 03.82	119 49.87	4905	9800 97.56	9796 03.97	-119.29	-196.67
HS-3	39 03.66	119 49.85	4874	9800 97.33	9796 06.48	-198.40	-196.12
HS-4	39 03.49	119 49.60	4820	9800 97.08	9796 10.60	-197.28	-195.13
HS-5	39 03.34	119 49.33	4690	9800 96.86	9796 16.75	-198.70	-196.41
HS-6	39 03.47	119 49.16	4710	9800 97.05	9796 16.96	-197.48	-195.36
us-7	39 03.56	119 48.96	4701	9800 97.18	9796 17.19	-197.93	-195.76
BM 4653	39 03.95	119 48.28	4653	9800 97.75	9796 20.42	-198.15	-196.7
11S- 8	39 03.68	199 48.08	4647	9800 97.36	9796 18.31	-200.22	-198.97
HS-9	39 03.74	199 48.48	4753	9800 97.44	9796 15.53	-196.73	-194.97
HS-10	39 03.62	119 48.54	4656	9800 97.27	9796 20.26	-197.64	-195.88
HS-11	39 03.62	119 48.68	4701	9800 97.27	9796 17.69	-197.52	-195.68
HS-12	39 04.37	119 40.03	5694	9800 98.37	9795 69.85	-186.88	-185.61
HS-13	39 04.45	119 39.77	5840	9800 98.49	9795 61.52	-186.57	~185.3
IIS-14	39 04.25	119 40.26	5591	9800 98.19	9795 77.58	-185.16	-184.08
HS-15	39 04.07	119 40.43	5452	9800 97.93	9795 84.98	-185.83	-184.87
HS-16	39 04.01	119 40.63	5390	9800 97.84	9795 88.01	-186.43	-185.76
HS-17	39 03.99	119 40.97	5302	9800 97.81	9795 91.31	-188.38	-187.74

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	HS-18	39 04.04	119 41.23	5245	9800 97.89	9795 92.34	-190.85	-190.25
	HS-19	39 03.91	119 41.48	5187	9800 97.69	9795 95.64	-190.83	-190.23
	HS-22	39 03.53	119 41.92	5070	9800 97.14	9796 05.48	-187.45	-186.81
	BM 5136	39 03.56	199 41.58	5136	9800 97.18	9796 00.95	-188.07	-187.55
	HS-23	39 03.35	119 42.12	5058	9800 96.87	9796 07.40	-185.99	-185.12
	HS-24	39 03.23	119 42.38	5076	9800 96.69	9796 05.59	-186.54	-185.51
	HS-25	39 03.04	119 42.56	4965	9800 96.41	9796 11.53	-186.98	-186.17
	HS-26	39 02.92	119 42.77	4917	9800 96.24	9796 11.58	-189.64	-188.65
	HS-27	39 02.80	119 42.97	4859	9800 96.06	9796 13.20	-191.32	-190.59
	HS-28	39 02.83	119 43.18	4824	9800 96,11	9796 14.94	-191.73	-190.81
8	HS-29	39 02.83	119 43.40	4788	9800 96.11	9796 16.23	-192.60	-191.60
	HS30	39 02.83	119 43.72	4746	9800 96.11	9796 18.76	-192.59	-191.88
- 1	NS-31	39 02.93	119 44.05	4737	9800 96.25	9796 18.59	-193.45	-192.70
	HS-32	39 02.91	119 44.42	4693	9800 96.22	9796 17.38	-197.26	-196.58
: .	HS-33	39 03.65	119 50.86	5317	9800 97.31	9795 73.99	-204.30	-198.16
	HS-34	39 03.52	119 51.08	5570	9800 97.12	9795 58.70	-204.22	-194.63
	HS-35	39 03,75	119 50.65	5164	9800 97.46	9795 83.22	-204.40	-199.28
	HS-36	39 03.80	119 50.39	5056	9800 97.53	9795 91.78	-202.39	-198.79
	HS-37	39 03.83	119 50.01	4944	9800 97.58	9796 00.43	-200.50	198.22
	HS-38	39 02.99	119 44.51	4696	9800 96.34	9796 15.39	-199.19	-198.55

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HS-39	39 03.15	119 44.50	4697	9800 96.58	9796 16.37	-198.38	-197.59
HS-40	39 03.43	119 44.50	4697	9800 96.99	9796 17.46	-197.71	-196.64
HS-41	39 03.48	119 44.82	4670	9800 97.06	9796 16.29	-200.58	-199.62
llS-42	39 03.45	119 45.15	4655	9800 97.02	9796 16.45	-201.27	-200.52
HS-43	39 03.42	119 45.45	4650	9800 96.97	9796 15.61	-202.36	-201.29
HS-44	39 03.48	119 45.78	4642	9800 97.06	9796 13.93	-204.61	-203.52
HS-45	39 03.49	119 46.10	4634	9800 97.08	9796 16.26	-202.77	-201.66
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Station	Latitude	Longitude	Elevation (Feet)	Theoretical Gravity (mg)	Observed Gravity (mg)	Simple Bouguer (mg)	Complete Bouguer (mg)
DF 30	38 58.80	119 50.28	5475	9800 90.18	9795 61.76	-199.92	-190.94
BM 4694W	38 58.77	119 50.00	4694	9800 90.14	9796 01.23	~207.27	-199.93
BM 4685	38 58.52	119 50.18	4685	9800 89,77	9796 02.10	-206.56	-199.96
BM 4676	38 58.27	119 49.83	4676	9800 89.40	9795 98.96	-209.88	-205,73
DF 32	38 58.27	119 49.48	4680	9800 89.40	9795 98.16	-212.44	-209.21
DF 31	38 58,26	119 49.28	4679	9800 89,39	9795 9 4.99	-213.66	-210,55
BM 4678	38 58.27	119 49.03	4678	9800 89.40	9795 93.58	-215.14	-212.14
BM 4688	38 58,26	119 47.91	4688	9800 89.39	9795 91.66	-216.45	-215.09
DF 33	38 58.25	119 47.56	4690	9800 89.37	9795 91.97	-216.00	-214.67
DF 34	38 58.25	119 47.28	4695	9800 89.37	9795 92.11	-215.56	-214.38
BM 4698	38 58,23	119 46.70	4698	9800 89.34	97 9 5 93.53	-213.93	-213.01
BM 4694E	38 58,57	119 46.68	4694	9800 89.84	9795 94.39	-213.81	-212.89
DF 2	38 58.57	119 45.75	4711	9800 89.84	9795 98.62	-208.56	-207.96
BM 4714	38 58,57	119 45.59	4714	9800 89.84	9795 99.59	-207.41	-206.82
DF-1	38 58.57	119 45.47	4715	9800 89.84	9796 00.46	-206.52	-205.93
DF-3	38 58.57	119 45.32	4718	9800 89.84	9796 01.58	-205.18	-204.64
DF-4	38 58.58	119 45.16	4721	9800 89.86	9796 02.78	-203.81	~203.29
BM 4743	38 58,56	119 44.47	4743	9800 89.83	9796 05.57	-199.68	-199.38
BM 4767	38 58.56	119 43.93	4767	9800 89.83	9796 01.09	-202.72	-202.45

GRAVITY DATA OF TRAVERSE DF

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DF 6 38 58.57 119 43.42 4790 9800 89.84 9796 01.49 -200.95 -201.1 DF 7 38 58.57 119 43.15 4805 9800 89.84 9795 99.14 -201.32 -201.3 DF 8 38 58.57 119 42.92 4820 9800 89.84 9795 99.14 -202.28 -202.2 DF 9 38 58.57 119 42.63 4832 9800 89.64 9795 97.65 -202.28 -202.3 DF 10 38 58.49 119 42.43 4836 9800 89.64 9795 97.08 -202.49 -202.3 DF 11 38 58.44 119 41.83 4882 9800 89.64 9795 94.97 -201.75 -201.75 DF 12 38 58.43 119 41.47 4895 9800 89.61 9795 94.97 -200.46 -200.7 DF 13 38 58.42 119 41.05 4916 9800 89.62 9795 94.67 -200.00 -199.7 BH 4962 38 58.61 119 40.57 4962 9800 89.61 9795 93.81 -197.60 -197.2 DF 14 38 58.62 119 40.08 5005 9800 90.00 9795 93.81 -198.32 <	DF	5	38	58.56	119	43.69	477 9	9800	89.83	9796	02.29	-200,80	-200.54
DF 7 38 58.57 119 43.15 4805 9800 89.84 9796 00.22 -201.32 -201.1 DF 8 38 58.57 119 42.92 4820 9800 89.84 9795 99.14 -201.50 -201.3 DF 9 38 58.57 119 42.63 4832 9800 89.84 9795 97.65 -202.28 -202.3 DF 10 38 58.49 119 42.43 4836 9800 89.64 9795 97.08 -202.49 -202.3 DF 11 38 58.43 119 41.83 4882 9800 89.64 9795 95.72 -202.30 -202.7 DF 13 38 58.41 119 41.47 4895 9800 89.61 9795 94.96 -200.94 -200.7 DF 14 38 58.38 119 41.29 4904 9800 89.62 9795 94.67 -200.00 -199.7 DF 15 38 58.62 119 40.57 4962 9800 89.61 9795 94.67 -200.00 -199.7 BH 4962 38 58.62 119 40.33 4975 9800 89.91 9795 93.81 -197.60 -197.2 DF 16 38 58.62 119 40.08 5005 9800 90.00 9795 91.38 -198.32 <	DF	6	38	58.57	119	43.42	4790	9800	89.84	9796	01,49	-200.95	-200,76
DF 8 38 58.57 119 42.92 4820 9800 89.84 9795 99.14 -201.50 -201.3 DF 9 38 58.57 119 42.63 4832 9800 89.84 9795 97.65 -202.28 -202.23 DF 10 38 58.49 119 42.43 4836 9800 89.72 9795 97.08 -202.30 -202.13 DF 11 38 58.46 119 42.10 4861 9800 89.64 9795 94.97 -201.75 -201.5 DF 12 38 58.43 119 41.43 4882 9800 89.64 9795 94.97 -200.44 -200.7 DF 13 38 58.41 119 41.47 4895 9800 89.62 9795 94.66 -200.46 -200.2 DF 14 38 58.42 119 41.05 4916 9800 89.62 9795 94.67 -200.00 -197.7 DF 16 38 58.62 119 40.57 4962 9800 89.91 9795 91.38 -197.60 -197.2 DF 17 38 58.62 119 40.08 5005 9800 90.00 9795 91.38 -198.32 -197.9 DF 19 38 58.83 119 39.62 5031 9800 90.22 9795 90.67 -197.70	DF	7	38	58.57	119	43.15	4805	9800	89.84	9796	00.22	-201,32	-201.13
DF 9 38 58.57 119 42.63 4832 9800 89.84 9795 97.65 -202.28 -202.2 DF 10 38 58.49 119 42.43 4836 9800 89.72 9795 97.08 -202.49 -202.3 DF 11 38 58.46 119 42.10 4861 9800 89.68 9795 95.72 -202.30 -202.1 DF 12 38 58.43 119 41.83 4882 9800 89.64 9795 94.97 -201.75 -201.75 DF 13 38 58.41 119 41.47 4895 9800 89.61 9795 94.96 -200.94 -200.7 DF 14 38 58.38 119 41.29 4904 9800 89.62 9795 94.86 -200.06 -199.7 DF 15 38 58.62 119 40.57 4962 9800 89.83 9795 93.81 -197.60 -197.2 DF 16 38 58.62 119 40.33 4975 9800 89.01 9795 93.81 -198.32 -197.9 DF 17 38 58.83 119 39.83 5018 9800 90.11 9795 89.86 -199.05 -198.2 DF 19 38 58.83 119 39.41 5043 9800 90.36 9795 89.78 -198.00	DF	8	38	58.57	119	42.92	4820	9800	89.84	9795	99.14	-201.50	-201.30
DF 10 38 58.49 119 42.43 4836 9800 89.72 9795 97.08 -202.49 -202.3 DF 11 38 58.46 119 42.10 4861 9800 89.68 9795 95.72 -202.30 -202.1 DF 12 38 58.43 119 41.83 4882 9800 89.64 9795 94.97 -201.75 -201.5 DF 13 38 58.41 119 41.47 4895 9800 89.61 9795 94.97 -200.94 -200.7 DF 14 38 58.38 119 41.29 4904 9800 89.62 9795 94.67 -200.04 -200.2 DF 15 38 58.42 119 41.05 4916 9800 89.62 9795 94.67 -200.00 -199.7 BM 4962 38 58.62 119 40.57 4962 9800 89.81 9795 93.81 -197.60 -197.2 DF 16 38 58.62 119 40.08 5005 9800 90.00 9795 91.38 -198.32 -197.9 DF 17 38 58.62 119 40.08 5005 9800 90.22 9795 90.67 -197.70 -196.8 DF 19 38 58.75 119 39.41 5043 9800 90.36 9795 89.78 -198.00	DF	9	38	58.57	119	42.63	4832	9800	89.84	9795	97.65	-202.28	-202.28
DF 11 38 58.46 119 42.10 4861 9800 89.68 9795 95.72 -202.30 -202.1 DF 12 38 58.43 119 41.83 4882 9800 89.64 9795 94.97 -201.75 -201.5 DF 13 38 58.41 119 41.47 4895 9800 89.61 9795 94.96 -200.94 -200.7 DF 14 38 58.38 119 41.29 4904 9800 89.62 9795 94.86 -200.04 -200.2 DF 15 38 58.42 119 41.05 4916 9800 89.62 9795 94.17 -200.00 -199.7 BH 4962 38 58.62 119 40.57 4962 9800 89.83 9795 94.19 -197.91 -197.6 DF 16 38 58.62 119 40.33 4975 9800 89.91 9795 91.38 -198.32 -197.9 DF 17 38 58.62 119 40.08 5005 9800 90.00 9795 91.38 -198.32 -197.9 DF 18 38 58.75 119 39.83 5018 9800 90.22 9795 90.67 -197.70 -196.8 DF 20 38 58.92 119 39.41 5043 9800 90.50 9795 89.78 -198.00	DF	10	38	58.49	119	42,43	4836	9800	89.72	9795	97.08	-202.49	-202.32
DF 12 38 58.43 119 41.83 4882 9800 89.64 9795 94.97 -201.75 -201.5 DF 13 38 58.41 119 41.47 4895 9800 89.61 9795 94.96 -200.94 -200.7 DF 14 38 58.38 119 41.29 4904 9800 89.56 9795 94.86 -200.46 -200.2 DF 15 38 58.42 119 41.05 4916 9800 89.52 9795 94.67 -200.00 -199.7 BH 4962 38 58.56 119 40.57 4962 9800 89.83 9795 93.81 -197.60 -197.2 DF 16 38 58.62 119 40.33 4975 9800 89.91 9795 93.81 -197.60 -197.2 DF 17 38 58.62 119 40.08 5005 9800 90.00 9795 91.38 -198.32 -197.9 DF 18 38 58.75 119 39.83 5018 9800 90.22 9795 90.67 -197.70 -196.8 DF 20 38 58.92 119 39.41 5043 9800 90.36 9795 89.78 -198.00 -197.3 DF 21 38 58.93 119 39.24 5082 9800 90.50 9795 87.21 -198.38	DF	11	38	58.46	119	42.10	4861	9800	89.68	9795	95.72	-202.30	-202.15
DF 13 38 58.41 119 41.47 4895 9800 89.61 9795 94.96 -200.94 -200.7 DF 14 38 58.38 119 41.29 4904 9800 89.56 9795 94.86 -200.46 -200.2 DF 15 38 58.42 119 41.05 4916 9800 89.62 9795 94.67 -200.00 -199.7 BH 4962 38 58.62 119 40.57 4962 9800 89.83 9795 94.19 -197.91 -197.60 DF 16 38 58.62 119 40.03 4975 9800 89.00 9795 91.38 -198.32 -197.9 DF 17 38 58.62 119 40.08 5005 9800 90.00 9795 91.38 -198.32 -197.9 DF 18 38 58.75 119 39.83 5018 9800 90.11 9795 89.98 -199.05 -198.2 DF 19 38 58.92 119 39.41 5043 9800 90.36 9795 89.78 -198.00 -197.9 DF 21 38 59.02 119 39.24 5082 9800 90.50 9795 87.21 -198.38 -197.9 DF 22 38 58.93 119 39.24 5082 9800 90.37 9795 87.21 -198.80	DF	12	38	58.43	119	41.83	4882	9800	89.64	9795	94.97	-201.75	-201.59
DF 1438 58.38119 41.2949049800 89.569795 94.86-200.46-200.2DF 1538 58.42119 41.0549169800 89.629795 94.67-200.00-199.7BH 496238 58.56119 40.5749629800 89.839795 94.19-197.91-197.60DF 1638 58.62119 40.3349759800 89.919795 93.81-197.60-197.2DF 1738 58.62119 40.0850059800 90.009795 91.38-198.32-197.9DF 1838 58.75119 39.8350189800 90.229795 90.67-197.70-196.8DF 1938 58.83119 39.6250319800 90.369795 89.78-198.00-197.3DF 2038 58.92119 39.4150639800 90.369795 87.21-198.38-197.9DF 2138 58.93119 39.0851079800 90.379795 85.15-198.80-198.33DF 2338 58.98119 38.8351239800 90.559795 79.12-202.42-201.9DF 2438 59.05119 38.3352139800 90.649795 73.62-204.24-203.7DF 2538 59.11119 38.3352139800 90.689795 73.15-204.15-203.6DF 2638 59.14119 38.2552239800 90.689795 73.15-204.15-203.6	DF	13	38	58.41	119	41.47	4895	9800	89.61	9795	94.96	-200.94	-200.75
DF 1538 58.42119 41.0549169800 89.629795 94.67-200.00-199.7BH 496238 58.56119 40.5749629800 89.839795 94.19-197.91-197.6DF 1638 58.62119 40.3349759800 89.919795 93.81-197.60-197.2DF 1738 58.62119 40.0850059800 90.009795 91.38-198.32-197.9DF 1838 58.75119 39.8350189800 90.119795 89.98-199.05-198.2DF 1938 58.83119 39.6250319800 90.229795 90.67-197.70-196.8DF 2038 58.92119 39.4150439800 90.369795 89.78-198.00-197.3DF 2138 58.92119 39.2450829800 90.369795 85.15-198.80-198.33DF 2338 58.93119 39.0851079800 90.379795 81.42-201.65-201.2DF 2438 59.05119 38.8351239800 90.559795 79.12-202.42-201.9DF 2538 59.11119 38.3352139800 90.649795 73.62-204.24-203.7DF 2638 59.14119 38.2552239800 90.689795 73.15-204.15-203.6	DF	14	38	58.38	119	41.29	4904	9800	89.56	9795	94.86	-200.46	-200.27
BH 4962 38 58.56 119 40.57 4962 9800 89.83 9795 94.19 -197.91 -197.6 DF 16 38 58.62 119 40.33 4975 9800 89.91 9795 93.81 -197.60 -197.2 DF 17 38 58.62 119 40.08 5005 9800 90.00 9795 91.38 -198.32 -197.9 DF 18 38 58.75 119 39.83 5018 9800 90.11 9795 89.98 -199.05 -198.2 DF 19 38 58.83 119 39.62 5031 9800 90.22 9795 90.67 -197.70 -196.8 DF 20 38 58.92 119 39.41 5043 9800 90.50 9795 89.78 -198.00 -197.3 DF 21 38 59.02 119 39.24 5082 9800 90.50 9795 87.21 -198.38 -197.9 DF 22 38 58.93 119 39.08 5107 9800 90.37 9795 81.42 -201.65 -201.2 DF 23 38 58.93 119 38.83 5123 9800 90.55 9795 79.12 -202.42 -201.9 DF 24 38 59.11 119 38.33 5213 9800 90.64 9795 73.62 -204.24	bF	15	38	58.42	119	41.05	4916	9800	89.62	9 795	94.67	-200.00	-199.75
DF 16 38 58.62 119 40.33 4975 9800 89.91 9795 93.81 -197.60 -197.2 DF 17 38 58.62 119 40.08 5005 9800 90.00 9795 91.38 -198.32 -197.9 DF 18 38 58.75 119 39.83 5018 9800 90.11 9795 89.98 -199.05 -198.2 DF 19 38 58.83 119 39.62 5031 9800 90.22 9795 90.67 -197.70 -196.8 DF 20 38 58.92 119 39.41 5043 9800 90.36 9795 89.78 -198.00 -197.3 DF 21 38 58.92 119 39.44 5082 9800 90.37 9795 85.15 -198.80 -197.9 DF 22 38 58.93 119 39.08 5107 9800 90.37 9795 85.15 -198.80 -198.3 DF 23 38 59.05 119 38.83 5123 9800 90.55 9795 79.12 -202.42 -201.2 DF 24 38 59.05 119 38.33 5213 9800 90.64 9795 73.62 -204.24 -203.7 DF 25 38 59.14 119 38.25 5223 9800 90.68 9795 73.15 -204.15	BM	4962	38	58.56	119	40.57	4962	9800	89.83	9795	94.19	-197.91	~197.61
DF 17 38 58.62 119 40.08 5005 9800 90.00 9795 91.38 -198.32 -197.9 DF 18 38 58.75 119 39.83 5018 9800 90.11 9795 89.98 -199.05 -198.2 DF 19 38 58.83 119 39.62 5031 9800 90.22 9795 90.67 -197.70 -196.8 DF 20 38 58.92 119 39.41 5043 9800 90.36 9795 89.78 -198.00 -197.3 DF 21 38 59.02 119 39.24 5082 9800 90.37 9795 87.21 -198.38 -197.9 DF 22 38 58.93 119 39.08 5107 9800 90.37 9795 85.15 -198.80 -198.3 DF 23 38 58.98 119 38.63 5123 9800 90.55 9795 79.12 -201.65 -201.2 DF 24 38 59.05 119 38.59 5150 9800 90.55 9795 73.62 -204.24 -203.7 DF 25 38 59.11 119 38.25 5223 9800 90.68 9795 73.15 -204.15 -203.6	DF	16	38	58.62	119	40.33	4975	9800	89.91	9795	93.81	-197.60	-197.23
DF 18 38 58.75 119 39.83 5018 9800 90.11 9795 89.98 -199.05 -198.2 DF 19 38 58.83 119 39.62 5031 9800 90.22 9795 90.67 -197.70 -196.8 DF 20 38 58.92 119 39.41 5043 9800 90.36 9795 89.78 -198.00 -197.3 DF 21 38 59.02 119 39.24 5082 9800 90.50 9795 87.21 -198.38 -197.9 DF 22 38 58.93 119 39.08 5107 9800 90.37 9795 85.15 -198.80 -198.3 DF 23 38 58.98 119 38.83 5123 9800 90.55 9795 79.12 -201.65 -201.2 DF 24 38 59.05 119 38.59 5150 9800 90.55 9795 79.12 -202.42 -201.9 DF 25 38 59.11 119 38.33 5213 9800 90.64 9795 73.62 -204.24 -203.7 DF 26 38 59.14 119 38.25 5223 9800 90.68 9795 73.15 -204.15 -203.6	Đ₽	17	38	58.62	119	40.08	5005	9800	90.00	9795	91.38	-198.32	~197.95
DF 19 38 58.83 119 39.62 5031 9800 90.22 9795 90.67 -197.70 -196.8 DF 20 38 58.92 119 39.41 5043 9800 90.36 9795 89.78 -198.00 -197.3 DF 21 38 59.02 119 39.24 5082 9800 90.50 9795 87.21 -198.38 -197.9 DF 22 38 58.93 119 39.08 5107 9800 90.37 9795 85.15 -198.80 -198.33 DF 23 38 58.98 119 38.83 5123 9800 90.55 9795 79.12 -201.65 -201.2 DF 24 38 59.05 119 38.33 5213 9800 90.64 9795 73.62 -204.24 -203.7 DF 25 38 59.11 119 38.25 5223 9800 90.68 9795 73.15 -204.15 -203.6	DF	18	38	58.75	119	39.83	5018	9800	90.11	9795	89.98	-199.05	~198.22
DF 20 38 58.92 119 39.41 5043 9800 90.36 9795 89.78 -198.00 -197.3 DF 21 38 59.02 119 39.24 5082 9800 90.50 9795 87.21 -198.38 -197.9 DF 22 38 58.93 119 39.08 5107 9800 90.37 9795 85.15 -198.80 -198.3 DF 23 38 58.98 119 38.83 5123 9800 90.44 9795 81.42 -201.65 -201.2 DF 24 38 59.05 119 38.59 5150 9800 90.55 9795 79.12 -202.42 -201.9 DF 25 38 59.11 119 38.33 5213 9800 90.64 9795 73.62 -204.24 -203.7 DF 26 38 59.14 119 38.25 5223 9800 90.68 9795 73.15 -204.15 -203.6	DF	19	38	58.83	119	39.62	5031	9800	90.22	9795	90.67	-197.70	~196.82
DF 21 38 59.02 119 39.24 5082 9800 90.50 9795 87.21 -198.38 -197.9 DF 22 38 58.93 119 39.08 5107 9800 90.37 9795 85.15 -198.80 -198.3 DF 23 38 58.98 119 38.83 5123 9800 90.44 9795 81.42 -201.65 -201.2 DF 24 38 59.05 119 38.59 5150 9800 90.55 9795 79.12 -202.42 -201.9 DF 25 38 59.11 119 38.33 5213 9800 90.64 9795 73.62 -204.24 -203.7 DF 26 38 59.14 119 38.25 5223 9800 90.68 9795 73.15 -204.15 -203.6	DF	20	38	58.92	119	39.41	5043	9 800	90.36	9795	89.78	-198.00	-197.35
DF 22 38 58.93 119 39.08 5107 9800 90.37 9795 85.15 -198.80 -198.3 DF 23 38 58.98 119 38.83 5123 9800 90.44 9795 81.42 -201.65 -201.2 DF 24 38 59.05 119 38.59 5150 9800 90.55 9795 79.12 -202.42 -201.9 DF 25 38 59.11 119 38.33 5213 9800 90.64 9795 73.62 -204.24 -203.7 DF 26 38 59.14 119 38.25 5223 9800 90.68 9795 73.15 -204.15 -203.6	DF	21	38	59.02	119	39.24	5082	9800	90.50	9795	87.21	-198.38	~197.97
DF 23 38 58.98 119 38.83 5123 9800 90.44 9795 81.42 -201.65 -201.2 DF 24 38 59.05 119 38.59 5150 9800 90.55 9795 79.12 -202.42 -201.9 DF 25 38 59.11 119 38.33 5213 9800 90.64 9795 73.62 -204.24 -203.7 DF 26 38 59.14 119 38.25 5223 9800 90.68 9795 73.15 -204.15 -203.6	DF	22	38	58.93	119	39.08	5107	9800	90.37	9795	85.15	-198.80	-198.39
DF 24 38 59.05 119 38.59 5150 9800 90.55 9795 79.12 -202.42 -201.9 DF 25 38 59.11 119 38.33 5213 9800 90.64 9795 73.62 -204.24 -203.7 DF 26 38 59.14 119 38.25 5223 9800 90.68 9795 73.15 -204.15 -203.6	DF	23	38	58.98	119	38,83	5123	9800	90.44	9795	81.42	-201.65	-201.23
DF 25 38 59.11 119 38.33 5213 9800 90.64 9795 73.62 -204.24 -203.7 DF 26 38 59.14 119 38.25 5223 9800 90.68 9795 73.15 -204.15 -203.6	DF	24	38	59.05	119	38,59	5150	9800	90.55	9 795	7 9 .12	-202.42	-201.98
DF 26 38 59.14 119 38.25 5223 9800 90.68 9795 73.15 -204.15 -203.6	DF	25	38	59.11	119	38,33	5213	9800	90.64	9795	73.62	-204.24	-203.75
	DF	26	38	59.14	119	38.25	5223	9800	90.68	9795	73.15	-204.15	-203.66

II 21

DF 27	38 59,27	119 38.04	5248	9800 90.87	9795 69.93	-206.06	-205.58
DF 28	38 59.27	119 37.82	5290	9800 90.97	9795 66.75	-206.82	-206.31
DF 29	38 59,32	119 37.52	5390	9800 90.94	9795 60.26	-207.28	-206.70

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Appendix III

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Daily on-site drilling logs of CC-1, CC-2, BSD-1, BSS, BSD-2

13 Feb 80

Carson City, NV

School Site Well CC #1

Longyear Co., Drilling Contractor-Sedilia, CO Crew:

NBMG Personnel J. Bruce, D. Trexler, T. Flynn

Comment: Longyear crew arrived in Carson City on 12 Feb and set up rig at approximately 1630 hrs.

13 Feb

0700 Longyear crew arrives (0800 CO time) Set up and used tricone bit to set 22 ft of hole for surface casing.

0801 J. Bruce arrives site

0805 T. Flynn arrives.

- 0810 J. Bruce, T. Flynn discuss project with Gil Speaker, Longyear Tool pusher.
- 0815 Drill crew putting on hammer

0835 Trexler arrives on site with equipment

0845 First sample taken at 20 ft with hammer

- 0850 Start drilling with hammer
- 0900 Pause in drilling to install temporary probe
- 0905 Start drilling again. Move Carryall to front of rig for equipment set up. Return air temperature 10.0°C @ 25 ft. Sample taken.
- 0910 30 ft depth sample taken. Return Temperature.
- 1000 Drilling slows down a bit. Been taking samples at 5 ft intervals. Up to the 90 ft interval now.
- 1010 Temperature probe is buried in chips
- 1015 Depth 100' dry
- 1030 TD 110 still dry trouble with chips not coming out of the hole water truck not here yet.

1034 112' chips moist

1040 Well starts to make water

III-2

13 Feb 80

Carson City, NV

School Site Well CC #1

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NBMG Personnel J. Bruce, D. Trexler, T. Flynn

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- 1010 Temperature probe is buried in chips
- 1015 Depth 100' dry
- 1030 TD 110 still dry trouble with chips not coming out of the hole water truck not here yet.

1034 112' chips moist

1040 Well starts to make water

1535 Tripping out of hole

1545 Rod binding in trip out during last two joints

1555 Rods out of hole

1600 Discussed with Gil Speaker what time backhoe will arrive for work. Approximately 9:00 AM.

1615 Secure site and depart for office.

Day #2	14 Feb 80
0800	Bruce arrives at site. H.P. & Greg (Longyear) already on site propping rig for drilling. Greg brings in full load of water. John (H.P.) mentions he heard press release on morning TV news, story associated with public hearings in Sparks today.
0805	Trexler arrives
0815	Flynn arrives - backhoe should arrive approximately 9 AM this morning to dig sump.
0845	Rig prepped and ready to drill, waiting for backhoe. Check hole visually - no water visible, but appears to be bridge at about 40 ft.
0930	Move water truck to off load drill pipe. Truck stuck in mud, still no backhoe.
1000	Trexler and Flynn go into town for errands. Move water truck out of mud and place off tail end of rig.
1005	Begin transferring rod off truck.
1010	Truck getting stuck in mud again, stopped offloading rod.
1030	Backhoe arrives.
1045	Unloading backhoe down by 5th St. construction.
1130	Trexler to Reno
1200	Backhoe working on water pit - drill stem is being lowered into hole.
1215	One rod apparently plugged as no air return coming up annulus. Changed rod.
1224	HH water at approximately 130-135 ft. Blowing water with each joint now.
1230	Sump almost complete. Blowing lots of water, depth 160 ft.
1235	Reach TD begin drilling. Koenig arrives.
1255	180 ft sample taken some chips - soft - chlorite rich? Gray-Green.
	FB= 1.4 C=32.5
1308	185 ft sample taken. Soft green material as vein filling in grey green fine to medium grain metavolcanic.
1330	Drilling with heavy foam reached 200 ft level. Sample taken.

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III-5

1415 Continued use of heavy foam.

C=38.7 FB= 4.5 T=17.5

- 1430 Reached 220 ft interval still drilling with foam. Aids the chip lift.
- 1445 New stem. Heavy foam.

C=43.8 FB= 5.8 T=16.5

- 1500 Sample taken at 225. Shows two rock types. Formation providing lots of water. Heavy foam still being used. Gary Ferguson shows up at site (Longyear, Denver).
- 1520 Still much water in formation heavy foam. Reached 230' level.
- 1530 Sample taken at 235' level. Same stuff John Woods suggests may have to use tri-come bit to get water and chips out of hole.

C=43.8 T=16.8 FB= 4.2 EP=16.8 Envirolab probe in sump.

- 1545 Sample taken at 240' interval. Mixed bag formation still producing mucho water - sump pit filled to top with foam about 1/2 way with water.
- 1600 FB= 6.8 C=44.2 T=16.2
- 1615 Reach 250' level. Sample taken. Same stuff still lots of water.
- 1625 FB= 7.9 C=44.2 T=17.3
- 1635 Sample at 255'. Same materials very small amount of sample.
- 1650 Sample at 260'. Same rock types plus what appears to be a piece of quartz from a vein.

FB= 7.2°C C=40.2°C T=16.9°C EP=17.2°C

- 1705 Sample taken at 265'. Similar materials to inverval above.
- 1712 EP probe 17.1°C (downstream in return flow).

1720	Sample taken at 270'. Same materials but smaller fraction of
	friable rock.
1730	EP - 16.6°C
1750	Sample taken at 275'. Same materials
1755	EP=17.2
	FB- 8.2
	(#44.3 T=12.0 (in cim)
	1-13.9 (III AIF)
1803	Reached 280' level.
	EP=17.0
1820	Begin to close down shift.
	FB= 9
	T=18
	C=45
1830	Begin to secure rig for shift end.

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III-7

15	Feb	80
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Day 3 0725 Trexler arrives at site. No crew, water level 15 in. below top of Berm. 0740 Flynn arrives at side. No crew. Set up temperature probes, water bucket. 0800 Crew arrives; Ken, John, Craig. 0810 Ken begins backhoe work to expand sump. Crew readles rig for drilling. 0830 Foam barrel (FB)=10°C Truck (T)=11°C (C)=20°C Collar 0835 Set up Envirolab probe in return water chanel. No temperature recorded. 0930 Drill stem stuck in hole - due to caving. 0955 Gary Ferguson arrives at site. 1015 Drill stem still stuck in hole. John goes for fuel. Gary Ferguson says it looks grim! 1050 Ken shuts down rig for fuel filter replacement. 1055 Ken starts up rig agin. 1130 Craig goes for more water. Rig still stuck. Moved up about 18". Gary digging supplemental sump. 1255 1305 Craig back with water truck. Jim Bruce arrives - still stuck in hole. Trexler back to Reno. 1330 1430 Forest King shows up for a 10 minute chat. Very happy we are drilling here. John Hancock shows up to see what is happening. Still stuck. 1445 Shut down rig to let hydraulic cool down - getting too hot to be 1500 effective. 1550 Ken Taylor, 2460 Pinyon Hills, C.C., stopped by to check on well condition. He just had well drilled by Forest King. Having problems with Forest King. Tom Flynn going over to temperature log Mr. Taylor's well. Start rig up again to try to free string. Still Stuck. Rotation 1605 a little less now. 1610 George Ghusn arrives.

III-8

- 1620 Ken (driller) starts enlarging sump.
- 1640 Ken takes over on rig trying to free string.
- 1715 Flynn returns from Pinyon Hills. Probe cable gets tangled. He will try again tomorrow.
- 1740 Ferguson arrives with casing 30' lengths. Rig capabilities can handle 24' length.
- 1815 Rods unstuck and pulled up 3'. Still binding, but looks good.
- 1835 Rods still binding and stuck but about 8' out of hole now.
- 1845 Ghusn leaves site.

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- 1900 First joint free, ready to disconnect. Need one more foot to disconnect, still binding about 19' off bottom.
- 1908 First joint free, but crocked.
- 1916 First joint in rod rack.
- 1955 32' off bottom and still stuck, but gradually coming out.
- 2002 Second joint out of hole.
- 2005 Third joint out of hole. Joint really tight, doesn't want to break.
- 2008 Third joint out; fourth joint out but tight. Appears that hole is free. Binding part appears to be about 40' off bottom.
- 2010 Joints coming out good now, but highly torqued up.
- 2040 Out of hole, but hammer twisted off probably at bottom of casing. Hammer wedged about 50' down.
- 2100 Secure site.

16 Feb 80

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- 0900 Bruce arrives, crew just beginning to run down rods trying to fish out rod which is about 30' off bottom; wash out hole as they go down to try to clean around tool.
- 0945 Tom and Pat arrive.
- 0955 Tom and Pat depart to measure Ken Taylor's well.
- 1005 Gary Ferguson arrives. About 18' off bottom.
- 1015 Tripping out of hole to switch over to mud parts for mud drilling. Should be at airport around noon.

Del Landing, President of Carson City School Board drops by. Asked how operation was going. He is familiar with drilling as he owns a portion of an oil and gas rig. Day #5

0800	Bruce ar	rives a	it site,	crew p	repping rig	for	ope	ratio	1, no	work	: on
	17 Feb.	Tool s	till in	hole,	converting	rig	to	d rill	with	mud	and
	try to r	etrieve	tool.								

- 0815 Greg arrives with water truck.
- 0830 Gary Ferguson arrives with parts for mud drilling.
- '0945 Put tricome bit on to clean out hole, and running in to clean out hole with mud to fish out hammer.
- 0950 Adding LCM (cottonseed) directly down the hole, loosing circ, added about 1/2 bag.
- 1000 Mixing more mud. Have used all mud in mud pit 12'x6'x4' deep, adding 5 bags bentonite.
- 1015 Hipres. pop-off valve on compressor keeps blowing off.
- 1045 Replace gasket on regulator.
- 1110 Running string into hole and washing out.
- 1115 2nd joint added. 25' returns gained. LCM seems to be working.
- 1130 Mud pump intake clogs, have to clean.
- 1135 3rd joint added.
- 1145 4th joint added.
- 1155 Sth joint added.
- 1202 6th joint added, 120'.
- 1209 8th joint added, 160'

1215 9th joint added.

1240 11th joint added. Shutting down due to weather.

Day 6	19 Feb 80
0900	Flynn arrives. Drilling with mud approximately 2 in over the bit which is at the 280' interval (\pm 2'). The drillers plan to wash out the hole over the bit and will attempt to recover it with a custom-made friction socket. This will be further described when it is fabricated. Ken, John and Craig have been at site since 0800.
0915	Jim Bruce arrives.
0920	Gary Ferguson arrives with casing for friction socket.
0945	Drillers start tripping stem to begin fishing operation. Carryall get stuck in mud behind rig.
1015	We get carryall unstuck.
1040	Tricone bit is being removed from stem, replaced with hammer sub.
1045	Drillers are attempting to spear bit with sub.
1120	Final drill stem is being lowered into hole. Getting ready to spear bit.
1125	On top of hammer, working rod up and down on hammer.
1128	Appear to have snagged hammer, slowly rotating trying to screw into hammer.
1130	Both Ken and John feel its been snagged. Begin pulling out of hole. Rod binding at about 4' off bottom, same spot as when we were stuck. John feels that this is where the tool came off before.
1140	About 6' of bottom coming up very slowly, still some binding.
1225	Running back in hole with tricone bit.
1300	On bottom and ready to drill.
1305	Drilling. Install temperature probes; one at intake end of mud pit; one at return end of mud pit, and one in casing still.
1318	290'. No sample.
1340	300'. Sample taken. John into town for diesel. Raining cats and dogs plus wet snow. Mud samples have very fine cuttings and a lot of cottonseed shells. Drilling rate pretty good.
1350	305' sample.
	Cr 19.5 returns Mp 11.4 mud pit Cc 19.0 collar
	Raining and cold winds from southwest.
	III-11

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- 1405 Drilling proceeding quite well. Still using mud. Chips too fine to identify in field. Weather continues to be bad. Down to 315' interval.
 - Mp 13.0 Cr 19.8 Cl 21.8
- 1430 Drilling at 325' mark.
 - Cr 21.8 Cc 21.8 Mp 11.6

Unable to make field description due to fineness of cuttings and cottonseed content.

1450 Down to 335' interval. No recovery at 330'.

- 1500 Cr 21.8 Mp 12.3
- 1505 Collected sample at 340' level. Still impossible tosee any chips for identification. They are very small, black, and obscured by both mud and cottonseed. The weather continues to be very cold, windy, and very rainy. Drilling continues at a good pace with mud.
- 1520 Samples recovered at 345' are black-fine-medium grained metavolcanics. Some felsic material present. Slight break in weather. Still windy and cold.
- 1530 Mp 11.2 Cr 23.1 Temperature of return beginning to rise at 350' level. Cc 21.9
- 1550 Sample recovered at 355' interval. Looks like same stuff still very fine grained - using sump pond to remove mud and cottonseeds. Clouds are breaking up overhead, but some rain is still falling from clouds to southwest. Rig continues to drill with mud, but more slowly now.
- 1600Cr 24.2Mp 11.0Return mud continues to increase in temperature.Cc 22.2Drilling is slow about 357' mark.
- 1630 Sample at 360' mark. Forest King shows up.
- 1645 Cr 24.1 Mp 11.6 At 365' mark sample taken. Forest King gone. Cc 22.4
- 1700 Sample taken at 370' level same stuff. The weather had held off, rain wise, until now. Rainy again, but looks like it might stop soon. Drilling continues with some hard spots.
1705 Sample taken at 375' level same stuff.

Sample taken at 380' same stuff. Gary Ferguson leaves site. 1715 Cr 24.0 Mp 12 In stream flow - not in mud pit. Ce 22.8

Temperatures seem to be holding steady.

Sample collected at 385' level. Looks like same stuff - possibly 1730 more andesitic but hard to tell with all the mud.

1745 Sample taken at 390' level.

> Cr 23.3 Mp 12.5 Things have cooled a bit. Cc 23.1 Sample taken at 395' mark same stuff.

Sample at 400' - begin to wash out to trip stem. 1800

Cr 28.0 and falling Mp 12.7 Cc 22.5

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All 400' of stem tripped out of hole. Tricone looks good - Rig down. 1845

20 Feb 80

Day 7 Flynn arrives at site, Ken, John and Craig are putting drill stem 0815 into hole. Weather is clear and cold 0820 Temperature probes set up at Collar Cc Mud Pit Mp No temperatures taken yet. Mud Return Cr Forest King was here for 10 minutes. Told Flynn about some geothermal projects he has going with P. Langston at Carson Hot Springs and a possible project at Wabuska. He now has a portable unit to measure AT at known flow rates in a hot well bore. John says a gentleman reporter from the Appeal was here - asked if anything positive had been found - Ken told him about the 72°F mud returns - John told him to come back later to chat with Flynn. 0900 All 400' of stem in hole, drilling begins. Cr 25.1 9.3 Mp Cc 21.5 Samples at 405' and 410' - same black stuff. 0915 0930 Small sample taken at 415'. Flynn asked Ken to move bucket closer to the hole in order to catch a larger sample. Drilling goes well. Cr 22.9 Mp 12.0 Cc 22.1 0935 Good sample taken at 420' . Chips are coarser and rock looks like a medium-fine grained basic rock - no visible alteration many chips mud stained. 0945 Sample taken at 425' level. Looks like the same stuff. Weather getting bad - snow and wind. Sample taken at 435' level - same stuff. 0955 Cr 25.8 Mp 17.7 Cc 22.3 1010 Sample taken at 440'. Looks the same - black-white grains in this bag. Medium-fine grained-muddy. Weather has cleared. Drilling smooth. Took some photos of mud drilling and catch bucket - also of Ken and John.

- 1023 Sample taken at 445' level. Some grains show medium-grained black-white (salt/pepper) mineralogy. Drilling still smooth, weather OK
 - Cr 27.2 Mp 18.8 Cc 24.7
- 1035 Sample taken at 450' level. Sample resembles grabs black-white medium grained. Difficult to see any alteration. Drilling still smooth, weather holding.
- 1045 Sample taken at 455' level. Sample continues as fine-medium grained black-white rock. Gary Ferguson arrives at site. Weather holding. Drilling smooth.
- 1100 Gary Ferguson says mud flow rate is 250 GPM. Drilling looks like is tougher now.

Cr 26.3 Mp 19.2 Cc 24.2

- 1105 Sample taken at 460' level. Rock looks the same. Fine-medium grained black and white minerals - Gary says that hole will be chemically cleaned with LFN-OX (lignite). We plan to perforate 10' intervals to the water table, leave the top 6" casing and cement to 20' level.
- 1130 Sample taken at 465' level. No lithologic change. Gary backs up casing truck to drill rig. Temperature holding steady. Drop here - steady.

Cr 26.3 Mp 15.8 Cc 24.5

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- 1145 Sample taken at 470' level. Lithology unchanged
- 1200 Sample taken at 475'. Lithology unchanged.
- 1215 Crew preparing casing for hole. Fitting couplings on tubes.

Cr 26.8 Mp 17.5 Cc 24.6

1220 Sample recovered at 480' level. Lithology unchanged; crew still working on casing cooling. Weather is blowy and colder.

III-15

Sample taken at 485' level. Lithology unchanged. Crew still 1240 working on casing couplings. Cr 26.6 Mp 15.0 Cc 25.1 1250 Sample taken at 490' level. Lithology unchanged. One more 15' drill stem to go. Crew continues to work on casing. 1300 Last 15' section of drill stem now being rigged in. 1305 Drilling continues smoothly on last drill stem. Cr 27.5 Mp 19.4 Cc 25.5 Sample collected at 495' level. Lithology unchanged. Gary starts 1320 work on perforating casing at 10' intervals. Ken says they will trip the stem when hole is completed, change to a slightly smaller bit, go back and flush hole. 1330 Jim Bruce arrives at site. Cr 28.3 Mp 19.2 Cc 25.5 Gary will cut slots from 320'-500'. 1350 Reach 500' level. Sample taken. Lithology unchanged. Cr 32.0 Mp 20.8 Cc 25.5 Based on jump in temperature, Jim told drillers to go another 5'. 1400 Tom runs into town, to bank and for coffee. 1415 Reach 505'. Use as T.D. Cr 33.0 Mp 20.6 Cc 25.5 Prepping for tripping out of hole, then will run in and clean hole 1415 out with Barfos (cleans out mud by breaking it down). Circulating to clean out hole. 1425 Still circulating about 1' off bottom. Cr 32.8 Mp 20.6 Cc 25.6

III-16

- 1430 Beginning to trip out of hole.
- 1515 Flynn returns. Gary and Bruce talk about casing hole. Gary wants to shut down after tripping out and Barfos the hole tomorrow, because otherwise the crew would probably not finish casing the hole until late tonight.
- 1535 Out of hole with string.

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1600 Rig down and secure site.

21 Feb 80 '

Day	8
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- 0930 Bruce and Flynn arrive at site. 6 inches of snow on ground and still falling. We pulled two cars out of ditch in Washoe Valley. Crew here since about 0800 includes Gary, Ken, John, Craig. All 500' of drill stem in hole. Draining mud pit into water sump in preparation for chemically washing the hole. Saw short article and photo in Nevada Appeal about our drilling. KOLO ran the TV interview last night.
- 1000 Circulating with Barfos.
- 1020 Mud out of hole only Barfos returns. Now getting ready to trip out.
- 1030 Cleaning temperature probe and other equipment in truck. Tripping out. Bruce and Gary go to check other site.
- 1150 Bruce and Gary return, second site inaccessible due to over 12" of snow. Will probably have to get a blade to clear road.
- 1150 Out of hole and breaking bit off rods, and stacking rods on truck. Getting ready to run casing.
- 1200 Running casing into hole, 189' of slotted casing will be put in hole first.
- 1255 Tenth joint of casing in the hole, all 9 joints which are slotted are in the hole.
- 1330 Dick Wiliford showed up and asked to see the driller's license. Nobody has a driller's license and the operation is shut down until we can get a licensed driller on site.

22 Feb	80
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- 1210 Crew arrives.
- 1215 Casing setting begins
- 1257 Last segment of casing bottoms in hole. Ten 23' sections with couplings were used to complete the hole.

Carson City, NV Community College Site Well - CC#2 Longyear Co., Drilling Contractor, Sedalia CO. Crew - Ken Dfaart John Woods Greg ? Darrel Nfkuda NBMG Personnel - T. Flynn B. Koenig J. Bruce D. Trexler G. Ghsun CC#2 22 Feb 80 1500 Begin to grade road for rig. 1600 Set up rig at site. 1630 Bruce leaves. 1720 No drilling yet. Koenig and Flynn check out. 1830 Start drilling. 1930 Shut down drilling at 95'. Some caving, most material is decomposed granite. 2000 Rig down. Day 2 23 Feb 80 0830 Flynn and Bruce arrive. No drillers yet; at CC#1 picking up vehicles. 0900 John and Ken arrive, Greg sick, bring backhoe with them. 0910 John and Ken return to CC#1 to pick up casing truck. 0940 George Ghusn arrives. Bruce and Flynn setting up temperature probes. 0950 John and Ken return with casing truck, waiting on Gary Ferguson who is picking up 7" casing to case hole as DG wants to cave. Trexler arrives. Drillers reached 95' level last night and quit. 1015 Need more casing. Lithology is D.G. all the way down. Some large cobbles in some samples. No water yet. 1045 Gary and Darrel arrive with casing, buttress joint casing, so we will have to weld joints. 1050 Start up rig. Ready to run casing. 1100 Running first joint casing. III-20

- 1105 Welding first joint casing.
- 1115 Two joints in the hole.

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- 1125 Third joint in the hole.
- 1145 Fifth (last) joint casing in the hole, 97' (2' exposed. Will try to clean out hole bottom with tricone and are going to let casing settle the exposed 2'.
- 1150 Getting ready to clean out hole.
- 1155 Running rods into hole, new tricone bit on, will work out hole with air till water volume increases.
- 1210 Depth 100'. Running sixth rod in hole. Drilling rat 1'/25 sec. = 25'/minute. Material appears to be G.D.
- 1213 Cutting window into casing. Refueling.
- 1219 Dennis and Tom set up temperature sensor. Drilling underway again.
 - 1223 -105 sample taken (ST) Barrel Temperature (B) 12.5°C Return Temperature (R) 21.0°C
 - 1225 110 ST
 - 1226 115 ST
- 1227 Fitting 7th rod in hole. ST At 120'

1234 ST - 125'

- 1236 ST 130'
- 1238 ST 135'
- 1240 ST 140' 7th rod
- 1245 Reach water table, or water seam at 140', water volume decreased below 140'. ST - 145'
- 1246 ST 150'
- 1247 ST 155' Lith - D.G.
- 1250 ST 160' Lith - D.G. 8th rod down hole

1255	ST - 165' Lith - D.G.
1257	ST - 770 [†] Good OL D.G.
1300	B=5.5°C R=12.0°C Depth 175' Sample taken same D.G 180'.
1302	Hit something hard at almost -180'.
1306	ST - 180' Lith D.G. + chips of bedrock or boulder. 9th rod down hole
1311	ST - 185'
1313	ST - 190'
1315	ST - 195'
1318	ST - 200' 10th rod down hole
1321	11th rod being installed.
1322	B=5.3°C R=16.2°C Very little fluid coming up. Depth 205'.
1324	ST - 205' Lith - D.G.
1333	ST - 210'
1335	ST - 215' Lith - some aplite, in D.G.
1337	ST - 220' 11th rod down hole
1347	Drilling resumed.
1350	ST - 225'
1352	ST - 230'
1354	ST - 235' R=17.3°C at 235' B=5.8°C
1355	ST at 240' - last one. Begin to flush hole. Some epidote in aplite dikes.
1408	Drillers tripping out.
1425	Last drill stem tripped out of hole.

III-22

Casing truck has been moved into position for unloading. Crew begins to case the hole. Bottom casing is plugged. No casing will be perforated. George goes to CC-1 to change locks.

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Preliminary Temperature Profile at CC-1

- 1000 Arrive at site nobody around. Hole has not been cemented. 2'x2' space dug out around casing. 3'-4' - Begin to set up Envirolab cable.
- 1010 Cable in place probe at 100' level. Allowing 3-5 minutes for equilibration.

1025 Drill crew arrives to cement hole. Break down probe.

1045 Out of hole. Cementing begins.

DEPTH	TEMP	TIME
100'	15.6	1015
150'	15.9	1020
300*	17.8	1030
400'	19.1	1033
459'	19.6	1036

25 Feb 80

29 Mar 80

Big Smoky Valley Drilling Project

Darrough's Site - Hole BSD

NBMG Personnel: J. Bruce, B. Koenig, G. Ghusn

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Con	ments:	Begin drilling 1: pm. Hole begun in alluvial material, no water, air only. Sample 1 10' 0.5 cm frags appear to be Darrough Felsite in fine grained (0.5-1 mm) matrix Hole blown @ \approx 12', cobbles of grey chert and Darrough Felsite (DF)
		came to surface. Drilling stopped @ 1:45 pm hole caving - depth before caving 215' 3:07 pm drilling restarted using foam-water-mud-thickener.
090	00	Meet drill crew @ site, begin search for H20 for drill rig.
10	00	Wine Glass Ranch will allow water to be taken from their pond (owner - Carl Hass (sp?)).
11	15	Water truck @ rig, start up rig to warm up. Putting new 7 7/8" tri-come bit, #201.
11	34	Begin drilling.
11	57	1st 20' regular rod mounted, drilling continues.
12	03	20' sample taken, many rock types of varicolored cherts, colors vary from black to reddish purple.
12	35	50' sample, samples have been collected @ 5' intervals, mostly coarse-med coarse alluvium. Rough going at 50'.
1.2	40	Losing circulation @ 50'. Return temp 15°C.
12	43	Circulation regained.
12	50	New 20' section added.
13	03	60' sample taken, losing circulation, chips now average 0.2 cm size
13	04	55' lost circulation.
13	25	65' sample still small chip size.
		No sample between 65'-75'
		30 Mar 80
13	40	New 20' rod added, circulation lost @ 75'.
13	58	Newly added rod pulled, foam in compressor, attempting to regain circulation.

III-25

Darrough's Site - BSD

30 Mar 80 cont.

1413 Second 20' rod removed.

1427 3rd rod removed.

1433 4th removed (a string being pulled to inspect the bit).

- 1448 String being reinserted, groundwater in hole @=55' (former zone of lost circulation).
- 1543 Circulation established to 75^t, string being removed for placement of surface casing.
- 1615 String out.

1700 Casing movement blocked @ 50', operations suspended for this day.

31 Mar 80

- 0800 Arrive on site, surface casing in to a depth of "50", stopped by an obstruction.
- 0830 Water being circulated to clear the hole.
- 0850 Casing cut and drilling within casing with smaller bit begun.
- 0935 String being pulled, one joint pulled.
- 1000 Tilt mast to slide cut casing back over the string.
- 1010 Rewelding casing together, now have 61 ft of casing string.
- 1025 Driving casing & blowing out annulus. Casing down to about 53 ft. Blowing approximately 40 gpm of water from the formation.
- 1040 Driving casing by blowing cuttings out below casing and then forcing casing down with rod tong on top of casing. Casing depth 54.5 ft.
- 1120 Cut a notch in the casing to act as a blooey line and are cleaning out the hole and driving the casing with the power head, best method to date.
- 1200 Casing beginning to drive better because added an 18" sub to the string, thus cleaning the hole at a greater distance ahead of the casing.
- 1245 Casing down to 58 ft driving casing seems to be going much easier.
- 1255 New rod on switched to foam.
- 1305 Sample taken @ "75'.
- 1312 Sample taken @ "80".
- 1330 Change from 20 ft joint and replaced with a 15' joint so bit is not as far ahead of the casing. Added a 10 ft section of casing.

Darrough's Site - BSD

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31 Mar 80 cont.

- 1350 Welding casing together, total casing string 71 ft. Approximately 58 ft in the hole.
- 1405 Begin driving casing again, by 1410 have driven 2 ft more.
- 1530 70 ft of casing in the hole, changing the 15 ft joint and replacing with a 20 ft joint. Adding 7' more to the casing string (total casing string 78') will try to drive 5 more feet of at casing.
- 1550 Begin driving casing again.
- 1610 Surface casing set to 759 blowing hole using air.
- 1635 New 20' section being added, hole @ = 80'.
- 1640 Foam added, drilling continuing.
- 1720 100' depth achieved. 100' sample may not be representative material averages 1-2 mm, no large chips.
- 1740 Rig shut down for the day, hole sluffed about last 5 feet.

1 Apr 80

0750 Arrive at site.

0800 Rigging up for mud drilling to prevent hole collapse.

- 0854 New tri-cone bit installed
 - 0930 Hook up mud pump and begin to mix mud. Valve on mud pump is leaking. So shut down & begin repair of valve.
 - 1050 Hole being filled with mud.
 - 1115 ²400 gal of mud pumped but no returns.
- 1121 Switching to air to unplug hole plus mud being mixed in water truck.

1250 Start drilling with air-mud mix @ 105'. Temp is 10.2C. Sample taken @ 105' - rock frags contain a previously unseen rock which appears to be a poorly sorted subangular white sedimentary rock (a quartzite) and possibly contains feldspar frags.

1255 110' sample taken, same materials.

- 1300 115' sample taken, same materials.
- 1305 120' sample taken, same rock types. Size of frags avgs. 0.3 cm (smaller than previous 5 samples (2).

1310 New 20' rod added.

Darrough's Site - BSD

1 Apr 80 cont.

1310 Return $T = 12.4^{\circ}C.$ 125' sample same rock types, fine to pebble size chips, return 1320 13.1°C. 1330 130' same rock types (bit sticking) mostly fine frags 3 mm, returns 13.6°C. 1333 135' same rock types, size 2 mm - pebble. Return $T = 14.1^{\circ}C$. 1337 1344 140', return T = 14.5°C, drilling markedly slower, possibly a boulder. 1352 140! sample same rock type, larger frags made up of altered DF. 1418 Still drilling hard material @ 140'. New 20' rod being added. 1425 Foam added to prevent collapse. 1450 1455 145' sample taken, 1 frag of possible opaline sinter otherwise same rock types. 1510 150' sample, no sinter like frags present, return T = 14.3°C. 155' sample generally same rocks but some ball like clay material 1520 present. 1526 Return $T = 14.2^{\circ}C.$ 1530 160' sample, same material including ball clay which is iron stained. String broken new 20' rod being added. 1538 165' sample, same materials, more clay balls plus vf grained thinly 1547 bedded sandstone or quartzite fragment. 1603 170' sample - limited amount of sample - heavy foam being used ball like clay absent. 175', return T = 16.2°C. Sample taken similar materials, no clay, 1620 possible opaline frag. 180' sample taken some materials, limited amount of sample, frags 1630 largely <3 mm. New 20' section of drill rod being added. return $T = 18^{\circ}C.$ 185' sample, same materials, tuff, quartzite, chert, DF, large frags 1642 avg. 1-2 cm plus 1 clay ball.

3 Apr 80

Big Smoky Valley Drilling Project

Holes BSD#1 & BSS#1

- 0830 Arrive at BSD #1.
- 0900 Begin breakdown of rig at BSD #1.
- 1030 Rig down and on the road to Spencer's site (BSS #1).
- 1100 Bruce departs to locate rig at BSS #1.
- 1150 Bruce meets rig at BSS #1, while Koenig & Ghusn help restore BSD #1 to an acceptable environment.
- 1215 Frenchie arrives at Frontier to set up his trailer.
- 1330 Frenchie and Bruce begin set up of rig at BSS #1.
- 1350 Rig up and Pinkie arrives, send Pinkie to get water at Spencer's (55 gals).
- 1440 Pinkie returns, start drilling.
- 1430 Down to 25 feet some caving on the hole.
- 1450 Adding second 20' joint, total string length now 58', depth 30', return T, 17.7°C.
- 1455 @ 50 ft formation a littler harder, 500 lbs wt. on bit.
- 1515 55 ft, return T, 19.8°, still a stiff formation.

BSS #1

- 1520 String binding @ about 50-55'.
- 1540 Depth 65', hole is sluffing in due to big annulus and lack of good air flow, only minor problem. Can get lift by adding foam, but not very well. Will try to drill to about 85' and set casing (6"). Return T, 16.9°C, very little air return.
- 1600 Will case hole at 78' depth and try to drive any excess casing down, current depth 75 ft.
- 1610 78' depth, tripping out to set casing. Hole staying open now, occassional sluff.
- 1730 Last joint of casing being run down.

7 Apr 80

Big Smoky Valley Drilling Project

Hole BSD 2 (280' north of BSD)

NBMG Personnel: Trexler, Koenig

- 1430 Arrive on site.
- 1530 Rig erected and leveled.
- 1613 Backhoe arrives to dig mud pit.
- 1718 Mud pit complete shutdown for day.

8 Apr 80

- 0800 Arrive on site.
- 0810 Mud being mixed in pit.
- 0850 Drilling begins with centralizer and large tri-cone.
- 0909 Hole drilled to 15' new 20' rod added above stabilizer. (Samples have been taken @ 5, 10, and 15 feet).

0930 String being pulled to set casing (6") to 22.5 feet.

Sample log

5' Chip size varies from 1 mm-2 cm. Rock types include gray and gray-green and tan chert, various phases of the Darrough Felsite (DF), black groundmass with white plag phenocrysts, reddish-purple groundmass with white plag phenos and quartz. Also present is a very fine grained green (light) rock with small frags which may be plag and contains disseminated spots of iron staining - possible green mineral this rock may be a phase of the DF or an altered phase of it, also present is a fine grained whitish rock which appears to contain quartz, feldspar, and ferromags which are being altered to goethite - may be intrusive or extrusive.

10' Chip size 1 mm-0.5 cm, same rock types, perhaps a somewhat greater proportion of chert materials.

15' Chip size 2 mm-5 mm, same rock types, some DF frags showing epidote alteration - plus what appears to be a micro breccia or pyroclastic rock with a feldspathic matrix/groundmass with angular quartz, feldspar, and rock chips? Rock has a light greenish white overall hue, some reddish purple chert.

20' Chip size 0.5-2 cm, same rock types plus a whitish quartz and feldspar bearing chip which appears to be igneous and has some iron staining but no visible ferromags.

BSD 2	
	o apr ou cont.
1401	Circulation lost a =72', sump intake cleaned, circulation regained.
1408	75' sample, 50% non iron stained clay, 50% previous rocks chip size =0.75 cm.
1409	80° return T = 12.9°C.
1410	80' sample, chip size 0.3-2.0 cm, 40% sandy clay with small rock chips and limited iron stain, 60% previous rock types.
1415	New 20' section of drill rod being added.
1417	85' sample, 95% cohesive sandy clay, 5% previous rocks chips #1 cm, some iron stain on clay.
1421	Return T = 13.6° C.
1423	$\frac{90^{\circ}}{\text{clay}}$ sample, chip size 1 mm-1.5 cm, >90% previous rock types, <10% clay with little iron stain.
1426	95' sample, chip size 3 mm-1 cm, >95% previous rock types, <5% clay.
1429	$=100^{\circ}$ return T = 14.0°C.
1430	100' sample, >90% previous rock types, >proportion of chert and whitish igneous rock compared to DF, <10 clay.
1433	New 20' section of drill rod added.
1438	105' sample, chip size 2 mm-0.8 cm, mostly 0.3 mm, >90% previous rock types, <10% cohesive sandy clay.
1441	<u>110'</u> sample, chips 3 mm-1 cm, >60% previous rock types, $\leq 40\%$ sandy clay with some iron stain.
1445	Return $T = 14.5$ °C.
1448	115' sample, chip size 2 mm-1 cm, >90% previous RX, <10% sandy clay.
1450	120' return T = 14.7°C.
1451	120' sample, 50% previous RX, 50% sandy cohesive clay, chip size 3 mm-1 cm.
1453	New 20 ^t drill rod added.
1458	125' chip size 0.3 cm-1.5 cm, >70% sandy clay, <30% previous RX.
1502·	130' chip size 2 mm-0.8 cm, >90% previous RX, <10% clay.
1506	Return $T = 15.0^{\circ}C$, sump $15^{\circ}C$.

III-34

BSD 2

8 Apr 80 cont.

1720 String being tripped out for bit change.

9 Apr 80

- 0750 Arrive on site.
- 0800 New 6" tri-cone being put on.

0810 Standing water in hole at approx. 25'.

- 0847 Hole open to 196', drilling begins.
- 0852 New 20' rod being added.
- 0903 <u>205'</u> sample, chip size 1 mm-0.6 cm, 20% sandy brown clay, 80% previous rocks.
- 0912 <u>210'</u> sample, size 2 mm-4 mm coarse sand and chips, 50% sandy brown clay, 50% previous RX.
- 0918 Return $T = 14.4^{\circ}C$, depth =214'.
- 0920 <u>215'</u> sample, 85% previous RX mostly chert, 15% brown sandy clay, chips 2 mm-5 mm.
- 0930 <u>220'</u> sample, 2 mm-1 cm, 80% previous RX, 20% brown sandy clay. Return T = 15.1°C.
- 0932 New 20' rod being added.
- 0941 <u>225'</u> sample, 70% previous RX, 30% brown sandy clay, 2 mm-5 mm.
- 0947 = 227' return T = 15.6°C.
- 1012 <u>230'</u> sample, 2 mm-0.5 cm, 50% brown sandy clay, 50% previous rock types largely DF.
- 1020 235' sample, same description as 230'.

1024 Mud pump overheating, drilling stopped to remedy.

- 1030 Drilling again started.
- 1038 =239' return $T = 16.9^{\circ}C$.
- 1041 240' sample, 2 mm-5 mm, 70% previous RX, 30% brown sandy clay.
- 1043 New 20' rod being added.
- 1052 =242' return $T = 16.7^{\circ}C$.

III-36

9 Apr 80 cont.

- BSD 2
- 1412 <u>305'</u> sample, chips 1 mm-6 mm, 75% rock chips are same type, 25% sandy brown clay.
- 1415 305' return T = 20.3°C.
- 1428 =309' return T = 20.5°C.
- 1501 <u>310'</u> sample, 2 mm-6 mm all rock chips >95% DF preceded by difficult drilling 308-310'. Probably a boulder.
- 1505 =312' return T = $20.7^{\circ}C$.
- 1514 <u>315'</u> sample, 2 mm-8 mm rock chips, 80% mostly DF, little chert, 20% brown sandy clay.
- 1531 320' return $T = 20.0^{\circ}C$.
- 1532 <u>320'</u> sample, 5 mm-1 mm, 60% sandy brown clay, 40% previous RX.
- 1533 Sump $T = 20.3^{\circ}C$, 15.42 return T = 19.2.
- 1540 String being tripped out for bit inspection and seal repair.

10 Apr 80

- 0800 Arrive on site new 5 5/8" tri-cone bit being added.
- 0820 String being lowered.
- 0827 Hole has some blockage at =55'.
- 0845 Prime lost on mud pump.
- 0905 Prime regained rod insertion continuing.
- 0925 Drill rod has a plug in core blocking mud flow may be a plugged bit - string being tripped out to locate the problem.
- 1026 Bit at surface being removed for inspection. Plug was a rock a join between sub and first 20' rod plus other obstructions in core of sub.
- 1047 Float sub valve and float sub cleaned string being reinserted.
- 1153 Drilling started at =315'.
- 1157 = 320° return T = 16.0° C.
- 1201 New 20[†] section of drill rod being added.
- 1210 <u>325'</u> sample, 1 mm-12. cm, 70% chips of previous rock types mostly DF, 30% brown sandy clay.

10 Apr 80 cont.

- 1503 New 20' rod being added.
- 1519 <u>385'</u> sample, 2 mm-9 mm, 65% brown sandy clay, 35% previous RX.
- 1525 =389' return $T = 19.5^{\circ}C$.
- 1526 390' sample, same description as 385'.
- 1542 395' sample, 1 mm-5 mm, 75% previous RX, 25% brown sandy clay.
- 1546 = 399' return T = 19.7° C.
- 1548 400' sample, 2 mm-7 mm, 70% previous RX, 30% brown sandy clay.
- 1553 New 20' rod being added.
- 1603 <u>405'</u> sample, 2 mm-7 mm, \leq 50% previous RX, \geq 50% sandy brown clay.
- 1609 409' return T = 19.9°C.
- 1612 <u>410'</u> sample, 80% sandy brown clay, 20% previous RX, 2-7 mm.
- 1622 <u>415'</u> sample, 1 mm-6 mm, 60% sandy brown clay, 40% previous RX.
- 1627 =419 return $T = 20.2^{\circ}C$.
- 1632 New 20' section being added.
- 1637 <u>420'</u> sample, 1-5 mm, 50% sandy brown clay, 50% previous RX.
- 1645 425' return $T = 20.2^{\circ}C$.
- 1645(42) <u>425'</u> sample, 2 mm-5 mm, 80% sandy brown clay, 20% previous RX. Note: bit practically pushed through from 421-427' fault?
- 1647 Drilling very slow @ =428'.
- 1651 <u>430'</u> sample, 2-5 mm, 70% rock chips almost all DF, 30% brown sandy clay, return $T = 20.6^{\circ}C$.
- 1659 435' sample, 2-4 mm, 60% sandy brown clay, 40% previous RX.
- 1701 =436' return T = 21.0°C.
- 1707 Still =436, drilling very slow.
- 1716 <u>440'</u> sample, 2 mm-7 mm, 80% sandy brown clay, 20% previous RX.
- 1717 New 20' rod being added.
- 1731 <u>445'</u> sample, 2 mm-6 mm, 75% sandy brown and whitish gray sandy clay, 25% previous rock types.

11 Apr 80

0748 Arrive on site.

BSD 2

0838 String trip out complete.

0900 Begin setting of 3" casing.

1109 Casing (3") set to TD (500') - hole will be flushed with Barofos.

CC no. I SCHEMATIC WELL COMPLETION DIAGRAM



IV 2





IV 6

Darrough Hot Springs Geothermal Power Plant

PROJECT DESCRIPTION

2007 Darrough Hot Springs Geothermal Power Plant PROJECT DESCRIPTION

2. Project Description

Location The Darrough Hot Springs is located approximately 200 miles east of Reno in Big Smoky Valley, Nye County, Nevada. The project is located approximately 10 miles northwest of Round Mountain and 60 miles north of Tonopah on Highway 376.

The project is situated on relatively flat ground which slopes eastward from Highway 376, and is at an elevation of 5,750 feet above sea level. The Darrough Hot Springs is located in Section 17 of Township 11 North Range 43 East of the Mount Diablo Meridian, Nevada. The BLM Geothermal Lease covers Section 18 of Township 11 North Range 43 East of the Mount Diablo Meridian, Nevada.



Project History

Since the late 1800s, the Darrough Hot Springs has been recognized as a well-known hot springs and geothermal resource. The USGS mapped the area and noted the Darrough Hot Springs as a prominent hydrothermal resource with high temperature surface hot springs and pools. In 1963, Magma Geothermal drilled a well in the northwest corner of the Darrough ranch. The Magma well reached a depth of 812 feet and recorded a temperature of 231° F and artesian flow rate through an 8 inch pipe of 1145 gallons per minute. The well is in good condition and with some minor rehabilitation will be the project's first production well.

In 1985, Oxbow Geothermal drilled a well on BLM land approximately 2000 feet east-northeast of the Magma well. The Oxbow well reached a depth of

- *Fluid Gathering and Injection Systems* The geothermal fluids will be gathering by a system of pipelines that transport the geothermal fluid from the wellheads to the power plant. The injection system will use pipes and pumps to inject the geothermal fluids back into the geothermal reservoir.
- *Power Plant* It is envisaged that the Darrough Hot Springs Geothermal Power Plant will utilize binary power plant design. A heat exchanger will transfer the heat from the geothermal fluid to a working fluid of pentafluoropropane which has a boiling temperature of 59° F. The working fluid will be flashed in turbine generator sets to produce electrical energy. This type of plant installation has been used very successfully at many geothermal projects in Nevada and California.
- *Cooling* Before the working fluid can be reused and heated again, it must be cooled and condensed into a liquid. This is usually done through air heat exchangers, but because Darrough Hot Springs has an adequate supply of cold water, it will use the more efficient water heat exchangers.
- Transmission Line Darrough Hot Springs Power Plant will deliver power to the Round Mountain substation approximately 10 miles southeast of the project. Sierra Pacific's 230 kV line runs north from the Round Mountain substation to the Gonder substation and east to PacifiCorp and LADWP's 230 kV 240 MW transmission line (indicated in blue on the OASIS map below) connecting directly to southern California.



energy production. Recent legislation in prohibited California Utilities from buying additional power produce by burning coal, even if it was produced outside the state. The Darrough Hot Springs Power Plant could supply 9,000 new southern California households with green power and prevent the burning of additional fossil fuels to supply those new homes.

Employment The company's head office currently employs 2 staff. The resource confirmation program will employ 4 persons from northern Nevada for drilling, area site preparation and building. Some 5 persons from the northern Nevada area have been employed in support roles during the confirmation drilling program. Approximately 15 experienced workers and professional staff from other jurisdictions will be employed on the drill crews and drilling support services and in supervisory or professional roles.

The capital construction of a geothermal generating plant and associated transmission line, substation and other facilities would employ some 5 personnel per year during the construction period. Once in operation, the geothermal plant and transmission facilities would employ only one person full-time. Work related to transmission route maintenance and similar services would be sub-contracted locally, with employment varying on a seasonal basis. Maintenance required on a binary geothermal power plant is very minimal and will be subcontracted to a power equipment maintenance contractor or the power equipment manufacturer maintenance division.

- *Expenditures* Some \$1 million has been budgeted for completion of the resource confirmation program, a feasibility study and an environmental assessment. The capital cost of a 12 MW generating plant and associated facilities is estimated at \$44 million over the 18 month construction period. Operational expenditures are estimated in the order of \$3.2 million annually. The project will pay \$183,000 in Nevada sales on the electricity sold and will generate a minimal payroll. Significant spin-off employment and business opportunities are expected with respect to the purchase of equipment, supplies and services from local and area sources.
- Downstream Benefits Geothermal projects in other jurisdictions have generated significant spin-off opportunities by providing heating for residential and commercial use, greenhouses, and land-based fish farms and spas – referred to as "downstream benefits."

The GAE may engage in potential spin-off projects such as aquaculture or greenhouse operations utilizing the generating plant's excess thermal energy and surface water used for cooling.

Recreational Development Outdoor recreational potential in the project area may include a youth camp, horseback riding, hiking and camping, fishing and hunting, and hot springs facilities. However this potential is extremely limited because of the remote location and limited commercial facilities, such as motels and restaurants. springs field 33 Picture of geothermal wellhead 34 McGee Geophysical Services magnetic survey of Darrough & Berg Ranches 35-44 Geologist Dennis Trexler's interpretation of magnetic survey 45 Drill Site Map 46 Halliburton Temperature Test 47 Darrough Water Analysis 2006 48 Darrough Development Cost Estimates 49 Darroug Revenue and O&M Pro Forma 50 Tax Benefit Investor IRR Analysis 51

1

Geothermal Resource Assessment

of

Darroughs Hot Spring and vicinity,

Big Smoky Valley, Nevada

Prepared for

Smoky Valley Geothermal P. O. Box 11560 Bainbridge Island, WA 98110

Prepared by

Dennis T. Trexler Geologic Consultant 115 Blair Place Reno. NV 89509

January 15, 2006

REGIONAL GEOLOGY AND GEOTHERMAL RESOURCES

General Geology and Structure

Geologically, the region is complex with a lithologic history extending from the pre-Cambrian to the Holocene. The Toiyabe Range forms the valley's western boundary within the study area and includes Pre-Cambrian and Paleozoic siliceous, argillaceous and calcareous sedimentary and meta-sedimentary rocks, Paleozoic lavas, Mesozoic intermediate to acidic intrusives, Tertiary lavas, tuffs and sediments. The Toquima Range forms the valley's eastern boundary and contains rocks similar to those found in the Toiyabe Range. Quaternary to recent alluvial, fluvial, lacustrine and playa deposits form the valley floor.

Structural features of the region are also indicative of a long and complex history. Evidence can be found for regional metamorphism, including several periods of folding, largescale low-angle faulting (related to Robert's Mountain Thrust), large-displacement high-angle faulting (associated with the Basin and Range tectonics), small- to moderate-scale faulting in alluvial materials, and numerous intrusive events.

A generalized geologic map outlines the distribution of some of the lithologies and structural features of the study area, Figure 1. More detailed information is available in Ferguson and Cathcart (1954), Kleinhampl and Ziony (1967), Means (1962), Meinzer (1917), McKee (1968), McKee (1972), McKee (1976), Speed and McKee (1976) and Stewart and Carlson (1978).

Gravity Survey

A gravity survey performed by the Division of Earth Sciences personnel as part of a larger survey of Big Smoky Valley, conducted for the U.S. Department of Energy, shows an abrupt gravity decrease in the area of Darroughs Hot Springs, Figure 2. This anomaly is probably related to a buried fault along which the basement rocks have been systematically

Environmental Isotopes

Hydrogen and oxygen stable light isotope data from the Darroughs Hot Springs area demonstrate a complex scenario of mixing of geothermal and non- thermal waters Table 2 and Figure 4. Three of the four thermal fluids sampled at Darroughs exhibit an oxygen shift of seven to nine per mil. Although a minor amount of carbonate rocks are present in the Toiyabe Range near the Darroughs surface geothermal site, chemical analysis has shown the fluids to be deficient in calcium by more than

an order of magnitude compared to non-thermal fluids in the area. In addition, these springs are not depositing calcareous tufa. Based on these facts and the magnitude of the 18-oxygen shift,

Table 2

Sample Name	Sample Number	D°/ ₀₀	0°/ _∞	Temp. °C
Darrough Well	DB-1	-131	-8.4	90.5
North Spring	DB-2	-130	-6.7	71.2
South Spring	DB-3	-128	-15.1	68.0
Darroughs Pool	DB-4	-129	-8.1	95.5
Aqueduct Stream	DB-5	-123	-10.8	1.8

Hydrogen and oxygen stable light isotopes of Darroughs Hot Springs

it seems reasonable to postulate that the isotopic compositions of the geothermal fluids are the result of a high temperature thermal history. One of Darroughs thermal fluids exhibits an isotopic composition falling within the meteoric range. This is thought to be the result of recharge, which occurs along a relatively shallow path, possibly in alluvial materials, where it is heated by conduction.

Temperature Probe Survey

A survey of the soil temperature was conducted at the Darroughs Hot Springs by drilling 2-meter (6.5 ft.) holes with a power auger (Trexler and others, 1980). Twenty-nine drill holes were used to prepare the isotherm map presented in Figure 5. Examination of the patterns in the figure indicates that the thermal fluids migrate in the near surface, along distinct paths which extend eastward from the approximate locations of the springs labeled "71" and "68". These paths may be former channels in the alluvial materials through which the hot springs surfaced.

that the 265°F temperature is out of place when one considers that a temperature of 230°F was measured 25 feet below the 755 ft. depth. If the temperature is 265°F at 755 feet, one would expect higher temperatures at greater depths. However, the temperatures at 780 and 812 feet are consistent with three previous temperatures of approximately 230°F measured higher in the well. Flow line temperatures never exceeded 101°C (214°F) with a flow pressure of 8 psig through an 8-inch line at a flow rate of 1145 gpm. Static (shut in) pressure was 47 pounds per square inch (gauge) (psig).

In August 1980, a consultant reported that 5 temperature gradient holes were completed in the area. Figure 7 indicates the location of 7 temperature gradient holes used for analysis of subsurface temperatures. However, only 3 can be confirmed based on descriptions from the report (Meidav, 1980, unpublished).

One temperature gradient-hole (TG-7) was drilled by UNLV personnel to a depth of 500 feet under a U.S. DOE contract in March 1980. The temperature gradient measured in the 500-foot temperature gradient hole (TG-7) is shown in Figure 8. Temperature gradients from other temperature gradient holes range from 6.5°C per 100 feet in TG-2 to a low of 2.1°C per 100 feet in TG-5 on the Wineglass Ranch property. The temperature gradient in the bottom 100 feet of TG-6, located on the Berg Ranch was 5°C per 100 feet.

Temperature gradient drilling indicates the localized extent of the near surface reservoir that was also identified by the two-meter probe survey conducted by UNLV personnel under U.S. DOE contract.

In April 1981, Geothermal Resources International drilled a 2000 ft. temperature gradient hole near the Darroughs Ranch. The hole was located in the SW1/4 of the NE1/4 of Section 18, T11N, R43E. Information on the lithilogies and temperatures encountered in this hole are proprietary, a copy of the driller's log in included in Attachment 1. The lack of further interest in the area by GRI is a matter to be contemplated. Were temperatures encountered below those
CONCLUSIONS

1) Gravity data indicate that the surface manifestation of geothermal activity in the Darroughs Ranch area of Big Smoky Valley is controlled by faulting of the basement rocks underlying the unconsolidated valley fill.

2) Based on major element geochemistry, the geothermal fluids are distinctly different from cold surface waters in the area. The high concentrations of silica (108-122 ppm) indicate reservoir equilibrium temperatures near 132°C (270°F).

3) Isotopic analyses of geothermal fluids indicate that they are of meteoric origin. The geothermal fluids show large oxygen isotope shifts, which indicate a history of high temperature.

4) The near surface manifestation of the thermal anomaly, detected by a 2-meter temperature probe survey, indicates the migration of geothermal fluids is controlled by faulting.

5) Exploration drilling at Darroughs Hot Springs indicates subsurface temperatures of 230°F were encountered at a depth of less than 800 feet. Temperature gradients measured in 500-foot temperature gradient holes range from 2.1°C to 6.5°C per 100 feet. A 2,520-foot deep test hole drilled by Oxbow Geothermal, approximately 0.5 mile east of Darroughs Hot Springs, had a BHT of 221.8°F. A temperature gradient hole (TG-6) dilled on the Berg property, north of the Darrough Ranch, has temperature gradient of 5°C in the bottom 100 feet of the hole.

6) Based on gravity data, 2-meter temperature probe surveys and temperature gradient drilling, the geothermal resource in Big Smoky Valley in the vicinity of Darroughs Hot Springs is localized along a fault which trends NNE from the center of Section 19, T.11N., R.43E., through

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Figure 2. Simple and Complete Bouguer anomaly, and topography of the Darrough Hot Springs area.



Tigure 4. Oxygen and hydrogen stable light isotopic composition of thermal and non-thermal fluids from the Darroughs Hot Springs. Worldwide meteoric water line after Graig (1963).



DEPIN IN FART

TEMPERATUR': ^OF

Figure 6. Temperature log of Magma well (DB-1) prepared from driller's report.



Figure 8. Temperature gradient profile of TG-7.

DARR OUGHS HOT SPRINGS GROUND





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GPS Positioning

A Trimble Model GeoExplorer XT GPS receiver was used to provide navigation and positioning. The receiver was configured to receive differential corrections in real-time from WAAS (Wide Area Augmentation System) geo-stationery satellites. This system is operated by the United States Government Federal Aviation Administration. The resulting positions usually have an accuracy of about two meters or better. The GPS receiver was set up to output a NMEA string of positional data to be recorded on the magnetometer along with the magnetic readings. The NMEA string format that was used is the GGA format described below:

Field Meaning

- 1 UTC of position fix
- 2 Latitude
- 3 Direction of Latitude (N or S)
- 4 Longitude
- 5 Direction of Longitude (E or W)
- 6 GPS Quality Indicator:
- 0: Fix not available or invalid
 - 1: GPS fix
 - 2: Differential GPS fix
 - 4: RTK (fixed)
 - 5: RTK (float)
- 7 Number of Satellites in fix
- 8 HDOP
- 9 Orthometric Height
- 10 Units of orthometric height
- 11 Geoid Separation
- 12 Units of geoid separation
- 13 Age of differential correction
- 14 Reference Station ID

The positions of the magnetic readings were recorded on the G-858 magnetometer in WGS-84 latitude and longitude.

Magnetic Profile Lines

A total of 62 line kilometers were surveyed along 31 profiles oriented at a bearing of N70W with a length of 2000 meters. A line location map is shown below. The substantial gaps in the lines are at locations where the recording magnetometer was paused to avoid collecting data near fences, powerlines, building structures, and other cultural objects present on the survey area. The survey required 4 days of field work to complete with a single operator.

DATA PROCESSING

Overview

After downloading the magnetic data from the magnetometers onto a notebook PC, diurnal corrections were applied using the Geometrics software package, *MagMap2000*. Geosoft compatible XYZ files were then generated with WGS-84 geographic coordinates for each magnetic measurement. After importing the XYZ files into a Geosoft Oasis montaj database, NAD27 UTM coordinates were generated, profiles were prepared, and additional editing was performed as necessary. The editing mostly consisted of deleting readings affected by cultural noise and deleting dropouts which are large-amplitude negative spikes that occur when the magnetometer sensor is tilted too far from a vertical orientation.

Mapping and Gridding

The Darroughs Hot Springs Total Magnetic Field data was gridded, mapped and, contoured to insure high quality data were collected. A Reduction to Magnetic Pole (RTP) was calculated to account for inclination of the magnetic field. Two images of the contoured Total magnetic Field are shown below, one with the colored grid and one without the colored grid. The contour interval is five nT.

A horizontal magnetic gradient map is also shown below.



Total Magnetic Intensity -Darroughs Hot Springs Ground Magnetic Survey

DATA FILES

Raw Data Files

All of the raw data files for the project will be delivered on a CD. Base magnetometer files are in ASCII format with the file extension *.stn.* Field magnetometer files are in binary format with the filename extension *.bin.* The *.stn* and *.bin* files are unedited. XYZ files are output from MAGMAP 2000 and contain the raw measurements, diurnal corrections, and WGS-84 latitude and longitude. Files are named with the date and line number(s).

Geosoft Database File

The Geosoft database file with the all of the processed and edited ground magnetic data included on the CD is named *magfeb15.gdb*.

Final XYZ Files

The Geosoft database file was exported as an XYZ file in csv format then imported into Excel and is named *darroughs_gmag_final.xls*.

Map and Grid Files

The file names for the map files used to create the maps in this report are as follows and are on the accompanying CD:

mag_feb_15_rtp_smooth.grd, .map, .jpg
line_loc.map, .jpg
horizontal_gradient.grd, .map, .jpg

Submitted by:

Christopher Magee Consulting Geophysicist



Proposed Drill Site Locations

Darrough property boundary

Berg property

Potential Drill sites 1st 2nd 3rd



Darrough Water Analysis 022706.xls:MIS01110

AQUATIC RESEARCH INCORPORATED LABORATORY & CONSULTING SERVICES 3927 AURORA AVENUE NORTH, SEATTLE, WA 98103 PHONE: (206) 632-2715 FAX: (206) 632-2417

CASE FILE NUMBER:MIS011-10PAGE 1REPORT DATE:02/27/0601/25/06DATE SAMPLED:01/14/06DATE RECEIVED:01/25/06FINAL REPORT, LABORATORY ANALYSIS OF SELECTED PARAMETERS ON WATERSAMPLES FROM GARY W. TRIPPCalledon and a statement of the sta

CASE NARRATIVE

One water sample was received by the laboratory in good condition. The water sample was analyzed according to the chain of custody. No difficulties were encountered in the preparation or analysis of these samples. QA/QC data is retained by the laboratory.

SAMPLE ID	pН	conductivity (umhos/cm)	ALKALINITY (mg/CaCO3/l)	AMMONIA (mg/l)	NITRATE (mg/l)	NITRITE (mg /l)
DARROUGH RANCH HOT SPRINGS	8.99	537	152	0.039	0.010	0.070
SAMPLE ID	CHLORIDE (mg/l)	SULFATE (mg/l)	FLUORIDE (mg/l)	BORON (mg/l)	CALCIUM (mg/l)	MAGNESIUM (mg/l)
DARROUGH RANCH HOT SPRINGS	12.8	55.1	18.0	0.290	1.63	<0.100
· · · · · · · · · · · · · · · · · · ·	POTASSIUM (mg/l)	SODIUM (mg/l)	LITHIUM (mg/l)	SILICON (mg/l)	ARSENIC (mg/l)	BARIUM (mg/l)
SAMPLE ID						
DARROUGH RANCH HOT SPRINGS	4.30	125	0.449	49.0	0.0281	<0.005

SAMPLE DATA

	IRON
SAMPLE ID	(ug/l)
DARROUGH RANCH HOT SPRINGS	0.084

SUBMITTED BY:

Steven Lazoff Laboratory Director



AMERICAN WEST ANALYTICAL LABORATORIES

463 West 3600 South Salt Lake City, Utah 84115 November 02, 2007

Jay Hamilton Hamilton Environmental L.L.C. 485 W. 1400 N. Suite E Orem, UT 84057

TEL: (801) 244-4585 FAX: (801) 224-1893

RE: Truckee

Dear Jay Hamilton:

Lab Set ID: L80809

American West Analytical Labs received 1 sample on 11/1/2007 for the analyses presented in the following report.

(801) 263-8686 Toll Free (888) 263-8686 Fax (801) 263-8687 e-mail: awal@awal-labs.com

> Kyle F. Gross Laboratory Director

All analyses were performed in accordance to National Environmental Laboratory Accreditation Program (NELAP) protocols unless noted otherwise. If you have any questions or concerns regarding this report please feel free to call. The abbreviation "Surr" found in organic reports indicates a surrogate compound that is intentionally added by the laboratory to determine sample injection, extraction and/or purging efficiency.

Thank you.

Approved by aboratory Director or designee

Report Date: 11/2/2007 Page 1 of 2

All analysis applicable to the CWA, SDWA and RCRA are performed in accordance to NELAC protocols. Pertinent sampling information is located on the attached Chain-of-Custody. This report is provided for the exclusive use of the addressee. Privileges of subsequent use of the name of this company or any member of its staff, or reproduction of this report in connection with the advertisement, promotion or sale of any product or process, or in connection with the re-publication of this report for any purpose other than for the addressee will be granted only on contact. This company accepts no responsibility except for the due performance of inspection and/or analysis in good faith and according to the rules of the trade and of science.

e-mail:

ORGANIC ANALYSIS REPORT

	Client: HamiltonEnvironmentalL.L.C. ProjectID: Truckee	Contact:	JayHamilton
AMERICAN WEST ANALYTICAL LABORATORIES	LabSampleID: L80809-01A FieldSampleID: Truck-68-04 Collected: 10/26/20073:48:00PM Received: 11/1/2007	Analyz	ed: 11/2/20076:21:00AM
	AnalysisRequested: SW8260B/5030B		
	Analytical Results	82	260-W-MBTEXN/TPH
463 West 3600 South	Units= mg/L DilutionFactor= 1		Analytical
Salt Lake City, Utan 84115	Compound	ReportingLimit	Result
	Methyltert-butylether	0.0020	< 0.0020
	Benzene	0.0010	0.0018
	Toluene	0.0020	0.0023
	Ethylbenzene	0.0020	< 0.0020
(801) 263-8686	Xylenes, Total	0.0020	< 0.0020
Toll Free (888) 263-8686	Naphthalene	0.0020	< 0.0020
Fax (801) 263-8687	TPH C6 to C10 (GRO)	0.020	< 0.020
e-mail: awal@awal-labs.com	TPH C11 to C15 (DRO)	0.020	0.032
	Surr:1,2-Dichloroethane-d4	81-143	93.6
Kyle F. Gross	Surr:4-Bromofluorobenzene	85-115	96. 7
Laboratory Director	Surr:Dibromofluoromethane	80-124	96.8
	Surr:Toluene-d8	88-120	99.5

All analysis applicable to the CWA, SDWA and RCRA are performed in accordance to NELAC protocols. Pertinent sampling information is located on the attached Chain-of-Custody. This report is provided for the exclusive use of the addressee. Privileges of subsequent use of the name of this company or any member of its staff, or reproduction of this report in connection with the advertisement, promotion or sale of any product or process, or in connection with the re-publication of this report for any purpose other than for the addressee will be granted only on contact. This company accepts no responsibility except for the due performance of inspection and/or analysis in good faith and according to the rules of the trade and of science.

American West Analytical Labs

RUSH

01-Nov-07

WORK ORDER Summary

Work Order L80809

Client ID:	HAM100		QC Level: QC 1					
Project:	Truckee		Location:	\sim		Contact: Jay Hamilton		
Comments:	Next Day Rush; QCLe	vel: QC 1		HOK-DB				-el
Sample ID	Client Sample ID	Collection Date	Date Received	Date Due	Matrix	Test Code	Storage	(
L80809-01A	Truck-68-04	10/26/2007 3:48:00 PM	11/1/2007	11/2/2007	Aqueous	8260-W-MBTEXN/TPH	PurgeFridge	6

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Page 1 of 1



CHAIN OF CUSTODY RECORD

Ori I

Fovironmenta	485 West -	1400 North	, Orem,	, Utah ∤	84057	7 (801) 224	-458!	5 Fax 2:	24-18	93							V			Lab	ID#	8	080	<i>1</i> 9
H.E. CONTACT: Jay Hami Hon LAB:		PROJEC PHONE:	T#		SITE T	WC.	ĸe	2	<u>}</u>			•		Sigr		e.' Z€	Le.	1+	24	11-0		line.	10/2	Date 6 [0 7	*
SAMPLE ID Muck - 68 - 04	DATE	TIME	MATRIX		T GRAB	NO. OF CONTAINERS	TPH-Casoline	TPH - Diesel	EPA 8260 B (MBTEXN)	EPA 8020 (BTEXN)	EPA 8010	EPA 1664 (O&G)	EPA 1664 (TPRH)	EPA 8240/624 (VOCs)					SAN				REMAF	₹KS	
Special Instructions:			Signati	ure:	4	- Cl				~	ļ		18	ale/	Ume 07	7	Sign		, [1		/	L 11-1)ate/Tim	10
Danatura t			Relinqu	uished	By: þ	rint)	J	- <u>/</u> 	1 /1	lar	nı	l +a	~~~/ ~~/	77-1	55a	Ÿ	Rece	eived By: (pr	n / k int) S	lon	, 4			//	5
Relinquished By: (print)	Date/Tim	<i></i>	Signatu Dispato	ched B	 y: (prir	 nt) [,]	******	,						a(e/)			Sign Rece	eived for Lal		 By: þrin	 t)		L	/ate/ 1 kn	

• •							•	L	ab Set ID.	:	80	1809				
Samples Were:				OC Tar	e Was:				ontainer '	Tyne:			······	N	o. Rec.	
D Shipped By:				Prese	nt on Or	iter Pac	kage		AWALS	upplied)	Plastic					
V Hand Delivered	1		-	$\nabla \Pi V_{4}$			I/A		A DAAL C	upplied /	Clear G	1966			······	· ·
A mbient	4 			Imbral		uter no			AWALD	upplied	Ambar	Glass				
	•	·····				ластра То ПХ	CRABU	~ [끔	AWALS	upplied 1			Viala			
Tommomotive	115 00						<u>V/A</u>		AWALS	принео			Viais			
Temperature					esent of	i Sampie		나브	Amber L	Clear L	neleads		o Headsp	ace	····	
Rec. Broken/Leal	ting LI Yes LX NO	LJ N/A			<u>s D</u>	<u>10 U</u>			Non AW/	AL Supp	hed 60	ntainer				
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Properly Preserve	d DXYes DNo	Π Ν/Α	No	otes:												
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Rec. Within Hold	X Yes D No				· .		\backslash	Di	screpanc	ies Betw	een La	bels and	COC		Yes	C
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Ammonia		All pris OK								ļ,	<u> </u>		-			+
						-							-	-		<u>+</u> -
Cuanida	$\frac{\text{pH} \sim \text{H}_2 \text{SU}_4}{\text{DH} \sim 12 \text{ NeOH}}$	1									<u> </u>					-
Cyaniuc Metala	nH <2 UNO															+
NO. & NO.	$\frac{pH < 2H < 0}{pH < 2H < 0}$				+											-
Nutrients	$pH < 2H_2SO_4$ $pH < 2H_2SO_4$										ļ				· · · · · · · · · · · · · · · · · · ·	
	<u>pH <2 H2504</u>						· ·								1 :	-
Phenols	pH <2 H.SO.															
<u>Sulfide</u>	$\frac{\text{pH} \sim 11_{2} \times 0_{4}}{\text{nH} \sim 0 \times 0 \times 0 \times 12}$						+	· · ·					+		1	+
TKN	nH <2 H.SO.												-	<u> </u>		
TOC	nH <2 H.PO		÷								<u> </u>					+
	$pH < 2H_{SO}$			· · · · ·					-		+					1.
гри	pH <2 HCI															+
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					<u> </u>			<u>├</u>		\sim						+
Procedure:	Pour a small amou Pour sample from Do Not dip the pH If sample is not pre Flag COC and not Place client convert	Int of sample in the Lid gently over wide paper in the sample served properly list fy client for further i sation on COC	sample li range pl bottle of its exten nstructior	d H paper r lid slon and ns	receiving	pH in the	appropria	te colum	n above			`			• . • .	

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October 23, 2007 AMERICAN WEST ANALYTICAL Jay Hamilton LABORATORIES Hamilton Environmental L.L.C. 485 W. 1400 N. Suite E Orem, UT 84057 TEL: (801) 244-4585 463 West 3600 South FAX: (801) 224-1893 Salt Lake City, Utah 84115 RE: Truckee Geothermal Lab Set ID: L80604 Dear Jay Hamilton: American West Analytical Labs received 1 sample on 10/19/2007 for the analyses presented in the following report. (801) 263-8686 All analyses were performed in accordance to National Environmental Laboratory Accreditation Toll Free (888) 263-8686 Program (NELAP) protocols unless noted otherwise. If you have any questions or concerns Fax (801) 263-8687 regarding this report please feel free to call. e-mail: awal@awal-labs.com

Kyle F. Gross Laboratory Director Pages 1 and 3 have been revised. Carbonate and bicarbonate alkalinity added to report.

Thank you.

Approved b

Laboratory Director or designee

Report Date: 10/23/2007 Page 1 of 3



INORGANIC ANALYSIS REPORT

Client: Hamilton Environmental L.L.C. Project ID: Truckee Geothermal Contact: Jay Hamilton

AMERICAN WEST ANALYTICAL LABORATORIES Lab Sample ID: L80604-01D Field Sample ID: **TR Well 68-04** Collected: 10/18/2007 3:35:00 PM Received: 10/19/2007

TOTAL METALS

463 West 3600 South Salt Lake City, Utah 84115

(801) 263-8686 Toll Free (888) 263-8686 Fax (801) 263-8687 e-mail: awal@awal-labs.com

> Kyle F. Gross Laboratory Director

	TOTAL METALS		Date	Method	Reporting	Analytical	l
	Analytical Results	Units	Analyzed	Used	Limit	Results	
h	Aluminum	mg/L	10/22/2007 1:38:00 PM	200.7	0.10	< 0.10	
h	Antimony	mg/L	10/19/2007 6:10:26 PM	200.8	0.0050	< 0.0050	
5	Arsenic	mg/L	10/19/2007 6:10:26 PM	200.8	0.0050	< 0.0050	
	Barium	mg/L	10/19/2007 6:10:26 PM	200.8	0.0020	0.024	
	Beryllium	mg/L	10/19/2007 6:10:26 PM	200.8	0.0010	< 0.0010	
	Boron	mg/L	10/22/2007 1:38:00 PM	200.7	0.50	3.9	
,	Cadmium	mg/L	10/19/2007 6:10:26 PM	200.8	0.0040	< 0.0040	
о 6	Calcium	mg/L	10/22/2007 1:38:00 PM	200.7	1.0	2.0	
7	Chromium	mg/L	10/22/2007 1:38:00 PM	200.7	0.010	< 0.010	
n	Copper	mg/L	10/19/2007 6:10:26 PM	200.8	0.0040	< 0.0040	
	Iron	mg/L	10/22/2007 1:38:00 PM	200.7	0.050	3.4	
is vr	Lead	mg/L	10/19/2007 6:10:26 PM	200.8	0.0050	< 0.0050	
,1	Magnesium	mg/L	10/22/2007 1:38:00 PM	200.7	1.0	< 1.0	
	Manganese	mg/L	10/19/2007 6:10:26 PM	200.8	0.0050	1.6	2
	Mercury	mg/L	10/23/2007 7:17:08 AM	245.1	0.00020	< 0.00020	
	Molybdenum	mg/L	10/22/2007 1:38:00 PM	200.7	0.040	< 0.040	
	Nickel	mg/L	10/19/2007 6:10:26 PM	200.8	0.0050	< 0.0050	
	Potassium	mg/L	10/22/2007 1:38:00 PM	200.7	1.0	2.1	
	Selenium	mg/L	10/19/2007 6:10:26 PM	200.8	0.0050	< 0.0050	
	Silicon	mg/L	10/22/2007 1:38:00 PM	200.7	0.050	0.94	
	Silver	mg/L	10/19/2007 6:10:26 PM	200.8	0.0050	< 0.0050	
	Sodium	mg/L	10/22/2007 3:06:00 PM	200.7	10	190	² #
	Thallium	mg/L	10/19/2007 6:10:26 PM	200.8	0.0020	< 0.0020	
	Zinc	mg/L	10/19/2007 6:10:26 PM	200.8	0.010	< 0.010	

² Analyte concentration is too high for accurate spike and/or RPD recovery.

² Analyte concentration is too high for accurate spike recovery.

The reporting limits were raised due to high analyte concentration.

Report Date: 10/23/2007 Page 2 of 3



INORGANIC ANALYSIS REPORT

HamiltonEnvironmentalL.L.C. Client: ProjectID: TruckeeGeothermal

Contact: JayHamilton

AMERICAN WEST ANALYTICAL LABORATORIES

e

L80604-01 LabSampleID: Field Sample ID: TR Well 68-04 Collected: 10/18/20073:35:00 PM

Received: 10/19/2007

	Analytical Results	Units	Date Analyzed	Method Used	Reporting Limit	Analytical Result	
162 West 2600 South	Alkalinity,(AsCaCO3)	mg/L	10/22/2007 7:00:00 AM	2320B	20	130	
Salt Lake City, Utah	Bicarbonate (As CaCO3)	mg/L	10/22/2007 7:00:00 AM	2320B	20	130	
84115	Carbonate (As CaCO3)	mg/L	10/22/2007 7:00:00 AM	2320B	10	< 10	
	Chloride	mg/L	10/22/2007 6:34:00 AM	300.0	20	30	
	Conductivity	µmhos/cm	10/22/2007 10:00:00 AM	2510B	2.0	940	
	Fluoride	mg/L	10/22/2007 6:34:00 AM	300.0	2.0	70	
(801) 263-8686	Nitrate (as N)	mg/L	10/19/2007 2:27:00 PM	353.2	0.010	< 0.010	
Toll Free (888) 263-8686 Fax (801) 263-8687	Nitrite (as N)	mg/L	10/19/2007 2:27:00 PM	353.2	0.010	< 0.010	
-mail: awal@awal-labs.com	pH @ 25° C	pH Units	10/19/2007 6:20:00 PM	4500H+B	0	8.21	Ħ
	Phosphorus, Total(asP)	mg/L	10/22/2007 2:56:00 PM	4500(P)F/B	0.050	0.092	1
Kyle F. Gross	Sulfate	mg/L	10/22/2007 6:34:00 AM	300.0	20	97	
Eaconatory Director	TDS	mg/L	10/19/2007 2:00:00 PM	160.1	20	490	
	TSS	mg/L	10/19/2007 5:15:00 PM	2540D	3.0	5.0	
	Turbidity	NTU	10/19/2007 2:45:00 PM	180.1	0.10	6.1	

H - Sample was received outside of holding time.

¹ Spike recovery indicates matrix interference. The method is in control as indicated by the laboratory control sample (LCS).

Report Date: 10/23/2007 Page 3 of 3

All analysis applicable to the CWA, SDWA and RCRA are performed in accordance to NELAC protocols. Pertinent sampling information is located on the attached Chain-of-Custody. This report is provided for the exclusive use of the addresses. Privileges of subsequent use of the name of this company or any member of its staff, or reproduction of this report in connection with the advertisement, promotion or sale of any product or process, or in connection with the re-publication of this report for any purpose other than for the addresses will be granted only on contact. This company accepts no responsibility except for the due performance of inspection and/or analysis in good feith and accepts the relative test of the test of the second second

America	n West Analytic	cal Labs			ŵ	wirslon	-1	
WORK (DRDER Summary				D n n	19-Oct-07		
Client ID: Project: Comments:	HAM100 Truckee Geothermal 2 Day Rush; QCLevel: 1	. Free Cyanide sent to C	QC Level: 1 Location: hemtech-Ford, Rad		SH ors Lab.	Work Order La		7
Sample ID	Client Sample ID	Collection Date	Date Received	Date Due	Matrix	Test Code	Storage	
L80604-01A	TR Well 68-04	10/18/2007 3:35:00 PM	10/19/2007	10/23/2007	Aqueous	2320B-ALK-W	oct 19 - wc	1
				10/23/2007		300.0-W	oct 19 - wc	1
				10/23/2007		COND-W	oct 19 - wc	1
				10/23/2007		NO2-W	oct 19 - wc	1
			······································	10/23/2007		NO3-W	oct 19 - wc	1
				10/23/2007		PH-W-4500H+B	oct 19 - wc	1.
L80604-01B				10/23/2007		Phos_Prep	oct 19 - po4	1
	· · · · · · · · · · · · · · · · · · ·			10/23/2007		PO4-TW-4500PF	oct 19 - po4 ~	1
L80604-01C	· · · · · · · · · · · · · · · · · · ·	4		10/23/2007	,	TDS-W	ww - tds/tss/turb	1
				10/23/2007	-	TSS-W-2540D	ww - tds/tss/turb	1
			· · · · · · · · · · · · · · · · · · ·	10/23/2007	······································	TURB-W	ww - tds/tss/turb	1
L80604-01D				10/23/2007		200.7PR	oct 19 - met	1
			· · ·	10/23/2007		200.8-W	oct 19 - met	1
			** - <u>-</u> ** · · · ··· - <u>-</u> · ··· <u>-</u> · ···	10/23/2007	.	200.8PR	oct 19 - met	1
<u></u>	· · · · · · · · · · · · · · · · · · ·		• .	10/23/2007		HG-DW	oct 19 - met	1
			· · · · · · · · · · · · · · · · · · ·	10/23/2007		HG-PREP-DW	oct 19 - met	1
				10/23/2007		ICP-DW	oct 19 - met	1
L80604-01E	······	•	· ·	10/23/2007		OUTSIDE LAB	Chemtech-Ford	1
L80604-01F		· · · · · · · · · · · · · · · · · · ·		10/23/2007		SUB-RADIONUCLIDES	Underwriters Lab	2

Hamilton

CHAIN OF CUSTODY RECORD

Ēr	vironmental	485 West 1	400 North	, Orem,	Utah	84057	' (801) 224	-458	5 Fax	224-	1893						Lab ID#	- 80604
H.E. CO	NTACT: V Hamilm		PROJEC	Τ#		SITE T	nu	kð	0	hen	the	mA	L		Signa	ature:	10	mult	10/11/07
LAB:	AWAL		PHONE:												Samp	oled By	: (print	Jay Ham. 1m	
. <i>TR</i> .	SAMPLE ID <u>L/c// 68-04</u>	DATE / 9//8/07	TIME 3: 3: J	R MATRIX	COMP	CRAB	V NO. OF CONTAINERS	TPH-Gasoline	TPH - Diesel	EPA 8260 B (MBTEXN)	A and TPH-Gasoline	C EFA 8020 (BIEXN)	EPA 1664 (O&G)	EPA 1664 (TPRH)	V EPA 8240/624 (VOCs)			Priority Priority (procenty # BEST SAMPLE LOCATIO Geothermac Fr Wall 68-04at Geothermac Vec Attach	L ble) r Awar can Do) in/REMARKS lurd thom truckee List.
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Special In	structions:			Signatu	ire: ,	7		 //							ate/Tj	ime ~	Signa	l Ire:	Date/Time
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Signature		Date/Tim	e	Relinqu Signatu	ished ire:	By: (p	rint)	1	Ay /	15A	<u>u l</u>	m		<i>(</i> 2	. 5 / ate/Ti	me	Rece Signe	ed By: (print)	Date/Time
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Relinquisi	ned By: (print)			Dispatc	hed B	y: (prin	ot)								-		Rece	ed for Laboratory By: print)	

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p.2

acility Name :			Depth of sampled water's	s origin :	•
Cility Owner			County:		
IDEP UIC Permit # :			Location :	Latituda	Longitude
Vell 10 # :			Sampler :		
Type of Well :	Monitor Produ	ction Injection	Date Sampled :		
		Extended	Name of Laboratory :		
UIC Sample LI	st 2- inorganic	Extended			
Parameter	Units	DW Standards	Initial Measured Values	Method	Method Description
otal dissolved solids	mg/L	500 - 1000		EPA 160.1	
oH	slandard units	6.5 - 8.5		EPA 150.1	
chloride	ma/L	250 - 400		EPA 300.0	Ion Chromatography
fluoride	ma/L	4		EPA 300.0	Ion Chromatography
sulfate	mg/L	250 - 500		EPA 300.0	Ion Chromatography
nitrate (as nitrogen)	mg/L	10		EPA 300.0	Ion Chromatography
nitrite (as nitrogen)	mg/L	1		EPA 300.0	ion Chromatography
aluminum	mg/L	0.05-0.2		EPA 200.8	ICP-MS
antimony	mg/L	0.006		EPA 200.8	ICP-MS
arsenic	ma/L	0.01*		EPA 200.8	ICP-MS
barium		2 ·		EPA 200.8	ICP-MS
bervilium	ma/l	0.004	1.	EPA 200.8	ICP-MS
cadmium	mg/2	0.005	-	EPA 200.8	ICP-MS
chromium	mg/L	0.1		EPA 200.8	ICP-MS
COpper	mg/L	1.0-1.3		EPA 200.8	ICP-MS
Cvanide (free cvanide)	mg/L	0.2			
lead	mg/L	0.015	·	EPA 200.8	ICP-MS
iron	mg/l	0.3 - 0.6		EPA 200.7	ICP
magnesium	mg/L	125 - 150		EPA 200.7	ICP
anganese		0.1	-	EPA 200.8	ICP+MS
marcury	mg/L	0.002		EPA 245 1	AA Cold Venor
nickel	mg/L	0.1		EPA 200.8	
selenium		0.05	_ <u> </u>	EPA 200.8	ICP-MS
silver	. mg/L	0.05		EPA 200.8	ICP-MS
thallium	mg/L	0.002		EPA 200.8	ICP-MS
zinc	mg/L	5		EPA 200.8	ICP-MS
adjusted gross alpha**	pci/L	15		EPA 900	
gross beta	ការខកា	4 .		EPA 900	
alkalinity (CaCO3)	mo/l	-		SM 2320 B	
bicarbonate				SM 2320 B	
boron	mo/L	-		EPA 200 8	
calcium	mg/L	-	······	EPA 200.7	
carbonate	mg/L	-		SM 2320 B	
EC	umhos/cm	at 25 degC		SM 2510 B	
lithium	mg/L	+		EPA 200.8	
nolybdenum	mg/L	-		EPA 200.8	
phosphorus, total	mg/L	-		EPA 365.1	
potassium	mg/L	-		EPA 200.8	
silica	mg/L	•	•	EPA 370.1 EPA 200.7	1
sodium	mg/L	`-		EPA 200.7	1
otal suspended solids	mg/L	•		EPA 160.2	1
urbidity	NTU	-		1	1

Rev 6/2006

ie: Detection limits must be at least as low as primary or secondary drinking water standards where applicable.

"Please indicate detection limit instead of stating "Non-Detect". Initial Measured Values are the first values collected under the application. Metals shall be sampled and analyzed as total metals. **Adjusted gross alpha particle activity doesn't include radon and uranium activity.

Lab Set ID: 80604

Samples Were:			T	COC Tape Was:					Container Type:]	No. Rec.				
Shipped By:				Present on Quter Package					NI AWAL Supplied Plastic									
Hand Delivered									WAL Supplied Clear Glass									
D Ambient				Unbroken on Outer package					AWAL Supplied Amber Glass							· · · · · · · · · · · · · · · · · · ·		
AChilled				□Yes □No W/A					AWA Supplied VOA/TOC/TOX Vials									
Temperature	55 °C			Pr	esent on	Sample	3		ПА	mber	NClear П	Headsp	ace \square No	Headsp	ace			
Rec. Broken/Leak	ing I Yes No	ΠΝ/Α		ПУе		ίο ΓΙΝ	[/A		אח	on AW.	AL Sunn	lied Con	tainer	F				
Notes:				Unt	roken	n Samp	le		Not	es:		<u>110 a Con</u>			L			
				ПҮе	s. ON		í/A											
Properly Preserve	d VolYes □No	ΠΝ/Α		Notes:								\mathbf{N}						
Notes:													مان ف	17	· *			
												•		• •				
Rec. Within Hold YIYes II No									Disc	repanc	ies Betw	een Lab	els and	COC		TYes No		
Notes:									Note	es:								
·	4					· · ·							11 A.			· .	· .	
	i i					4								•				
		· · · · · · · · · · · · · · · · · · ·														_		
Bottle Type	Preservative	All pHs OK					·	· .				L			<u></u>			
Ammonia	$pH < 2 H_2SO_4$				ļ	· ·						:		·	<u> </u>			
COD	$pH < 2H_2SO_4$															· .		
Cyanide	PH>12 NaOH			·				·		- 1	<u> </u>	L		·	-			
Metals	pH <2 HNO ₃		• •															
NO ₂ & NO ₃	$pH < 2 H_2SO_4$	· · · · · · · · · · · · · · · · · · ·			·						· · · ·			·				
Nutrients	$pH < 2 H_2SO_4$			_			ļ					ļ			 	-		
<u>0&G</u>	pH <2 HCL			_						·····			1					
Phenois	$pH < 2 H_2SO_4$						ļ	· .						<u> </u>				
Sulfide	pH > 9NaOH, ZnAC					· .	_	- 	· · · ·		ļ	·		ļ				
TKN	$pH < 2 H_2SO_4$					ļ			·					-				
TUC	$pH < 2 H_3 PO_4$		•				ļ								·	·		
TPO ₄	$pH < 2H_2SO_4$	V								·	· .		······					
IFH	pH <2 HCL											·				+	+	
			•															
· · · · · · · · · · · · · · · · · · ·							<u> </u>	<u> </u>		·····				·				
·					· · · · · · · · · · · · · · · · · · ·		{		<u> </u>	···							+	
Procedure: 1 2)	Pour a small amour Pour sample from L Do Not din the ph r	t of sample in the id gently over wide	sampl a range	le lid e pH paper e or lid	·.						[]				:			
3, 4) 5) 6) 7)	If sample is not pres Flag COC and notify Place client convers Samples may be ad	served properly list y client for further i sation on COC	t its ex instruc	tension and tions	receiving	pH in the	appropria	ite co	lumn a	above			·		•			

All interpretations of log data are opinions based on inferences from electrical or other measurements. We do not guarantee the accuracy or correctness of any interpretation or recommendation and we shall not be liable or responsible for any loss, cost, damages or expenses incurred or sustained by anyone resulting from any interpretation or recommendation made by any of our employees or agents. REMARKS Rig: WFT UNIT 14125 Service Order # 138813 MELL LOGGED PER CUSTOMER REQUEST BHT 210. WELL SHUT IN APPROXIMATELY 1 MONTH PRIOR TO LOGGING OPERATIONS ACCORDING TO CUST Prints: Prints: EQUIPMENT DATA Bit Size Run No. Tool Type Tool No. Other Well Status FLOWING 1 CCL - Telemetry CTLA-123 Shurface Pressure GAMWA RAY GRTW-131 Status	CASING RECORD SIZE MT/FT GRADE TYPE JOINT TOP SURFACE STRING 9.625 N/A N/A SURF PROT. STRING 7.00 N/A N/A 4200' LINER TING 7.00 N/A 4200'	MAX. REC. TEMP. F Z10.1 deq/f EST. CEMENT TOP N/A N/A TIME VELL READY ROA TIME VELL READY ROA TIME VELL READY ROA TIME LOGGER ON BTM. 11:00 EQUIP. NO. 14125 LOCATION CASPER JAMES GIBBONS RECORDED BY MARK KERR JAMES GIBBONS VITNESSED BY ROB OUICK TUBING RECORD NUN NO. BIT FROM TO ONE 10.75 SURF 4200	LOG MEASURED FROM KELLY BUSHING G DATE 11-06-07 DATE 11-06-07 RUN NO. DNE DEPTH DRILLER 7000' DEPTH DRILLER 6842' BTH. LOG INTERVAL 6842' OPEN HOLE SIZE 10.75 TYPE FLUID MATER DENS. VISC.	COMPANY RASER TECH WELL #68-04 FIELD TRUCKEE GEOTHERMAL FIELD TRUCKEE GEOTHERMAL FIELD TRUCKEE GEOTHERMAL FIELD TRUCKEE GEOTHERMAL FIELD TRUCKEE GEOTHERMAL FIELD TRUCKEE GEOTHERMAL FIELD TRUCKEE GEOTHERMAL SE 1/4 SW 1/4 TWP.12N RGE43E ELEV. N/A ELEV. K	TEMPERATURE / GAMM. COLLAR LOG


































DEPTH SCALE: 5":100' VERSION: 70712117R" UP LOG 138813 MAINUP1 FINISH DEPTH: -3.9 Feet DIRECTION: UP DATE: 11/07/2007 TIME: 12:21 MODE: RECOMPUTE RECOMPUTED DATE: 11/07/2007 TIME: 13:39

































	6900								
Gamma Ray		<u></u>	TEMPE	RATURE					
0 API 150	0.0	I	DegreesFa	renheit 		300.0			
Collar Locator				DELTA	TEMPERATURE				
-18000 Millivolts 2000				-0.500 D	egF/Foot	0.500			
START DEPTH: 6912.1 DIRECTION: UP DATE: 11/07/2007 TIME: 18:59 MODE: RECOMPUTE RECOMPUTED DATE: 11/07/2007 TIME: 13:38 138813 MAINUP1									
UP LOG DEPTH SCALE: 5":168' VERSION: 76712117R"									

		DEPTH		DEPTH	UNITS
Collar Locator	- 3567	323.8	2929	281.3	Millivolts
Ganna Ray	8	1.3	94	243.2	API
DELTA TEMPERATURE	-8.656	99.9	-0,006	350.7	DegF/Foot
TOP DEPTH: 358.7 F	eet				
TH SCALE: 5":100'					/ERSION: 78712117R"



138813 UPRPT

Tenpe	rature		1
Weight Length Max. Diameter	5.14 lbs/2.33 kg 2.23 ft/0.68 m 1.375 in/34.93mm	<u>Temp. CFTA - 119</u>	

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01/01/88	12:00	0.0 F	Ver	Job
	Gamma Ray Bef	ore Survey (Calibration	
Ca	Tool Type: GRT-	WA	Serial No	: shallow
•########	Background C	alibrator	Standard	Units
	0.0	120.0	140.0	API
Delta Counts	Per Sec: 120.0	CP	S/API = 0.85	7
 ۱				
01/01/88	12:00	0.0 F	Ver	Job
	Gamma Ray Aft	er Survey Ca	alibration	
	Tool Type: GRT-	WA	Serial No	: shallow

Calibrator No:

0.0

Delta Counts Per Sec: 120.0 CPS/API = 0.857

			······			
01/01/88	12:00	0.0 F	Ver	Job		
	Temperature M	laster Survey	Calibration			
	Tool Type: C	FT-AA	Serial No:	shallow		I
					·	

120.0 140.0

Background Calibrator Standard

Units

API