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An Analysis of the Response of the Raft River Monitor Wells to the 1979 Injection Tests

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# AN ANALYSIS OF THE RESPONSE OF THE RAFT RIVER MONITOR WELLS TO THE 1979 INJECTION TESTS

Susan G. Spencer Don M. Callan

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#### **ABSTRACT**

The geothermal resource for the Department of Energy's (DOE) Raft River Geothermal 5 MWe Power Project is located in a closed ground water basin in southcentral Idaho. Chemical analyses indicate the existence of natural communication along fractures between the geothermal reservoir and the shallower aquifers developed for irrigation. Much of the ground water that is presently used for irrigation is of poor quality. Injection of geothermal fluids at intermediate depths may increase communication between the reservoir and the aquifer, resulting in further degradation of shallow ground water quality over time. Seven monitor wells, ranging in depth from 150 m to 400 m, were drilled to evaluate the potential for this degradation. Monitoring of these wells during two 21-day injection tests at the Raft River Geothermal Injection Well-6 (RRGI-6) indicates two types of response in the shallow aquifer system:

- 1. The water level in Monitor Well-4 (MW-4) increased an average of 0.4 m/week during injection, indicating direct fracture connection between the injection zone and the aquifer penetrated by MW-4
- 2. Water levels in MW-5, MW-6 and MW-7 showed a "step function" decrease which coincided with the period of the injection tests. Analyses indicate that this response may be caused by elastic deformation in the aquifer matrix.

#### **ACKNOWLEDGMENTS**

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# AN ANALYSIS OF THE RESPONSE OF THE RAFT RIVER MONITOR WELLS TO THE 1979 INJECTION TESTS

#### INTRODUCTION

Preliminary geological and geophysical work conducted by the U.S. Geological Survey (USGS) in 1973 and 1974 indicated a geothermal energy resource in the southern Raft River Valley, Idaho (Figure 1). Geochemical research based on shallow aquifer data suggested the presence of a 150° C resource at a depth of approximately 1300 m. In late 1974, the U.S. Department of Energy (DOE), the Raft River Rural Electric Cooperative (RRREC), and the Idaho Department of Water Resources (IDWR) initiated a cooperative venture to investigate the generation of electrical energy using the moderate temperature geothermal fluid. The first deep exploratory well, Raft River Geothermal Exploratory Well-1 (RRGE-1), confirmed the presence of the resource. The Department of Energy (DOE) began design of a 5 MWe binary power plant to demonstrate the technical feasibility and environmental acceptability of generating electricity utilizing a binary cycle. Construction of the power plant began in August, 1978, with the plant scheduled to be operational by October 1980.

Seven geothermal wells were drilled to evaluate the production and injection possibilities of the reservoir. Production wells RRGE-1, RRGE-2, RRGE-3, and Raft River Geothermal Production Well-5 (RRGP-5) were drilled to depths of 1490 to 1980 m (Figure 2). Injection Wells RRGI-6 and RRGI-7 were drilled to a depth of 1160 m for injection. Well RRGI-4 was initially drilled as an injection well to a depth of 850 m and was later deepened to 1650 m and completed as a production well (RRGP-4).

RRGE-1, RRGE-2 and RRGE-3 will be pumped to produce the 150 L/s at 140° C required to operate the power plant. Injection pumps have been installed at RRGI-6 and RRGI-7 to inject an estimated 120 L/s at wellhead pressures of 2400 to 2800 kPa. The remainder of the fluid produced will be consumed in the plant cooling cycle. RRGP-4 and RRGP-5 were used for hydraulic

fracturing experiments and are not considered an integral part of the present supply and injection system.

As DOE's geothermal development program continued, concerns were expressed about the effect that development might have on the quality and supply of ground water in the basin. Modeling of the shallow aquifers by the U.S. Geological Survey<sup>1</sup> indicated that it would take 100 years for geothermal production to affect the shallow aquifers currently being developed for irrigation. There was concern, however, that high pressure injection at intermediate depths (500 - 1000 m) would adversely affect nearby irrigation wells.

Because of this concern, DOE has established a monitoring program to evaluate the potential for these adverse effects. Eight wells drilled by DOE and the USGS were monitored during injection tests in 1979. This report summarizes the data collected on the water level changes in these wells during these injection tests and presents an analysis of these responses.

# BACKGROUND Geology

The Raft River Valley is a structural downthrown block bounded by the Jim Sage and Cotterel Mountains the west, the Raft River Range on the south, and the Black Pine and Sublett Ranges on the east (Figure 3). The Jim Sage and Cotterel Mountains are primarily Tertiary volcanic and sedimentary rocks. The Black Pine and Sublett Ranges are composed of Paleozoic limestones and sandstones. The Raft River Range, an anomalous east-west trending range, contains Precambrian adamellite and Paleozoic sediments.<sup>2</sup>

The deepest wells in the valley terminate in quartz monzonite, indicating that the floor of the basin is similar to the Precambrian rocks exposed in the Raft River Range. Precambrian quartzites and schists overlie the basement rock and are

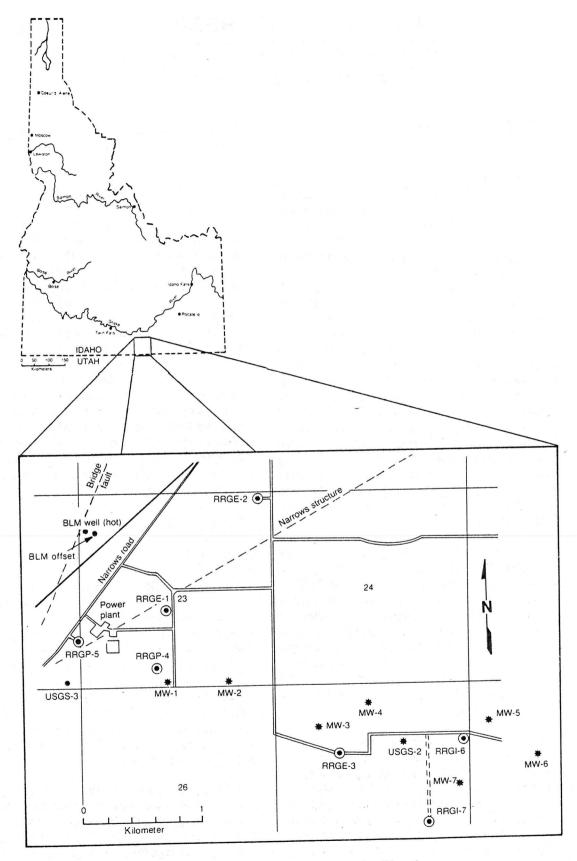


Figure 1. Raft River Geothermal Area and well locations.

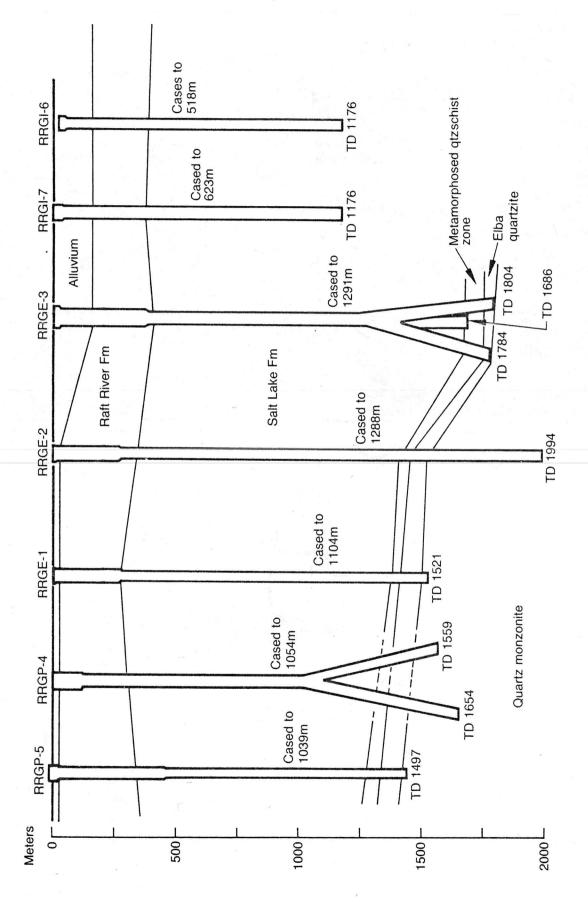
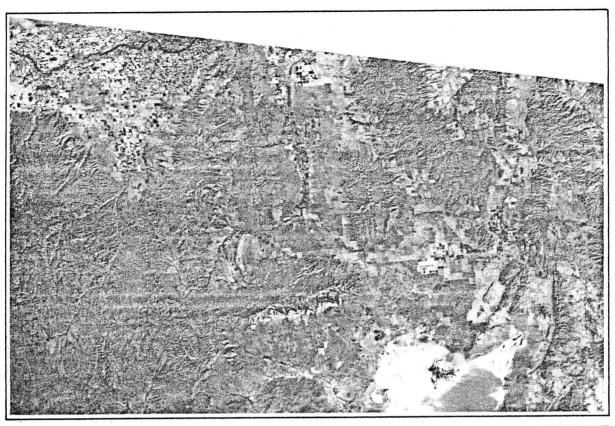


Figure 2. Raft River geothermal wells.



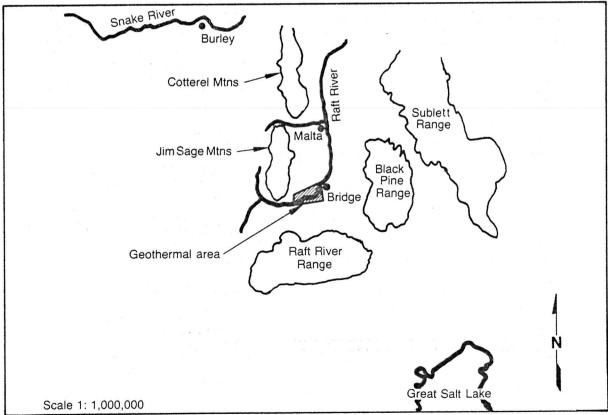


Figure 3. Physiography of the Raft River Valley.

themselves overlain with sediments of the Tertiary Salt Lake Formation. This formation, which constitutes the majority of the basin sediments, consists of unconsolidated quartzose silts and sands, tuff, quartzite and rhyolite gravels. The Salt Lake Formation is overlain by Pleistocene sand, gravel, silt and clay of the Raft Formation. The youngest deposits in the basin are alluvial and fluvial sediments (see Reference 2).

The meandering Raft River has cut through the deposits near the center of the valley and has contributed to the depositional and erosional sequences. The variety of sediment sources and transport mechanisms complicates lithologic correlation of the upper 300 m of sediments in the southern Raft River Valley.

The basin is a downthrown block in contrast to the upthrown Jim Sage Mountains. The steep, north-south trending fault scarp on the east face of the Jim Sage Mountains has a displacement of 900 m. This steep fault scarp has resulted in numerous landslides and alluvial fans which are intrinsic to the filling of the valley.<sup>3</sup>

The structural geology plays a key role in the production of geothermal fluids in the resource area. The present interpretation of the production mechanism is that detached-normal faulting of the Tertiary Salt Lake Formation sediments provides a highly-fractured and permeable rock section that allows for fluid movement. Recharge is apparently provided by the numerous faults at or near the valley surface, while thermal convection within the metamorphosed basement section is thought to provide the heat source.

## Hydrology and Water Quality

The Raft River basin encompasses an area of 3870 km<sup>2</sup> in southcentral Idaho and northern Utah. Precipitation ranges from 25 cm per year in the valley to over 80 cm in the surrounding mountains. The principal stream in the basin is the Raft River, which originates in the Goose Creek Mountains in northwestern Utah and flows east and north to its confluence with the Snake River.

During the summer months, nearly all surface water in the basin is diverted for irrigation. Consequently, flow in the Raft River is totally dissipated between Bridge and Malta during the irrigation season. The Raft River is primarily a losing stream in the vicinity of the geothermal development, a condition which is enhanced by a declining water table during late spring and summer.<sup>4</sup>

Ground water in the basin occurs both in unconfined and confined conditions in the poorly consolidated sediments of the Salt Lake Formation, and in the sands and gravels of the Raft Formation and recent alluvial deposits. Recharge to these aquifers results from precipitation in the surrounding mountains and infiltration from streams and irrigation water. Walker and others (see Reference 5) estimate that the upper 60 m of saturated deposits contain 11 km<sup>3</sup> of water. Based on an analysis of precipitation and evapotranspiration, the groundwater yield of the basin was estimated at less than 0.2 km<sup>3</sup> (see Reference 5).

The shallow aquifers can be considered water table aquifers, although some wells reveal locally confined conditions. Piezometric surfaces in several of the geothermal production wells are over 100 m above land surface. Because of this increase in head with depth, each aquifer is probably recharged, in part, by upward leakage from underlying aquifers (see Reference 1). In the geothermal area, wells as shallow as 120 m tap hot water, and nearly all irrigation wells in the area show chemical and thermal evidence of upward leakage from the geothermal resource.

Ground water withdrawal for irrigation in the basin has increased substantially since 1948. Most irrigation wells are concentrated in an area within 3 km of the Raft River, and ground water level declines along the river have been most severe. Measurements of water levels since 1952 show more than 15 m of decline north of Malta and nearly 6 m of decline just east of the geothermal development (see Reference 1). In 1963, the state of Idaho declared the basin a critical ground water area, closing it to further ground water development. The subsequent study of the basin by Walker and others (see Reference 5) indicated that a total of more than 0.6 km<sup>3</sup> of ground water had been removed from storage by the end of the 1966 irrigation season.

Ground water quality varies widely in the basin. The total dissolved solids (TDS) concentration of well and spring water averages 750 mg/L and ranges from 120 mg/L to 3200 mg/L (see Reference 5). Most of the ground water is of the

sodium chloride or calcium bicarbonate type. Variations are induced by well depth and location with respect to streams, areas of irrigation water recharge, and areas of recharge from deeper aquifers.

A summary of chemical analyses from ground water in selected wells is shown in Table I. Water from wells in the vicinity of the geothermal area has elevated temperatures and total dissolved solids, a result of mixing of shallow ground water with recharge from the geothermal reservoir. For example, water from a well 20 km west of the geothermal area (15S24E27daa1) has a temperature of 13° C and TDS of 720 mg/L, while water from a well within the geothermal area (15S26E23abd1) has a temperature of 29° C and TDS of 2400 mg/L. These wells are approximately the same depth.

Analyses of water samples from the geothermal wells show a variation in TDS (Table I). The basis for this variation is not clear due to the limited number of data points. Trilinear plots (Figure 4a, 4b, and 4c and Table 2) of water chemistry from shallow and deep wells indicate that the geothermal fluids are of similar percentage composition, even though the TDS may differ. The linearity of the anion and cation plots (Figure 4a) suggests dilution of the rising geothermal fluids resulting from recharge to the valley.

An enlargement of the anion plot (Figure 4b) indicates that there are several groups of wells in the high chloride region. Geothermal wells RRGE-1 and RRGP-5 plot in a different location than RRGE-3, RRGI-6 and RRGI-7, indicating that there are variations within the geothermal reservoir. Differences between the order of geothermal wells on the cation and anion plots may be due to reactions occurring in the water as it moves up the fractures. The juxtaposition of shallower wells such as MW-4 and geothermal wells such as RRGI-6 indicates that these wells may directly intersect fractures that conduct geothermal fluids upward. It would not be surprising to see these wells respond to the production or injection of geothermal fluids. The location of other shallow warm wells (such as 15S26E23abdl) on the plot indicates that the water from these wells is a mixture of geothermal fluids and shallow ground water.

#### MONITORING PROGRAMS

Since 1974, DOE and Idaho Department of Water Resources (IDWR) have conducted a series of geochemical and environmental monitoring programs. The objectives of these programs are to:

- 1. Determine the extent of natural communication between aquifers in Raft River
- 2. Monitor the chemical and hydrologic effects of the geothermal development
- 3. Predict the long-term impacts of geothermal development on the shallow aquifers developed for domestic use and irrigation.

#### Irrigation Wells

The initial monitoring programs included semiannual chemical analyses of water taken from 22 irrigation wells near the geothermal development. Several problems were encountered during the monitoring program which limit the usefulness of the data. These problems included the following:

- 1. Access to the irrigation wells was limited to the irrigation season (April to October)
- 2. Wells pumped one year were not necessarily pumped the next
- Significant seasonal variations in the pumping rates of individual wells exist
- 4. Information about the depth and construction of irrigation wells is difficult to obtain or is nonexistent.

#### **Monitor Wells**

An interagency (DOE, USGS, IDWR) meeting was held in 1976 to review the irrigation well monitoring program and to make recommendations for a new program. The recommendations included the drilling of a series of monitor wells in the valley to solve some of the problems encountered in the irrigation well monitoring. The

Representative analyses of water from selected wells in the Raft River Basin Table 1.

230 107 10 56 5.9 2 2.4 27 27 1570 71 80 1570 71 80 2930 197 136 6 4.9 0.4 6 6 6 4.9 0.4 6 6 7.7 7.1 7.1	RRGE-1 (mg/L)	RRGE-2 (mg/L)	RRGE-3 (mg/L)	RRGI-6 (mg/L)	MW-1 (mg/L)	MW-3 (mg/L)	MW-4 (mg/L)	MW-5 (mg/L)	MW-6 (mg/L)	15S24E27daa1 (mg/L)	15S26E23abd1 (mg/L)
32         30         54         25         14         56         5.9         2           5.1         3.7         3.1         5.9         5         24         5.9         2           1.4         0.4         3.4         3.2         25         2.4         27         80           2100         2220         1350         1400         230         1570         71         86           94         80         60         67         29         87         46         6           3640         3680         2400         2420         717         2930         197         13           7.1         3.4         5.4         4.9         0.6         4.9         0.4         13           60         66         48         51         27         63         86         9           60         66         48         51         27         63         86         9           7.3         7.9         7.6         7.8         7.8         7.7         7.1         -           71         -         71         98         29         44         13         5           71	35		178	214	215	170	217	107	230	107	107
5.1         3.7         3.1         3.2         2.4         27           1.4         0.4         3.4         3.2         2.4         27           2100         2220         1350         1400         230         1570         71           94         80         60         67         29         87         46         6           3640         3680         2400         2420         717         2930         197         136           7.1         3.4         5.4         4.9         0.6         4.9         0.4         137           60         66         48         51         27         63         86         9           6380         6270         4300         4370         1229         4820         7.0         24           7.3         7.1         98         29         44         13         2           71         -         71         98         29         44         13         2           71         99         152         335         105         11	38		105	32	30	. 54	25	14	99	5.9	23
1.4         0.4         3.4         3.2         25         2.4         27           2100         2220         1350         1400         230         1570         71         80           94         80         60         67         29         87         46         6           3640         3680         2400         2420         717         2930         197         136           7.1         3.4         5.4         4.9         0.6         4.9         0.4         136         136           7.3         25         46         41         101         44         182         12         12           60         66         48         51         2.7         63         86         9         9           7.3         7.9         7.6         7.8         7.7         7.1         -         74           71         -         7.1         98         2.9         44         13         -           71         -         71         98         2.9         44         13         -           71         99         152         335         105         11         11	1.1 9.1		3.1	5.1	3.7	3.1	3.2	0.3	3.1	0.1	2.0
2100         2220         1350         1400         230         1570         71         86           94         80         60         67         29         87         46         6           3640         3680         2400         2420         717         2930         197         130           7.1         3.4         5.4         4.9         0.6         4.9         0.4         130         130         130         130         130         130         130         130         132         4.9         0.4         130         120         240         1229         4820         0.4         1220         240         1229         4820         7.7         7.1         -         -         740         1229         4820         720         240         240         240         240         133         133         103         11         13         2         14         11         14         11         14 <t< td=""><td>0.6 0.13</td><td></td><td>0.5</td><td>1.4</td><td>0.4</td><td>3.4</td><td>3.2</td><td>25</td><td>2.4</td><td>27</td><td>5.5</td></t<>	0.6 0.13		0.5	1.4	0.4	3.4	3.2	25	2.4	27	5.5
94         80         60         67         29         87         46         6           3640         3680         2400         2420         717         2930         197         136           7.1         3.4         5.4         4.9         0.6         4.9         0.4         136           7.3         25         46         41         101         44         182         12           60         66         48         51         27         63         86         9           6380         6270         4300         4370         1229         4820         720         244           71         —         71         98         29         44         13         2           1176         399         152         305         152         335         105         11	441		1194	2100	2220	1350	1400	230	1570	71	808
3640         3680         2400         2420         717         2930         197         136           7.1         3.4         5.4         4.9         0.6         4.9         0.4         127         128<	156		165	94	80	09	19	53	87	46	99
7.1         3.4         5.4         4.9         0.6         4.9         0.6           73         25         46         41         101         44         182         12           60         66         48         51         27         63         86         9           7.3         7.9         7.6         7.8         7.8         7.7         7.1         -           6380         6270         4300         4370         1229         4820         720         246           71         -         71         98         29         44         13         2           1176         399         152         305         152         335         105         11	189		2260	3640	3680	2400	2420	717	2930	197	1303
73         25         46         41         101         44         182           60         66         48         51         27         63         86           7         7.3         7.9         7.6         7.8         7.7         7.1           6380         6270         4300         4370         1229         4820         720         2           71         71         98         29         44         13           1176         399         152         305         152         335         105	5.6 8.7		4.9	7.1	3.4	5.4	4.9	9.0	4.9	0.4	4.9
60         66         48         51         27         63         86           7.3         7.9         7.6         7.8         7.8         7.7         7.1           6380         6270         4300         4370         1229         4820         720         2           71         71         98         29         44         13           1176         399         152         305         152         335         105	8		4	73	25	46	41	101	4	182	123
2         7.3         7.9         7.6         7.8         7.7         7.1           6380         6270         4300         4370         1229         4820         720         2           71         -         71         98         29         44         13           1176         399         152         305         152         335         105	53		09	09	99	48	21	27	63	98	06
6380         6270         4300         4370         1229         4820         720         2           71         —         71         98         29         44         13           1176         399         152         305         152         335         105	7.3 7.6		7.2	7.3	7.9	7.6	7.8	7.8	7.7	7.1	l
71         98         29         44         13           1176         399         152         305         152         335         105	1290		4100	6380	6270	4300	4370	1229	4820	720	2400
1176 399 152 305 152 335 105	144		149	11		7.1	86	29	4	13	29
	1994		1804	1176	399	152	305	152	335	105	110

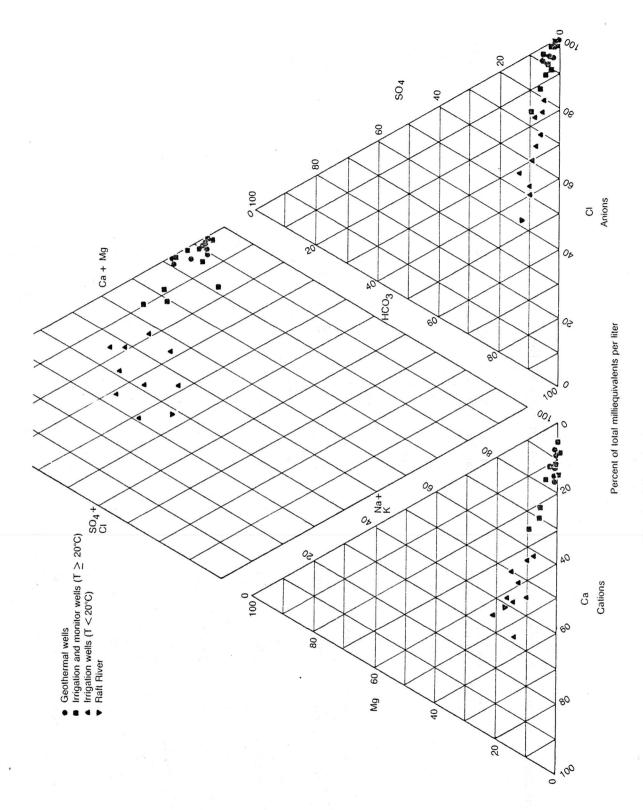
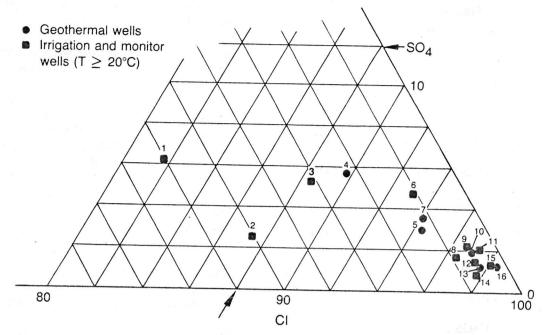
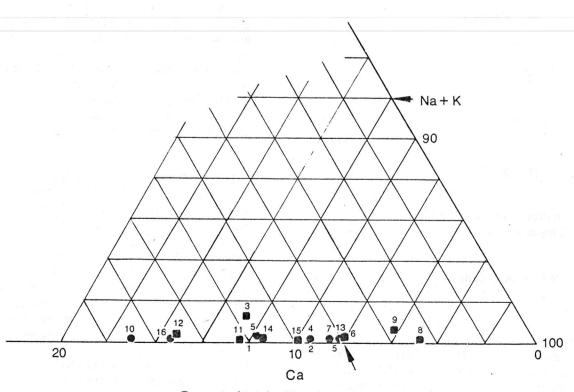


Figure 4a. Trilinear plot of chemical analyses from surface and ground water.



Percent of total milliequivalents per liter

Figure 4b. Enlargement of anion plot.



Percent of total milliequivalents per liter

Figure 4c. Enlargement of cation plot.

Table 2. Key to trilinear plots in Figure 4a

Well Depth (m)  1. 15S27E19CCC1 125  2. MW-7 152	
2. MW-7 152	
3. 15S26E23abd1 110	
4. RRGE-2 1994	
5. RRGE-1 1520	
6. BLM 126	
7. RRGP-5 1501	
8. USGS-3 434	
9. MW-6 335	
10. RRGE-3 1804	
11. Crook's 165	
12. MW-4 305	
13. RRGI-6 1176	
14. USGS-1 336	
15. MW-1 399	
16. RRGI-7 1176	

monitor wells were to be located so that potential changes would be detected prior to actual effects in nearby irrigation and domestic wells.

When DOE funding became available for the monitor well program, only one injection well, RRGI-4, had been located. Monitor wells MW-1 and MW-2 were drilled to monitor injection tests in that well. Since that time, five more monitor wells have been drilled. These seven wells and three USGS exploratory holes (USGS-2, USGS-3, and the BLM Offset well) form the nucleus of the injection monitoring program at Raft River. Each of the wells is equipped with either a Stevens water level recorder or a digiquartz pressure transducer

to provide continuous records of fluctuations in the piezometric surface in each well. Information on well completion, water chemistry, water temperature, and the lithology of the formations penetrated by each of the wells is presented in Appendix A and is summarized below.

Monitor Well-1 (MW-1). MW-1 is located 200 m to the southeast of RRGI-4 (see Figure 1) and was drilled to a depth of 400 m. The well has a shut-in pressure of 300 kPa. The quality of the water produced from MW-1 is nearly the worst encountered in the basin (refer to Table 1).

Monitor Well-2 (MW-2). MW-2 was drilled near the Crook hot well to monitor the effects of injection on the Crook well and the effects on the shallow aquifer of pumping this well. Borehole temperatures in the well exceeded 90° C at 80 m, but significant fluid production was not encountered until a depth of 160 m was reached.

Monitor Wells-3, 4, 5, 6, 7 (MW-3, 4, 5, 6, 7). MW-3, MW-4, MW-5, MW-6, and MW-7 were located and drilled to monitor injection in RRGI-6 and RRGI-7. MW-3, which is 152 m deep, and MW-4, which is 305 m deep, reveal similar conditions. The average temperature gradient in these two wells (26° C/100 m) is the highest gradient encountered in the five monitor wells drilled near RRGI-6 and RRGI-7. The elevation of the water level in MW-4 is 1470 m (datum National Geodetic Vertical Datum of 1929) which is 20 m above the adjacent water table. This indiates a greater degree of confinement and/or increased pressure with depth due to hydrothermal processes.

The thermal gradient in MW-5, MW-6 and MW-7 is lower than that of the other monitor wells (average gradient of 11° C/km), indicating poorer hydraulic communication with the geothermal system. Total dissolved solids in MW-5 and MW-7 average 1300 mg/L, while MW-6 produces water with a TDS of 4600 mg/L. Temperatures in MW-6 do not indicate natural influence from the geothermal system; however, the quality of water from this well is similar to that encountered in RRGI-6 and RRGI-7 (see Figures 4a, 4b, and 4c).

Raft River Geothermal Injection Well-4 (RRGI-4) Injection Tests. RRGI-4 injection tests during 1978 indicated vertical connection between the injection zone and shallower aquifers. 6 Three of the four wells monitored

showed positive response to each of the injection tests which ranged in length from 40 minutes to 10 days. Of particular interest was the response measured in the BLM Offset well. The water level in this well, which is 123 m deep and 1240 m from the injection well, rose more than 1.5 m during the 10-day injection test. It appears that monitor wells USGS-3, MW-1 and the BLM Offset intersect shallow fractures which are connected to the injection zone. These fractures are probably the pathways for the natural connection between the geothermal resource and shallower aquifers. RRGI-4 has subsequently been deepened to a production well. Therefore, the results of these tests may not be directly applicable to potential impacts from injection during operation of the 5MW plant. However, they do provide an indication of the nature and magnitude of the reservoir-aquifer connection.

# MONITOR WELL RESPONSE IN 1979

The aquifers penetrated by the monitor well network are evidently sensitive to external influences such as barometric pressure changes, earth tides, irrigation pumping, and geothermal injection. There is no evidence to indicate sensitivity to geothermal fluid withdrawal.

#### General Trends

One calendar year (1979) of records from the monitor wells has been analyzed. Water level records from six monitor wells are shown in Figure 5. The hydrographs of MW-3, MW-4, MW-5, MW-6 and MW-7 illustrate one major annual cycle of ground water fluctuations, peaking at the beginning of May and declining to their lowest levels at the beginning of October.

Ground water levels rose from January until May at an average rate of 0.01 m/day in MW-3, MW-5, MW-6 and MW-7. Based on long-term USGS data, this rise is a continuation of trends which usually begin in October in response to recovery from the previous irrigation season and recharge from precipitation. The period of declining water levels from May to October coincides closely with the main irrigation season and is probably a response to pumping drawdown.

Over the calendar year, the net water level decline in MW-3, 5, 6 and 7 was between 0.7 and 0.9 m. Based on only one year of records, it is not possible to attribute this decline to specific causes. However, records from USGS-2, which include data for the longest period available for a well near the geothermal area, indicate that water levels have declined at a similar annual rate over the past four years. Water level declines from one year to the next may be due to a combination of the following:

- 1. Lower than average regional recharge from precipitation
- 2. Decreased recharge from deeper aquifers
- 3. Local ground water withdrawal.

A period of record covering several years will be required to identify a water budget for the geothermal area.

#### Barometric Response

Several of the monitor wells responded sufficiently to changes in barometric pressure for calculation of barometric efficiencies. These responses are indicated in Table 3.

The records from MW-1, MW-2, USGS-2, and USGS-3 do not allow calculation of barometric efficiencies.

### Response to Irrigation

Irrigation pumping has a major influence on the shallow aquifers. The signature of the monitor well hydrographs is shaped primarily by response to irrigation withdrawals. The impact of irrigation withdrawals effectively masks any recharge from precipitation. Water levels in monitor wells 3, 4, 5, 6 and 7 and USGS-2 reflect withdrawals during the irrigation season and recovery during the remainder of the year. Monitor well 5 clearly responds to several individual irrigation wells. Monitor wells 3 and 7 appear to respond to a lesser degree to nearby irrigation wells. Monitor wells 4 and 6 and USGS-2 do not show any clearly defined response which may be correlated to



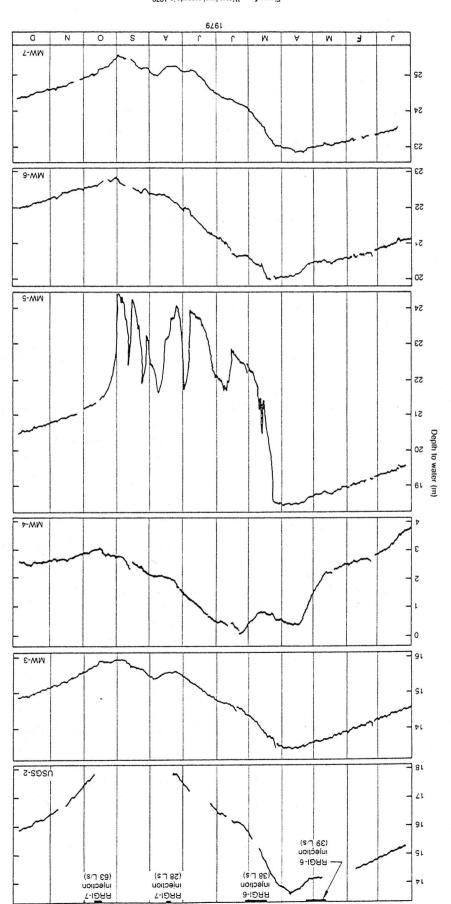


Figure 5. Water level records in 1979.

Table 3. Barometric efficiencies of monitor wells 3 through 7

Monitor Well	Barometric Efficiency
MW-3	40%
MW-4	50%
MW-5	55%
MW-6	60%
MW-7	50%

localized individual pumping activities. Therefore, the rate and magnitude of water level decline in monitor wells during the irrigation season probably reflects not only interference from adjacent wells but also interference from regional pumping.

# Responses to Geothermal Fluid Injection

During 1979, two 21-day injection tests were conducted at RRGI-6. The first of these was

conducted in March and April before the irrigation season commenced. The recovery period for the first test included part of the irrigation season and the second injection test was conducted during that same season. Monitor well responses were masked by the decline in water levels due to irrigation pumping.

Injection of geothermal fluids into RRGI-6 at depths below 525 m resulted in two types of response in the shallow aquifer system. During both 21-day injection tests, there was an obvious increase in water level in MW-4 in response to the injection (Figure 6). The total response, corrected for background trends, was approximately 1.2 m at an injection rate of 38 L/s. There was approximately four days lag time between the beginning of injection and the response in MW-4. This response indicates that relatively direct communication may exist between RRGI-6 and the aquifer penetrated by MW-4.

At the end of the year, the water level in MW-4 was more than 1 m above the level a year earlier (Figure 5). The water levels in the remaining monitor wells were as much as 1.5 m below that of a year before, reflecting trends recorded for USGS-2 in previous years. Even though there was recovery at RRGI-6 following both injection tests,

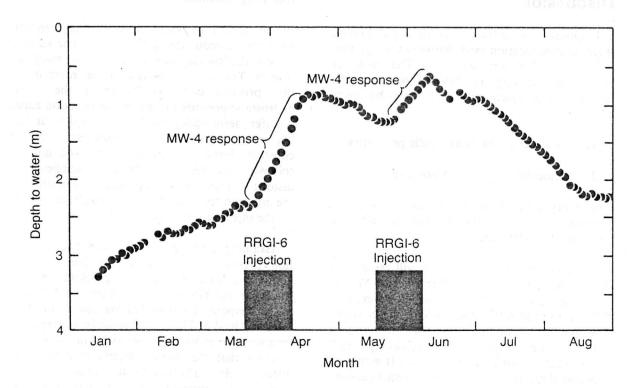


Figure 6. MW-4 water level record showing response to injection.

there appeared to be little corresponding recovery in MW-4. The water level declines in MW-4 following injection appear to be primarily responses to regional ground water declines due to irrigation.

Three monitor wells, MW-5, MW-6 and MW-7, showed an indirect response to RRGI-6 injection. This response was a "step-function" decrease in water level which corresponded closely to the beginning and end of the RRGI-6 injection test (see Figure 7). The relative amplitude of the response appears to be related to the barometric efficiency in each well, indicating that the response may be due to elastic deformation of the aquifer matrix.

Two short-term injection tests into RRGI-7 were carried out in August and October 1979. These tests were less than 100 hours in duration, not a long enough period to produce interpretable responses in most monitor wells. However, fluctuations in water levels of MW-3 and MW-7 coinciding with the October injection test may also represent aquifer dilation. Confident interpretation of responses requires a longer test period.

#### Discussion

It appears that, at least in the vicinity of MW-4, direct communication exists between the injection zone and shallower aquifers. The lack of immediate recovery in MW-4 following the termination of injection to RRGI-6 may be due to the following factors:

- 1. Local variations in hydraulic properties
- 2. Permeability related to pressure.

One theory is that the communication between the injection zone and MW-4 may be along a "soft-sediment fracture."

Sustained injection to RRGI-6 will result in a significant increase in the water level of MW-4. With the data presently available, however, it is difficult to predict the magnitude of the increase. The significance of this projected response as a potentially degrading factor to shallow groundwater quality is difficult to quantify. It would be expected that, as a result of long-term injection, poor quality fluids in the injection zone would

move up into shallower aquifers. It is important to note, however, that the undisturbed water-bearing zones intercepted by MW-4 initially contained water of poor quality, presumably because natural communication with the injection zone has existed historically.

MW-6 is at the same depth as MW-4 and is located closer to RRGI-6. However, this monitor well did not respond to injection into RRGI-6 like MW-4 did. The preferential nature of the injection response suggests that fractures may be the controlling mechanism for communication. If this is the case, the environmental significance of geothermal injection in Raft River will depend on the horizontal and vertical extent of these fractures.

Injection into RRGI-6 produces an apparant local matrix distortion effect on the overlying shallow aquifers. The response is reflected as a measurable decline in water levels in MW-5, MW-6 and MW-7 (see Figure 7). This response is evidently related to the elasticity of the matrix of the shallow aquifers. This matrix distortion in the shallow aquifer system did not change the normal ground water trend. Figure 7 shows that after deformation occurs, the water level curves follow the same slope trends that existed prior to and following injection.

The decline in water levels during injection represents a reduction in the piezometric surface in the shallow aquifer system of as much as 0.15 m. This is in response to a maximum injection pressure of 1100 kPa above the initial hydrostatic pressure present in the injection zone. Aquifer deformation took place rapidy at the beginning of the RRGI-6 injection test, remained constant during injection, and relaxed quickly following the test. This behavior implies that distortion does not increase with the duration of the injection test, and may be primarily dependent on the injection pressure.

Assuming a linear relationship between injection pressure and distortion of the overlying aquifer matrix, hydrostatic pressure in the shallower aquifers would be reduced by 5 kPa or less in response to projected maximum injection rates at RRGI-6. This would result in a corresponding water level decline of about 0.4 m. This result assumes that the aquifer matrix is capable of distorting elastically by a greater degree than it has thus far demonstrated. The magnitude of this

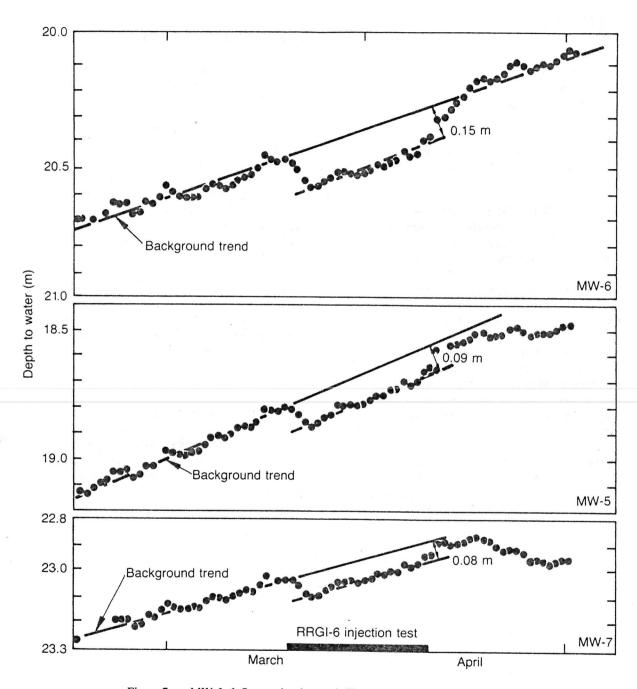


Figure 7. MW-5, 6, 7 water level records illustrating aquifer distortion.

expected pressure distortion is not great and therefore should not represent a serious environmental concern.

#### CONCLUSIONS

On the basis of one calendar year of records from the monitor wells, during which time two 21-day injection tests were conducted, the following conclusions may be drawn:

- 1. Monitor well hydrographs depict primarily irrigation withdrawal and recovery characteristics rather than a natural hydrologic cycle.
- 2. Monitor well 1, USGS-3, and the BLM Offset well are hydraulically connected to the injection zone in RRGI-4. This connection is probably fracture-related.
- 3. Monitor wells 3, 4, 5, 6, and 7 reflect semiconfined aquifer conditions with barometric efficiencies of 40-60%.
- 4. Monitor well 4 shows a rapid response to RRGI-6 injection. The potential environmental impact of this response may take a long time to become evident and may not necessarily occur in the immediate vicinity of the injection wells.
- Monitor wells 5, 6, and 7 show aquiferdistortion responses to injection through RRGI-6. These responses do not imply an immediate environmental impact.

6. Injection tests at RRGI-7 to date have not been of sufficient duration to satisfactorily identify responses in the monitor wells.

#### RECOMMENDATIONS

In addition to continuing the existing monitoring and chemical sampling program, the following actions should be taken:

- 1. Build-up pressures in RRGI-6 and RRGI-7 should be monitored carefully and continuously to detect deviations.
- 2. All monitor wells should continue to be observed closely, and instrumented where necessary. Bottom-hole temperatures in MW-4 and MW-6 should be measured at least quarterly.
- 3. Land surface elevations should be accurately measured before, during, and shortly after a sustained period of injection to determine if aquifer dilation is detectable at the surface. The surveys should focus on the region of MW-5, 6, and 7.
- 4. The USGS reflection seismic data presently being analyzed should be reviewed, when available, to substantiate present hydrogeologic concepts (in particular, fracture locations and orientations). Monitoring procedures should be ammended accordingly, if warranted.

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- 5. E. H. Walker, L. C. Dutcher, S. O. Decker and K. L. Dyer, *The Raft River Basin, Idaho-Utah, as of 1966: A Reappraisal of the Water Resources and Effects of Ground-water Development*, Idaho Department of Water Administration Information Bulletin 19, August 1970.
- 6. S. G. Spencer, J. F. Sullivan, N. E. Stanley, 1978 Annual Report, INEL Geothermal Environmental Program, TREE-1340, April 1979.
- 7. S. Petty, "Soft Sediment Fractures," private communication, EG&G Idaho, Inc., January 15, 1980.

# APPENDIX A Monitor Well Logs

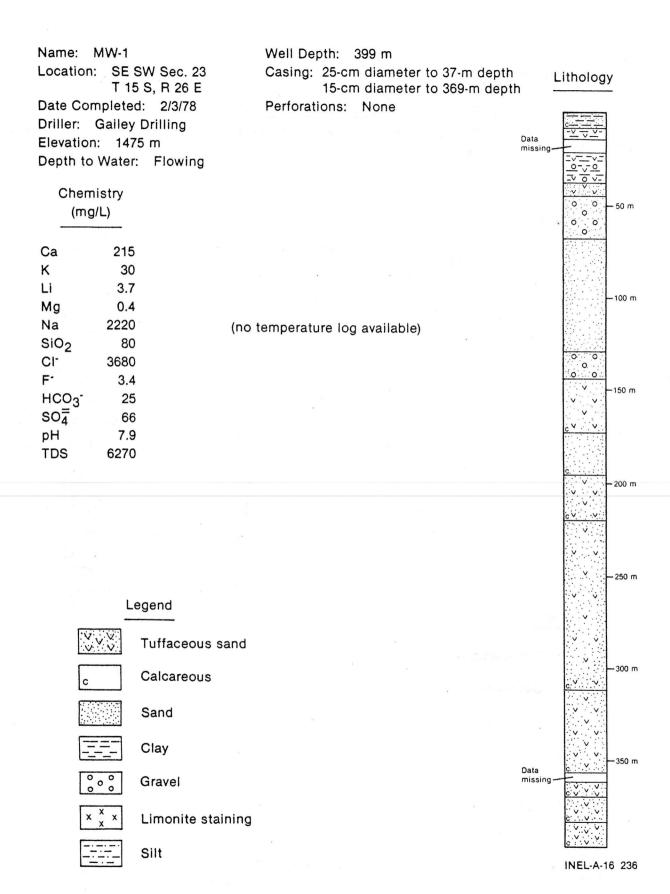


Figure A-1. Monitor Well-1 Log.

Location: SE SE Sec. 23

T 15 S, R 26 E

Date Completed: 1/6/78
Driller: Stan Lloyd Drilling

Depth to Water: Flowing

Well Depth: 174 m

Casing: 20-cm diameter to 166-m depth

Perforations: 154-to 166-m depth

Surface Temperature: 58°C

Bottom Hole Temperature: 106°C

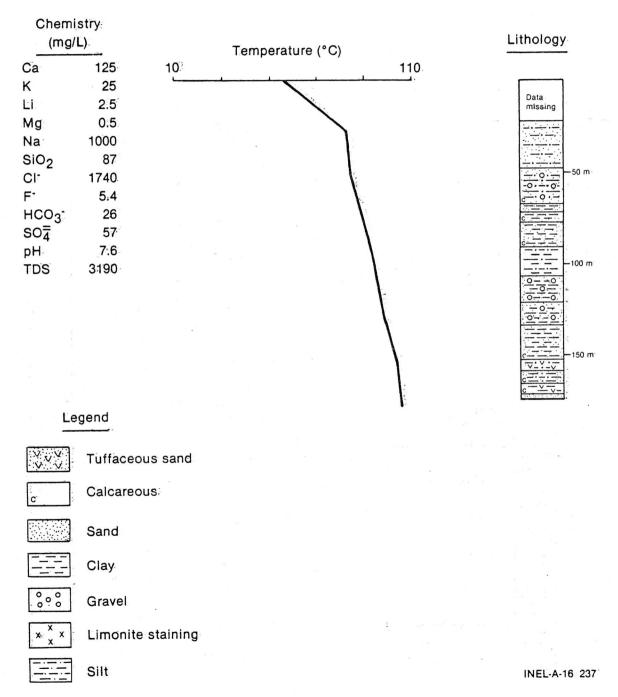


Figure A-2. Monitor Well-2 Log.

Location: SENW Sec. 25

T 15 S, R 26 E

Date Completed: 8/1/78

Driller: Stan Lloyd Drilling

Elevation: 1472 m

Depth to Water: 15 m (8/1/78)

Well Depth: 153 m

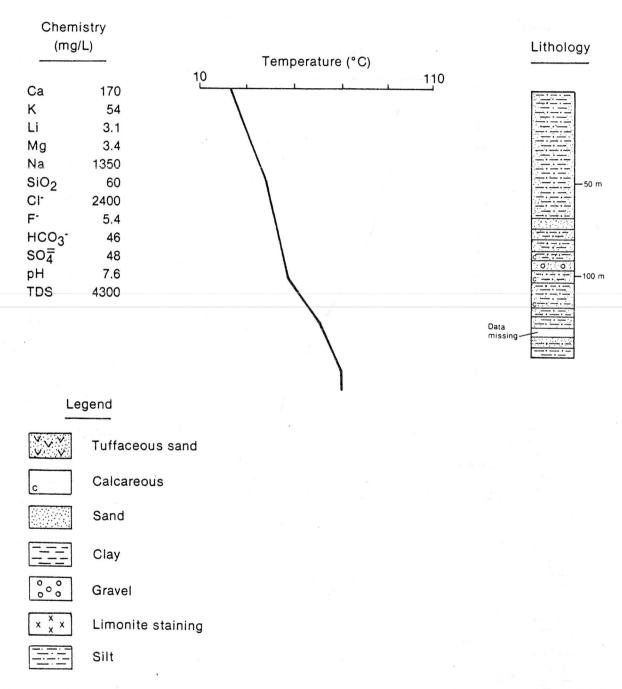
Casing: 30-cm diameter to 61-m depth

20-cm diameter to 153-cm depth

Perforations: 50 slots between

140-and 153-m depth

Surface Temperature: 24°C
Bottom Hole Temperature: 71°C



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Figure A-3. Monitor Well-3 Log.

Location: NE NW Sec. 25

T 15 S, R 26 E

Date Completed: 7/31/78

Driller: Stan Lloyd Drilling

Elevation: 1468 m

Depth to Water: 3 m (7/31/78)

Well Depth: 305 m

Casing: 25-cm diameter to 171-m depth

20-cm diameter to 254-m depth

Perforations: 105 slots between

225-and 254-m depth

Surface Temperature: 20°C

Bottom Hole Temperature: 97°C

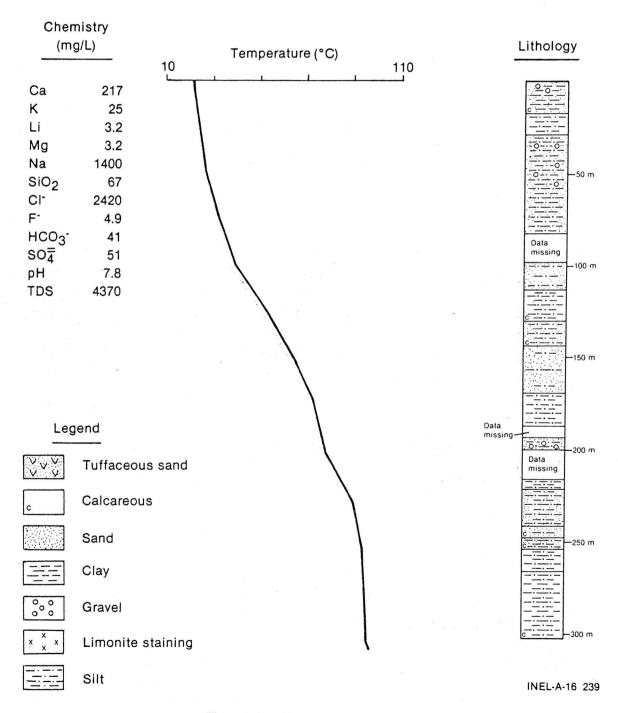


Figure A-4. Monitor Well-4 Log.

Location: NW NW Sec. 30

T 15 S, R 27 E

Date Completed: 8/20/78

Driller: Stan Lloyd Drilling

Elevation: 1466 m

Depth to Water: 22 m (8/20/78)

Well Depth: 152 m

Casing: 30-cm diameter to 61-m depth

20-cm diameter to 136-m depth

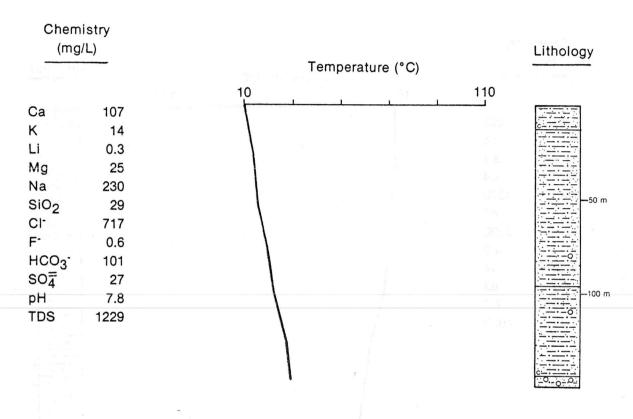
Perforations: 54 slots between

124- and 136-m depth

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Surface Temperature: 13°C

Bottom Hole Temperature: 28°C



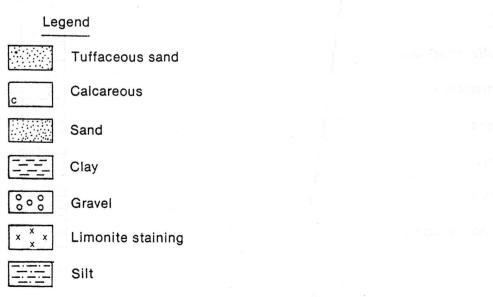


Figure A-5. Monitor Well-5 Log.

Location: SE NW Sec. 30

T 15 S, R 27 E

Date Completed: 6/15/78

Driller: Gailey Drilling

Elevation: 1469 m

Depth to Water: 21 m (3/1/79)

Well Depth: 305 m

Casing: 25-cm diameter to 46-m depth

15-cm diameter to 274-m depth

Perforations: None

Surface Temperature: 11°C

Bottom Hole Temperature: 44°C

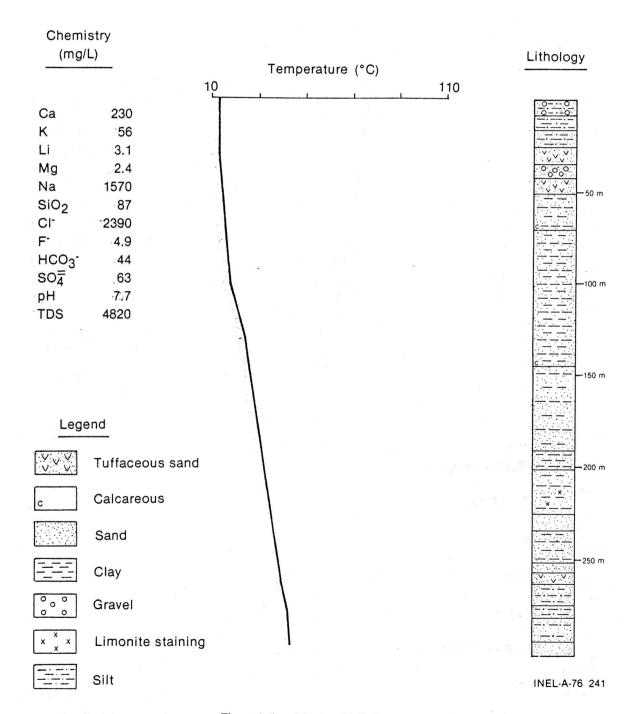


Figure A-6. Monitor Well-6 Log.

Location: NE SE Sec. 25

T 15 S, R 26 E

Date Completed: 9/6/78

Driller: Stan Lloyd Drilling

Elevation: 1474 m

Depth to Water: 21 m (9/6/78)

Well Depth: 152 m

Casing: 30-cm diameter to 61-m depth

20-cm diameter to 152-m depth

Perforations: 50 slots between

140-and 152-m depth

Surface Temperature: 20°C

Bottom Hole Temperature: 35°C

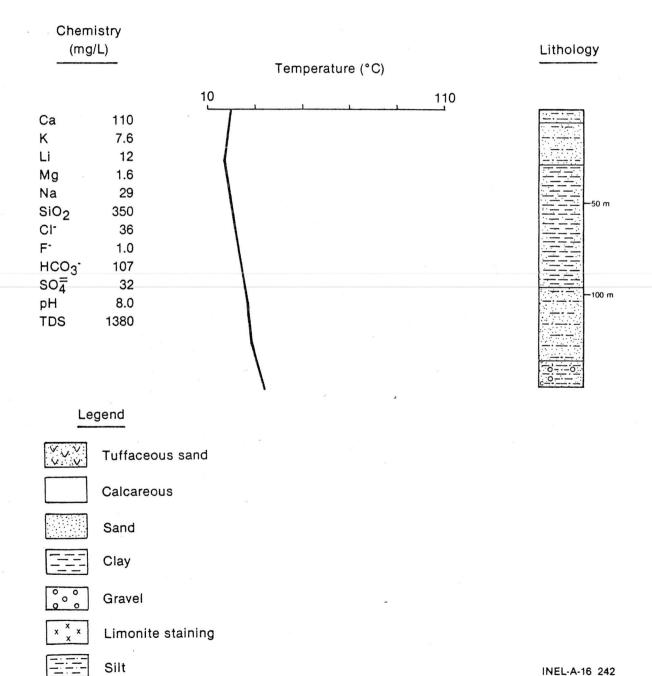


Figure A-7. Monitor Well-7 Log.