

EXPANDED SELF-POTENTIAL SURVEY

ANIMAS PROSPECT
HIDALGO COUNTY, NEW MEXICO

Prepared for AMAX Exploration, Inc., Geothermal Group

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Plates (in back pocket)

1. Survey Lines, Swallow Fork Peak 7 1/2' Quadrangle
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3. " " , Steins " "
4. " " , Cotton City " "
5. (see Fig. 10, transparent overlay)

Introduction

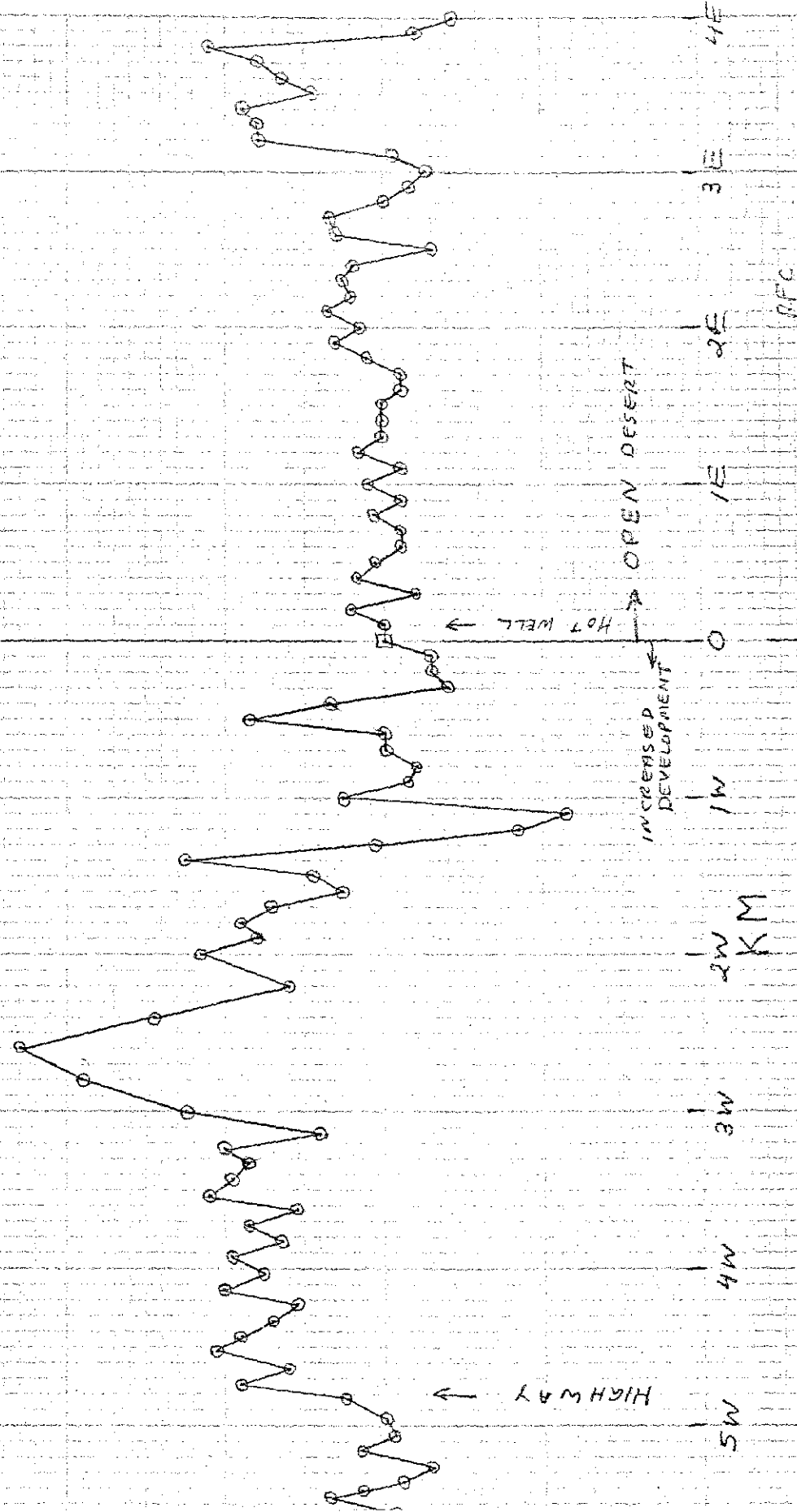
On 11-19 March, 1977, a self-potential survey covering approximately 120 km² was conducted in the Animas, New Mexico area. The locations of the survey lines are shown in Plates 1-4. Survey and data reduction procedures, data for three earlier lines, and a description of the equipment used are given in an earlier report (Corwin, 1977a) and will not be repeated here. This report includes listings (in the Appendix) and plots (Figs. 1-9) of the raw and corrected data for lines SP-1A and SP-3A, which are the westward extensions of two previous lines (SP-1 and SP-3, respectively) and seven additional lines (SP-4 through SP-9); a summary plot of the smoothed data from all nine lines (Fig. 10), and a brief discussion of the significance of the results. No significant telluric activity during the survey periods was seen on the telluric current monitor, and no corrections were made for telluric variations (the telluric monitor read between 6450 W and 6550 W on line SP-1; Plate 3).

Survey Results

1) Description of data

The corrected, unsmoothed data plotted at a horizontal scale of 1 in = 1 km for lines SP-1 through SP-9 is shown in Figs. 1-9 respectively. The data for all nine lines, smoothed by use of a 3-point running mean, is plotted at 1:62500 map scale in Fig. 10, and also included as an overlay as Plate 5. Each of the lines will be discussed briefly below, beginning with line SP-1 and moving first to the north and then to the south.

LECTED SELF-POTENTIAL DATA, LINES SP-1 AND 1A, ANIMAS, N.M.

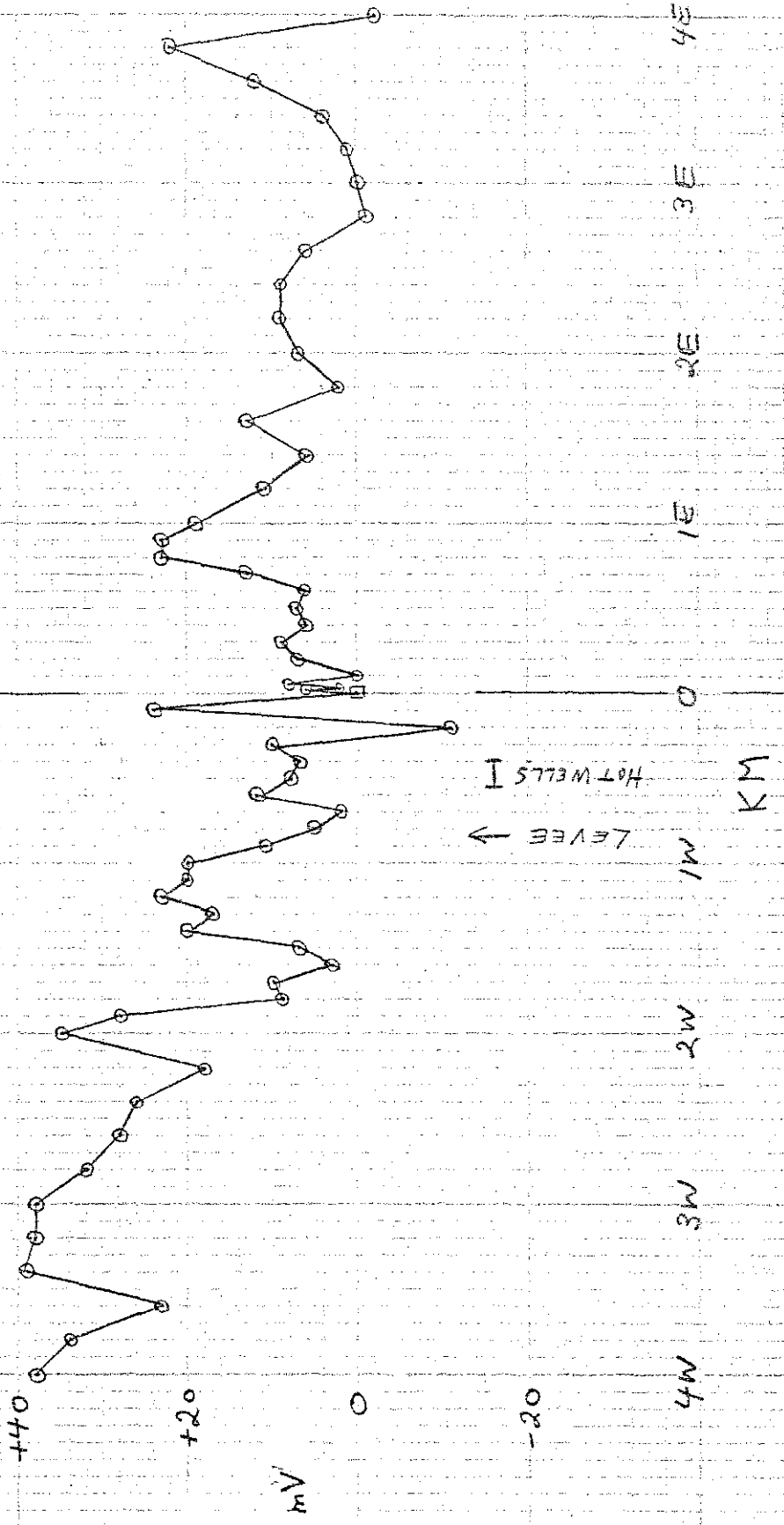


F 107.2

RFC
4-15-77

0,5P-1

CORRECTED SELF-POTENTIAL DATA LINE SP-2 ANIMAS, N.M.



HOT WELLS I
LEVEE →

O, SP-1

CORRECTED SELF-POTENTIAL DATA, LINES SP-3 AND 3A ANIMAS, N.M.

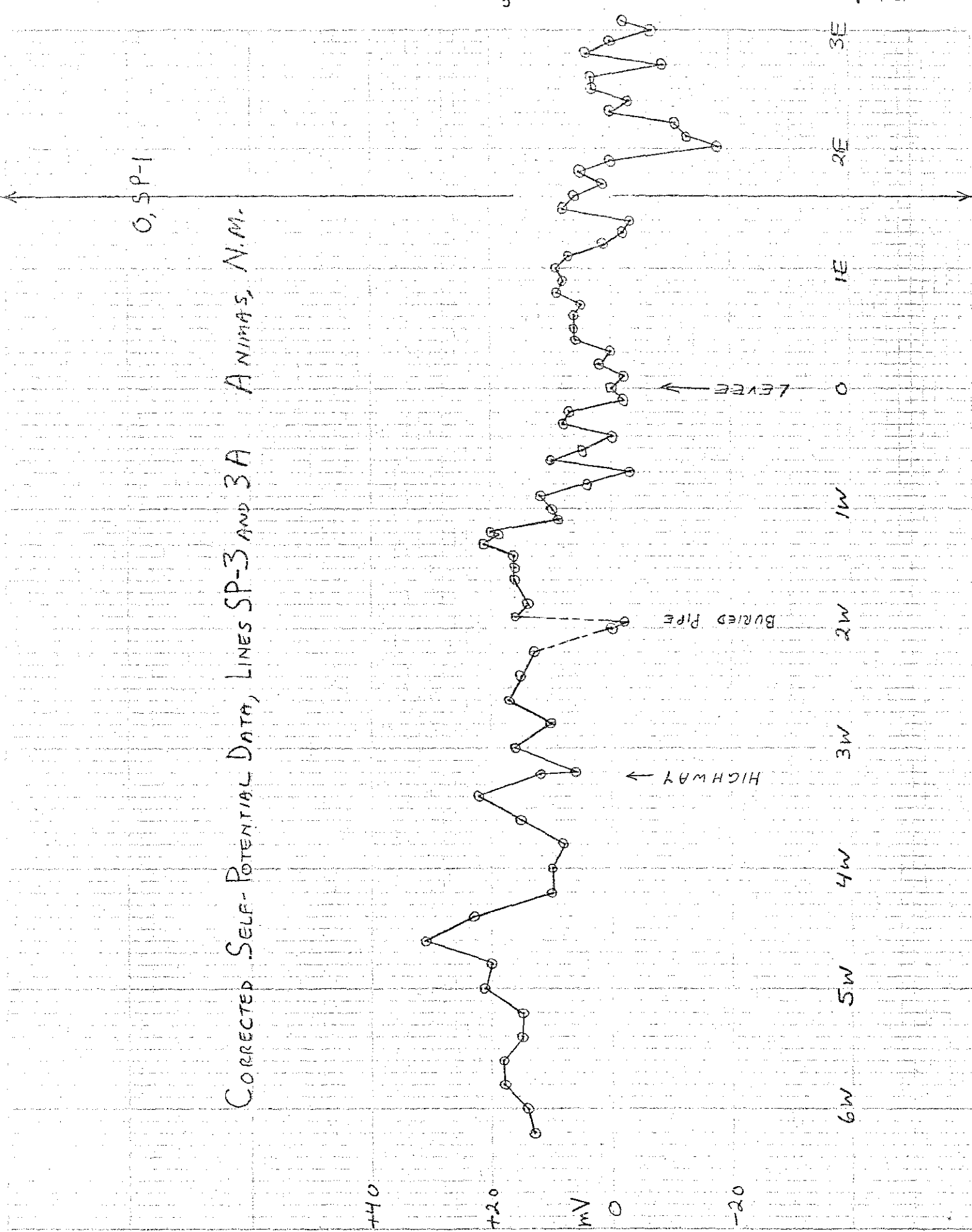
+40
+20
0
-20
mV

6W 5W 4W 3W 2W 1W 0 IE 2E 3E

HIGHWAY ←

BURIED PIPE ←

← LEVEE



CORRECTED SELF-POTENTIAL DATA LINE SP-4 ANIMAS, N.M.

O, SP-1

+40

+20

mV

-20

6W

5W

4W

3W

2W

1W

0

1E

2E

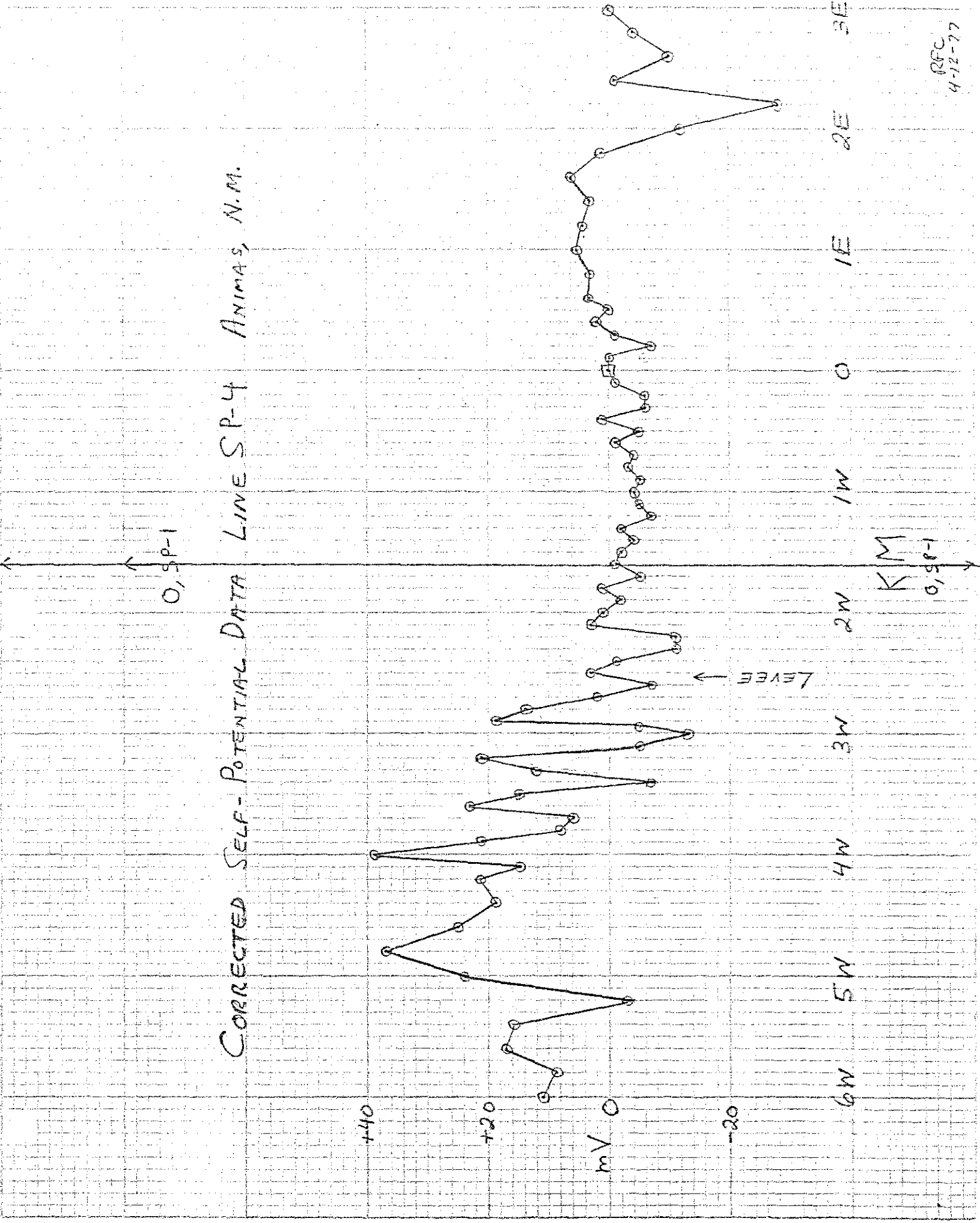
3E

LEVEL

KM

O, SP-1

RFC
4-12-77

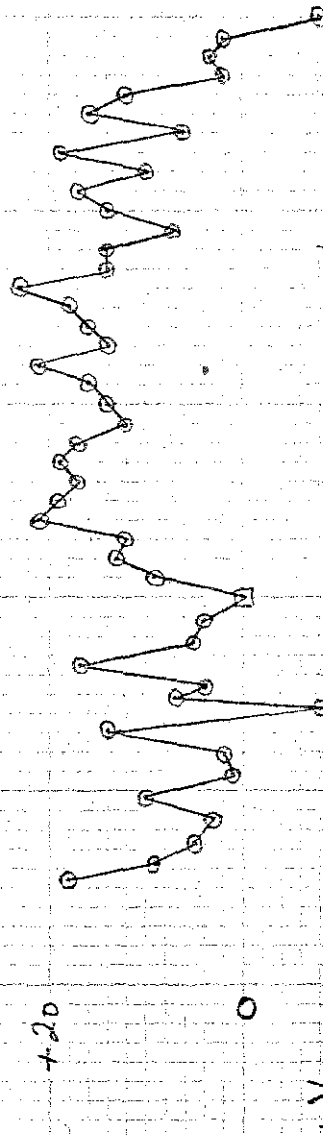


CORRECTED SELF-POTENTIAL DATA LINE SP-5

ANIMAS, N.M.

13 MARCH 77

O, SP-1



INCREASED DEVELOPMENT ←

→ OPEN DESERT

2W ← HIGHWAY

1W

0

1E

2E

3E

KM

RFC
4-13-77

V. G. V

CORRECTED SELF-POTENTIAL DATA LINE SP-6 ANIMAS, N.M. 14-15 MAR 77

0, SP-1

+20

mV

0

-20

LEVEL ←

5W

4W

3W

2W

1W KM

1E

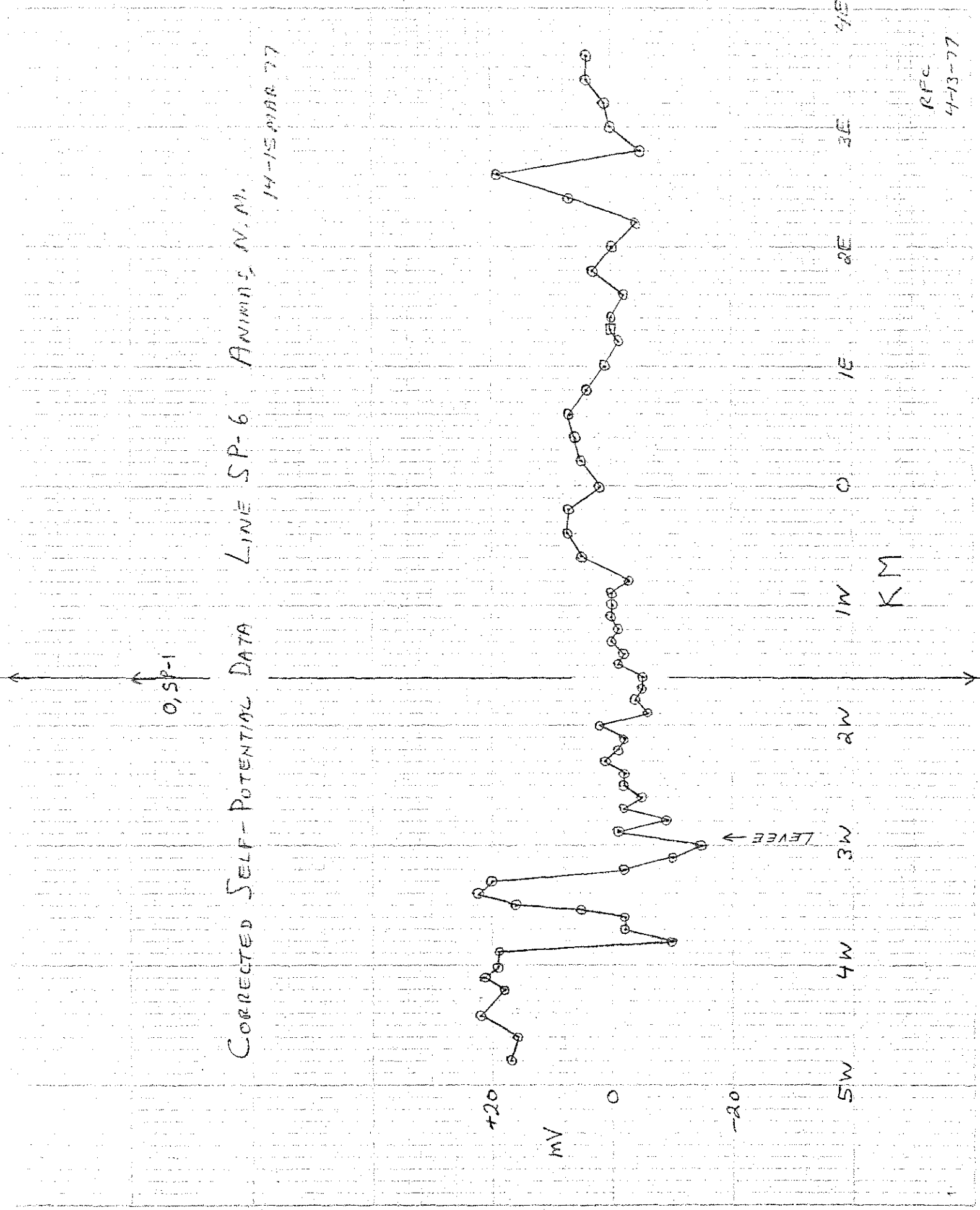
2E

3E

4E

RFC

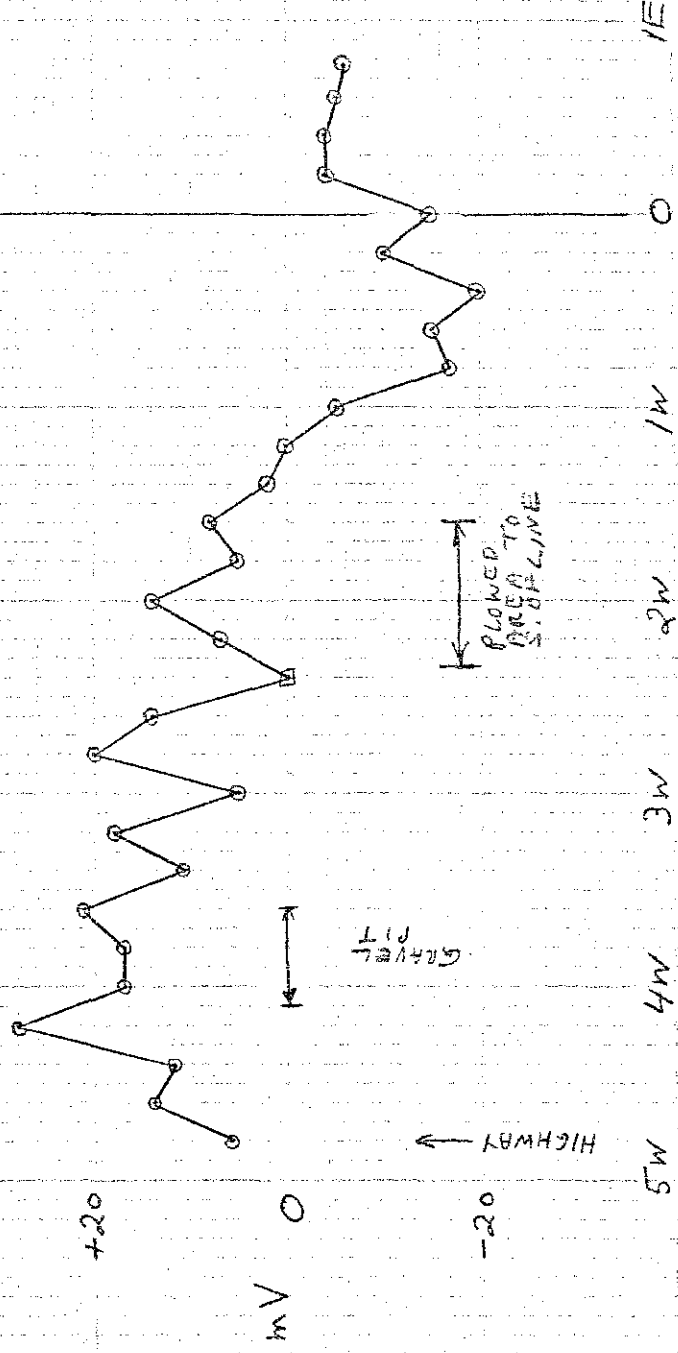
4-13-77



O, SP-1

CORRECTED SELF-POTENTIAL DATA LINE SP-7 ANIMAS, N.M.

17 MARCH 77

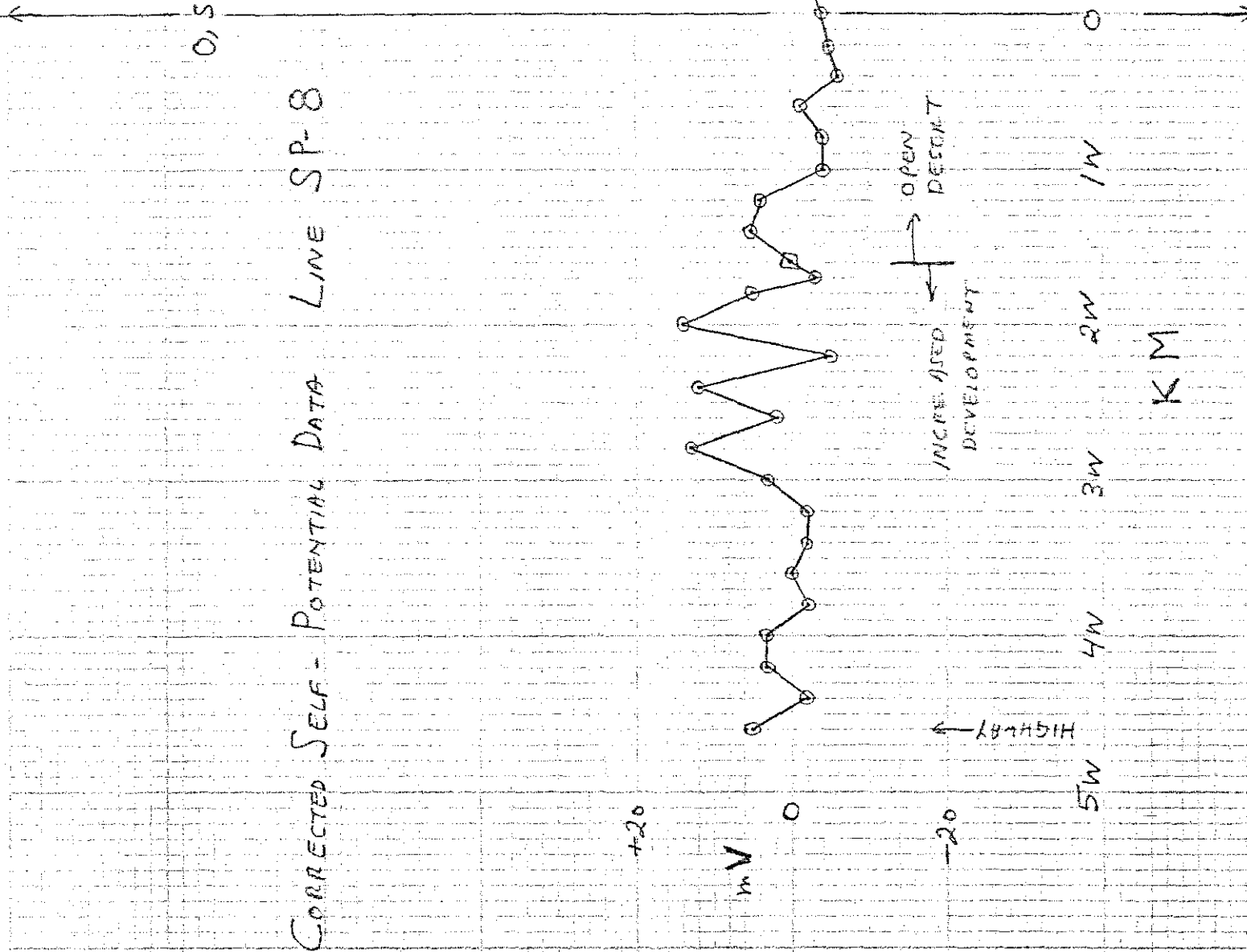


RFC
4-14-77

RFC
4-14-77

CORRECTED SELF-POTENTIAL DATA LINE SP-8 ANIMAS, N.M. 18 MARCH 77

0, SP-1



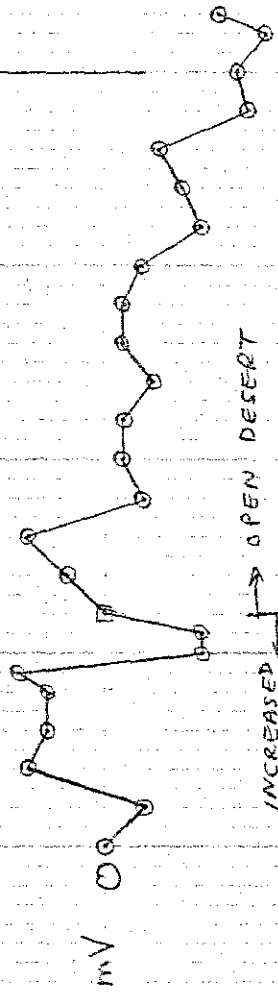
CORRECTED SELF-POTENTIAL DATA LINE SP-9 ANIMAS, N.M.

19 MARCH 77

0, SP-1

+20

mV



INCREASED DEVELOPMENT ←

→ OPEN DESERT

-20

4W

3W

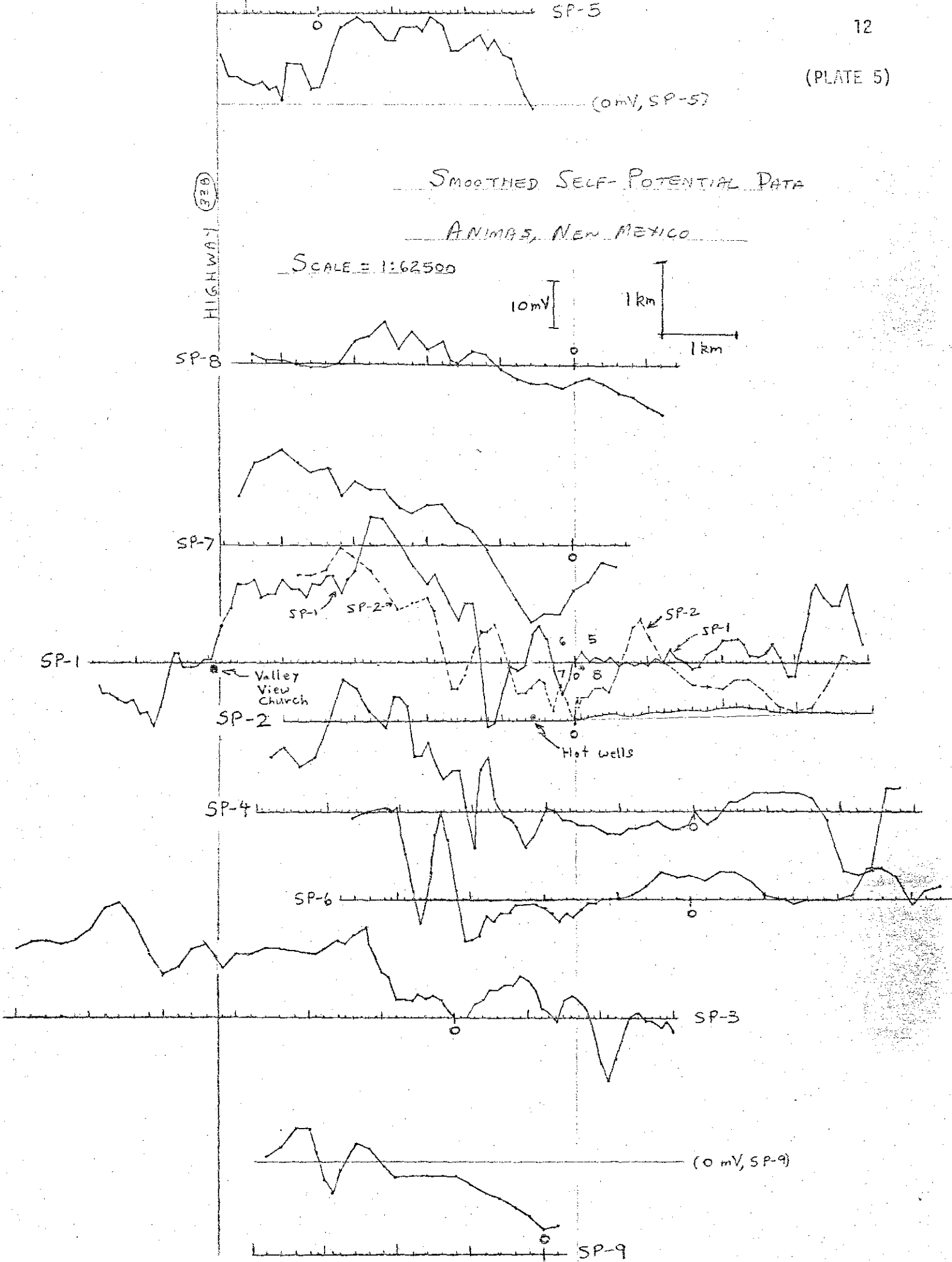
2W

1W

KM

REC

4-14-77



Line SP-1

The westward extension of line SP-1 revealed that the steep westward positive climb of the data to the west of the thermal area reverses at about 2.5 km W, forming a large, broad positive anomaly. Other features of this line are discussed in the previous report.

Line SP-2

Features of this line are discussed in the previous report. The levee separating the more developed area to the west from more open desert to the east (described below) is at 0.85 km W.

Line SP-4

This line is generally similar in character to line SP-1, showing the positive anomaly to the west, a "quiet zone" between about 2 W and 1.5 E, and a negative anomaly centered at about 2.2 E, similar in location but of opposite polarity to anomalies at roughly the same location on lines SP-1 and SP-2. A levee at 2.5 W marks a topographic break and a transition from generally open desert to the east to more built-up and heavily grazed (and possibly irrigated) conditions to the west. Many readings west of the levee were taken in soil which obviously had been disturbed by plowing, road shoulders, and heavy grazing. (These conditions apply to all lines to the west of the levee, or to the west of the onset of increased cultural development). The increased self-potential activity on line SP-4 appears to begin a few hundred m to the east of the levee.

Line SP-6

This line appears similar to line SP-4. The positive anomaly at 2.6 E is similar to but somewhat smaller than the similarly located anomalies on lines SP-1, SP-2, and SP-4, and the increased activity to the west again begins near the levee, which bears to the southwest between lines SP-4 and SP-6.

Line SP-3

The westward extension of line SP-3 showed a much smaller positive rise to the west than for the lines to the north, with no real indication of the positive anomaly seen to the west on lines SP-1 and SP-4. The levee is located at 0 km on SP-3 but there is no apparent change in the character of the data at the levee on this line.

Line SP-9

The positive westward rise of the data is still seen on line SP-9, although smaller in magnitude than on the lines to the north. The transition from open desert to the east to an area of large, actively pumping irrigation wells to the west takes place at 2.8 W. While there is an increase in self-potential activity at this point, it is not as large as that seen on the lines to the north, where the irrigation and pumping activity was much less. The small westward positive rise of the data from 0.3 km E to about 1 km W takes place in open desert, unlike the northern lines (SP-1 through SP-3) in which this trend is seen in a more developed area. An eastward extension of line SP-9 to see if a negative anomaly developed at 0 km would have been useful, but was precluded by lack of time and access.

Line SP-7

This line shows a strong similarity to line SP-2, with a well-developed negative anomaly centered at about 0.5 km W, most of which was mapped in open desert. Little effect was seen from a highly disturbed area running through a gravel pit from about 3.6 to 4.1 km W.

Line SP-8

Aside from a gentle westward rise, little activity is seen on this line. Unless it has moved considerably to the east, the negative anomaly of SP-7 is absent from SP-8. Open desert to the west begins at 1.6 W, and a definite increase in self-potential activity to the west correlates with increased development. The increased activity, however, is much smaller than that seen on the equally developed lines to the south of SP-7.

Line SP-5

Self-potential activity on SP-5 is considerably greater than on SP-8, with a suggestion of the steep rise and positive anomaly to the west characteristic of lines SP-7 through SP-6. Increased development to the west begins at 1.8 E on SP-5, but is not reflected in the data. In retrospect, it would have been worthwhile to extend this line to the east (access in this case is not difficult).

2) Importance of cultural activity

The most important question regarding this survey is whether the steep positive rise to the west and the negative area enclosing the known thermal activity (best seen on lines SP-7 and SP-2, but possibly present

on all the lines to the south of SP-7) are related to the thermal activity or are artifacts of cultural development. Arguing for a cultural origin for these features are the facts that moist and/or plowed ground have been known to produce positive self-potential readings, and that the onset of increased self-potential activity and a positive westward trend to the data are very closely coincident with such conditions on lines SP-8, SP-1, SP-6, and SP-9, although the effect is smallest on SP-9, where pumping and irrigation are greatest. However, the same type of conditions did not seem to affect the data on lines SP-5, SP-7 (where the single plowed area was 50 m to the south of the line), SP-2 (where a high level of self-potential activity persisted throughout the entire line), SP-4 (where the increased activity began several hundred m to the east of the levee), or SP-3. Also arguing against a cultural origin for the westward positive trend (and to some extent the increased noise level) in developed areas is the fact that there was no consistent correlation between soil type or degree of disturbance in these areas and the point-to-point variations or general trend of the data; e.g., moist, plowed areas did not always produce more positive readings, and obvious cultural disturbances such as the gravel pit on SP-7 and the heavy pumping and irrigation on SP-9 did not lead to variations as large as those seen in the known thermal area.

Obviously, it is impossible to decide definitely from the discussion above whether the observed self-potential variations are caused by thermal activity, cultural noise, or some combination of the two. As with any other geophysical data, the self-potential data must be considered along with all other available information about the area. From the material above, and in light of the discussion to follow, it seems that there is at least a good possibility that the negative anomaly enclosing the thermal area

and, to a lesser extent, the westward rise of the data are related to the thermal activity.

Relation of self-potential data to thermal activity

The relation of self-potential and geothermal activity in general was discussed in an earlier report (Corwin, 1977 a) and will not be repeated here. Some features of this expanded survey do, however, merit additional comment.

First, there is a definite resemblance between this data and that obtained at Roosevelt Hot Springs KGRA, Utah (Corwin, 1977 b), although the activity is at a smaller scale at Animas. In both cases a negative area seems to enclose the area of known thermal activity, roughly centered on a fault thought to act as a conduit for the thermal fluids (the Dome fault at Roosevelt, and a north-south trending fault which closely follows the section line passing through the zero of line SP-1 and extends from north of SP-5 to the hot wells on SP-2 (Reeder, 1957)). Also in both cases a positive anomaly seems to flank one side of the negative, although at Animas the positive roughly coincides with a low resistivity zone possibly related to a thermal water sink (Jiracek and Smith, 1976; Mazzella, 1976), while at Roosevelt the positive is on the opposite side of the fault from a similar low-resistivity zone (Ward and Sill, 1976 a and 1976 b). The negative anomaly on lines SP-7 and south, then, would appear to be the most significant feature of the data.

Second, the anomaly appearing at the eastern end of lines SP-1, SP-2, SP-4, and SP-6 is significant, as it occurs in an area of open, undeveloped desert. Quite possibly it is caused by a fault (or fault zone, based on its significant width). Although it is not known whether thermal activity occurs along the fault, an area of interest certainly is indicated.

Third, a striking similarity is seen between the self-potential pattern on the central lines (SP-7 through SP-4) and the map of temperature at 1 m depth given by Kintzinger (1956), shown in Fig. 11 (the 1:62500 plot may be overlaid on Fig. 11, as they are almost the same scale). The edge of the westward rise of the data on these lines corresponds to the western boundary of the thermal anomaly, with a similar, but smaller, rise at the eastern boundary. It is interesting that the same self-potential pattern appears to continue to the south of the observed shallow thermal anomaly.

Conclusions

Assuming that the features of the self-potential data are not significantly influenced by cultural development, and that the broad central negative anomaly and the steep westward rise are related to thermal activity, the northern boundary of the zone of maximum interest lies between lines SP-7 and SP-8 (although there is a hint of increasing activity on line SP-5). The zone appears to extend at least to line SP-6 on the south, and may extend, with diminishing amplitude (possibly indicative of increasing depth to the source) to line SP-9. The mechanism by which the anomalies are generated probably is a combination of thermoelectric coupling and streaming potentials (discussed in Corwin, 1977 a), but analytical techniques for relating the observed anomalies to source parameters are not yet developed.

meat and then returned to
 an, and do not attract any re-
 sults if living oysters are near.
 (*Merccnaria*) and mussels (*Fol-*
 placed in aquaria with *O. im-*
 and oysters, do not attract snails;
 that crawl on them do not stay

specimens and records of the Charles-
 Museum indicate that *O. impressa* is
 commonest *Odostomia* in South
 olina; it has been taken from a num-
 of localities by many collectors, start-
 with Edmund Ravenel prior to 1870.
 or (3) and various shell collectors'
 les mention that *O. impressa* often
 as on oyster beds. At Bears Bluff,
 of the population is found between
 above and 1 ft below mean low-
 or level. At the beginning of July
 the individuals collected ranged
 3.3 to 5.2 mm in height and aver-
 4.2 mm. These older snails soon dis-
 and, at the end of July they
 replaced by a younger group of
 0.7 to 3.3 mm high, with a mode at
 mm.

SEWELL H. HOPKINS
 Bears Bluff Laboratories, Wadmalaw
 Island, South Carolina, and A. & M.
 College of Texas, College Station

References

- 1. Loosanoff, *Science* 123, 1119 (1956).
- 2. T. Abbott, *American Seashells* (Van Nostrand, New York, 1954).
- 3. W. Miner, *Field Book of Seashore Life* (Van Nostrand, New York, 1950).

Geothermal Survey of Hot Ground near Lordsburg, New Mexico

In the late fall of 1954, newspapers
 reported live steam and boiling water is-
 suing from shallow wells being drilled in
 the area between the Pyramid and the
 Gila Mountains, 15 miles south-
 west of Lordsburg, N.M. Marx
 of the research and development
 division of the New Mexico Institute of
 Mining and Technology, made a pre-
 liminary examination of the area in De-
 cember 1954, at which time water sam-
 ples were collected for analysis. Shortly
 after it was recommended that a
 formal survey of the area be made.
 The locations of three principal wells
 in the area are shown by solid circles in
 Fig. 1. These wells penetrate approxi-
 mately 50 ft of sand and claylike soil
 underlain by 20 ft of warm-water-bearing
 gravel. The water-bearing gravel rests on
 a thickly impervious layer of clay that
 is approximately 8 ft thick, which in turn
 rests on rhyolite rock. As the drilling
 proceeds through the clay, the
 temperatures are encountered, and

the water becomes superheated as con-
 tact is established with the hot rhyolite.
 Two of the three wells were completed
 at 5 to 10 ft into the rhyolite. One of
 these behaved like a geyser when it was
 disturbed by the drilling tools. The third
 well, which was completed at the upper
 surface of the rhyolite, can be pumped
 at the rate of 200 to 300 gal of boiling
 water per minute.

A geothermal survey was made using
 resistance thermometers, with the ele-
 ments installed 1 m below the ground
 surface. The thermometers were made
 by installing a thermistor element at the end
 of a thin (0.25-in. diameter) Bakelite
 tube, which was subsequently filled with
 insulating material. Two fine copper
 wires connect the thermistor to extended
 leads at the upper end of the tube, where
 resistance measurements were made with
 a portable impedance bridge. The ther-
 mistor elements at 20°C had a resistance
 of 18,000 ohm and a sensitivity of ap-
 proximately 550 ohm per degree centi-
 grade. A hole for receiving the ther-
 mometer tube was made by driving a
 stake 4 ft in length into the ground, and
 the excess space around the tube was
 filled with dry sand. This arrangement
 gave steady-state resistance measure-
 ments 30 minutes after installation.

The temperature anomaly is mapped
 on Fig. 1 with a contour interval of 2°C.
 Points of temperature observation are in-
 dicated by open circles.

The maximum observed temperature
 at 1 m below the surface was 23°C, ap-
 proximately 12°C higher than the corre-
 sponding readings outside the anomalous
 region. At one station, a thermistor re-
 mained in the ground for 5 days, during
 which time the air temperature changed
 from -5°C to +22°C. However, no
 change in temperature at the 1-m depth
 was noted during this interval, and in
 general, during the time of the study, no
 changes of temperature at this depth were
 observed. One thermistor has been in-
 stalled permanently at a depth of 6 m
 for the purpose of detecting possible
 changes in ground temperatures at that
 depth throughout an extended period.

Temperature readings were taken at
 both 1- and 2-m depths at three locations
 in the warmest area, and a mean vertical
 gradient of 10°C/m was determined.
 Calculations based on a reasonable value
 of the heat conductivity of the earth ma-
 terial and the observed temperature gra-
 dient indicate a power flow of approxi-
 mately 7500 kw for the area enclosed by
 the 18°C contour line.

Ranchers of the neighborhood have
 noticed that the winter snows melt almost
 immediately over an area approximately
 0.5 mile in diameter in the neighborhood
 of the wells. Distinct changes occur in
 vegetation at the edges of the thermal

anomaly. This is especially striking to-
 ward the south end of the area, where
 the temperature contour lines are close
 together. On the southeast, creosote
 bushes begin to grow where the anomaly
 ends. On the southwest, the hot area cuts
 through a cotton field. Over the hot area,
 the cotton stalks grow only 6 in. tall,
 whereas off the anomaly they attain a
 height of about 2 ft. Aerial photographs
 show the outline of the hot region as re-
 vealed by changes in vegetation at the
 edges.

Three hypotheses might explain the
 origin of the heat: (i) Hot steam and
 vapors, ascending from great depth along
 faults and fractures, are the source of
 heat. (ii) A post-rhyolite and relatively
 recent intrusive has been emplaced be-
 neath the rhyolite and is the source of
 heat. (iii) The rhyolite is itself the heat
 source. Since, however, the rhyolite, if
 correlated with similar rhyolites in ad-
 jacent areas, is probably of mid- to late-
 Tertiary age, it is highly improbable that
 its original heat could be retained.

It is possible that further study will
 indicate the true heat source. In the
 meantime, it would appear desirable to
 employ modern core-drilling methods,
 using compressed air, for the purpose of
 drilling deeper into the rhyolite mass for
 more significant temperature measure-
 ments.

Because of the high thermal gradient,
 an attempt was made to detect possible
 potential differences generated by the
 differential movement of ions in an elec-
 trolyte subject to a temperature gradient
 (Soret effect). Ground potentials owing

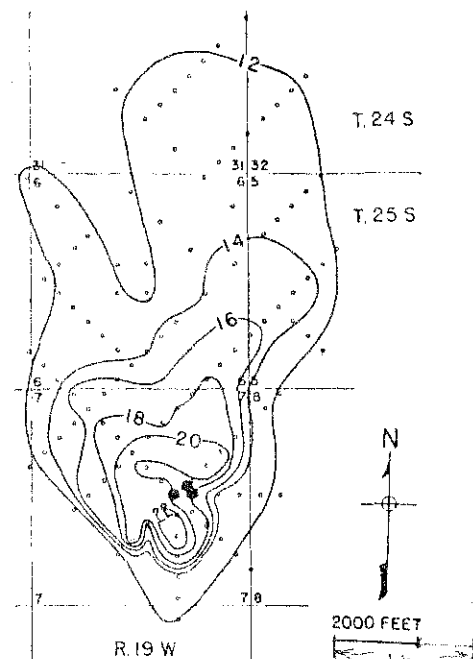


Fig. 1. Geothermal map. Temperature 1 m below surface; contour interval 2°C.

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- Ward, S.H., and Sill, W.R., 1976 a, Dipole-dipole resistivity delineation of the near-surface zone at the Roosevelt Hot Springs area: Technical report, vol. 76-1, ERDA contract E-1-76-S-07-1601, Univ. of Utah, Salt Lake City.
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APPENDIX

SELF-POTENTIAL DATA LINE SP-1A ANIMAS, N.M.

(Line SP-1A is the westward continuation of line SP-1)

(* Col. ④ includes +16 mV to tie 3670E on SP-1A to 2800W, SP-1) 11 March 77

| ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦ | ⑧ |
|----------------|---------------|--------------------------|--|----------------------------|------------------------------------|------------------------------|---|
| STATION (m) | TIME (MST) | ΔV_{RAW} (mV) | CORRECT, DELETE POLARIZAT. (mV) | ΔV_{FINAL} (mV) | 3-POINT RUNNING MEAN (mV) | STATION ON SP-1 (m) | COMMENT |
| 100E | 1244 | -29 | +21 | -8 | -7 | 6360W | (6460W on SP-1) at abandoned houses; power lines Soil is dry-appearing clay |
| 200E | 1254 | -27 | +21 | -8 | -8 | 6260W | |
| 300E | 1259 | -29 | +20 | -9 | -9 | 6160W | |
| 400E | 1304 | -29 | +20 | -9 | -8 | 6060W | |
| 500E | 1310 | -25 | +19 | -6 | -9 | 5960W | |
| 600E | 1317 | -32 | +19 | -13 | -11 | 5860W | |
| 700E | 1321 | -33 | +18 | -15 | -14 | 5760W | |
| 800E | 1331 | -33 | +18 | -15 | -10 | 5660W | |
| 900E | 1336 | -18 | +17 | -1 | -3 | 5560W | |
| 1000E | 1342 | -10 | +17 | +7 | +3 | 5460W | Soil dryer, loose N-S linear mound = pipeline? |
| 1050E | 1441 | -11 | +14 | +3 | +3 | 5410W | |
| 1100E | 1351 | -18 | +16 | -2 | -2 | 5360W | |
| 1200E | 1356 | -22 | +16 | -6 | -2 | 5260W | Previously cultivated. |
| 1300E | 1402 | -12 | +15 | +3 | -1 | 5160W | Soil wetter, muddy |
| 1400E | 1407 | -16 | +15 | -1 | +1 | 5060W | |
| 1500E | 1413 | -14 | +14 | 0 | +1 | 4960W | Cross road to N shoulder; disturbed |
| 1630E | 1427 | -9 | +14 | +5 | +8 | 4830W | Across highway, on N side |
| 2W | 1511 | -19 | +14 | -5 | -7 | 6462W | |
| 25W | 1506 | -21 | +14 | -7 | -5 | 6485W | |
| 100W | 1501 | -17 | +14 | -3 | - | 6560W | |
| 1700E | 1547 | +4 | +14 | +18 | +12 | 4730W | Reference now at 1630E |
| 1800E | 1552 | -2 | +14 | +12 | +17 | 4630W | |
| 1900E | 1556 | +7 | +14 | +21 | +17 | 4530W | |
| 2000E | 1601 | +3 | +15 | +18 | +18 | 4430W | |

LINE SP-1A (Cont'd)

| ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦a | ⑦ |
|-------|------|-----|-----|-----|-----|-------|--|
| 2100E | 1607 | -1 | +15 | +14 | +14 | 4330W | |
| 2200E | 1613 | -4 | +15 | +11 | +15 | 4230W | |
| 2300E | 1618 | +5 | +15 | +20 | +15 | 4130W | |
| 2400E | 1623 | -1 | +16 | +15 | +18 | 4030W | |
| 2500E | 1627 | +3 | +16 | +19 | +16 | 3930W | |
| 2600E | 1632 | -3 | +16 | +13 | +16 | 3830W | |
| 2700E | 1639 | +1 | +16 | +17 | +14 | 3730W | |
| 2800E | 1644 | -5 | +16 | +11 | +17 | 3630W | |
| 2900E | 1649 | -5 | +17 | +22 | +17 | 3530W | |
| 3000E | 1654 | +2 | +17 | +19 | +19 | 3430W | |
| 3100E | 1659 | 0 | +17 | +17 | +19 | 3330W | |
| 3200E | 1705 | +3 | +17 | +20 | +15 | 3230W | 6 m. E. of $\frac{1}{11} \frac{2}{12}$ |
| 3300E | 1712 | -10 | +18 | +8 | +18 | 3130W | |
| 3470E | 1724 | +7 | +18 | +25 | +20 | 3000W | |
| 3670E | 1734 | +10 | +18 | +28 | +30 | 2800W | |

LINE SP-3A

16 MARCH 77

(Continuation of line SP-3)

* Col. ④ includes +16mV to tie to line SP-3 at 1600W

| ① | ② | ③ | ④ * | ⑤ ✓ | ⑥ | ⑦ |
|--------|------|-----|-----|-----|-----|---|
| 1600W | 1326 | 0 | - | +16 | +15 | Ref. at 1600W; ΔV = +16mV |
| 1800W | 1333 | -8 | +22 | +14 | +15 | |
| 1900W | 1448 | -5 | +21 | +16 | +14 | |
| 1950W | 1444 | -19 | +17 | -2 | - | Exposed, buried pipeline? do not use data |
| 2000W | 1341 | -17 | +17 | 0 | - | |
| 2200W | 1347 | -8 | +21 | +13 | +15 | |
| 2400W | 1353 | -5 | +20 | +15 | +15 | |
| 2600W | 1358 | -2 | +19 | +17 | +14 | |
| 2800W | 1403 | -8 | +18 | +10 | +14 | |
| 3000W | 1408 | -2 | +18 | +16 | +11 | |
| 3200W | 1415 | -11 | +17 | +6 | +11 | E. shoulder of highway |
| 3200+W | 1424 | -5 | +17 | +12 | +13 | W. shoulder of highway |
| 3400W | 1527 | +4 | +18 | +22 | +16 | Reference now at 3200+W |
| 3600W | 1533 | -3 | +18 | +15 | +15 | |
| 3800W | 1542 | -10 | +18 | +8 | +11 | |
| 4000W | 1548 | -8 | +18 | +10 | +9 | |
| 4200W | 1555 | -8 | +18 | +10 | +14 | |
| 4400W | 1601 | +5 | +18 | +23 | +21 | |
| 4600W | 1608 | +13 | +18 | +31 | +25 | |
| 4800W | 1618 | +1 | +19 | +20 | +24 | |
| 5000W | 1624 | +2 | +19 | +21 | +19 | |
| 5200W | 1629 | -4 | +19 | +15 | +17 | |
| 5400W | 1634 | -4 | +19 | +15 | +16 | |
| 5600W | 1641 | -1 | +19 | +18 | +17 | |
| 5800W | 1646 | -1 | +19 | +18 | +17 | |
| 6000W | 1652 | -5 | +19 | +14 | +15 | |
| 6200W | 1700 | -6 | +19 | +13 | 0 | |

LINE SP-4

12 MARCH 77

| | ① | ② | ③ | ④ | ⑤ [✓] | ⑥ | |
|-------|------|------|----|-----|----------------|---|----------------------------------|
| | 0 | 0954 | 0 | - | 0 | - | At 1/4 sect. $\frac{319}{17916}$ |
| 100E | 1002 | -6 | +6 | 0 | -2 | | |
| 200E | 1008 | -12 | +5 | -7 | -3 | | |
| 300E | 1013 | -6 | +5 | -1 | -2 | | |
| 400E | 1019 | -2 | +4 | +2 | 0 | | |
| 500E | 1024 | -3 | +3 | 0 | +2 | | |
| 600E | 1031 | 0 | +3 | +3 | +2 | | |
| 800E | 1038 | +1 | +2 | +3 | +4 | | |
| 1000E | 1044 | +4 | +1 | +5 | +4 | | |
| 1200E | 1054 | +3 | +1 | +4 | +4 | | |
| 1400E | 1104 | +3 | 0 | +3 | +4 | | |
| 1640E | 1112 | +7 | -1 | +6 | +3 | | At section line |
| 1800E | 1121 | +2 | -1 | +1 | -2 | | |
| 2000E | 1131 | -10 | -2 | -12 | -13 | | |
| 2200E | 1139 | -25 | -3 | -28 | -14 | | |
| 2400E | 1146 | +2 | -3 | -1 | -13 | | |
| 2600E | 1156 | -6 | -4 | -10 | -5 | } 2 } ' At topographic break On steep up slope " | |
| 2800E | 1205 | +1 | -5 | -4 | -5 | | |
| 3000E | 1224 | +6 | -6 | 0 | - | | |
| 100W | 1427 | +5 | -6 | -1 | -3 | | |
| 200W | 1431 | 0 | -6 | -6 | -4 | | |
| 300W | 1438 | 0 | -6 | -6 | -4 | | |
| 400W | 1444 | +7 | -6 | +1 | -3 | | |
| 500W | 1451 | 0 | -5 | -5 | -2 | | |
| 600W | 1458 | +4 | -5 | -1 | -3 | | |

LINE SP-4 CONT'D

12 MAR 77

| ① | ② | ③ | ④ | ⑤ [✓] | ⑥ | ⑦ |
|-------|------|-----|----|----------------|-----|---|
| 700W | 1503 | +1 | -5 | -4 | -3 | |
| 800W | 1509 | +2 | -5 | -3 | -4 | |
| 900W | 1515 | 0 | -5 | -5 | -4 | |
| 1000W | 1522 | +1 | -5 | -4 | -5 | |
| 1100W | 1529 | 0 | -5 | -5 | -5 | |
| 1200W | 1534 | -3 | -4 | -7 | -5 | |
| 1300W | 1539 | +2 | -4 | -2 | -4 | |
| 1400W | 1545 | 0 | -4 | -4 | -3 | |
| 1500W | 1551 | +2 | -4 | -2 | -3 | |
| 1600W | 1602 | +5 | -4 | -1 | -3 | |
| 1700W | 1611 | -1 | -4 | -5 | -2 | |
| 1800W | 1616 | +5 | -4 | +1 | -2 | |
| 1900W | 1621 | +1 | -3 | -2 | 0 | |
| 2000W | 1626 | +4 | -3 | +1 | +1 | |
| 2100W | 1634 | +6 | -3 | +3 | -2 | |
| 2200W | 1639 | -8 | -3 | -11 | -6 | |
| 2300W | 1644 | -8 | -3 | -11 | -8 | |
| 2400W | 1651 | +2 | -3 | -1 | -3 | |
| 2500W | 1656 | +6 | -3 | +3 | -2 | |
| 2600W | 1702 | -5 | -2 | -7 | -1 | |
| 2700W | 1708 | +4 | -2 | +2 | +3 | |
| 2800W | 1712 | +16 | -2 | +14 | +12 | |
| 2900W | 1721 | +21 | -2 | +19 | +9 | |

Soft, wet soil. Plowed to 5.

LINE SP-4 CONT'D

20 MAR 77

* Cor. ① includes +19 mV for tie to 2900 W

| | ① | ② | ③ | ④* | ⑤✓ | ⑥ |
|------------|-----|-----|-----|-----|----|----------------|
| 2900W 0908 | - | - | - | +19 | | |
| 2950W 1254 | -11 | +6 | -5 | 0 | | Ref. at 2900W. |
| 3000W 0920 | -32 | +19 | -13 | -8 | | |
| 3100W 0924 | -23 | +18 | -5 | +1 | | |
| 3200W 0929 | +3 | +18 | +21 | +9 | | |
| 3300W 0933 | -5 | +17 | +12 | +9 | | |
| 3400W 0938 | -24 | +17 | -7 | +7 | | |
| 3500W 0949 | -1 | +16 | +15 | +10 | | |
| 3600W 0956 | +8 | +15 | +23 | +15 | | |
| 3700W 1001 | -9 | +15 | +6 | +12 | | |
| 3800W 1007 | -6 | +14 | +8 | +12 | | |
| 3900W 1012 | +9 | +13 | +21 | +23 | | |
| 4000W 1018 | +26 | +13 | +39 | +25 | | |
| 4100W 1029 | +3 | +12 | +15 | +25 | | |
| 4200W 1035 | +9 | +12 | +21 | +18 | | |
| 4400W 1042 | +8 | +11 | +19 | +22 | | |
| 4600W 1052 | +15 | +10 | +25 | +27 | | |
| 4800W 1059 | +27 | +10 | +37 | +29 | | |
| 5000W 1107 | +15 | +9 | +24 | +19 | | |
| 5200W 1117 | -11 | +8 | -3 | +12 | | |
| 5400W 1124 | +8 | +8 | +16 | +10 | | |
| 5600W 1132 | +10 | +7 | +17 | +14 | | |
| 5800W 1148 | +2 | +7 | +9 | +12 | | |
| 6000W 1155 | +5 | +6 | +11 | - | | |

LINE SP-5

ANIMAS N.M.

13 MARCH 77

| | ① | ② | ③ | ④ | ⑤ | ⑥ |
|-------|------|-----|----|-----|-----|---|
| 0 | 1152 | 0 | — | 0 | +4 | |
| 100E | 1158 | +5 | +4 | +9 | +8 | |
| 200E | 1203 | +11 | +4 | +15 | +13 | |
| 300E | 1207 | +11 | +3 | +14 | +17 | |
| 400E | 1212 | +18 | +3 | +21 | +18 | |
| 500E | 1218 | +17 | +2 | +19 | +19 | |
| 600E | 1223 | +15 | +2 | +17 | +18 | |
| 700E | 1227 | +18 | +1 | +19 | +18 | |
| 800E | 1232 | +16 | +1 | +17 | +16 | |
| 900E | 1236 | +12 | 0 | +12 | +14 | |
| 1000E | 1241 | +14 | 0 | +14 | +14 | |
| 1100E | 1251 | +17 | -1 | +16 | +17 | |
| 1200E | 1256 | +22 | -1 | +21 | +17 | |
| 1300E | 1303 | +16 | -2 | +14 | +17 | |
| 1400E | 1308 | +18 | -2 | +16 | +16 | |
| 1500E | 1313 | +21 | -3 | +18 | +19 | |
| 1600E | 1321 | +26 | -3 | +23 | +18 | |
| 1700E | 1327 | +18 | -4 | +14 | +17 | |
| 1800E | 1332 | +18 | -4 | +14 | +12 | |
| 1900E | 1341 | +12 | -5 | +7 | +12 | |
| 2000E | 1347 | +19 | -5 | +14 | +13 | |
| 2100E | 1353 | +23 | -6 | +17 | +14 | |
| 2200E | 1359 | +16 | -6 | +10 | +15 | |
| 2300E | 1404 | +26 | -7 | +19 | +12 | |
| 2400E | 1410 | +13 | -7 | +6 | +14 | |
| 2500E | 1418 | +26 | -8 | +16 | +11 | |

Ref. elect. ~ 2m E of metal cattle guard

Flat, grassy, heavily grazed
from 1300W to 1900E

"Culture" ends - relatively
undisturbed desert begins

LINE SP-5 (CONT'D)

| | ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦ |
|-------|------|-----|-----|-----|-----|-------------|-------------------------------|
| 2600E | 1422 | +20 | -8 | +12 | +10 | | |
| 2700E | 1429 | +11 | -9 | +2 | +6 | | |
| 2800E | 1433 | +12 | -9 | +3 | +2 | | |
| 2900E | 1441 | +12 | -10 | +2 | -1 | | |
| 2960E | 1446 | +2 | -10 | -8 | - | | |
| | | | | | | True meters | |
| 100W | 1621 | +14 | -10 | +4 | +3 | 115 | Paced distances: 100 to 115 m |
| 200W | 1626 | +15 | -10 | +5 | +9 | 230 | |
| 300W | 1631 | +26 | -9 | +17 | +9 | 345 | |
| 400W | 1636 | +13 | -9 | +4 | +9 | 460 | |
| 450W | 1758 | +16 | -9 | +7 | +1 | 518 | |
| 500W | 1642 | 0 | -8 | -8 | +4 | 575 | |
| 600W | 1648 | +26 | -8 | +14 | +3 | 690 | |
| 700W | 1653 | +10 | -8 | +2 | +5 | 805 | |
| 800W | 1659 | +9 | -8 | +1 | +4 | 920 | |
| 900W | 1706 | +17 | -7 | +10 | +5 | 1035 | |
| 1000W | 1711 | +10 | -7 | +3 | +6 | 1150 | |
| 1100W | 1718 | +12 | -7 | +5 | +6 | 1265 | |
| 1200W | 1723 | +15 | -6 | +9 | +11 | 1380 | |
| 1300W | 1729 | +24 | -6 | +18 | - | 1450 | 25m E of E edge of highway |

LIVE SP-6

ANIMAS, N.M.

14-15 MARCH 77

| ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦ |
|-------|------|-----|----|-----|----|---|
| 1300E | 1127 | 0 | - | 0 | 0 | Ref. at 1300E Begin 14 Mar. |
| 1400E | 1132 | -5 | +5 | 0 | -1 | |
| 1600E | 1139 | -6 | +4 | -2 | 0 | at $\frac{16}{21} \frac{15}{22}$ |
| 1800E | 1149 | -1 | +4 | +3 | 0 | |
| 2000E | 1157 | -3 | +3 | 0 | 0 | |
| 2200E | 1207 | -6 | +2 | -4 | +1 | |
| 2400E | 1214 | +5 | +2 | +7 | +7 | |
| 2600E | 1223 | +18 | +1 | +19 | +7 | |
| 2800E | 1231 | -5 | 0 | -5 | +5 | |
| 3000E | 1236 | 0 | 0 | 0 | -1 | |
| 3200E | 1250 | +2 | -1 | +1 | +2 | |
| 3400E | 1301 | +6 | -2 | +4 | +3 | |
| 3600E | 1316 | +6 | -2 | +4 | - | End line to E |
| 1200E | 1423 | +2 | -3 | -1 | 0 | |
| 1000E | 1456 | +4 | -3 | +1 | +1 | Ref. now at 1200E, +2 wrt 1300E |
| 800E | 1511 | +7 | -3 | +4 | +4 | +2 mV included in col. ③ for tie to 1300E |
| 600E | 1518 | +9 | -2 | +7 | +6 | |
| 400E | 1524 | +8 | -2 | +6 | +6 | |
| 200E | 1531 | +7 | -2 | +5 | +4 | |
| 0 | 1538 | +4 | -2 | +2 | +5 | at $\frac{17}{20} \frac{16}{21}$ |
| 200W | 1549 | +9 | -2 | +7 | +5 | |
| 400W | 1556 | +8 | -1 | +7 | +6 | |
| 600W | 1602 | +6 | -1 | +5 | +3 | |
| 800W | 1612 | -2 | -1 | -3 | +1 | End 14 Mar |

SP-6 CONT'D

15 MARCH 77

| | ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦ |
|-------|--|-----|----|-----------------|----|----|---|
| | * Cal. 4 includes -2 mV to tie to 800W | | | | | | |
| 3200W | 1013 | - | - | -* | -2 | +2 | Ref at 3200W, $\frac{13}{24} \frac{18}{19}$ |
| 3100W | 1028 | -9 | -1 | -10 | -9 | | |
| 3000W | 1033 | -14 | -1 | -15 | -9 | | |
| 2900W | 1044 | 0 | -1 | -1 | -8 | | Level at 2940W |
| 2800W | 1051 | -8 | -1 | -9 | -4 | | |
| 2700W | 1056 | -1 | -1 | -2 | -5 | | |
| 2600W | 1103 | -4 | -1 | -5 | -3 | | |
| 2500W | 1109 | -1 | -1 | -2 | -3 | | |
| 2400W | 1120 | -1 | -1 | -2 | -1 | | |
| 2300W | 1125 | +2 | -1 | +1 | -1 | | |
| 2200W | 1130 | 0 | -1 | -1 | -1 | | |
| 2100W | 1135 | -1 | -1 | -2 | -1 | | |
| 2000W | 1141 | +2 | -1 | +1 | -2 | | |
| 1900W | 1150 | -4 | -2 | -6 | -3 | | |
| 1800W | 1155 | -2 | -2 | -4 | -5 | | |
| 1700W | 1203 | -3 | -2 | -5 | -3 | | |
| 1600W | 1211 | -3 | -2 | -5 ^v | -4 | | |
| 1500W | 1217 | +1 | -2 | -1 | -3 | | |
| 1400W | 1226 | 0 | -2 | -2 | -1 | | |
| 1300W | 1233 | +2 | -2 | 0 | -1 | | |
| 1200W | 1239 | +1 | -2 | -1 | 0 | | |
| 1100W | 1245 | +2 | -2 | 0 | 0 | | |
| 1000W | 1251 | +2 | -2 | 0 | 0 | | |

SP-6 CONT'D

15 MARCH 77

| | ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦ |
|-------|------|-----|----|-----|-----|---|--|
| 900W | 1256 | +2 | -2 | 0 | -1 | | |
| 800W | 1303 | -1 | -2 | -3 | +1 | | End line to E |
| 3300W | 1451 | +23 | -3 | +20 | +13 | | Begin line to W. Ref 3200W |
| 3400W | 1457 | +25 | -3 | +22 | +19 | | |
| 3500W | 1502 | +19 | -3 | +16 | +14 | | |
| 3550W | 1515 | +8 | -3 | +5 | +6 | | |
| 3600W | 1509 | +1 | -3 | -2 | 0 | | |
| 3700W | 1521 | +1 | -3 | -2 | -5 | | |
| 3800W | 1526 | -7 | -3 | -10 | +2 | | |
| 3900W | 1532 | +22 | -3 | +19 | +10 | | |
| 4020W | 1539 | +22 | -3 | +19 | +20 | | |
| 4100W | 1544 | +24 | -3 | +21 | +19 | | |
| 4200W | 1549 | +21 | -3 | +18 | +20 | | |
| 4420W | 1700 | +25 | -3 | +22 | +19 | | |
| 4600W | 1616 | +19 | -3 | +16 | +18 | | |
| 4800W | 1625 | +20 | -3 | +17 | - | | at $\frac{19}{23} \frac{13}{24}$ End line to W |

LINE SP-7

ANIMAS, N.M.

17 MARCH 77

| | ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦ |
|-------|------|-----|----|-----|-----|---|---------------------------------|
| 2400W | 0927 | 0 | - | 0 | +8 | | Ref. at 2400W |
| 2200W | 0940 | +1 | +6 | +7 | +7 | | |
| 2000W | 0946 | +9 | +5 | +14 | +9 | | |
| 1800W | 0954 | 0 | +5 | +5 | +9 | | |
| 1600W | 1002 | +3 | +5 | +8 | +5 | | |
| 1400W | 1008 | -2 | +4 | +2 | +3 | | |
| 1200W | 1014 | -4 | +4 | 0 | -1 | | |
| 1000W | 1021 | -8 | +3 | -5 | -7 | | |
| 800W | 1027 | -20 | +3 | -17 | -12 | | |
| 600W | 1036 | -18 | +3 | -15 | -17 | | |
| 400W | 1043 | -22 | +2 | -20 | -15 | | |
| 200W | 1049 | -12 | +2 | -10 | -15 | | |
| 0 | 1059 | -17 | +2 | -15 | -10 | | At $\frac{31}{6} \frac{32}{15}$ |
| 200E | 1104 | -5 | +1 | -4 | -8 | | |
| 400E | 1111 | -5 | +1 | -4 | -4 | | |
| 600E | 1118 | -5 | 0 | -5 | -5 | | |
| 750E | 1122 | -6 | 0 | -6 | - | | Endred; end line to E |
| 2600W | 1327 | +16 | 0 | +16 | +12 | | |
| 2800W | 1337 | +20 | 0 | +20 | +14 | | |
| 3000W | 1343 | +5 | 0 | +5 | +14 | | |
| 3200W | 1351 | +18 | 0 | +18 | +11 | | |
| 3400W | 1359 | +11 | 0 | +11 | +17 | | |

LINE SP-7 (CONT'D)

17 MAR 77

| ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦ |
|-------|------|-----|---|-----|-----|------------------|
| 3600W | 1404 | +21 | 0 | +21 | +16 | At gravel pits |
| 3800W | 1411 | +17 | 0 | +17 | +18 | |
| 4000W | 1417 | +17 | 0 | +17 | +21 | |
| 4200W | 1424 | +28 | 0 | +28 | +19 | |
| 4400W | 1430 | +12 | 0 | +12 | +18 | |
| 4600W | 1437 | +14 | 0 | +14 | +11 | |
| 4800W | 1443 | +6 | 0 | +6 | - | At paved highway |

LINE SP-8

ANIMAS, N.M.

18 MARCH 77

| | ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦ | |
|------------|-----|----|-----|-----|---|-------------------|---------------------------------|--|
| 1600W 0849 | 0 | - | 0 | 0 | 0 | 0 | Ref. at 1600W, 1/4 sect., 25/30 | |
| 1400W 0859 | -4 | +9 | +5 | +3 | | | | |
| 1200W 0907 | -4 | +8 | +4 | +2 | | | | |
| 1000W 0913 | -12 | +8 | -4 | -1 | | | | |
| 800W 0921 | -11 | +7 | -4 | -3 | | | | |
| 600W 0927 | -8 | +7 | -1 | -4 | | | | |
| 400W 0938 | -12 | +6 | -6 | -4 | | | | |
| 200W 0945 | -11 | +6 | -5 | -5 | | | | |
| 0 0954 | -9 | +5 | -4 | -4 | | at 1/4 sect 29/30 | | |
| 200E 1001 | -7 | +4 | -3 | -3 | | | | |
| 400E 1007 | -7 | +4 | -3 | -4 | | | | |
| 600E 1018 | -10 | +3 | -7 | -6 | | | | |
| 800E 1027 | -10 | +3 | -7 | -7 | | | | |
| 1000E 1034 | -10 | +2 | -8 | -9 | | | | |
| 1200E 1041 | -13 | +1 | -12 | -11 | | | | |
| 1400E 1048 | -13 | +1 | -12 | - | | | End line to E | |
| 1700W 1221 | -3 | 0 | -3 | +1 | | | | |
| 1800W 1227 | +6 | -1 | +5 | +5 | | | | |
| 2000W 1232 | +15 | -1 | +14 | +3 | | | | |
| 2200W 1238 | -3 | -2 | -5 | +7 | | | | |
| 2400W 1245 | +14 | -2 | +12 | +3 | | | | |
| 2600W 1251 | +5 | -3 | +2 | +9 | | 50m. E. of houses | | |

LIVE SP-8 (CONT'D)

| | ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦ |
|-------|------|-----|----|-----|----|---|---|
| 2800W | 1302 | +16 | -3 | +13 | +6 | | |
| 3000W | 1308 | +7 | -4 | +3 | +5 | | |
| 3200W | 1316 | +2 | -4 | -2 | 0 | | |
| 3400W | 1327 | +3 | +5 | -2 | -1 | | |
| 3600W | 1333 | +5 | -5 | 0 | -1 | | |
| 3800W | 1340 | +4 | -6 | -2 | 0 | | |
| 4000W | 1347 | +9 | -6 | +3 | +1 | | |
| 4200W | 1354 | +10 | -7 | +3 | +1 | | |
| 4400W | 1401 | +5 | -7 | -2 | +2 | | |
| 4600W | 1408 | +13 | -8 | +5 | - | | |

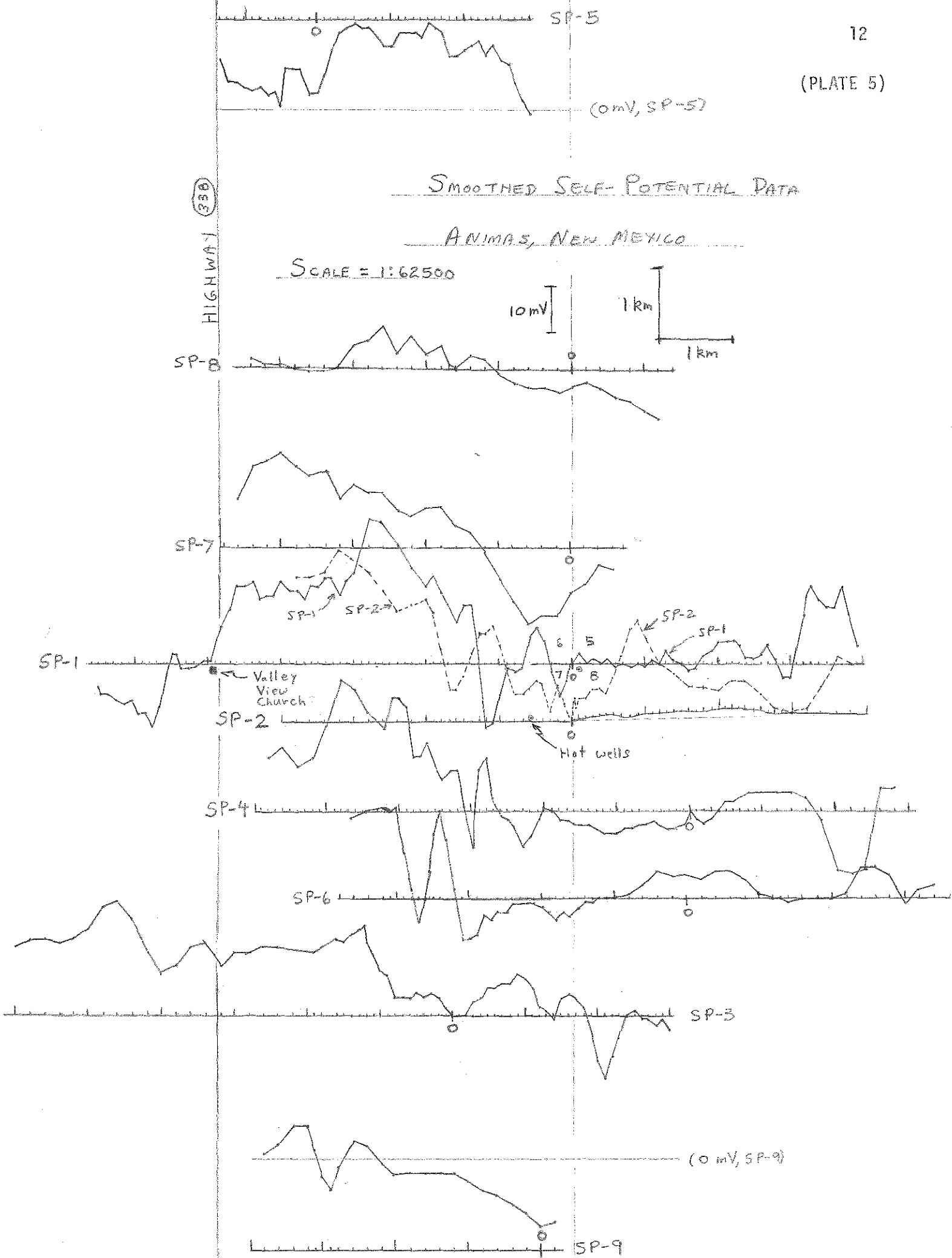
End line to W.

LINE SP-9

ANIMAS, N.M.

19 MARCH 77

| ① | ② | ③ | ④ | ⑤ | ⑥ | ⑦ |
|-------|------|-----|-----|-----|-----|-------------------------------|
| 2800W | 0859 | 0 | - | 0 | -2 | Ref. at 2800W. Power pde 20mW |
| 2600W | 0908 | +5 | -1 | +4 | +4 | |
| 2400W | 0918 | +9 | -1 | +8 | +3 | |
| 2200W | 0924 | -2 | -2 | -4 | -1 | |
| 2000W | 0931 | 0 | -2 | -2 | -3 | |
| 1800W | 0938 | +1 | -3 | -2 | -3 | |
| 1600W | 0944 | -2 | -3 | -5 | -3 | |
| 1400W | 0954 | +2 | -4 | -2 | -3 | |
| 1200W | 1001 | +2 | -4 | -2 | -3 | |
| 1000W | 1008 | +1 | -5 | -4 | -5 | |
| 800W | 1020 | -5 | -5 | -10 | -7 | |
| 600W | 1027 | -2 | -6 | -8 | -8 | |
| 400W | 1032 | 0 | -6 | -6 | -10 | |
| 200W | 1039 | -8 | -7 | -15 | -12 | |
| 0 | 1046 | -7 | -7 | -14 | -15 | |
| 200E | 1053 | -9 | -8 | -17 | -14 | |
| 300E | 1102 | -4 | -8 | -12 | - | 58m SW of S31/S32 |
| 2900W | 1331 | +1 | -11 | -10 | -7 | Note: wells, pumps, pipes |
| 3000W | 1221 | -2 | -8 | -10 | -4 | along line 2800W-4000W |
| 3100W | 1321 | +20 | -11 | +9 | +2 | |
| 3200W | 1227 | +14 | -8 | +6 | +7 | |
| 3400W | 1236 | +15 | -9 | +6 | +7 | |
| 3600W | 1244 | +17 | -9 | +8 | +3 | |
| 3800W | 1251 | +6 | -10 | -4 | +1 | |
| 4000W | 1257 | +10 | -10 | 0 | - | End line to W |





(338)

SMOOTHED SELF-POTENTIAL DATA

ANIMAS, NEW MEXICO

SCALE = 1:62500

10mV

1km

1km

HIGHWAY

SP-8

SP-7

SP-1

SP-2

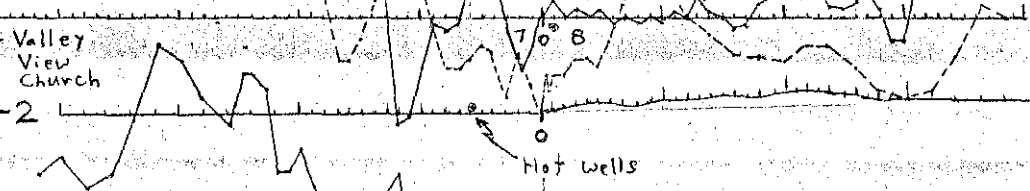
SP-4

SP-6

SP-3

(0. mV, SP-9)

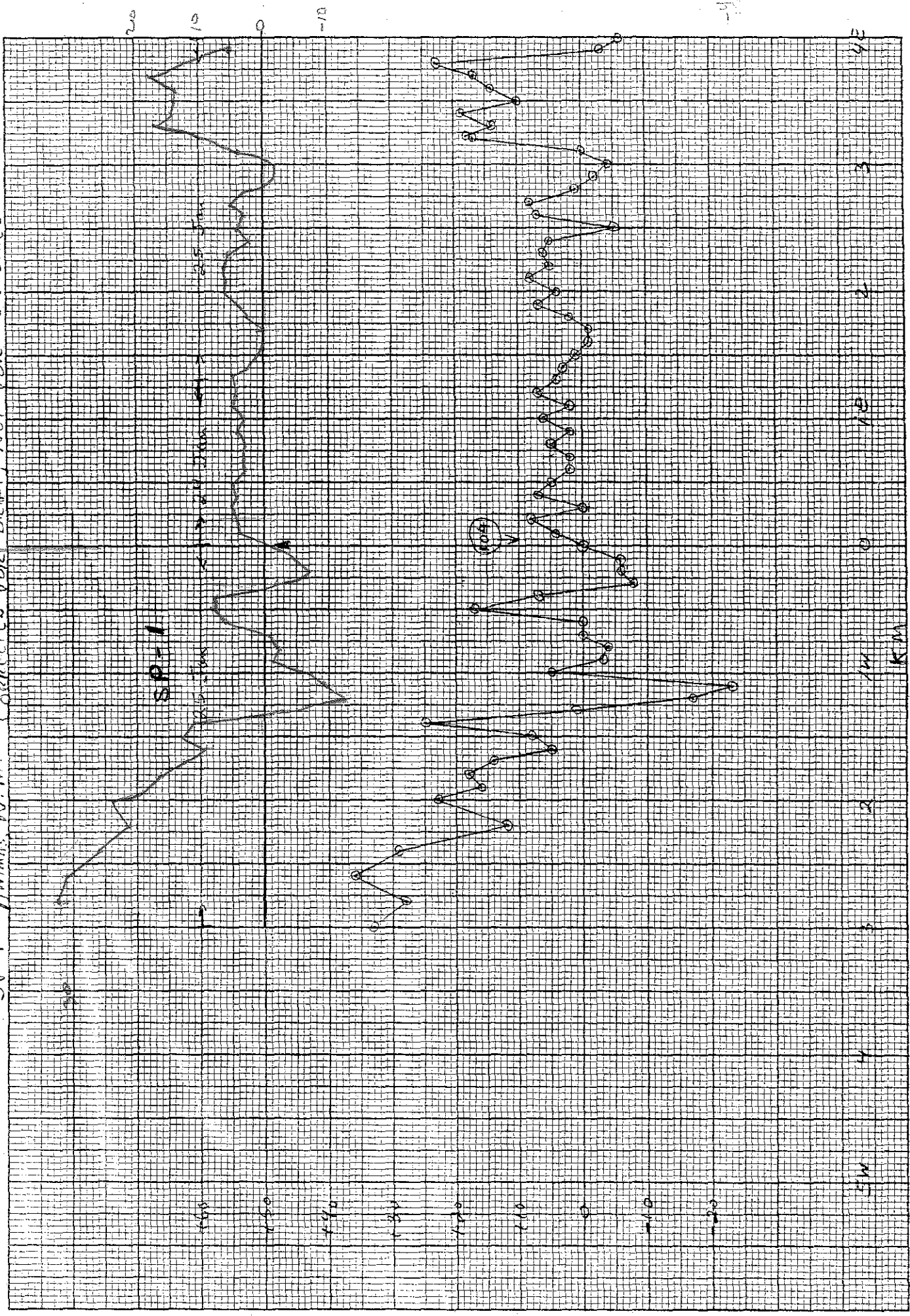
SP-9



10 X 10 TO 1/2 INCH 48 1322
7 X 10 INCHES
KEUFFEL & ESSER CO.

37 34-50 10
1 10 95 10

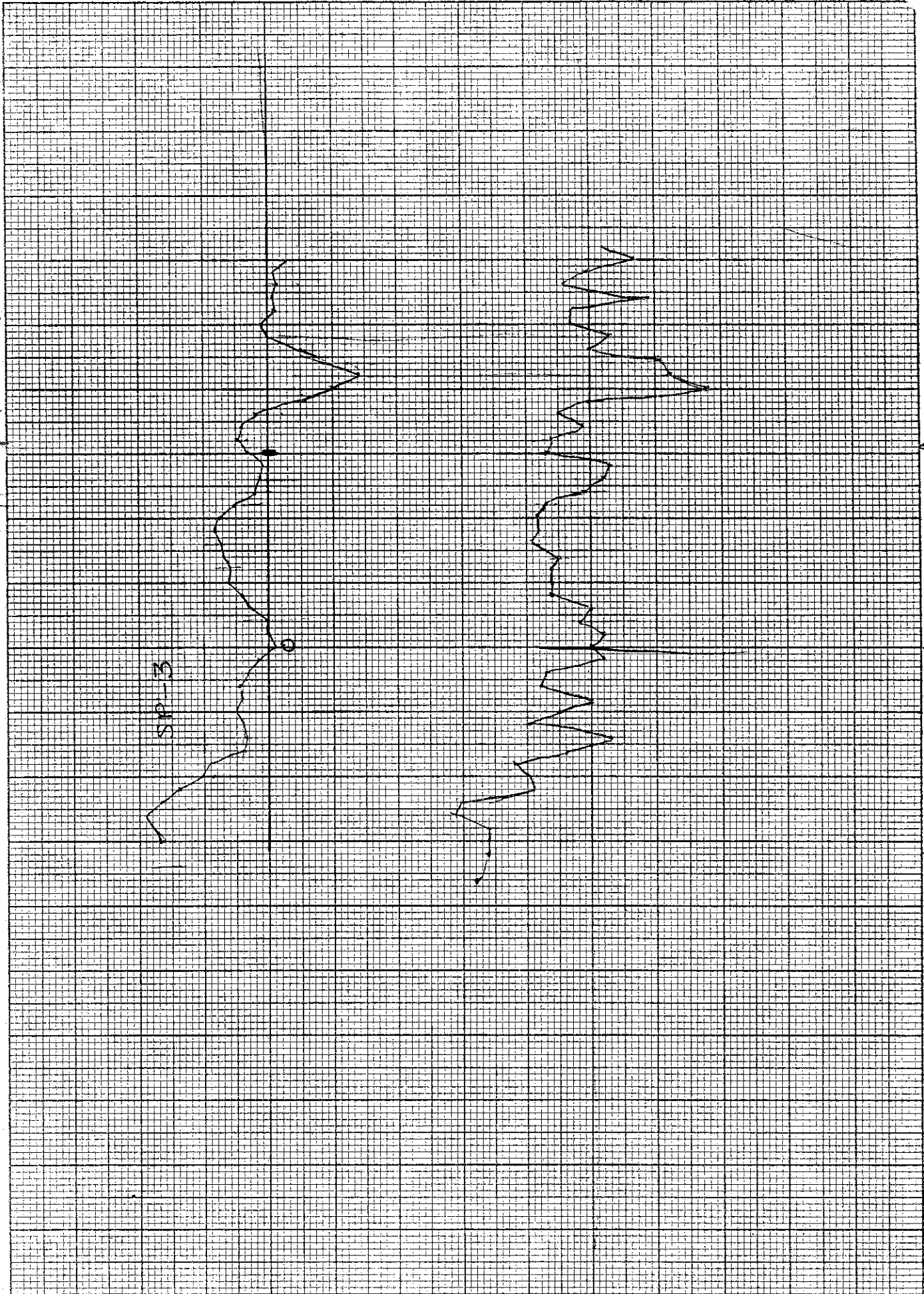
SP-1 Animas, N.M. CORRECTED FOR DEF. NOT FOR TELLURICS



KE 10 X 10 TO 1/2 INCH 46 1322
7 X 10 INCHES MADE IN U.S.A.
KEUFFEL & ESSER CO.

SP-3

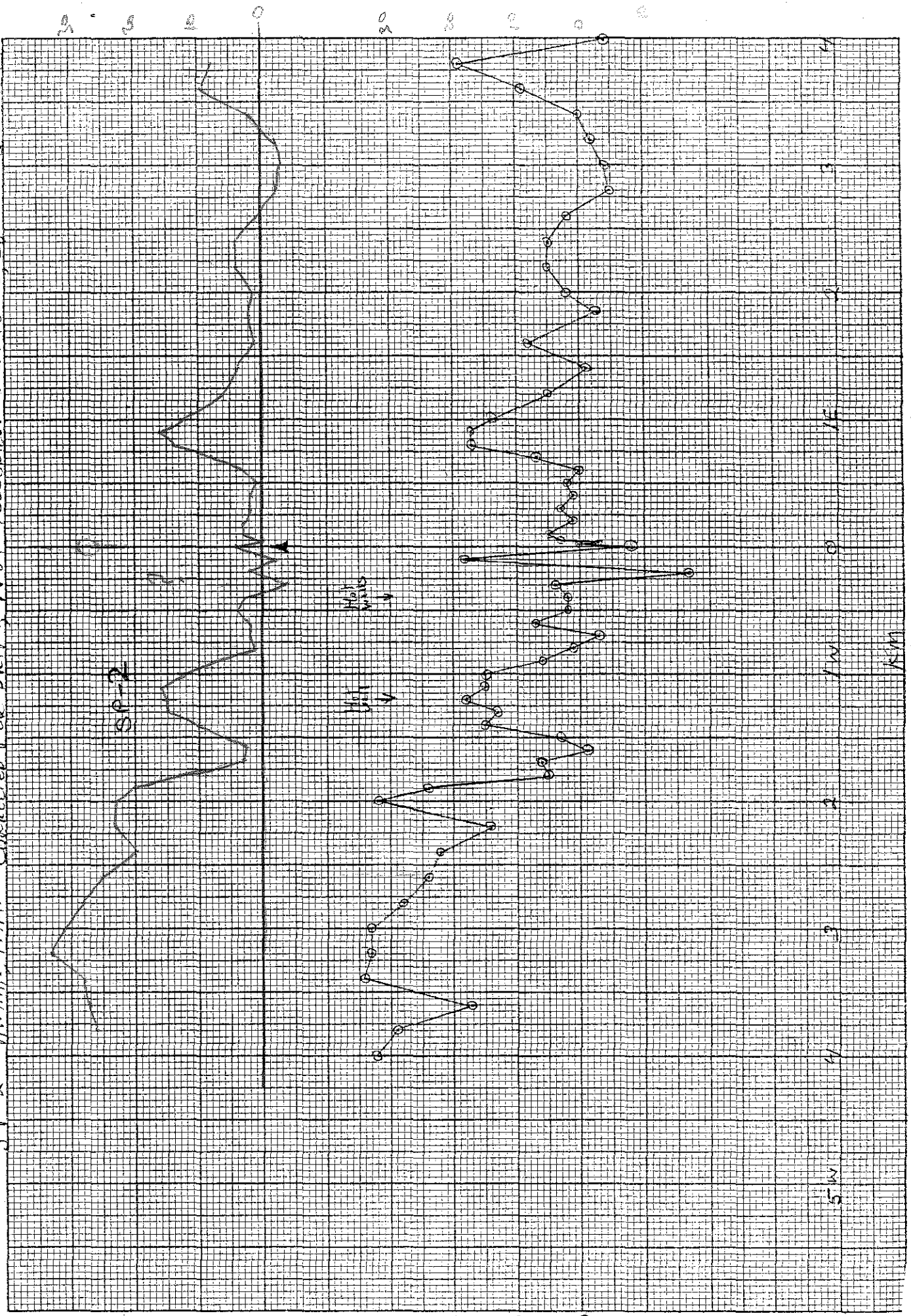
SP-3



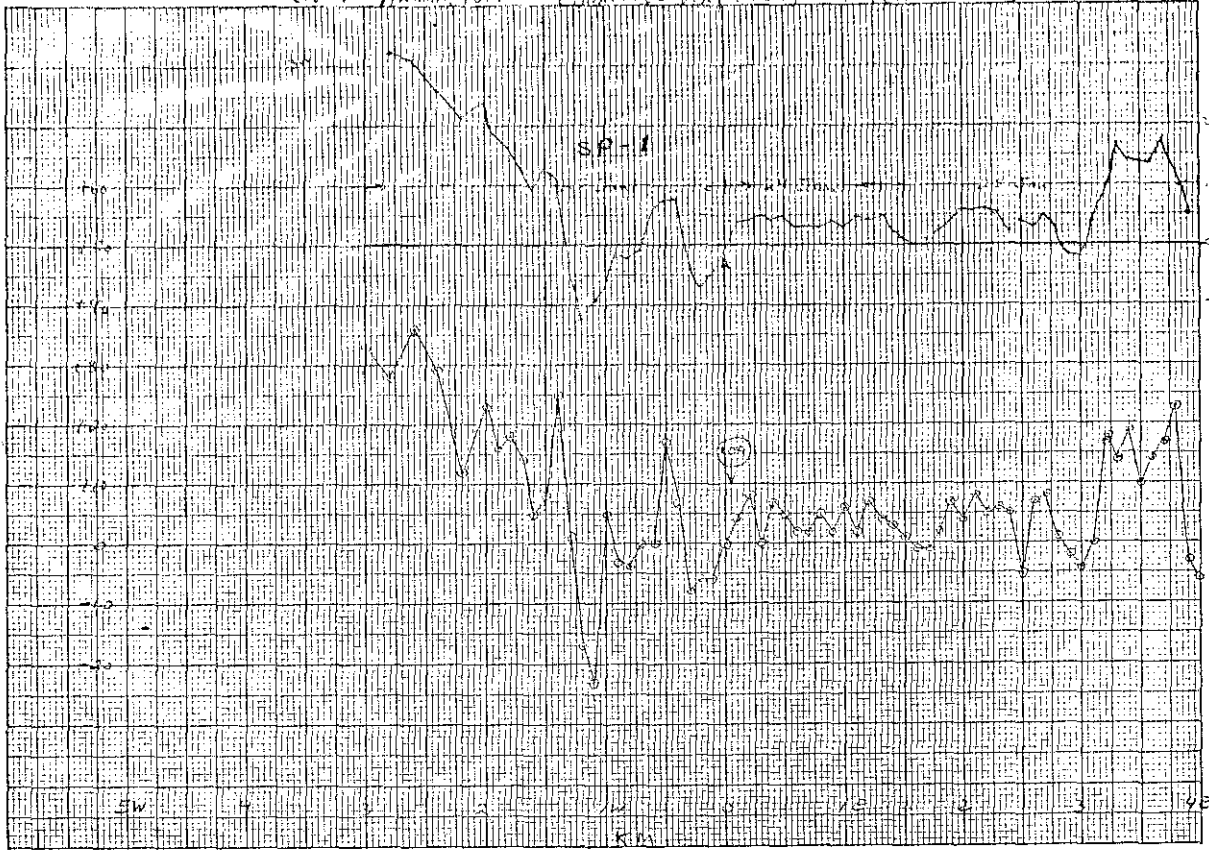
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14
TE
Saw

KE 10 X 10 TO 1/2 INCH 46 1322
7 X 10 INCHES
MADE IN U. S. A.
KEUFFEL & ESSER CO.

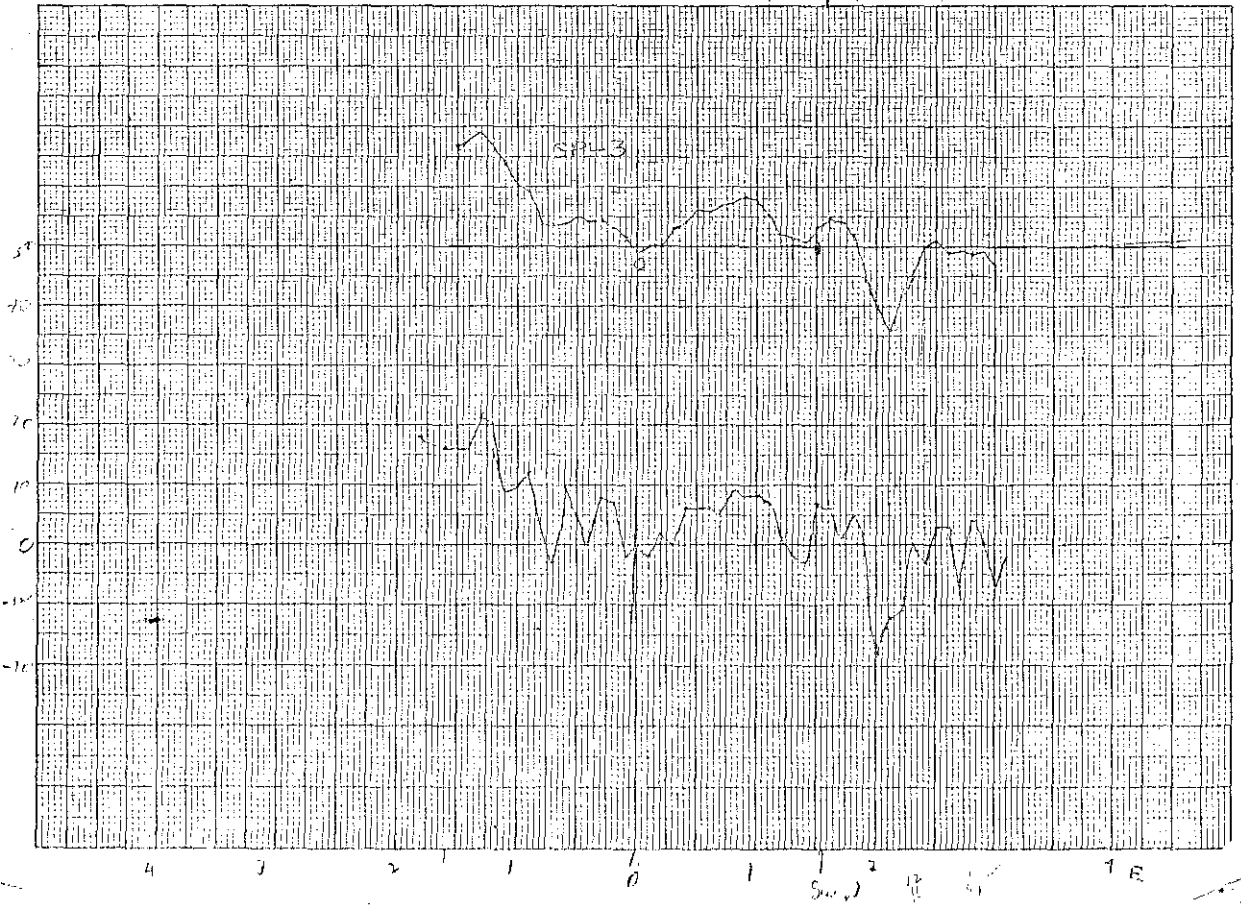
SP-2 ANIMAS, N.M. CORRECTED FOR DRIFT NOT TELLURIC. REC. TO O, SP-1 26 JAN 77



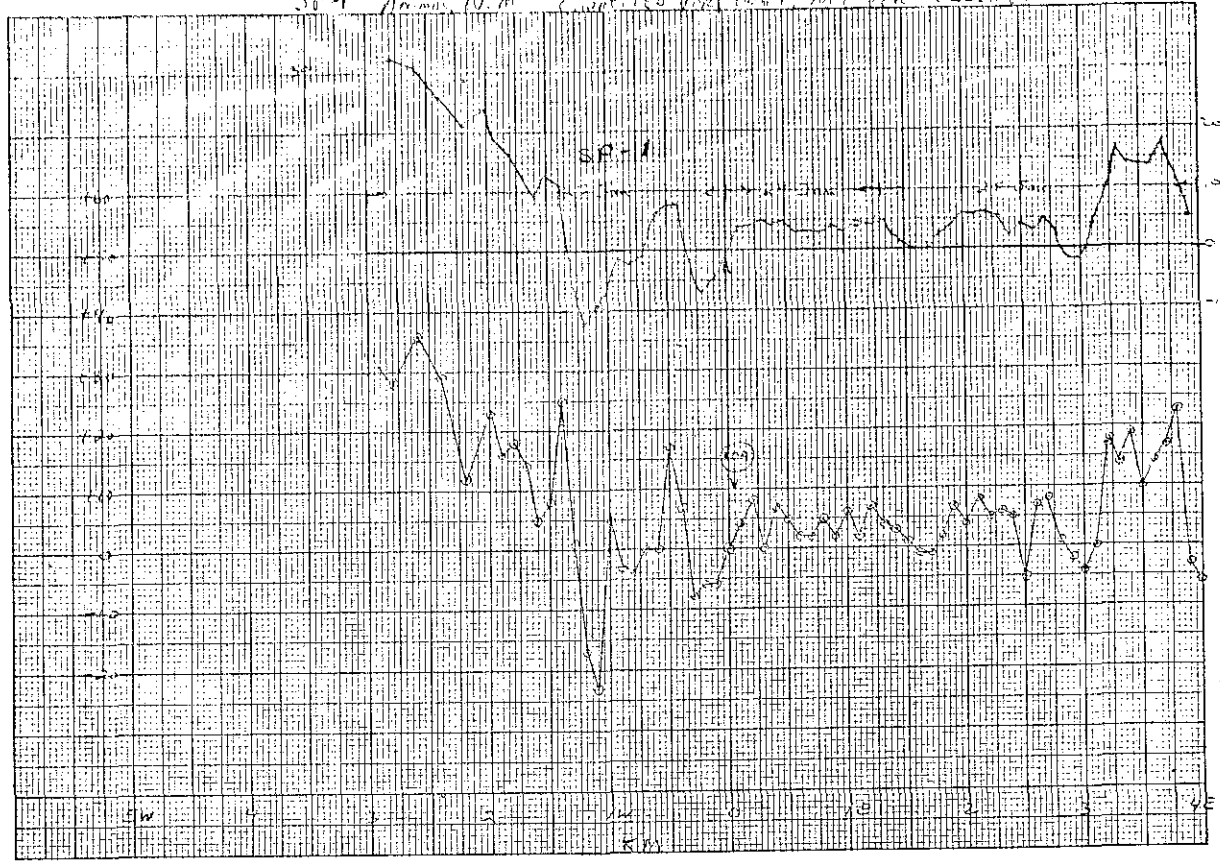
SP-1 Dennis N.M. Corrected for Dist. Air Fall Temperature



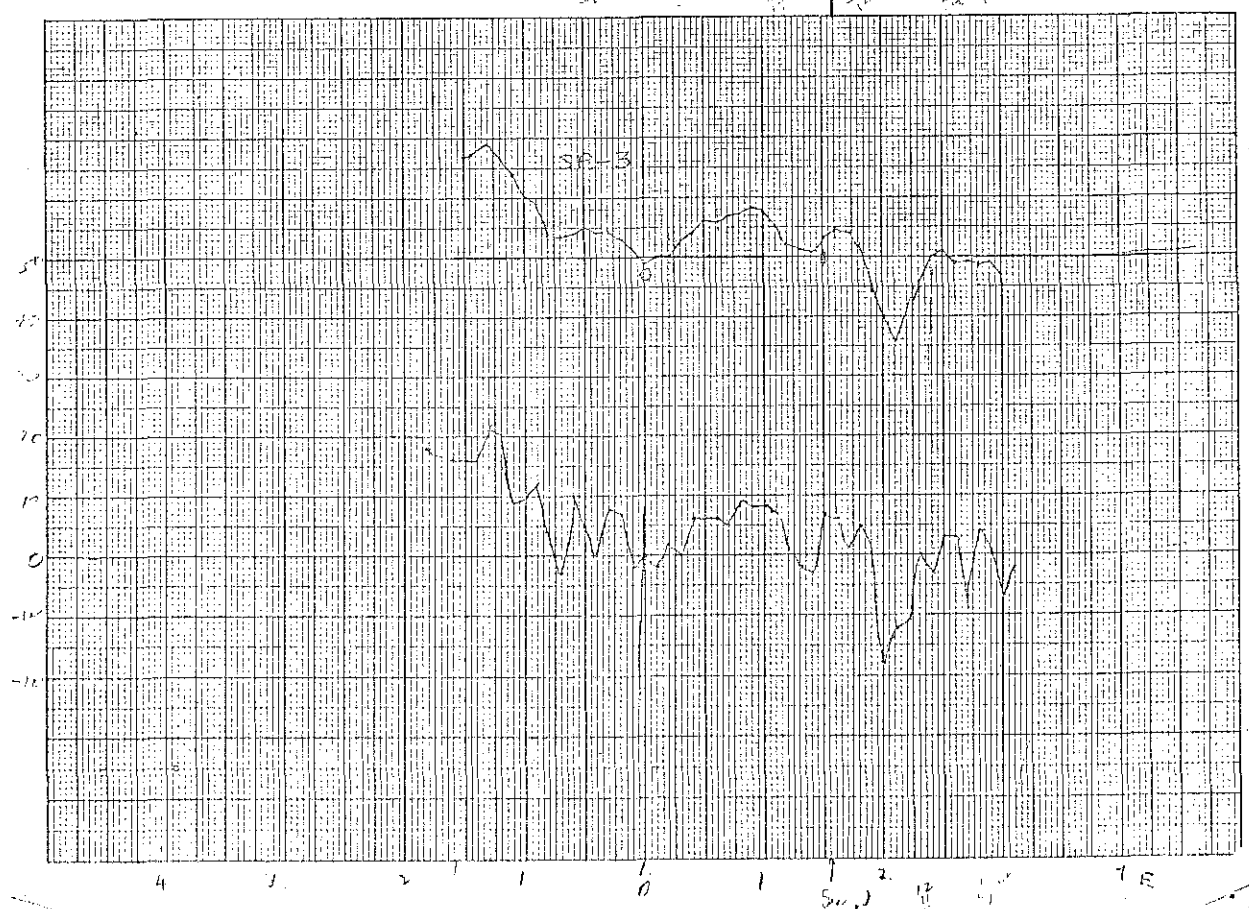
SP-3



SP-1 Annu. N.M. (WPT. 150) For NORTHERN FILL TOLLING



SP-3



ANIMAS SP

| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|--------|---------------|-----------------------|------------------|--------------------|--------------------|------|--------------|
| STA | MST TIME | DRIFT Δ | V _{obs} | V _{corr.} | Survey Ref. Adjust | | |
| LINE A | 19 Mr 79 | ADD | ms | | | | |
| 1 | A0 | 1340 | 0. | 0. | 0. | | |
| 2 | a | 1340 | 0. | -6.8 | -6.8 | | |
| 3 | 200 | 1350 | 0. | -5.0 | -5.0 | | |
| 4 | 400 | 1400 | -.1 | 0.0 | -.1 | | |
| 5 | 600 | 1410 | -.1 | +4.0 | +4.1 | | |
| 6 | 1/4 SUN (800) | 1419 | -.1 | -2.0 | -2.1 | | |
| 7 | 1000 | 1429 | -.1 | +3.0 | -3.1 | | |
| 8 | 1200 | 1439 | -.1 | -7.6 | -7.6 | | |
| 9 | 1400 | 1449 | -.2 | 0.0 | -.2 | | |
| 10 | + (1600) | 1450 | -.2 | -5.5 | +5.7 | | |
| 11 | 1800 | 1500 | -.2 | -3.0 | -3.2 | | |
| 12 | 2000 | 1508 | +.2 | -3.0 | -3.2 | | |
| 13 | 2200 | 1517 | +.2 | -1.0 | -1.2 | | |
| 14 | 1/4 S (2400) | 1529 | +.2 | -2.0 | -2.2 | | |
| 15 | 2600 | 1600 | -.3 | +4.0 | -14.3 | | |
| 16 | 2800 | 1606 | -.3 | -5.0 | -5.3 | < | ← Tie with C |
| 17 | a' | 1730 | -.5 | +6.8 | -6.8 | | |
| 18 | | | ADD | | | | |
| 19 | DRIFT: | 1340 - 1409 | 0. | | | | |
| 20 | TIME | 1400 - 1444 | -.1 | | | | |
| 21 | -5 | 1445 - 1529 | -.2 | | | | |
| 22 | | 1530 - 1614 | -.3 | | | | |
| 23 | | 1615 - 1700 | -.4 | | | | |
| 24 | | 1700 - 1730 | +.5 | | | | |
| 25 | LINE B | 20 Mr 79 | | | Subst. 35m | | |
| 26 | 0 | 0930 | | 0. | | | |
| 27 | b | 0930 | | +4.8 | | | |
| 28 | A 0 | 0934 | -.33 | 3.8 | 3.47 | 0. | |
| 29 | 200 | 0950 | -.83 | 2.7 | 1.87 | -1.6 | |
| 30 | 400 | 0956 | -1.1 | 1.6 | 0.5 | -2.9 | |
| 31 | 600 | 1001 | -1.3 | 2.4 | 6.1 | +2.6 | |
| 32 | 1/4 S 805 | 1007 | -1.5 | 0.5 | -1.0 | -4.5 | |
| 33 | 1000 | 1014 | -1.8 | 11.5 | 9.7 | +6.2 | |
| 34 | 1200 | 1020 | -2.1 | 3.8 | 1.7 | -1.7 | |
| 35 | 1400 | 1026 | -2.3 | 8.9 | 6.6 | 3.1 | |
| 36 | 1610 | 1033 | -2.6 | 7.1 | 4.5 | 1.0 | |
| 37 | 1800 | 1040 | -2.9 | 9.2 | 6.3 | 2.0 | |
| 38 | 1/4 SUN 2000* | 1047 | -3.19 | 9.0 | 5.8 | 2.3 | |
| 39 | b | 1121 | -4.6 | +9.4 | +4.80 | 1.3 | |
| 40 | DRIFT | 9.4 - 4.8 = 4.6 | | | | | |
| | | 1120 - 0930 = 110 min | 2.49 mi/hr | | | | |

| STA | MST | +2.2/kw | | | | | |
|---------------|-----------|----------|------------------|-------------------|-----------------------|---|---|
| LINE C | TIME | DRIET Δ | V _{obs} | V _{corr} | V _{adjusted} | | |
| | 20 Apr 29 | ADD | | | | | |
| 0 | 12.20 | | 0 | 0 | -8.5 | | |
| 0b | 12.20 | | -2.3 | | | | |
| 200 | 12.31 | -0.04 | -0.6 | -0.6 | -9.1 | | |
| 400 | 12.40 | -0.07 | -2.6 | -2.7 | -11.2 | | |
| 600 | 13.00 | -0.10 | +2.0 | 1.9 | -10.6 | } | |
| " | 15.28 | | +3.8 | 3.2 | -9.3 | | } |
| 800 | 15.49 | | +3.0 | 2.3 | -10.2 | | |
| 1000 | 15.56 | | +4.2 | 3.5 | -9.0 | | |
| 1200 (600) | 16.03 | | -0.3 | -1.1 | -9.5 | | |
| 1400 | 16.08 | | +2.3 | 1.5 | -10.0 | | |
| 1600 | 16.15 | | 0. | -0.8 | -9.3 | | |
| 1620 (2800mA) | 16.18 | -0.79 | +1.0 | +3.2 | -5.3 | | |
| 0b | 16.53 | -0.9 | -1.4 | -2.3 | | | |
| LINE D | | +1.65/kw | | | | | |
| 0 | 16.53 | | 0 | 0 | -8.5 | | |
| 0b | 16.53 | | +1.4 | | | | |
| | 18.35 | | -1.4 | +1.4 | -7.1 | | |
| 200 | 17.12 | | 3.8 | 1.3 | -4.2 | | |
| H | 17.18 | | 1.9 | 2.6 | -5.9 | | |
| 600 | 17.23 | | -4.9 | -4.1 | -12.6 | | |
| 800 | 17.28 | | -2.0 | -1.0 | -9.5 | | |
| 1000 | 17.33 | | +5.0 | 6.4 | -2.1 | | |
| ↓ | 17.39 | | -0.9 | -9.6 | -18.1 | | |
| 1400 | 17.44 | | -2.0 | -0.6 | -9.1 | | |
| 1600 | 17.50 | | -7.5 | -5.9 | -14.4 | | |
| 1800 | 17.56 | | 5.2 | 6.9 | -1.6 | | |
| H | 18.00 | | -1.5 | 1.3 | -7.2 | | |
| LINE E | | -2.20/kw | | 0 = -7.0 | | | |
| 0 | 10.45 | | 0.2 | 0. | -7.0 | | |
| 0b | 10.45 | | -10.5 | | | | |
| | 14.20 | -8.0 | -2.5 | -10.5 | -17.5 | | |
| 200 | 10.58 | | -4.4 | -1.9 | -11.9 | | |
| 400 | 11.05 | | 0. | -0.7 | -7.7 | | |
| 600 | 11.15 | | 4.4 | 3.3 | -3.7 | | |
| 800 | 11.20 | | 9.5 | 8.2 | +1.2 | | |
| 1000 | 11.26 | | 21.4 | 19.9 | 12.9 | | |
| 1200 | 11.31 | | 3.6 | 1.9 | -5.1 | | |
| 1300 | 11.35 | | -10.9 | -13.5 | -29.5 | | |



| LINE E Cont'd | TIME | DIST Δ ADD | V_obs | V_corr | V_adj'd |
|------------------|-------|---------------|-------|--------|------------|
| 1 1400 | 11.40 | | -1.2 | -3.2 | -10.2 |
| 2 " | 12.01 | | -1.1 | -3.9 | -10.9 |
| 3 1600 | 12.20 | | 1.3 | -2.2 | -9.2 |
| 4 1675 | 13.42 | | -9.7 | -16.3 | -23.3 |
| 5 1800 | 12.28 | | +7.5 | 3.7 | -3.3 |
| 6 2000 | 12.33 | | +8.9 | 4.5 | -2.9 |
| 7 2200 | 12.44 | | -6.5 | -10.9 | -17.9 |
| 8 2400 | 12.47 | | -9.9 | -14.4 | -21.4 |
| 9 2600 | 12.53 | | -6.9 | -11.7 | -18.7 |
| 10 2800 | 12.59 | | -9.5 | -14.5 | -21.5 |
| 11 3000 | 13.03 | | -.7 | -5.8 | -12.8 |
| 12 3200* | 13.08 | | -12.6 | -17.9 | -24.9 |
| 13 | | | | | |
| 14 | | | | | Sub: -24.9 |
| 15 LINE F | | 5.0 ft | | | |
| 16 06 | 15.20 | 2.23/hr | 3.8 | | -24.9 |
| 17 06 | 16.30 | | 6.4 | 3.8 | -21.1 |
| 18 200 | 15.25 | | -5.0 | -5.2 | -20.1 |
| 19 400 | 15.30 | | +5.9 | 5.1 | -19.8 |
| 20 600 | 15.37 | | 18.0 | 17.4 | -7.5 |
| 21 700* | 15.43 | | 1.3 | 0.4 | -24.9 |
| 22 1000 | 15.50 | | 8.7 | 7.6 | -17.3 |
| 23 1200 | 15.55 | | 9.0 | 7.7 | -17.2 |
| 24 1400 | 16.00 | | 16.2 | 14.7 | -10.2 |
| 25 1500* | 16.05 | | 16.0 | 14.3 | -19.6 |
| 26 | | | | | |
| 27 | | | | | |
| 28 | | | | | |
| 29 | | | | | |
| 30 | | | | | |
| 31 | | | | | |
| 32 | | | | | |
| 33 | | | | | |
| 34 | | | | | |
| 35 | | | | | |
| 36 | | | | | |
| 37 | | | | | |
| 38 | | | | | |
| 39 | | | | | |
| 40 | | | | | |

COREWIN SP

| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-----------|-------------|------|-----------|-------------|-------------|------|------|
| LINE SP-1 | | AGE | AGE | SP-1 | | AGE | |
| STA | m.v (lined) | -3 | -7 | STA | m.v (lined) | -6 | |
| | | | (-10 tot) | | | | |
| 1 | 0 | 3 | 0. | -7. | 3.2 E | 13. | 0. |
| 2 | 100E | 0 | -3. | -10. | 3.7 | 16 | +3. |
| 3 | 200 | 4 | | -6. | 3.8 | 22 | +9. |
| 4 | 300 | -4 | | -14. | 3.9 | -4. | -17. |
| 5 | 400 | 3 | | -7. | 4.0 | -7. | -20. |
| 6 | 500 | 1 | | -9. | | | |
| 7 | 600 | -2 | | -12. | 0.1 W | -6. | -19. |
| 8 | 700 | -2 | | -12. | .2 | -6. | -19. |
| 9 | 800 | 1 | | -9. | .3 | -8. | -21. |
| 10 | 900 | -2 | | -12. | .4 | 7. | -6. |
| 11 | E 1000 | 2 | -1. | -8. | .5 | 17 | +4. |
| 12 | 11 | -2 | | -12. | .6 | 0. | -13. |
| 13 | 12 | 3 | | -7. | .7 | 0. | -13. |
| 14 | 13 | 0 | -3. | -10. | .8 | -4. | -17. |
| 15 | | | AGE -6 | (-13 total) | .9 | -3. | -16. |
| 16 | 1. E | 5 | -1. | -8. | 1.0 | 5. | -8. |
| 17 | 1.3 | 4 | -2. | -9. | 1.1 | -23. | -34. |
| 18 | 1.4 | 2. | | -11. | 1.2 | -17. | -30. |
| 19 | 1.5 | 0 | | -13. | 1.3 | 11. | -2. |
| 20 | 1.58 | -3 | | -16. | 1.4 | 25. | +12. |
| 21 | 1.6 | -2. | | -15. | 1.5 | 9. | -4. |
| 22 | 1.7 | -2. | | -15. | 1.6 | 5. | -8. |
| 23 | 1.8 | 1. | | -12. | 1.7 | 14 | +1. |
| 24 | 1.9 | 6. | | -7. | 1.8 | 18 | +5. |
| 25 | 2.0 | 3 | | -10. | 1.9 | 16. | +3. |
| 26 | 2.1 | 7. | | -6. | 2.0 | 23. | +10. |
| 27 | 2.2 | 4 | | -9. | 2.2 | 12 | -1. |
| 28 | 2.3 | 5. | | -8. | 2.4 | 27 | +16. |
| 29 | 2.4 | 4. | | -9. | 2.6 | 36 | +23 |
| 30 | 2.5 | -6. | | -19. | 2.8 | 27 | +15. |
| 31 | 2.6 | +6. | | -7. | 3.0 W | 23. | +20. |
| 32 | 2.7 | 7. | | -6. | | | |
| 33 | 2.8 | 0 | | -13. | | | |
| 34 | 2.9 | -3 | | -14. | | | |
| 35 | 3.0 | +5. | | -18. | | | |
| 36 | 3.225 | 17. | | +4. | | | |
| 37 | 3.1 | +1 | | -14. | | | |
| 38 | 3.2 | +16. | | +3. | | | |
| 39 | 3.3 | 16. | | +3. | | | |
| 40 | 3.4 | 18 | | +5. | | | |
| | 3.5 | 9 | | -4. | | | |

ANIMAS
SP Survey



77-3-17

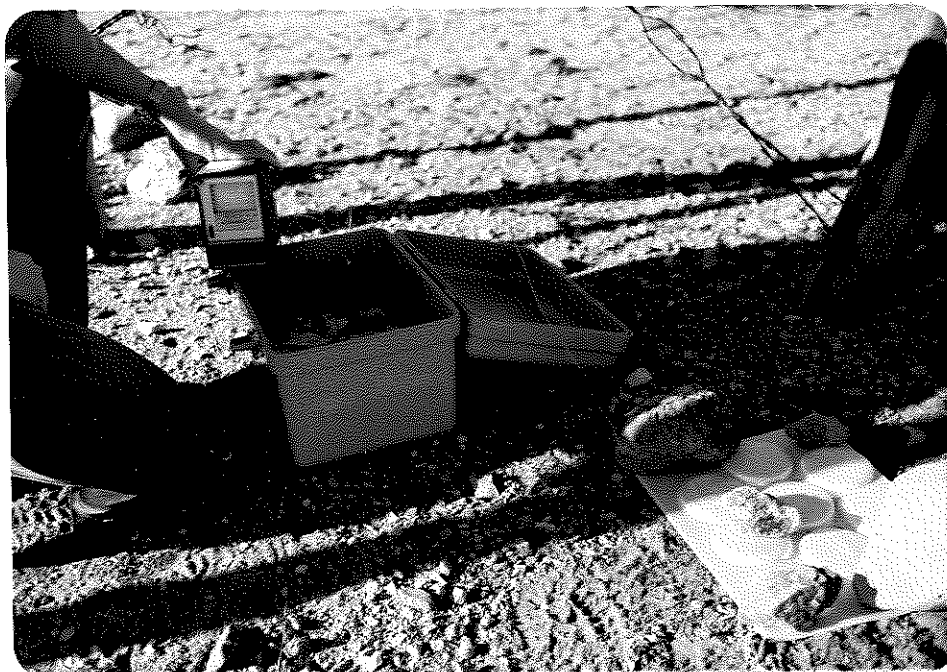
ANIMAS
SP Survey



77-1-31

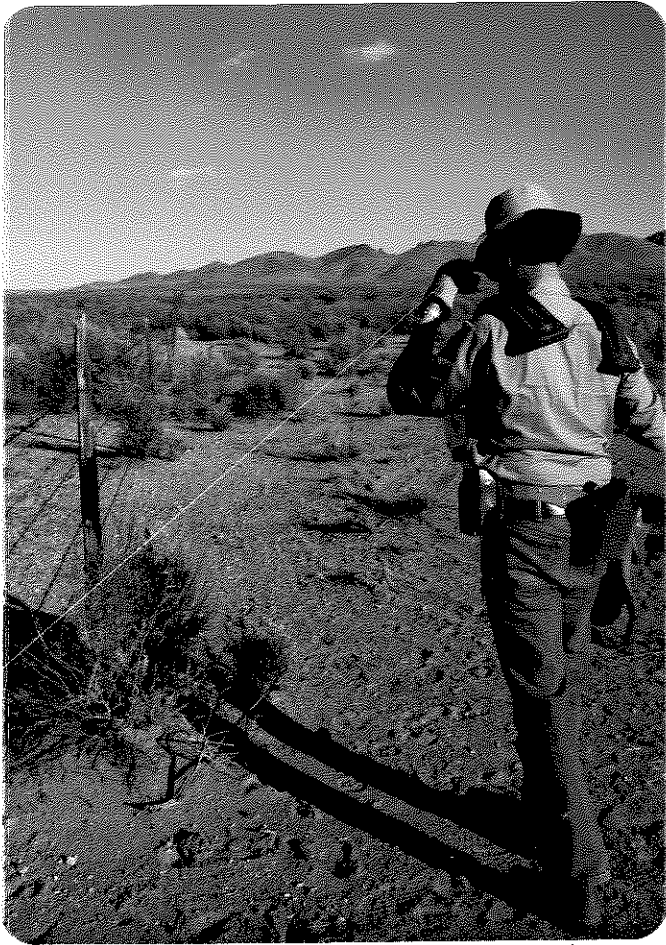


77-1-33



77-1-33

ANIMAS
3P. SURVEY



77-1-34



77-1-34



77-1-35

ANIMAS Self Potential 1977

R.21W R.20W

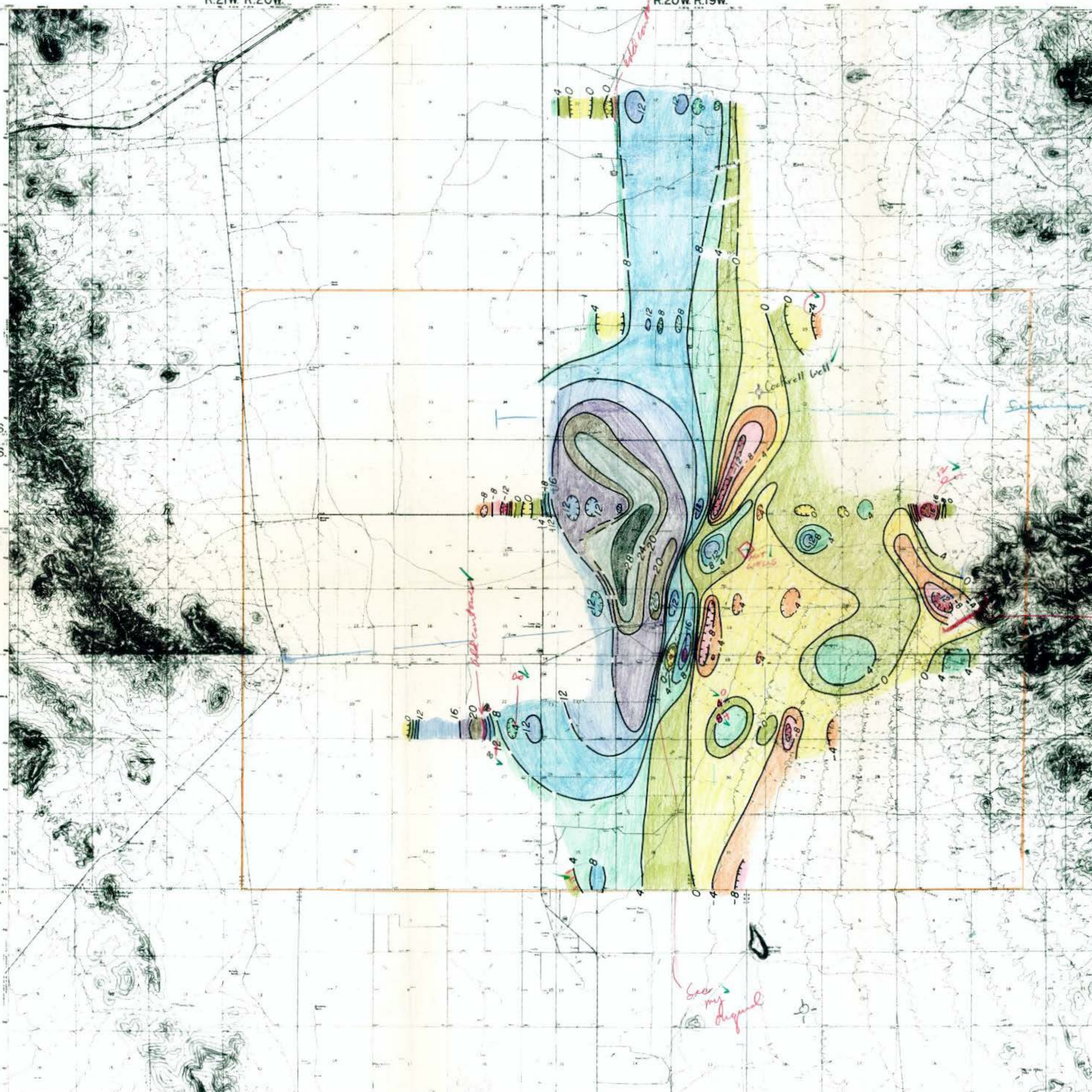
R.20W R.19W

T.24S

T.25S

T.25S

T.26S



See my diagram

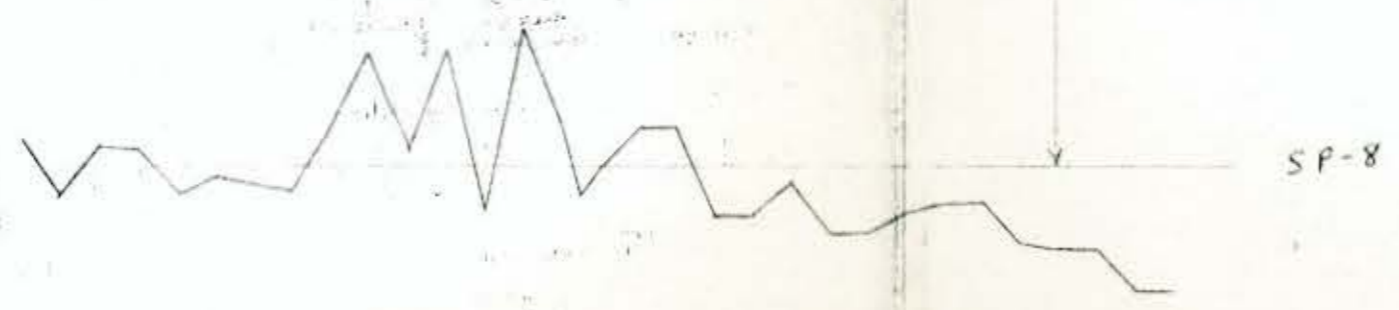
all combined

Cookrell Well

See my diagram



SP-5
4.8 km

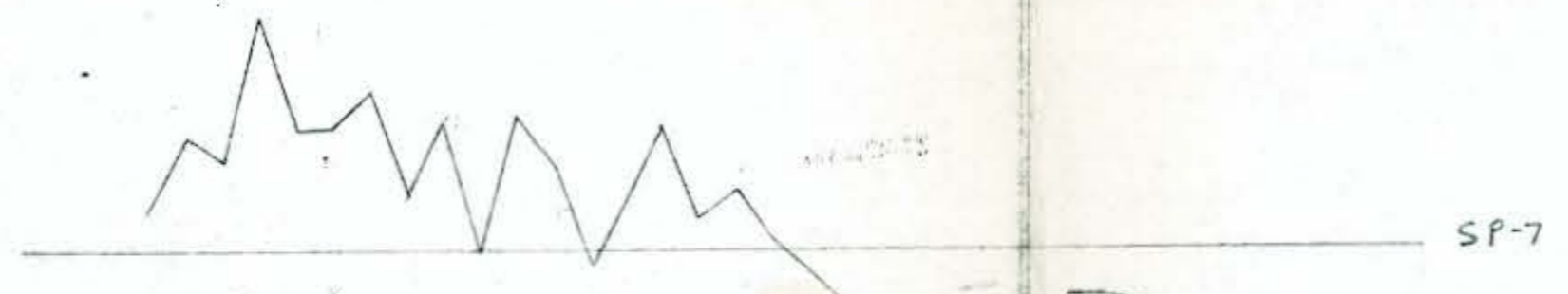


SP-8

SELF-POTENTIAL DATA: PARTIALLY CORRECTED, UNSMOOTHED

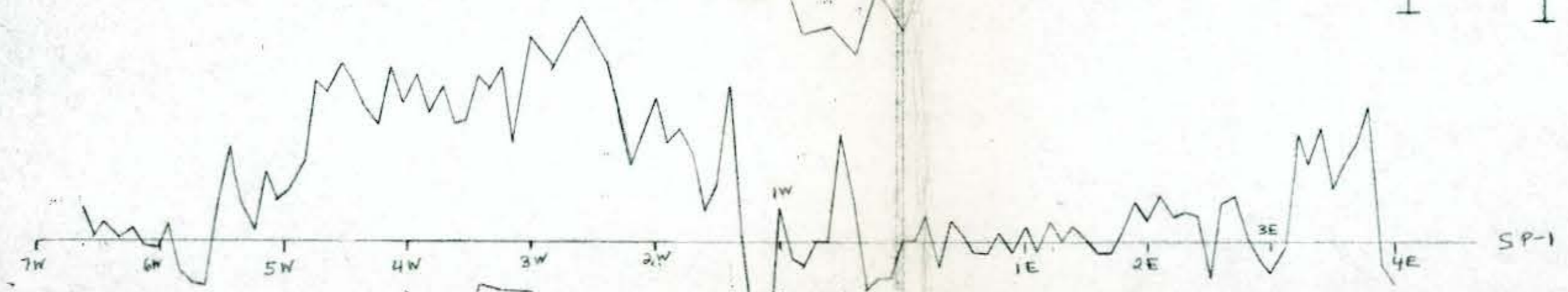
ANIMAS PROSPECT, HIDALGO COUNTY, N.M.

JAN-MAR 1977



SP-7

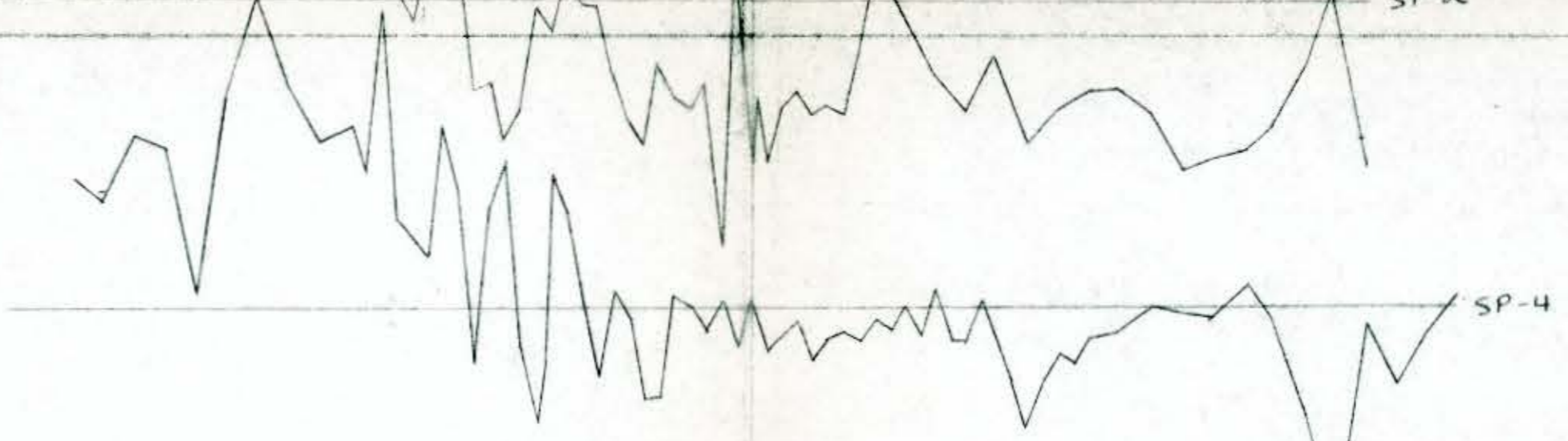
20mV
1 km N-S
1 km E-W



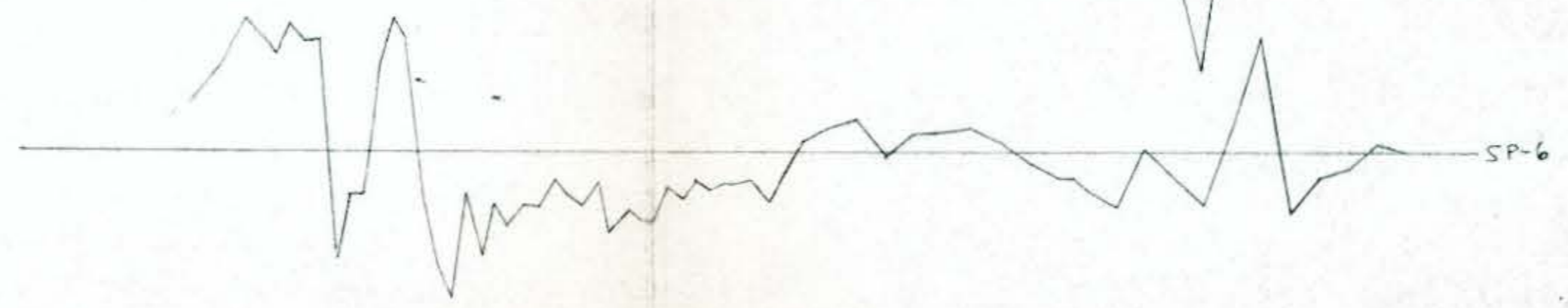
SP-1



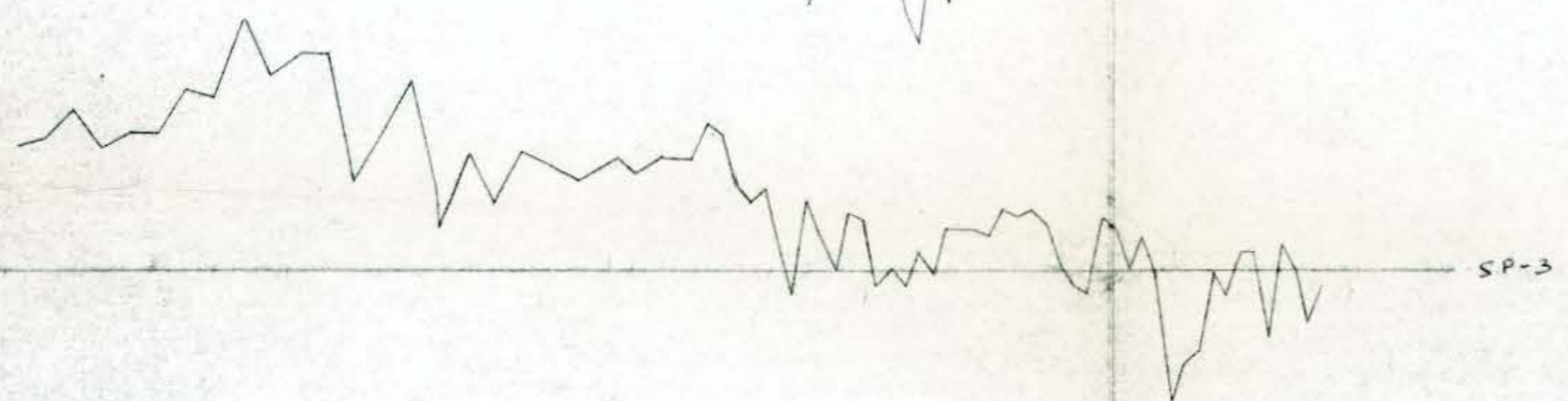
SP-2



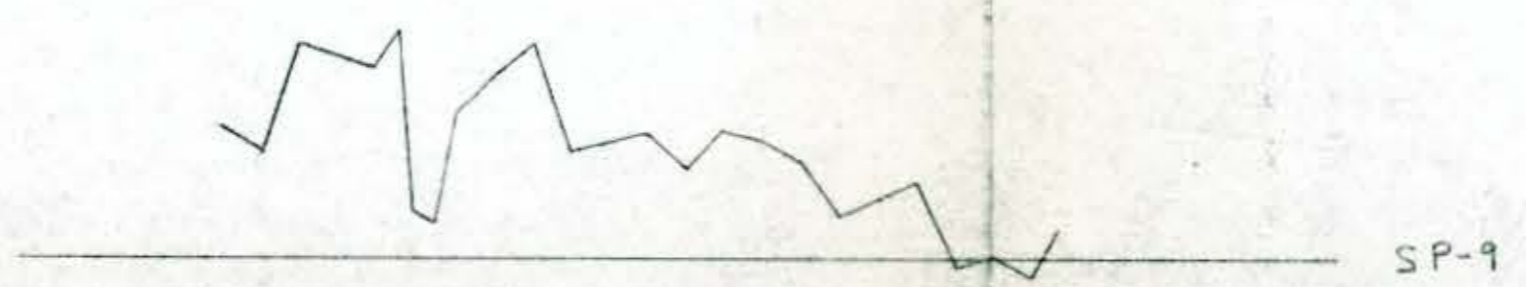
SP-4



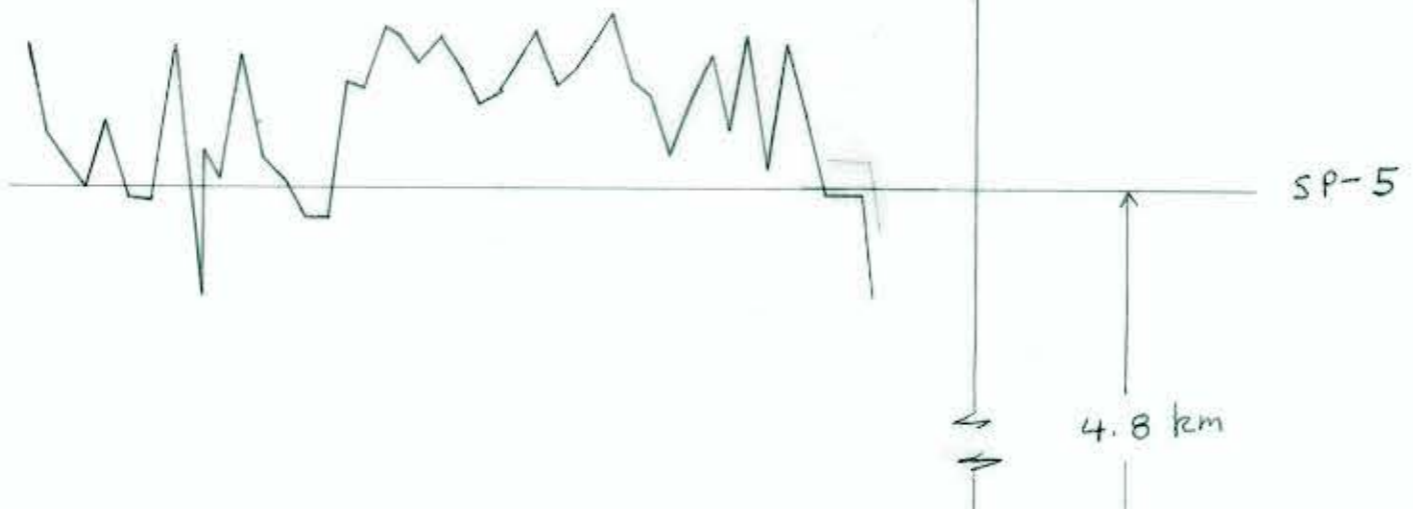
SP-6



SP-3



SP-9



SELF-POTENTIAL DATA: PARTIALLY CORRECTED, UNSMOOTHED

ANIMAS PROSPECT, HIDALGO COUNTY, N.M.

JAN-MAR 1977

